There's progress in instruments in all areas. Equipment that can calibrate, correct, test or diagnose itself may soon be commonplace. Also, more synthesized signal gens and temperature-measuring instruments are appearing on the scene. In addition, the 488 bus is finding ever wider use, despite some problems. See page 43.
### Conductive Plastic Trimmers at Carbon Prices.

Just when you thought “low cost” also meant “low performance”, along comes the dazzling new Bourns® Model 3355. Compare it to the CTS 201, Mepco 46X or Pher PT15. Our revolutionary conductive plastic element vs. their carbon... fact is we outperform them all. To prove it, we spec important characteristics such as CRV at 1% and a TC of 500 PPM/°C... the others don’t. And only the 3355 has board-wash capability, a UL-94V-1 flammability rating and an optional choice of nine rotor colors. The standard blue is priced at just 11¢ each (100,000 pieces)... about what you’d expect to pay for the lower performance carbon types.

Send today for complete details on a colorful new way to design in superior performance for your cost effective needs — the Model 3355 Trimmer. Direct or through your local distributor.

**TRIMPOT PRODUCTS DIVISION, BOURNS, INC., 1200 Columbia Ave., Riverside, CA 92507. Phone: 714 781-5050 — TWX: 910 332-1252.**

#### CATALOG SHEET SPECIFICATION COMPARISONS

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<tr>
<th>CHARACTERISTIC</th>
<th>BOURNS 3355</th>
<th>CTS 201*</th>
<th>MECPO 46X*</th>
<th>PHER PT15*</th>
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<tr>
<td>Element</td>
<td>Conductive Plastic</td>
<td>Carbon</td>
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<td>No Spec</td>
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<tr>
<td>Flammability</td>
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</tr>
<tr>
<td>Board Wash Capability</td>
<td></td>
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</tbody>
</table>

*Source: CTS Series 201 Data Sheet, Mepco Data Sheet ME1004, Pher Data Sheet F-2002 Rev 7/73*
Our Model 3001 starts at $2,750. For that you get a signal generator that's already frequency programmable with 0.001% accuracy over the 1 to 520 MHz frequency range. If you also want to program your output power, we have a programmable attenuator option available for $500.

If you'd like to spend a little more, add our external frequency standard option for $150. That makes the accuracy the same as your standard. Or spend another $500 for an internal reference frequency standard with 5 x 10^-9 day stability. But if you want to spend much more than that, you're going to have to buy somebody else's signal generator. Count on at least $10,000. Frankly, we think your money would be better spent buying another Wavetek Model 3001.

Here's another advantage. If you need to get on the bus (now or later), our new Model 3910 Converter makes you GPIB compatible. But before you spend anything on any signal generator, get a demonstration of our Model 3001. That won't cost you a cent.

**SPECIFICATIONS**

- **Frequency Range**: 1-520 MHz
- **Accuracy**: ±0.001%
- **Resolution**: 1 kHz
- **Stability**: 0.2 ppm per hour
- **Output Range**: +13 dBm to -137 dBm
- **Flatness**: ±0.75 dB
- **AM Modulation**: 0-90%
- **FM Deviation**: 0-10 kHz and 0-100 kHz
- **Internal Modulation Rates**: 400 Hz and 1 kHz

WAVETEK Indiana Incorporated, PO Box 190, 66 North First Avenue, Beech Grove, Indiana 46107, Phone (317) 783-3221, TWX 810-341-3226.

You can pay a lot more for a programmable signal generator. But why?
Have it your way!

36 models to choose from, 10KHz-800MHz

It costs less to buy Mini-Circuits wideband RF transformers. The T-series (plastic case) and TMO series (hermetically sealed metal case) RF transformers operate with impedance levels from 12.5 ohms to 800 ohms and have low insertion loss, 0.5 dB typ. High reliability is associated with every transformer. Every production run is 100% tested, and every unit must pass our rigid inspection and high quality standards. Of course, our one-year guarantee applies to these units.

<table>
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<th>DC ISOLATED PRIMARY &amp; SECONDARY</th>
<th>UNBALANCED PRIMARY &amp; SECONDARY</th>
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<tr>
<td>Model</td>
<td>Model</td>
</tr>
<tr>
<td>Metal Case</td>
<td>Metal Case</td>
</tr>
<tr>
<td>Plastic Case</td>
<td>Plastic Case</td>
</tr>
<tr>
<td>Freq. Range, MHz</td>
<td>Freq. Range, MHz</td>
</tr>
<tr>
<td>Max. Insertion Loss, MHz</td>
<td>Max. Insertion Loss, MHz</td>
</tr>
<tr>
<td>Price, Model T</td>
<td>Price, Model T</td>
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<th>DC ISOLATED PRIMARY &amp; SECONDARY CENTER-TAP SECONDARY</th>
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<tr>
<td>Freq. Range, MHz</td>
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<tr>
<td>Max. Insertion Loss, MHz</td>
</tr>
<tr>
<td>Price, Model T</td>
</tr>
</tbody>
</table>

Designers Kit Available

(1K-1) — 2 transformers of each type T1-1, T2-1, T4-1, T9-1, T16-1

(1K-2) — 2 transformers of each type TMO-1, TMO-2, TMO-4

<table>
<thead>
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<th>Designers Kit Available</th>
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<tr>
<td>Price</td>
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<tr>
<td>Type</td>
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<tr>
<td>Total Input Power (%)</td>
</tr>
</tbody>
</table>

**WE’VE GROWN**

Customer attention to our products has been so overwhelming, we’ve been forced to move to larger facilities — THANKS.

International Representatives:
- AFRICA: Afrika (PTY) Ltd P.O. Box NW13, Johannesburg 2000, S. Africa
- AUSTRALIA: General Electronic Services. 99 Alexander Street, New South Wales, Australia 2065
- ENGLAND: Dale Electronics, Dale House, Whirl Road Trinity Green, Cambridge Surrey. C. EASTERN CANADA: 31 D. Hummel 2224 Maynard Avenue, Utica, NY 13502
- FRANCE: 51 D. - 31148 St. Etienne le Vieux. George - Sand 91120 Palaisseau, France
- GERMANY, AUSTRIA, SWITZERLAND, DENMARK: Industrial Electronics GmbH B6000 Frankfurt/Main Kupferstrasse 14 West Germany
- ISRAEL: Electromics Ltd. 69 Gordon Street, Tel-Aviv Israel
- NETHERLANDS, BELGIUM, LUXEMBOURG: Conex Veendhoek II, Hattem, Holland

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104 Design an IEEE-488 bus into an FPLA, and speed system operation. An extra benefit: The technique allows you to interface any number of instruments.
114 Standardized interfaces isolate a control computer from its remote processors. You gain design freedom, improve reliability, and save money, too.
124 Speed up PLLs in digital synthesizers. At least three methods can boost VCO slew rate in locked loops. Choose the best for your system.
130 Let your scope measure its own rise time—almost. Using the scope's internal generator, you not only can pin down an accurate t_r, but do it for less money.
136 Test converters fast. A simple circuit quickly finds nonlinearity, missing codes and other errors. Best of all, the circuit handles many kinds of converters.
142 Process controls are evolving fast. In set-point systems, logic often out-performs familiar analog circuits such as comparators and conditioners.
148 Improve your digital recorder with a latch circuit that catches all unexpected pulses. The circuit offers a choice of operating accuracies, too.
154 Adjust ferrite-core constants, to suit your coil design needs. You needn’t be limited to those shapes and sizes you find in the catalogs.
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Cover: Photo by Art Director, Bill Kelly.

Intel delivers the 8085, designers just

Sink your teeth into Intel's new 8085. You'll find it's the only microcomputer that combines the performance, economic advantages and total support it takes to be recognized as the new industry standard. So it's no surprise that there are already four announced sources for the 8085. In fact, the deeper you go, the better the 8085 gets.

The 8085, even more than the 8080 it succeeds, is a total design solution, not just a component. It delivers higher performance, for capabilities far beyond the 8080's. It has a higher level of integration, so you can design your products with fewer components, making them more competitive and more profitable. And to help you get those products to market quicker we've given the 8085 the industry's broadest base of system and development support.

Yet the 8085 is fully compatible with the 8080. So your investment in existing designs is protected, and implementing new designs is simplified by the wealth of 8080 software and peripherals at your disposal.

It all adds up to a design solution you won't be able to resist. That's true for a broad range of applications. The 8085 can be designed in as an economical stand-alone three-chip system using the 8085 CPU, the 8155 256-byte RAM with I/O and timer, and the 8755 2K-byte EPROM with I/O or its interchangeable 8355 ROM with I/O.

You can expand this basic system for larger applications using additional RAM, ROM, EPROM and Intel's complete family of first and second generation peripheral controllers, including our four new programmable peripheral controller chips—the 8271* Floppy Disc Controller, 8273* Synchronous Data Link Controller, 8275 CRT Controller and 8279 Keyboard/Display Interface. All these components including 8755 EPROM operate from a single +5V supply.

*Available 4th Quarter 1977
the new microcomputer can't resist.

A multiplexed data/address bus permits integration of many auxiliary system functions—such as clock generation, system control and multiple interrupts—onto the 8085 chip while maintaining 8080 compatibility and the same 40-pin package. And forward-thinking engineers will realize that it is also a link to Intel's future generation microcomputer products.

No microcomputer can match the 8085 as a total design solution because no microcomputer can come close to the 8085's support base. Support for the 8085 includes the Intellec® microcomputer development system with resident PL/M, the high level programming language that can cut months off your software development time. Intellec is the only development system with ICE-85™ providing in-system emulation for faster system development and debugging. Then there's application assistance, training classes and seminars worldwide. And a comprehensive development software library at your disposal.

The quickest way to get a taste of the 8085's power and versatility is with the SDK-85 System Design Kit. It's available now for only $250. You can order SDK-85 and all MCS-85™ components directly from your nearest Intel distributor: Almac/Stroum, Components Specialties, Cramer, Hamilton/Avnet, Harvey Electronics, Industrial Components, Pioneer, Sheridan, L.A. Varah, Wyle Liberty/Elmar or Zentronics.

Or, for more information on the 8085 and SDK-85, use the reader service card or write: Intel Corporation, 3065 Bowers Avenue, Santa Clara, California 95051. Telephone: (408) 246-7501.

intel delivers.
In 1967 we introduced the first high voltage test probe with a built-in meter. It became so popular that we have been adding new models ever since. Now there are five different versions to satisfy the demands of radio, television, appliance, audio, and electrical repair men in a wide variety of high voltage testing applications.

The five models are briefly described below. Our general catalog contains complete applications information, illustrations, specifications, and prices. Write for your free copy.

MODEL 4242—42,000 volts DC. Negative ground.

MODEL 3157—15,000 volts DC. Negative ground.

MODEL 4312—15,000 volts DC. Positive ground.

MODEL 3163—6,000 volts DC. Negative ground.

MODEL 3200—10,000 volts AC.

AVAILABLE THROUGH YOUR FAVORITE ELECTRONIC PARTS DISTRIBUTOR
Across the desk

What about Berliner?

I was astounded to find my grandfather's name conspicuous by its absence from your voluminous spread on the history of the telephone (ED No. 18, Sept. 1, 1977, p. 42). For your information, it was Emile Berliner's microphone that established the Bell System commercially, and saved it from destruction at the hands of the then-powerful Western Union.

In the Bell System's own publication, *Ten Men & The Telephone*, Emile Berliner is listed second only to Dr. Bell himself. Oh yes, you do mention my grandfather and Francis Blake—incorrectly, at that. But you do not see fit to include these two greats in your chart on p. 43, despite the fact that it was "the three B's" who put AT&T firmly on the map.

*Oliver Berliner*
Maker of the Microphone Award
P.O. Box 921
Beverly Hills, CA 90213

More capable than that

For future reference, there appears to be some confusion between the VDP-1000 and the VDP-400 video display processors from Lear Siegler (ED No. 16, Aug-2, 1977, p. 128), both of which were announced concurrently at the National Computer Conference. The first two sentences of your presentation are accurate for the VDP-1000. But 8 kwords of ROM, 3 kwords of refresh and scrolling, and 5 kwords for user discretion are characteristics of the VDP-400, not the VDP-1000. The VDP 1000, in fact, is envisioned as totally user-programmable, including the terminal-handling program. Thus, all 16 or 32 kwords are left to user discretion with the VDP-1000.

Moreover, the VDP-400 does not have VMOS, floppy-disc or stand-alone computing capability. It costs $2500.

*Charles Ramsey*

LeAnce & Reiser
Public Relations/Advertising
3189 Airway Avenue B
Costa Mesa, CA 92626

CIRCLE NO. 557

Misplaced Caption Dept.

Whaddaya mean the circuit blew?

Sorry. That's Jacopo Robusti's (Tintoretto) "Portrait of Vincenzo Morosini," which hangs in the National Gallery in London.

(continued on page 8)
Across the desk
(continued from page 7)

Over 40 and out

Your career and salary survey (ED No. 16, August 2, 1977, p. 36) offers convincing proof of age discrimination in employing U.S. EEs. "Just as in the oldest profession, inexperience is rewarded most in electrical engineering" (Irwin Feerst).

Strip off the under-25 newies who can't find the job yet and you have an interesting age vs response plot from your random survey. Plot that along with the number of EEs who graduated for each age group and you are left with one conclusion. There are a hell of a lot of older ex-EEs. If you're over 40, pray. Under 40, start planning for a new career. Not all ex-engineers can get elected president.

Dave Weigand, PE
904 Tyson Dr.
West Chester, PA 19380

Hidden treasure

John L. Alexander in his "Across the Desk" letter "Wage Busting Is The Real Issue" (ED No. 12, June 7, 1977, p. 8) states: "The fringe benefits for government employees lie in the area of 70% of their salaries...." My colleagues and I are looking for our short-fall of 40%.

W. M. Weinbach
Electronics Engineer
Naval Surface Weapons Center
White Oak Laboratory
White Oak, MD 20910.

Dept. of corrections

Responding to questions raised by Amarnath Sethuraman of the Astronautics Corp. of America in Milwaukee, Robert J. Stetson, author of "Design Your Own Data Terminal..." (ED No. 16, August 2, 1977, p. 56) offers the following corrections:

11, "...load-timing generator, the Count Down signal from the memory-ready. Printer-timing logic..." should be changed to "...load-timing generator. The Count Down signal from the memory-read/printer-timing logic...." On p. 59, column right, line 1 (Fig. 3) should be (Fig. 4). And on p. 61, column right, eight lines from the bottom, the Load signal is actually a Latch signal.

Inversion signs have been omitted from some signals. But timing is the essence in those cases and not polarity, which can be adjusted simply.

In addition to the corrections prompted by Mr. Sethuraman's questions, Mr. Stetson would like to change "serial 6-bit" on p. 56, column right, lines 10 and 12, to "serial 8-bit."

LSI chips do it, too

Your article in the August 2, 1977, issue (ED No. 16, p. 56) on how to interface the Victor Comptometer IMP 130 dot-matrix printer was well done. I wish to add, however, that now you can buy LSI chips that do the job. For example, the Cybernetic Micro Systems CY 480 Universal Printer Controller is a single-chip, 40-pin LSI device that controls 5 x 7 dot-matrix printers, including Victor, LRC, and Practical Automation models. Features include:

- 96-character (upper and lower case ASCII) generator.
- 48-character line storage.
- Variable-character-inch printing density.
- Graphics capability.

Erik K. Huang
Project Engineer
Microprocessor Systems Design
2460 Embarcadero Way
Palo Alto, CA 94303

Yehudi plot thickens

In answer to I. Borditch's query (ED No. 11, May 24, 1977, p. 7) about the "Yehudi circuit" (if my memory serves me right, my mother had a 78-rpm platter with the song, "Who's Yehudi??") a humorous song whose lyrics I cannot recall. The record was darn near 3/16 in. thick, so it had to be an early 78. Perhaps an old-timer will remember this song and be able to tell you more.

Norm Andrews

New Books


CIRCLE NO. 559

Active Network Design—C. S. Lindquist, Steward & Sons, P.O. Box 15282, Long Beach, CA 90815, 749 p. $21.95.

CIRCLE NO. 560

Memory Databook—National Semiconductor, 2900 Semiconductor Drive, Santa Clara, CA 95051, 550 p. $4.

CIRCLE NO. 561

FET Databook—National Semiconductor, 2900 Semiconductor Drive, Santa Clara, CA 95051, 277 p. $3.

CIRCLE NO. 562


CIRCLE NO. 563


CIRCLE NO. 564


CIRCLE NO. 565

Me an editor?

If you'd like to be among the first to know (and write about) what's going on in the electronics industry, you might enjoy being an editor.

We have openings at our home office in Rochelle Park, NJ. Call Ralph Dobriner at (201) 843-0550.

We got the name wrong

The magnetic-tape transport system described in ED No. 22, Oct. 25, 1977, p. 28 was not developed by Micro Components Corp., Waltham, MA. It was developed by Micro Communications Corp., 80 Bacon St., Waltham, MA. 02154; (617) 899-8111.

CIRCLE NO. 567
HP's new System 45: an efficient way to handle a small department's computing needs

In its compact, desktop-sized chassis, HP's new Series 9800 System 45 blends the speed and power of a minicomputer with the friendliness and convenience of a programmable desktop calculator. System 45 incorporates in a single package the high performance hardware and accessibility that scientists, engineers, designers and managers need to solve computational problems right in their own work area.

In less than 35.1 kilograms (77.5 pounds) System 45 integrates:
• an interactive keyboard with alphanumeric, control, editing, and special function keys.
• a dual processor that provides overlapped processing for increased throughput.
• a CRT with high-resolution graphics capability and an alphanumeric mode that offers an 80-character, 24-line screen.
• two built-in, 217k byte, high-speed tape transports, one of which is optional.
• 16k bytes of read/write memory expandable to 64k bytes.
• a unified mass storage that permits available storage devices to be addressed with device independent commands.
• ready-made I/O capability for BCD, bit parallel, bit serial, real-time clock and HP-IB interfaces.
• a powerful language—ANSI standard BASIC, with FORTRAN-like capabilities available on command—plus a library of utility and application programs.

For computer aided design, System 45 places the entire design process directly under your control. It lets you display parts tables, parts cross sections, or produce complete drawings.

For data acquisition, System 45 interfaces directly with instrumentation, with 15 levels of interrupt for flexible control.

For business administration, System 45 lets you increase efficiency in various areas of business such as: forecasting, inventory control, payroll, optimization and even text processing.

System 45 is also expandable. To meet your needs in the future, HP offers you an extensive line of peripherals including: flexible disks, large fixed discs (up to 50M bytes), a full page printer, plotters and more.

For more information, check B on the HP Reply Card.
New signal source combines choice of waveform and high accuracy with easy programming

Its very wide frequency range of 0.001 Hz to 50 MHz makes the 8165A the fastest waveform generator of its kind. Output amplitude and signal quality satisfy many analog and digital applications. Its easy-to-use HP-IB interface ensures rapid system integration at minimum cost.

The 8165A programmable signal source generates precision sines, square waves, pulses and triangles. Crystal control provides a frequency accuracy of 0.001% across the entire range.

Its variable, 20V peak-to-peak amplitude, and clean, 5 ns transition time pulses are perfect for digital applications. Amplitude and offset are programmable with 2% accuracy to 5 MHz.

Microprocessor control sets new standards in operator convenience. Keyboard and LED's together with the instrument’s high accuracy, allow direct entry and display of desired waveform parameters.

In systems, the intelligent 8165A cuts software development costs and computer time. Keystroke programmable means identical control sequences for front panel and bus-entered commands. Programming mnemonics for all keys are indicated on the front panel. Error detection and learn mode are also provided.

The 8165A stores parameters for 10 complete waveforms. An entire waveform can be stored and subsequently recalled simply by pressing two panel keys or by a single program step. Batteries provide storage of all parameters for up to four weeks.

 External trigger, synchronous gate, counted burst, VCO, FM and optional sweep modes provide the flexibility to use the 8165A in many different applications. The selectable 50 ohm source may be disabled, inverted or operated in dc mode. All specifications are guaranteed from 0 to 50°C for full confidence in system applications.

For more information check K on the HP Reply Card.

The 8165A offers choice of waveforms, wide frequency range, variable 20V amplitude, dc offset, direct parameter entry and readout, full HP-IB programmability.

Extend signal capability of popular 8654 and 8640 generators down to 10 kHz

New HF down converter now covers test applications in the 10 kHz to 11 MHz band.

A new down-converter, HP 11710B, translates signal inputs of 50.01 to 61.00 MHz from RF signal sources such as the HP 8654 and 8640 to the 10 kHz to 11 MHz frequency range. This wider frequency coverage provides a convenient extension to other applications such as IF testing at 262 kHz.

The 11710B preserves both the AM or FM modulation of the input signal. In fact, it permits higher FM peak deviations than the generators themselves.

Output flatness is ±0.5 dB referenced to 4 MHz and level accuracy is ±(1 dB + input level accuracy). Harmonics are greater than 35 dB below carrier (dBc) and spurious signals are below -60 dBc.

The internal reference oscillator is stable enough to yield a drift of less than 0.05 ppm/hr. and typical overall frequency accuracy of ±2 ppm.

A function selector allows straight-through switching so the total range (0.01 to 1100 MHz) of the signal source is available at the 11710B output port. Source inputs are tracked from 0 to -107 dBm in the down-converted mode and there is less than 1 dB loss in the straight-through modes.

For more information, check M on the HP Reply Card.
Extensive program support for HP 67/97

Hewlett-Packard presents a large selection of problem-solving software for personal programmable calculators. The software works with the HP-67 and HP-97 calculators to provide solutions for a wide range of applications including engineering, science or business.

You can solve your computational problems without writing programs—by using the Application Pacs. And with our Users’ Library Solutions, you follow the easy step-by-step instructions to enter the program yourself.

**Application Pacs.** Each Pac contains an instruction manual with up to 25 pre-programmed magnetic cards. Current Pacs include Statistics, Math, Business, Surveying, Games, Electrical and Mechanical Engineering—plus the new Navigation, Civil Engineering and Clinical Lab Pacs. They save you time and trouble researching, writing, debugging and documenting.

**The Users’ Library.** Over 1000 HP-67/97 programs and over 5000 easily modified HP-65 programs are currently available from the Library.

**Users’ Library Solutions Books** A series of comprehensive books containing the most popular programs from our Users’ Library covering applications in Engineering, Home Construction Estimating, Aviation, Energy Conservation and more. Each booklet contains 10 to 12 programs.

For more details on these calculators and these programs, check A on the HP Reply Card.

New software solutions for the HP-67 and HP-97 have been added to help increase your problem solving potential.

**New sweeper plug-ins offer expanded wideband performance**

Double-octave and communications band RF plug-ins for HP 8620C sweeper provide 2.0 to 8.6 GHz frequency coverage.

<table>
<thead>
<tr>
<th>Freq. (GHz)</th>
<th>2.2</th>
<th>8.6</th>
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</thead>
<tbody>
<tr>
<td>Insertion characteristics of 4-8 GHz bandpass filter. Lower rejection band (left portion of trace) shows freedom from harmonics in HP 86240B RF source.</td>
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</tbody>
</table>

For more information on these and other RF units for the 8620C sweeper, check N on the HP Reply Card.

**HP Journal features NMOS-II**

An article of interest, regarding HP's on-going research and development in LSI technology, is featured in the November 1977 issue of the HP Journal. It deals with HP's NMOS-II process, which made possible the high-performance, large-scale integrated circuits for fast 16-bit microprocessors, 16k read-only memories and a variety of special purpose random-logic chips.

The newest product featuring NMOS-II is the System 45 (cover article).

For your copy of the HP Journal, check P on the HP Reply Card.
New logic state analyzer is portable, totally programmable

A new small but powerful logic state analyzer interacts with its user through an easy-to-master keyboard. And, its programmability option provides the capability of a functional automatic digital test station.

The new 1602A logic state analyzer was designed for ease of use in production, field service and engineering. The layout of the keyboard leads you through a natural progression of keystrokes and entries are displayed, enabling you to check their accuracy every step of the way.

For use in design and troubleshooting of digital systems, the 16-bit wide and 64-word deep memory operates at clock speeds to 10 MHz, allowing the instrument to capture virtually any 64-word sequence in a system.

Measurements of system activity are displayed on the analyzer's LED readout in hexadecimal, decimal, octal, or binary format, eliminating the need for base conversions by the operator.

For more consistent and repeatable measurements, the HP Interface Bus option allows you to make automated functional tests of digital systems. The HP-IB option makes the 1602A totally programmable and able to dump its 64-word memory into the bus on command, for analysis by a desktop computing controller such as the HP 9825A.

Simplicity of use is also apparent in the quick connect and disconnect standard edge connector on the probe. Point-to-point probing on new equipment installed with similar connectors is now fast and easy. The single pod contains all 16 data lines, clock, qualifier and ground.

Weighing only 4.5 kg (ten pounds), it is small enough to fit into a briefcase. The price is small, too.

Can signature analysis make your service operation more efficient?

There's a good chance that it can. HP and over 100 other companies are currently implementing this new digital service strategy. And, they are cutting repair times, reducing spares inventories and streamlining documentation.

Today's microprocessor-based products are tough to troubleshoot. Tomorrow's digital products may be tougher, and the costs of board exchange, the traditional digital service strategy, tend to escalate rapidly in fast-growth, high-technology product lines.

Design signature analysis into your new products. Document the troubleshooting procedures with the appropriate signatures. Then, use the HP 5004A Signature Analyzer for component-level troubleshooting:

- on-site
- at the field office
- at the service center
- on the production line

This portable tester detects and displays unique signatures associated with nodes in digital products. By comparing actual signatures to correct ones as shown in the product manual, a technician can backtrace to the faulty node in a malfunctioning product.

Check into signature analysis. Make your service operation more efficient and prepare for the future at the same time.

For more details, check E on the HP Reply Card.

Many companies are streamlining field service of microprocessor-based products by troubleshooting to the component level with the 5004A signature analyzer.
New 4½ digit autoranging DMM with 1 mΩ, 1 µV dc, 10 µV ac sensitivity

The new HP 3466A 4½ digit, six-function autoranging digital multimeter combines low cost with high accuracy for both bench and field use.

Dc measurements can be made from 1 µV to 1.2 kV with a mid-range accuracy of ±0.03%. True rms ac measurement range is from 10 µV to 1200 volts with a mid-range accuracy of ±0.03% over a 20 Hz to 100 kHz bandwidth.

Ac and dc current measurement range is 10 nanoamps to two amps. Resistance range is 1 milliohm to 20 megs with a mid-range accuracy of ±0.03%.

An ohm zero adjustment on the front panel is provided. Milliohms may be offset on the front panel, allowing the zeroing out of test leads when making printed circuit, transformer, coil, or switch contact measurements.

A new diode test measurement capability is offered. The 3466A DMM displays the voltage drop across the diode junction in the forward direction, allowing the user to measure and identify germanium, silicon, light-emitting and Schottky diodes in units of volts, even though the instrument is in the ohms function.

The standard HP 3466A includes rechargeable, lead-acid batteries which provide 8 hours of continuous use. Option 001 offers ac power only. Should battery power be required in the future, the DMM can easily be modified in the field.

For more information, check H on the HP Reply Card.

Because of its ability to make wideband selectable ac plus dc true rms voltage and current measurements, the new HP 3466A digital multimeter can also measure such signals as digital pulse trains and sinusoidal waveforms.

Hard copy made easy with two new smart printers

Two new "smart" printers operating at 180 characters per second are now available from Hewlett-Packard. Both printers are controlled by a silicon-on-sapphire (SOS) microprocessor system designed by HP. The HP 2631 is designed for environments requiring a low-cost, high-performance printer. The HP 2635, with a keyboard, is suited to interactive environments.

The microprocessor control optimizes data manipulations, and printing and control functions. Consider the path taken by the print head. It is fast and bidirectional, that is, the printer chooses the most efficient direction to print right to left or left to right, increasing throughput as much as 50%. By the time one line is printed, the next several lines have been processed and stored in a buffer.

When ten or more adjacent spaces have been detected within a line, the head speeds to the next printable character at an accelerated rate of 450 cps.

The HP 2631/2635 offer as standard features those capabilities that are often optional on other printers. For example, there are three print modes that can be intermixed on a line—normal, expanded, (for titles and headings) and compressed. Vertical line spacing is variable under program control; the choices are 1, 2, 3, 4, 6, 8 or 12 lines per inch.

Both printers support the entire US ASCII 128-character set, including control codes which are accessible through the display functions. Use of a 7-column by 9-row dot matrix allows printing of true descenders, commas, semi-colons, and underlining. The printers also accommodate subscripts and superscripts.

A variety of interfaces are available including HP-IB, 8-bit duplex, 8-bit differential, and a general purpose parallel interface for OEM applications.

For more information, check F on the HP Reply Card.
New HP-IB switches for automatic test systems

The availability of individual HP-IB switch products gives you modularity and flexibility in the design of your automatic test equipment (ATE) system. These microprocessor-based switch products provide a flexible, high-performance and cost-effective solution for computer and desktop controller-based systems.

Up to 8 switch mainframes are controlled by the microprocessor-based HP 9411A Switch Controller, also capable of performing comprehensive self tests and fault isolation of all signal relays in the switching units.

Three new switches provide commercially available solutions to an important part of the ATE system—connecting the system to the unit-under-test (UUT).

HP 9413A VHF Switch provides flexible high-frequency switching of pulse and video signals up to 500 MHz. The unit accommodates up to 12 coaxial switch modules of two types: dual 1 x 4 or single 1 x 8.

HP 9414A Matrix Switch provides maximum flexibility for high-density, high-performance switching, allowing any UUT pin to be switched to any instrument in the ATE system. The 16-input Matrix Switch can be configured in 30-pin increments (UUT pins) up to 120 pins, expandable to 240 pins.

New automatic test systems are also available from Hewlett-Packard complete with HP-IB hardware and new software. The system controller is the HP 1000 with HP’s powerful Real Time Executive (RTE) operating system. RTE allows concurrent program preparation and testing. Comprehensive test program languages are available including BASIC, FORTRAN IV and TESTAID-III for digital testing.

For more information on individual HP-IB switch products and the new generation HP automatic test system, check L on the HP Reply Card.

Current tracing: a better way to detect supply to ground shorts

You’ve got a tight schedule to meet and those five bad boards on your desk can make the difference. Unfortunately, every one of them has a power supply to ground short and you don’t have the time it takes to repair them. Each of the boards is valuable, so you don’t want to scrap them, but it would take a couple of hours to fix each one and when you were finished, chances are the circuit traces would be damaged, IC legs cut and resoldered, or worse.

Well, there’s a better way—current tracing. This technique allows you to find Vcc to ground shorts in minutes, using two powerful hand-held IC troubleshooters from HP.

One, the 546A Logic Pulser, is connected between supply and ground on the unpowered faulty board and push-button programmed to output a 100 Hz pulse stream. The pulser delivers 650 mA current pulses that are easy to trace right to the one faulty point on the board.

The 547A Current Tracer allows you to find faults based on one simple principle: current flows to the lowest impedance point in a circuit, in this case a short between Vcc and ground. So, just adjust the sensitivity control so the tracer’s lamp is about half-brilliance and follow current pulses to the fault.

No board scrapping, no trace cutting, no unnecessary unsoldering and still the boards are repaired in a fraction of the time possible using any other method.

For more information, check C on the HP Reply Card.
Sliding load for 3.5mm coaxial lines operates from 2.0 to 26.5 GHz

For impedance measurements in coaxial transmission lines, the ultimate standard for a matched line is a sliding load. By sliding the load element along the line, its own small reflection effect can be eliminated.

Since the new APC-3.5 connector now permits design activity in 3.5 mm coaxial lines above 18 GHz, HP’s new 911C sliding load will provide for more accurate measurements from 2.0 to 26.5 GHz.

The 911C features interchangeable APC-3.5 fittings—either male or female connectors may be checked. For minimum discontinuity, the center conductor slides and locks. The movable terminating element has 5.5 cm travel—greater than 1/4 at the lowest operating frequency.

The connector and transmission line reflection coefficient for the female configuration is \(< 0.02 + 0.001 \times f\) (where f is frequency in GHz) 2 to 26.5 GHz. The male version is \(< 0.02\) across the full band. For the load element itself, the maximum reflection coefficient is \(< 0.01\) from 2 to 10 GHz and \(< 0.035\) from 10 to 26.5 GHz.

For details, check D on the HP Reply Card.

New displays with high light output

New large junction seven-segment displays are categorized for luminous intensity. Now available from Hewlett-Packard are new, high-efficiency red, and yellow displays designed for use in high light ambient conditions.

Output is typically 2300 millicandellas per segment at 100 mA peak, 20 mA average. These displays are designed for use in instruments, airplane cockpits, weighing scales and point of sale terminals.

The seven-segment displays offer a wide viewing angle and are easily mounted on P.C. boards or sockets. DIP spacing is the industry standard 7.62 mm (0.3 in.) on 2.54 mm (0.1 in.) centers.

The HDSP-3530/4030 are 7.62 mm (0.3 in) high while the HDSP-3730/4130 are 10.9 mm (0.43 in). These devices utilize high efficiency LED chips made from GaAsP on a transparent GaP substrate. The LEDs have a large area P-N junction permitting higher peak currents.

For more specifications, check I on the HP Reply Card.

HP publishes optoelectronics applications manual

Practical solutions to the most common applications problems of optoelectronic devices are fully analyzed in Hewlett-Packard’s Optoelectronics Applications Manual, one of the first books on these versatile design tools from a leading firm in the field.

The Manual covers such subjects as photometry/radiometry, contrast enhancement in visible displays, and reliability of optoelectronic components and their mechanical handling.

Designed both as a practical guide to the use of optoelectronic devices and as a foundation for the development of new design ideas, this volume demonstrates the broad potential for these components that exists in systems being designed today.

Of special interest to experienced designers is the Manual’s treatment of CTR degradation, a controversial and frequently misunderstood subject among users of optically coupled isolators.

Members of the applications engineering staff of the Hewlett-Packard Optoelectronics Division were involved in the preparation of the Manual, published by McGraw-Hill.

Copies are available from your HP franchised distributor.
Flexible synthesizer uses μP for FDM testing and other applications requiring precision signal source

The new 200 Hz to 80 MHz HP 3335A Synthesizer/Level Generator is designed for frequency division multiplex (FDM) testing as well as traditional synthesizer applications such as testing filters, mixers, phase detectors, attenuators or modulators.

With a resolution of 0.001 Hz and amplitude flatness of 0.15 dB over its entire range, the 3335A is useful for applications including testing of low-density carrier, radio baseband, high density cable carrier, in R & D, and in production tests. For automated instrumentation systems, the unit includes the HP Interface Bus as standard.

Microprocessor control provides flexibility in this moderate cost, high resolution synthesizer. In the sweep mode, the microprocessor computes the individual frequencies on each side of the center frequency and then controls automatic, manual and single sweep modes. At turn-on, the μP sets the instrument to 1 MHz and minimum amplitude so output loads will not be damaged.

Up to ten different instrument settings including frequency, amplitude, sweep width and center frequency may be stored in the ten memory registers for later recall—useful in a production environment where a specific list of repetitive test functions must be performed.

New microprocessor-based frequency synthesizer is used in applications wherever a high resolution, precision amplitude test signal is needed.

The 3335A synthesizer may be used as a tracking generator for the HP 3745A/B Selective Level Measuring Set for fast, accurate loop-back measurements and for end-to-end measurements. For unattended performance checks of systems on-line or for offset tracking of systems off-line, the generator/receiver system may be controlled via the HP Interface Bus.

Standard version of the 3335A synthesizer provides 50 and 75-ohm unbalanced outputs. Other options accommodate North American and CCITT communications applications.

For additional information on the synthesizer, check G on the HP Reply Card. For details on the 3745A/B SLMS, check O on the HP Reply Card.
Good news! Two new ten-bit digital-to-analog converters from the folks who know how to make them monolithically. And each is completely ‘complete’! Includes internal reference and output op amp. They are fast (1.5 µsec settling time), with voltage outputs, yet consume only 350mW (max) over the entire military temp range (−55°C to +125°C).

**DAC-05:** Sign-magnitude coding (sign-plus-ten-bits).

**DAC-06:** Two’s complement coding.

Both DACs are available now specified over the full temp range. Off the shelf to MIL STD-883A Level B. Reliability is enhanced by 100% burn-in, hermetic packaging for all parts, PMI’s famous triple passivation, low noise process and no laser trimming.

Data sheets are ready. Parts are on the shelf. Write, wire or phone. Precision Monolithics, Inc., 1500 Space Park Drive, Santa Clara, CA 95050. (408) 246-9222. TWX: 910-338-0528.

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Bell modems face redesign to meet FCC demands

By declining to review a lower court decision, the Supreme Court is forcing the Bell System to redesign its modems to bring them into compliance with FCC specifications. Though Bell is seeking to delay implementation of the decision, as of now it must have new equipment, perhaps as soon as January 1—or face giving up the modem market to independent suppliers that already have FCC registration.

The FCC requires that modems meet a set of standards to guarantee that no harm will come to the Bell system or its employees when the equipment is tied directly to telephone lines. But when the FCC demanded that Bell meet the same set of standards, the company balked, pointing out that since modems are installed and maintained by its own technicians, not by customers, the equipment is unlikely to cause hazards.

While Bell modems can meet most of the safety aspects of the FCC’s rules, some cannot meet all the requirements. For example, a modem cannot have user-accessible controls, such as strapping connections, that can be configured so that a hazard exists. “Older modems would not pass the test,” says Bob Hamer, product and services marketing manager at Bell in Morristown, NJ.

Under a “grandfather” clause in the FCC rules, Bell will continue to support the hundred or so different modem models that are already in the field. Bell modems and independent modems that are connected via data-access arrangement (DAA) modules need not be replaced, though all new models must have FCC registration before they can be installed on telephone lines.

In the past, a modem customer had to have the telephone company install a DAA before hooking up a modem from an independent supplier. The DAA rented for about $5 a month after a $10 installation charge.

Now, the protective functions of the DAA must be incorporated into the modem itself. The user has the telephone company install a data jack, which interfaces directly with the modem. The phone company installs the proper data jack when the customer gives the model or registration number of the modem. There is a one-time installation charge of about $30, and no rental fee.

The Bell System will likely continue offering DAAAs after January 1, though units already in the field will continue to be maintained, says Hamer.

The advantage to the customer of the new arrangement is lower cost, says Ken Krechmer, national sales manager at Vadic Corp., Sunnyvale, CA. Incorporating the features of the DAA into a modem raises its price about $30, so the total additional cost—including the $20 additional installation cost of the data jack—is about $50. But this additional cost will be paid back in 10 months because the $6 monthly charge for the DAA is eliminated.

Krechmer says that evidence of customer interest in direct-connected modems is the higher sales of the newer units—in one case, 1000 units per month compared with 200 units per month of a similar modem that lacks registered protective circuitry. This increase comes in spite of a lack of data jacks in some areas, he points out.

Hamer concedes that there is a shortage of data jacks, due in large part to an inability to forecast demand for modems from independent suppliers. “You don’t know how many are needed, but we’ll catch up, I’m sure,” he says.

At the same time, Bell is working on upgrades of some models to bring them into compliance, and may need completely new designs to replace units that are older or would be too expensive to rework. Though the FCC has not yet set a deadline for compliance, its original effective date for industry compliance was January 1, 1978.

Yet Bell is seeking a delay beyond the January 1 deadline to gain time to bring equipment into compliance. Opposing Bell’s request for a blanket temporary waiver is the Independent Data Communications Manufacturers Association in Washington, DC. “We have a final judgement in court, but there will be at least one further proceeding at the FCC,” says Herb Marks, general counsel to the IDCMA, which feels that the company has had enough time to study the standard, design equipment that complies, and have it registered at the FCC. In addition, the IDCMA feels the waiver request is too broad and indistinct. “There’s a range of things they could be asking,” says Marks.

As R & D spending goes, so goes our technology—down

The slow decline of American science and technology over the past decade continues, and if current levels of research and development spending don’t improve, it’s going to get a lot worse.

This ominous prediction was made recently by Dr. Thomas A. Vanderslice, vice president and group executive of General Electric’s Special Systems and Products Group, in an address before the Atlanta Rotary Club.

While industry spending for R & D has just about kept pace with inflation, Vanderslice noted, the federal government’s share of total R & D funds has dropped from almost two-thirds in 1966 to slightly over half in 1976. Even with the space programs taken out of the picture, the decline in R & D expenditures was still over 20% during the past decade, he pointed out.

Pointing to the impact of reduced federal spending for R & D on American universities, Vanderslice observed, “Perhaps the most drastic cutbacks made by the federal government have been in the graduate fellowship and traineeship programs—which provide the trained scientists and engineers we will need in the years ahead.”

This 10-year decline in spending contrasts sharply with the significant and even dramatic increases in funding undertaken by many other industrialized nations. Over the past 10 years, West Germany has increased her R & D expenditures a striking 40%—and Japan has hiked hers a monumental 74%. These increases, together with the high growth of plant and equipment investments and favorable tax policies, are producing strong productivity gains.
As if things weren't grim enough, Vanderslice added that the U.S. share of patents filed worldwide as well as the number of U.S. patents awarded to American inventors have both declined in the past decade. Meanwhile, U.S. patents granted to foreign inventors have more than doubled—an eye-opening measure of the foreign technological invasion of U.S. markets. The favorable patent balance with Japan has been dropping steadily since 1962, with Japanese patents on inventions in the U.S. increasing some threefold.

All these trends make it essential to wonder just how long the U.S. can continue to enjoy its favorable technological balance of trade, according to the GE executive. The U.S., he pointed out, has consistently been selling four to five times more technologically intensive products to other nations than it has purchased from them. This has been a major contribution to U.S. jobs and has resulted in an improvement in our balance of trade.

IC tester handles 120-pin devices

With the electronics at the test socket converted from discrete to hybrid and monolithic form, the Sentry automatic test system from Fairchild Systems Technology Division can handle 120 pins—twice as many as before.

The Sentry VIII's circuitry, mounted on cards near the test socket, includes comparators, converters, and op amps used for such analog measurements as level and polarity. In earlier designs, the cards were too large to mount 120 of them close enough to the test socket to minimize measurement errors caused by stray capacitance and other effects.

Each of the Sentry VIII's pins can be programmed to act as an input driver, output comparator, input clock, bias supply, load, or input/output. The earlier Sentry VII system has the same flexibility, but only up to 60 pins, and the Sentry IV system has as many as 120 pins, but no more than 60 of them can be assigned to any one function at a time.

The $500,000 Sentry VIII is designed for engineering characterization, startup production, and incoming inspection testing of very-large-scale ICs. Microprocessors, random-access memories, and random-logic circuits that require a tester with 120 pins are in development and, in some cases, are already in production for internal use, according to Gene Griggs, product marketing manager at Fairchild Systems Technology, San Jose, CA. Fairchild has already begun shipping Sentry VIII systems for such requirements, with "a significant number" going to Japan, he adds.

The Sentry VIII can perform functional tests at up to 10 MHz by feeding data into the device under test and comparing the device's outputs with expected values. In addition, the tester can check dc parameters at rates to 300 tests per second.

Direct addressing way up with 32-bit computer

A virtual memory that provides a direct-addressing capability of over 4-billion bytes is the main feature of the 32-bit VAX-11/780 (Virtual Address eXtension) computer. What's more, the virtual-memory operating system of this latest addition to Digital Equipment's PDP-11 line applies mainframe software technology so that programs much larger than the main memory can be run in a way that is transparent to the programmer.

The main memory contains an Error Correction Code MOS memory that uses 4-k MOS RAM chips. The smallest system configuration provides 128 kbytes of physical memory, expandable up to 2-million bytes. The instruction set, consisting of 234 instructions, nine addressing modes and five data types, includes integral floating-point, packed-decimal arithmetic, character-string manipulation and context-switching instructions.

A diagnostic console contains an LSI-11 microcomputer that provides automatic consistency and error checking to detect abnormal use of instructions or illegal machine conditions.

Like other PDP-11s, the VAX-11/780 uses both DCL and MCR command languages and implements Fortran-IV-Plus, Basic-Plus-2 and COBOL languages. A unibus connects the 11/780 to peripherals.

The VAX-11/780 begins at $130,000.

Small laser modulator requires less power

Cadmium-telluride-waveguide laser modulators, the first to be fabricated by proton bombardment, have several advantages over those made by conventional epitaxial processes.

These modulators require but a fraction of the power to give the same degree of modulation as competing devices in the 3 to 10-µm infrared region.

- The modulators are substantially smaller.
- The low optical absorption and high electro-optic coefficient of cadmium telluride permit these modulators to be fabricated in two forms: narrowband acousto-optic devices that use surface acoustic waves to defract the laser beam, and broadband electro-optic devices that operate by shifting the phase of the laser frequency.
- They can be produced at substantially lower cost.

Developed for the design of compact low-power carbon dioxide laser radars for the Air Force at MIT's Lincoln Laboratory, Lexington, MA, the cadmium telluride devices may prove useful with other infrared lasers in gas and pollution monitoring equipment.

The waveguides, according to Laboratory researchers D.L. Spears and A.J. Strauss, are formed by bombarding the selected areas of cadmium telluride wafers with protons from a Van der Graff generator. The acousto-optic modulators, which have a bandwidth of 1 MHz, use 27-MHz surface acoustic waves generated by interdigital electrode transducers.

This MIT modulator produces the same modulation level as that of germanium modulators 10 times larger.
Can you find solutions to your design and cost problems from these standard Bivar Packaging Aids?

Yes, because someone else probably had a similar problem before you did. In fact, during the past decade Bivar has introduced nearly 1,000 standard products, most designed originally to solve costly Printed Circuit Board packaging or component mounting problems. These have resulted in lower assembly costs, fewer rejects and improved quality of product appearance and performance. Take for example, the advantages of accurately supporting transistors, capacitors and other devices. Components are protected, insulated against heat damage and uniformly positioned by using Bivar PERMANENT MOUNTS and SPACERS, made of durable Nylon per MIL-M-20693A. Hundreds of standard styles for virtually any PCB component; low-cost and carried in stock by the thousands. For accurate, uniform component spacing above PCB surfaces, over 400 standard sizes of Bivar WASH-AWAY SPACERS assure proper filleting and heat dissipation, and eliminate lead stresses and strains, washing away in warm or hot running water without a trace of residue. These extremely low-cost devices, designed for exacting application for almost any component, substantially reduce rejects and rework.

Bivar can mean the difference in cost-savings and real PCB packaging design flexibility with the industry’s most complete line of SNAP-IN CARD GUIDES; lengths from 2 1/2" through 14", made of reinforced molded Nylon. Snap them into card cages or sheet metal at your spacing requirements. For 1/16" PCBs, these low-cost guides feature rigidity, card insertion and assembly ease, and are stocked for immediate shipment.

For new, demanding designs, Bivar Flame Retardant Card Guides offer the same range of sizes made of 94 V-0 U.L. rated material; help the designer to meet flammability specifications. New Deep Channel Card Guides, with a .200" slot depth for maximum retention under shock and vibration or for larger PCBs. All stocked at low, cost-savings prices.

Whether you are mounting components on PCBs, or packaging completed PCBs, Bivar can provide answers that will save time, money, and improve your product’s appearance. Find out about the Bivar "Cost Savers." Choose from over 900 standard products.

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Firmly support L.E.D.’s above PCB surfaces maintaining bases parallel to board surfaces, preventing parasitic effects and rigidity of mounts prevent bending or lifting of L.E.D.’s during handling and final assembly. Heights from .060" through .380" in .005" increments, 61 standard sizes are available from stock.

Components, circuitry and cards will be protected from undue stresses, and PCB insertion or removal will be easier with Bivar CARD EJECTORS, designed for 1/16", 3/32", and 1/8" boards; 18 styles, including locking versions to prevent accidental card release. Molded from Nylon per MIL-M-20693A, and U.L. rated 94 V-2 material, these helpful ejectors meet most demanding requirements. Ejectors can be marked permanently for identification, are available in 13 standard colors and are furnished with stainless steel mounting pins.

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Mostek's high-technology leadership in MOS/LSI is not limited to high-performance memories and microcomputers. One of our most significant achievements has been in the telecommunications field. The Tone I™ series of integrated tone dialers—MK 5084, MK 5085 and MK 5086—first introduced in 1974, are today finding their way into over a million telephone products a year. From this technological expertise has evolved a new generation of high-volume products designed for the telecommunication industry. The new Tone II™ series of integrated tone dialers is leading the way with even higher performance features. The MK 5089 and MK 5091 meet the most stringent requirements for an all-electronic telephone or CEPT compatibility. For U.S.A. telephone applications the MK 5090 fits perfectly. And the MK 5087 provides an upgraded pin-compatible replacement for the popular MK 5085 Tone I™ dialer. Packaged in 16-pin DIPs the Tone II™ series offers maximum system density for minimum cost. Mostek's new MK 5102 Inte-grated Tone Receiver provides high quality DTMF detection and decoding in a 16-pin package, with single-power supply and full microprocessor compatibility.

The MK 5098 Integrated Pulse Dialer offers button-to-pulse conversion to a rotary dialing phone, using only direct line power. An 18-pin version, MK 5099, will be available with re-dial features.

Mostek's new MK 5170 Repertory Dialer lets you use your imagination to design a wide variety of telephone-user options. It features an expandable number set, display of number dialed and a repertoire of other attractive features.

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Digital announces
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And thanks to the KT8-A all this memory is under new management. Not only does the KT8-A let you address up to 128K words of memory, but it also offers you memory relocation and memory protection, while asking little in operating system overhead so you get faster system performance.

What's the cost of these enormous advancements? That's the next attraction.

The new PDP-8A MOS memory models are available at prices that are as crowd-pleasing as their performance. For a 16K 8A205 you'll pay as little as $3900 (quan. 1). 8A425 with 64K is as low as $11,000. And the top of the line 8A625 with 128K is yours for as little as $18,050.

They're the new big-memory Eights from Digital. Step right up. Large memories aren't our only new trick.

New hardware and software improvements are also in the PDP-8 spotlight.

The VK8-A is a new low cost PDP-8A option that provides high quality video output plus keyboard and printer interfaces. Video character generation uses a super-sharp 9x9 dot matrix for high resolution on single or multiple CRT monitors up to one thousand feet away.

Also new for PDP-8 users is MACREL/LINKER—a sophisticated assembler with MACRO facilities that lets you implement, expand and update your system faster while reducing software development time.

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**Our Quiet Performer: SE/NE5534.**

If low noise is critical to your design, then you need our new SE/NE5534. There’s not another op amp around with better noise performance. With input noise specified at 4nV/√Hz at 1 kHz, this device can drive a 600-ohm load. Great for quality audio equipment and instrumentation/control circuits. Our quiet performer also offers a generous 10-MHz bandwidth and a respectable 13V/μsec slew rate.

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To: Signetics Information Services, 811 E. Arques Ave., P.O. Box 9052, Sunnyvale, CA 94086
Please send technical data and sample(s) for the following op amp(s):

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- High Slew SE/NE538
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CIRCLE NUMBER 13
The double-sided floppy from number 1

Double storage capacity.
Double media selection.
Double access speed.

Double your storage power with SA 850/851

Store twice as much data as a single-sided, double density drive, four times that of an IBM single-sided single density disk. Reach that data more than twice as fast with two heads and track-to-track access time of 3 ms. Choose from a wider selection of media—single or double-sided, single or double density, sector or hard sector formats. **Capacity.** The SA 850/851 gives you twice as much storage capacity as a single-sided, double density drive. Yet it requires no more cabinet space. One drive packs up to 1600 kbytes unformatted, or 1200 kbytes formatted. Double density gives you 1600 kbytes—compatible and equivalent to the newly announced IBM S/34 two-sided drive. The Shugart SA 850/851 is available now and this drive accepts FM and double density MFM or M2FM encoding.

**Speed.** Data access is faster, too. Just 3 ms track-to-track. Average seek time, including settling, is 91 ms. That’s 71 ms faster than IBM’s two-sided floppy. Remember lead screw actuators? Now you can forget them. The key to faster access is the new Shugart Fasflex™ metal band actuator which provides faster access time with positive, low friction head movement. This more efficient actuator requires less than half the power used by standard lead screw actuators.

**Compatibility.** Media compatible. SA 850/851 drives read and write data on any industry standard single-sided, single or double density diskette, two-sided IBM Diskette 2, 2D or equivalent. Drive Compatible. Upgrading from your existing SA 800/801 is easy. The SA 850/851 is identical in size, outline and electrical interface. Rack mounting? You’ve got it with the “skinny” SA 850R/851R version. Two units mount side-by-side in a 19-inch RETMA rack.

**Even more reliable.** Data integrity and system reliability begin with Shugart’s own read/write head—the same glass bonded ferrite/barium titanate head proven in more than 100,000 installations. Drive mechanical integrity rests on the same industry accepted die cast aluminum chassis technology used in all Shugart Drives. This rock solid recording platform is not a place to cut costs. Shugart keeps data safe, too. Write protect circuitry and a new I/O controlled programmable door lock for better data security are standard.

**First.** Shugart has a habit of being first. First with an IBM-compatible drive. First with double density drives. First with the minifloppy®. And now first to deliver a double-sided drive.

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**See both sides now.**
PRESENTING VMOS FROM A BIG TIME PRODUCER.

With a major producer like Fairchild behind it, you know VMOS is going to be a big star someday. So remember the name: Enhancement Mode Power Vertical Mosfet. Stagename: Fairchild VMOS.

VMOS transistors are going to make the big time by combining the advantages of vacuum tubes—or lower power FETS—with those of conventional power transistors.

AN AWARD WINNING PERFORMER.

Fairchild VMOS gives you high input impedance with direct interface to CMOS. It’s capable of super switching times—10 ns at 1 A. It has highly linear transfer characteristics, high GM, easy paralleling and biasing, protected gates, low Rds (on) and no second breakdown or thermal runway. And here’s the initial cast of characters:

### Device Performance

<table>
<thead>
<tr>
<th>Package</th>
<th>PD</th>
<th>ID</th>
<th>BVDSS</th>
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<td>2N6657</td>
<td>TO-3</td>
<td>25 W</td>
<td>2.0 A</td>
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<tr>
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<tr>
<td>FVN2</td>
<td>TO-39</td>
<td>6.25 W</td>
<td>2.0 A</td>
</tr>
<tr>
<td>2N6661</td>
<td>TO-39</td>
<td>6.25 V</td>
<td>2.0 A</td>
</tr>
</tbody>
</table>

Cross-section of Fairchild’s VMOS power transistor.

INTRODUCING A SUPERSTAR SUPPORTING CAST.

In addition to N-Channel VMOS, Fairchild is also producing the world’s first P-Channel Power Mosfets with all the features of N-Channel. This means you can now get a complementary product line in VMOS technology from a major Power source.

FEATURE PERFORMANCE AT A MATINEE PRICE.

Whether you’re designing CATV, MATV amplifiers, audio drivers, core memories, switching regulators, analog switches, pin diode drivers, lasers, transducer drivers, or microprocessor interfaces, state of the art designs are now possible. And just as importantly, they’re now affordable with Fairchild Power VMOS. Here are some examples:

<table>
<thead>
<tr>
<th>Device Type</th>
<th>PD</th>
<th>ID (on)</th>
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<td>6.25 W</td>
<td>1.5 A</td>
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NOW PLAYING AT A DISTRIBUTOR NEAR YOU.

For more information on VMOS, contact your Fairchild sales office or representative today. Or use the direct line at the bottom of this ad to reach our Power Division. Fairchild Camera and Instrument Corporation, 464 Ellis Street, Mountain View, CA 94042. Tel: (415) 962-3343. TWX: 910-379-6435.

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BELDEN 75TH ANNIIVERSARY

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Two contracts due on Army air-defense system

A $3-billion system to protect Army units in the field against low-flying enemy aircraft should enter the competitive development phase Dec. 3, following Defense Department approval of the concept Nov. 15. The Division Air Defense (Divad) program involves a new radar-directed cannon to be mounted on Army tanks. It will replace a variety of existing antiaircraft defenses, including the 20-mm Vulcan gun, the Nike-Hercules and Hawk missiles, and the shoulder-fired Chaparral and Redeye missiles.

From five major competitors the Army expects to select two for parallel-development contracts covering a two-year "shoot-off," including side-by-side field trials. Two firms are proposing the Swedish Oerlikon 35-mm gun: Raytheon, which would use the Dutch Hollandse Signaal radar, and General Dynamics, which would use a modified version of its own Navy shipboard Phalanx radar. Sperry Rand is proposing a version of its own Vigilante 35-mm gun with the Signaal radar. Ford Aerospace has selected the Bofors 40-mm gun and the Westinghouse radar used on the F-16 fighter, and General Electric is proposing a ground version of its 30-mm GAU-8 gun used on the A-10 aircraft, and the F-16 radar.

The gun is needed, according to the Army, because the current low-level defenses have been outranged and can be outmaneuvered by newer Soviet fighters designed especially for low-altitude operations and by modern missile-armed Soviet helicopters. Divad will be installed first in the Army's M48 tanks, but will be adaptable to other U.S. tanks and NATO tanks. It will complement the long-range Patriot (formerly SAM-D) antiaircraft missile system due to enter production at Raytheon in 1980.

Hemispherical antenna works like four phased arrays

An antenna with a dome covered by passive phase shifters—and a single planar array of active phase shifters mounted at the bottom—will do the job of four separate phased arrays in providing complete hemispherical coverage for antiaircraft and antimissile defense. Nearing completion by Sperry Gyroscope Co. at Great Neck, NY, the antenna is slated for delivery next year to the Army Missile Command at Huntsville, AL.

The new antenna consists of a 113-in.-diameter array of 4544 active ferrite phase shifters covered by a 98-in.-high dome. On the dome are 24,283 passive shifters capable of providing 24 increments of phase delay. The 330-lb dome is made of resin-filled fiberglass honeycomb, and the whole system, including electronics, weighs 1330 lb.

In tests to be conducted by the Army, the antenna will be operated at C-band to evaluate its possible use in an advanced air defense system for the 1990s. However, company officials say the same design can be used to provide hemispherical coverage for aircraft by building a smaller X-band or K-band antenna that can be mounted on the nose or tail of a fighter.

A prototype model had been built by Sperry Gyroscope for a ballistic-missile defense system, but that program was canceled after the U.S.-Soviet treaty
limiting antiballistic missile systems. Another prototype is being tested for ship defense by the company at MacArthur Field, Long Island, using electronics from the Terrier shipboard missile system.

Electronic-materials experiments set for Space Shuttle

Five material-processing experiments—three applicable to the electronics industry—will ride along on an early orbital flight test of NASA’s Space Shuttle, in 1979 or 1980.

The experiments will be placed in a package on the spacecraft and will require their own power supply and data-collection computer. The package itself will be completely automated and require no action by the Shuttle crew other than a command by one of the astronauts to begin the experiments.

Electronics-related experiments expected to exploit the zero-gravity properties of space include vapor growth of alloy-type semiconductor crystals (submitted by Dr. Herbert Wiedemeier of Rensselaer Polytechnic Institute), solid electrolytes containing dispersed particles (Dr. J. Bruce Wagner Jr., Arizona State University) and containerless preparation of advanced optical glasses (Ralph A. Happe, Rockwell International Corp.).

Neither the specific mission nor the exact configuration of the experiment package has been chosen, but NASA says the experiments are expected to be flown on one of the Shuttle’s first six orbital flight tests.

Harmonic emissions limit may curve CB interference

The growing problem of citizen’s band radios interfering with home-television reception can be solved by limiting CB harmonic emissions to 75 dB below their 4-W power limit. The solution was offered by the Electronics Industries Association to the Federal Communications Commission.

Harmonics have no communication value to the CB user, EIA explains, but may interfere with certain TV channels. While properly adjusted and operated CBs currently being manufactured aren’t likely to interfere with TV sets, EIA said it suggested the new standard because interference sometimes occurs in high-density housing areas. One cause of CB interference, according to the industry group, is the use of illegal linear power amplifiers on the CB sets. The FCC is grappling with the problem of what it can do about these illegal amplifiers.

Capital Capsules: Latin American airlines have begun sharing weather data gathered by the GOES-2 satellite and collected by Lineas Aeros Nicaragua (LANCIA), which distributes the information in Miami to route flights around tropical storms in the Caribbean. LANCIA receives one visual image and one infrared image every hour. Sharing the data are LACSA (Costa Rica), Varig (Brazil), Lan Chile, Air Panama, Aerolineas Aviateca (Guatemala), Tan Airlines (Honduras), Aero Condor (Colombia) and Aero Peru. . . . Citizen’s band radio sets will be installed by the Coast Guard at its search-and-rescue centers to supplement its vhf-FM and 2182-kHz national maritime communications and distress system. The Coast Guard hopes to respond more rapidly to calls for assistance from small craft, and intends to have the CB service available in time for the 1978 recreational boating season.
On the balance

a T900-Series Oscilloscope
gives you the most performance
for your dollar

Low-cost oscilloscopes traditionally offer a compromise in performance in return for low price. Over-simplified circuits reduce accuracy and require frequent calibration. Cost cutting in the selection of components limits reliability. With many low-cost scopes, the specs are there, but the performance isn’t.

There are no compromises with TEKTRONIX T900-Series Oscilloscopes. No corners have been cut where accuracy and reliability are concerned. And with six models to choose from, you can match the performance you require with your budget. Bandwidths range from 10 to 35 MHz. Four T900 Scopes feature dual trace and one has single shot storage. A rackmount model is also available.

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The dual channel, 15 MHz T922 is an excellent choice for classes in basic electricity and electronics. The large, bright 8 x 10 cm display makes classroom demonstrations more visible. The easy-to-use control layout makes learning signal measurement techniques simple and straightforward.

When you buy a T900-Series Oscilloscope, you also receive the full support of the Tektronix worldwide sales and service organization. T900 Accessories include a wide selection of probes, a low-cost camera, a versatile stand for convenient scope positioning and a viewing hood.

Performance, reliability and service. That’s why Tektronix is setting new standards for low-cost oscilloscopes.

T921—DC to 15 MHz; single trace, mono time base .................. $ 695*
T922—DC to 15 MHz; dual trace, mono time base .................. $ 850*
T932—DC to 35 MHz; dual trace, mono time base .................. $1125*
T935—DC to 35 MHz; dual trace, with delayed sweep ............... $1395*
T912—Storage Model, DC to 10 MHz; dual trace, mono time base .......... $1300*
T922R Rackmount—DC to 15 MHz; dual trace ....................... $1175*

Voltage probes are included on all T900 Oscilloscopes except the T922R.

For complete specifications on the T900 Oscilloscope Family, contact your Tektronix Field Engineer. Or write Tektronix, Inc. P.O. Box 500, Beaverton, OR 97077. (503) 644-0161, Ext. T900. In Europe, write Tektronix Limited, P.O. Box 36, St. Peter Port, Guernsey. Channel Islands.

*U.S. sales prices are F.O.B. Beaverton, OR. For price and availability outside the U.S., please contact the nearest Tektronix Field Office, Distributor, or Representative.

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The 990/10 is the most powerful member of the 990 computer family. Its architecture provides features that give you maximum processing power for your money. Like hardware multiply and divide. A 16-level hardware interrupt structure. 16 registers arranged in a workspace concept. I/O that’s directly programmable through the Communications Register Unit (CRU) and autonomously through a high-speed data bus. And, bit, byte and word addressing of memory.

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With the 990/10, you get a powerful instruction set with an extended operating feature that allows hardware to take over operations that software would normally execute. An optional mapping feature provides memory protection and memory expansion to 2 million bytes. And, optional error-correcting memory corrects single-bit errors for increased system reliability.

Full peripheral support.

As well as a range of standard peripherals, disk storage to 180 million bytes and magnetic tape with 800 and 1600 bpi options are available for low-cost mass storage and back-up.

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With common higher level languages, FORTRAN IV, COBOL and Multiuser BASIC, plus the 990/10 assembly language, you have all the tools you need for an efficient application program.

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The Model 175 also features auto­ polarity, automatic zero, 100 % over­ range, big, bright 0.43” LED display and comes equipped with both rechargeable NiCd battery module and battery charger/line adaptor.

Size: 5½” W x 1¼” H x 3½” D
13.97 x 4.45 x 8.89 cm

MODEL 245
Portable, 4½ Digit DMM
$295.00

Ideal for field use, the Model 245 is a rugged, truly miniature, lab-quality, 5-function instrument featuring a basic DC accuracy of ±0.05% of input ±1 l.s.d., ±0.05% resolution, 100% overranging, equipped with both rechargeable battery pack and battery charger/line adaptor.

Model 245 measures ACV (100µV to 500V RMS), DCV ±100µV to 1000V, Resistance 100 milliohms to 20 Megohms, AC and DC current 1 microamp to 2 Amps. AC voltage/current response, 30Hz to 50kHz.

Size: 5½” W x 1¼” H x 3½” D
13.97 x 4.45 x 8.89 cm

MODEL 248
Portable, 4½ Digit DMM
With True RMS Measurement
$345.00

This high-resolution instrument measures Resistance 100mΩ to 20MΩ, DC Volts ±10µV to ±16V, True RMS AC Volts 10µV to 500V, both DC Current and True RMS AC Current 10 nanoAmps to 2A. The Model 248 features sensitivity of 10µV. Basic DC accuracy is ±0.05% of input ±1 l.s.d., guaranteed for a full year, 100% over­ range, overload protection, large LED display, and comes complete with both rechargeable NiCd battery module and battery charger/line adaptor, with 6 hours of in-spec operation before requiring recharge.

Size: 5½” W x 1¼” H x 3½” D
13.97 x 4.45 x 8.89 cm

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$325.00

The same specifications and features as the Model 1455, line operation only.

MODEL 1455
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$355.00

Model 1455—all the virtues of a laboratory bench instrument with the added benefits of complete portability.

A five-function multimeter featuring ½” high display, and 100% overranging. Model 1455 measures 100µV to 1000VDC, 10µV to 500VAC, resistance 100 milliohms to 20 Megohms; AC and DC current, 1 microamp to 2 Amps. AC response, 30Hz to 50kHz.

Basic DC accuracy is ±0.02% of input ±1 l.s.d. for 6 months. Internal NiCd battery module and line cord recharger included.

MODEL 1450R
With True RMS
$895.00

The same specifications and features as Model 3400 but with TRUE RMS AC Volts $895.00. Also available with IEEE STD 488 interface unit Model 3410.
COUNTERS

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- Resistance 1 Mohm to 12 Megohms.
- Input Impedance through 10 VDC 2 and 4 wire Ratiohmic® Resistance Method. DC/DC and AC/DC Ratio. BCD output and voltage ratio are included at no extra cost.

MODEL 5740
100MHz, 7 Digit Multifunction Counter $295.00

The Model 5740 measures Frequency, Period, Period Average, Total Events and Elapsed Time.

The Model 5740 measures: Sinewaves, Square Waves, Pulses, Pulse Pairs, Complex Waves • Frequency: 5 Hz to 100 MHz; 10 ms/100 ms/1 sec./10 sec. gate times, resolution to 0.1 Hz • Period: 0.1 µsecond to 0.2 sec. • Period Average: 10, 100 and 1000 periods • Total Events: 0 to 9,999,999 (unlimited with “overflow” indicator) • Elapsed Time: 0 to 99,999.99 sec. (27.8 hrs) • Sensitivity to 10µV.

For complete information on these and other Data Precision instruments or a demonstration, contact your local Data Precision representative or Data Precision Corporation, Audubon Road, Wakefield, MA. 01880 USA (617) 246-1600. TELEX (0650) 949341.

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<th>Number</th>
<th>MA</th>
<th>(617) 245-5940</th>
<th>NY (S)</th>
<th>(212) 895-7177</th>
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<td>(205) 533-5896</td>
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CIRCLE NUMBER 20
The smart executive

Charlie started a company some years ago and it prospered. Under his guidance, it became the leader in its field as sales grew almost every year till they leveled off at about $10-million. Then the growth stopped.

Well, not exactly. In a good year, sales would rise to 11 or 12-million dollars, and in a poor year they would drop a million or two. Meanwhile, other companies passed Charlie’s company and, despite his technical prowess, his company slipped to third and sometimes fourth in its field. Charlie got upset.

Since he was responsible for the growth to $10-million, he reasoned, others must be responsible for the stagnation. So he spent lots of time issuing directives, shifting people around and changing company policies. Mostly this didn’t accomplish much except to disorient and demoralize his staff. Sometimes a policy shift brought more income — more often it wreaked havoc.

Like most of us, Charlie had an ego. So it was almost impossible for him to see that one of his policies could cause damage. Instead, he saw the problems always in terms of poor execution or, simply, underlying stupidity. To make matters worse, he let his people know just how inept he thought they were.

But one day something remarkable happened. With an insight rarely granted to most of us, Charlie was suddenly able to see himself clearly. He realized that while he was really good at developing a company to $10-million, he was poor at developing it further. So he appointed Jack to the presidency, then stepped out of his way.

Though he insisted that Jack furnish regular and detailed plans and progress reports, he steadfastly refused to interfere in the operations of the company. When an engineer, out of habit, would ask Charlie to rule on something, he’d always defer the decision with “Why don’t you talk to Jack about this? He’s so good at these things.”

Charlie’s company is now up to $20-million a year, and everybody always marvels at how brilliant Charlie was to appoint such a fine chief executive. Everybody knows that Jack’s doing a fine job running the company. But there are lots of fine company chiefs like Jack. The Charlies of this world are rare.

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GENERAL ELECTRIC

CIRCLE NUMBER 832
The truth about resistors:
If you use wirewound resistors, you probably specify either silicone or vitreous enamel coatings. Before you buy either coating, make sure you talk to someone who knows both. Because some companies that offer only one type of coating would have you believe that silicone and vitreous enamel work equally well in all applications and are therefore interchangeable.

Don't believe it.

The truth is this: many significant differences—in aging characteristics, resistance to heat, puncture, overloads and mechanical shock—not only can make a critical difference in your product’s performance, but in your company’s reputation, as well.

Let’s look at just one coating characteristic that can make a big difference. Silicone coatings tend to out-gas, giving off silicone vapors. When a silicone-coated resistor is subjected to heavy overloads, the coating can fail catastrophically in a cloud of smoke. But even in normal operation, silicone coatings can out-gas, contaminating sensitive equipment.

Many telephone equipment manufacturers have found, for example, that silicone deposits can foul relay contact surfaces, causing expensive maintenance and trouble-shooting headaches. So these manufacturers demand vitreous enamel-coated resistors for critical switching equipment.

Now, we’re not saying that vitreous enamel is always the answer. Some applications call for vitreous. Some call for silicone. That’s why Ohmite offers both. We can show you where one resistor works better and why; explain the options, costs and trade-offs involved. In fact, we can tailor a complete package to your overall resistive product requirements.

Before choosing one coated resistor over another, talk to the people who know resistors best: Ohmite.

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Get a copy of our free brochure, “The truth about resistors;” It contains a wealth of performance characteristics and application experience covering silicone and vitreous enamel-coated resistors. Circle the reader service number for your copy today.

CIRCLE NUMBER 834
Allen-Bradley introduces a new rotary switch for the MOD-POT series. Designed for signal level circuits. Tested for current levels as low as 15 milliamps, with 5-volt open circuit. Plus new conductive plastic resistance elements with low turning torque for velvet-smooth rotation. And CRV of typically less than 0.2%. Linear and modified log tapers (CW and CCW) available from 100 ohms to 1 megohm. All feature smooth characteristics, particularly at resistance roll-on and roll-off positions. Come to the original source for MOD-POTS. We have what you need; our distributors have them when your need is now. Ask for Publication 5217.
A probing look at key instrument areas:

What's wrong with the IEEE 488 bus ........................................ p. 48
Instruments that check themselves .......................................... p. 56
A roundup of circuit board testers ............................................ p. 64
Signal generators and synthesizers ........................................... p. 76
Temperature measuring instruments ........................................... p. 86
John Fluke speaks on the voltmeter ........................................ p. 96
The 1799 Digital/Analog Test System
An integrated system designed as a hybrid tester

Until now, if you wanted a combined digital/analog test system you had to choose between a digital tester with some added analog features or a powerful but expensive digital/analog tester which may well have had more capability than you needed. GenRad has now solved this problem by designing a fully integrated digital/analog test system in the medium-price range. By "fully integrated" we mean that the 1799 has been designed as a hybrid test system rather than merely being an enhanced digital test system—as most medium-priced hybrid testers are. This means, for instance, that the software and the hardware "talk" to each other in an efficient manner, and that the measurement "instruments" (in reality, purpose-designed modules) are controlled by high-level language statements rather than a string of meaningless ASCII characters. This, and many other benefits of the integrated "second-generation" approach, makes for a more cost-effective solution to your testing problems.
Focus your attention

The
1795-HD
Logic Test System
High performance at low cost

The GR 1795-HD is a new breed of logic-circuit test system. It contains the same program-preparation and diagnostic capabilities as the world-renowned GR 1792-series with CAPS, but at a much lower price. Now, for about the same initial investment required for much simpler systems, you can realize the cost effectiveness that can only be provided by a computer-controlled, simulator-based system. The 1795-HD is ideally suited for use in manufacturing operations, service depots, and in R & D where the simulator-based system is ideal for ensuring that new designs possess a high degree of testability.

The CAPS VIII Test System software is available as an option with each of these systems. CAPS is the most proven, the most accurate and the most widely used program-preparation and diagnostic software for logic boards available in the world today. That's why we claim...
Track Down Your Faults With A Bug Hound.

The GenRad 2220 Bug Hound will track down your shorts, opens, bad ICs, etc. in a fraction of the time it takes you now, including those hard-to-find shorts between power and ground.

Even though your automatic board tester may be giving you good diagnostics, it is still only telling you the electrical location of the faults. Finding the physical location can still be a time-consuming and expensive task. The GenRad 2220 Bug Hound solves this problem by providing the repair technician with a variety of testing techniques in one self-contained little package.

It has a unique new phase-sensitive current-tracing probe* which makes it easy to trace the correct track even when many narrow tracks are running very close together. In addition, it has a dc tracing capability, a connectivity tester, an ac current source, and a dc current source.

The GenRad 2220 is easy to use and in most applications will pay for itself in just a couple of weeks.

*Patent Pending
The 1796 Digital/Analog Test System
An ATE system with large-scale integration of test capability

Complex digital boards using LSI chips such as microprocessors, RAMS, ROMS, UARTS, etc. are no longer beyond the reach of PC board testers. To diagnose boards containing such devices, GenRad designed a completely new system from the ground up… the 1796. Its technical highlights include high-speed digital driver/sensors (dc to over 1.5 MHz), sophisticated analog stimulus and measurement modules, and a flexible switching matrix and PCB interface capability.

GenRad
is the difference in testers
Using the IEEE 488 standard instrument bus involves a lot more than buying bus-compatible instruments and a controller, taking them out of their boxes, plugging them together, and turning them on. There are problems, most of them minor. But being aware of problems before they happen can save hours of troubleshooting time.

The major hassle with IEEE 488 is its generality. While the standard writers tried to define the mechanical, electrical, and functional elements that allow instruments to communicate with each other over the bus, they purposely avoided restricting the operational characteristics of bus-compatible instruments so that an instrument using an IEEE 488 interface doesn't have to have a certain accuracy, speed, or set of ranges.

**Doing the same thing differently**

This generality, unfortunately, also means that different instruments are not prevented from doing the same things differently. Where one digital multimeter might be programmed for the 10-V full-scale range with a simple command, R10V, another DMM might require a series of seemingly meaningless alphanumeric characters.

Some examples of the commands needed to program different manufacturer's instruments are given in the applications manual for the Model 4051 graphic system controller from Tektronix Inc., Beaverton, OR. For example, 280 PRINT @W,32: "F5.67E3A1.23" sets a Wavetek Model 159 waveform generator for a 5.67-kHz sine wave with an amplitude of 1.23 V. A Fluke Model 6011A synthesized signal generator can be set for a 1.234-V, 5.678-kHz sine wave with a similar—but not identical—command, 280 PRINT @F,32: "5.678E3H1.234V." But to set a Hewlett-Packard Model 3330B automatic synthesizer for 5.678 kHz at −9 dBm requires an entirely different command, 280 PRINT @H,32: "L5.678>N9<."

Codes even more obscure than those are applied to some frequency counters. To set a counter to remote operation and measure frequency with a gate time of 10 s, among other parameters, requires 280 PRINT @D,32: "FA+1,NNAY+Y," for the Dana Model 9000 microprocessing timer/counter; 280 PRINT @F,32: "F OR4" for the Fluke Model 1953A universal counter/timer; and 280 PRINT @H,32: "E8F0GO E9I1J1" for the Hewlett-Packard Model 5345A electronic counter.

Besides shying away from limiting the operation of an instrument, IEEE 488 was made general enough to simplify adding a compatible interface to older products, says Maris Graube, corporate interface engineer at Tektronix. Older instruments that are designed to communicate via relatively simple binary-coded decimal ports cannot easily be converted to IEEE 488 interfaces if the conversion requires a change in the coding within the machine, says Graube. "The tendency was to make the specification weak so that previous instruments meet the standard."

**Flexibility isn't all bad**

The coding flexibility can also help the instrument user, points out Don Loughry, corporate interface engineer at Hewlett-Packard Co. of Palo Alto, CA. The communications code can be chosen to take maximum advantage of the interface bus.

In transmitting data from an autoranging digital voltmeter, for example, both a floating point and

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**Andy Santoni**  
Associate Editor
exponential response can be the simplest and least expensive to generate. Where very high speed is required, as in a data acquisition system, fixed-point numbers may be preferable.

Since the needs of the many engineers who join instruments into systems differ widely, a fixed standard could not meet even a majority of those needs, says Loughry. But a Recommended Practice is being developed to cover preferred methods for coding data for transmission on the IEEE bus. The document may be in the final stages of publication before the end of the year.

This addendum to IEEE 488 may solve another data-coding problem: Which bit first? Data words are sent over the bus's eight data lines in a bit-parallel, byte-serial format. But while the eight data lines determine which bit is most significant, the standard does not specify which byte—the first or last sent down the line—is most significant.

The user must determine which order an instrument's manufacturer has chosen by carefully examining the instrument's instruction manual. The system controller must then be programmed to organize the data bytes from each instrument in the proper sequence before performing any other operations on the data.

The recommended method for transmitting data is most-significant digit or character first, says HP's Loughry, and this technique will be incorporated in the document now being prepared.

Instruction manuals provided with bus-compatible instruments also come under fire from some users. Often, precious little space is devoted to explaining how the bus operates and how the instrument's quirks affect its operation on the bus, says Dale Mack, development engineer in switch design at Tektronix. Worse yet, says Mack, most manuals have no sample programs to help the user develop his own system.

Manuals should get better

Instruction manuals should improve as manufacturers gain more experience building and applying bus-compatible instruments, and learn the best ways to take advantage of the standard interface. Not only that, but as more bus-compatible instruments are designed, sections dealing with the IEEE bus in their manuals will be improved versions of sections on the bus in current manuals. Since instruction books are usually written just as a product's design has been completed and production is about to begin, there is rarely enough time to write a thorough document from scratch. Instead, parts of previous manuals are reorganized and rewritten to match the differences between an older product and a new one, according to the senior technical writer at one instrument maker.

Yet another bus-related problem is EMI. But incorporating the standard interface into new instruments rather than adding it on to older designs, may help alleviate this bother.

Either the high-frequency square-wave clock of a
The bus puts it all together: A Fluke 5100A calibrator provides signals and an 8500A DVM makes measurements under the control of a Tektronix 4051. Here, they check the calibration of a hand-held DMM.

system controller or the clock signal built into an instrument's IEEE-488 interface-conversion board can generate enough electromagnetic interference to affect the readings of a very sensitive instrument such as a microvoltmeter or a picoammeter, says Frank Capell, product planning manager in the precision instruments business unit at John Fluke Mfg. Co., Inc., Mountlake Terrace, WA. But newer instruments can use the clock signal already in the product, instead of generating it separately for the interface board. This, along with more careful shielding, should help minimize the EMI problem, says Capell.

A matter of interpretation

Manufacturers' varying interpretations of IEEE 488 can also cause headaches, Capell adds. In one case, the controller built by one manufacturer responds to a request for service from a device on the bus when it sees a transition from ZERO to ONE on the service-request line. A controller built by another manufacturer responds to a voltage level on the service-request line. Until engineers closely examined its operation, the former controller would intermittently fail to respond to a service request. "When things were thrashing around, the controller ignored the signal," says Capell. If the controller was busy when the edge occurred, it missed the transition and could not respond to the request. "The whole bus would hang up, waiting for a response," Capell recalls.

The devices on the bus all met the standard. The controller met the standard. But problems still occurred because of ambiguities in IEEE 488.

The document talks about sending messages, and relates messages to specific voltage levels, notes HP's Loughry. The best way to guarantee meeting the spec is to design equipment to respond to levels. But, Loughry admits, "the way devices are built, they do trigger on an edge."

Different controllers also require different program languages, points out Joe Flink, vice-president of product development at Rockland Systems Corp., West Nyack, NY. While most use some version of Basic, a fairly easy program language to learn, some controllers use a completely different nomenclature.

"Each language has its own particular quirks," agrees Tektronix' Graube. Different languages have different advantages that can affect the ease and speed with which a controller can perform a specific function, he says. These varying good points also make it difficult to choose among the available products.
Computers are powerful controllers

The limitations on the IEEE-488 bus imposed by the relatively slow speed and inflexibility of calculator-based bus controllers can be overcome by making a minicomputer or single-board computer the core of an instrument system. Several suppliers make interfaces to the standard bus:

- Hewlett-Packard, which conceived the bus system, has been selling an interface package for its 21MX and 2100-series minicomputers through its Data Systems Division in Cupertino, CA, since last spring. Called the 59310B, the $1000 hardware and software package enables a single mini to control several instrument clusters, allows the user to prepare programs on one terminal while the computer is executing test programs from another terminal, and operates with more than one programming language.

- Digital Equipment Corp. supplies the IBV-11 to interface the firm's LSI-11 computer systems to the bus. The $750 package consists of a printed-circuit card, a card that ends in a 488-standard connector, a software package and sample programs.

- Ziatech Corp. of Cupertino, CA, has developed an interface card to tie the SBC 80 single-board computer into IEEE-488 instrument systems. The ZT 80 can plug directly into an SBC or MDS backplane and handles interface actions with its own 8080 microprocessor. An on-board memory on the $950 board handles bus protocols and data buffering.

"I'm not sure how someone selects a controller without a knowledge of computers," says Graube.

Watch out for limits, too

While some difficulties with the IEEE bus stem from a lack of specifics, some users feel that problems may also be caused by restrictions the standard document does have. For example, no more than 15 devices may be interconnected by one contiguous bus. Moreover, the total transmission path length over the interconnecting cables cannot exceed 20 m. And the data rate across the interface on any signal line cannot exceed 1 Mb/s.

These limits cover the majority of systems likely to be tied together via a standard interface bus without excessively high costs, says HP's Loughry. Some users, like Tektronix' Mack, think the limitation on the number of instruments could someday be a problem, though it hasn't proven so yet. The largest system Mack has so far put together, a tester for measuring switch contact resistance and bounce, ties only five instruments to the bus.

The bus's speed is sufficient, says Mack, though some of the instruments built to use the bus don't take full advantage. They take much longer than necessary to acknowledge the receipt of commands or data, and Mack would like to see manufacturers build-in faster handshake logic.

Meanwhile, as if there weren't enough problems, the International Electrotechnical Commission has its own version of the standard. So far, IEC's Technical Committee 66, Working Group 3, which was responsible for drafting the document, hasn't been able to choose an appropriate connector. While most American representatives favor a 24-pin connector that is common in the United States, some European manufacturers prefer a 25-pin connector more readily available in Europe.

Which version do you use?

As it stands now, the IEC's standard is identical to IEEE 488, except that it lacks a mechanical section. A separate document has been drafted to cover the mechanical requirements of the standard bus, including the 25-pin connector. But for the time being, users of the standard bus must specify that products they buy conform to IEEE 488. Products that comply with another version of the standard, like the IEC's, may not meet the same requirements.

But even with the problems, most bus users are happy with IEEE 488. "The fact that you can plug things together easily is of enormous benefit," says Rockland's Flink. "It's not the best, but it's certainly a great step forward," says Tektronix' Mack. With a little perseverance, an engineer can make good use of the standard, they agree.
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AMPHENOL
CIRCLE NUMBER 24
What’s wrong with your instrument? It may tell you

"E 77, 4D01, +0.09032..." This isn’t a coded communiqué from James Bond, but encrypted messages sent by ailing test and measuring instruments. Indeed, equipment that can calibrate, correct, test or diagnose itself—and tell the user what’s wrong—may soon become commonplace as the latest spectrum analyzers, digital voltmeters, logic analyzers, X-Y recorders and other instruments move into lab, field and production. The benefits of such equipment are many; the disadvantages seem few.

Among the advantages: Calibration and maintenance are simpler, calibration periods are longer, troubleshooting is easier, and down time is shorter. In addition, users have more confidence in instrument measurements especially in unattended or automatic measurements. And in some cases, instrument performance is boosted.

The disadvantages aren’t as easy to spell out, but a few critics of self-test say that the benefits are costly and don’t necessarily justify the extra expense. Proponents reply that self-test mostly comes free. However, the two sides agree that not every instrument lends itself to self-testing.

Candidates for self-analysis

For example, equipment that is mainly analog in nature, like scopes and signal sources, doesn’t. But a digitally based instrument, like a logic analyzer or DVM, does. Instruments that carry some sort of processor are natural candidates for self-analysis. In fact, the rise of self-calibration and diagnosis goes hand-in-hand with the rise of so-called “smart” test equipment.

Certainly, the introduction of microprocessors into some T & M equipment is questionable. But once the \( \mu P \) is tucked inside, it can easily make decisions and provide the control switching and storage needed for diagnostic routines and correcting errors.

One of the first instruments to feature \( \mu P \)-controlled self-calibration and diagnosis is Systron-Donner’s 7115 5-1/2-digit DVM. In the 7115, autocalibration reduces the number of possible error-producing components from about 33 to just four resistors and a voltage reference. Autocalibration occurs automatically at power up, or after every 100th, 1000th, or 10,000th measurement (as the user desires), or on an external command.

During autocal, the 7115’s 4004 \( \mu P \) makes 16 measurements that cover all the zero and full-scale points of all modes and ranges. The results of the measurements are stored as constants, which are applied...
to a universal correction equation to give the final reading.

The constants also play a part in fault diagnosis. They take on predetermined error ranges based on the maximum expected drift caused by aging, temperature and other factors. If a constant exceeds the preset range, a warning indicator lights or an electrical flag is set. In effect, the instrument tells the user: "Investigate me; I might fail."

To check out the warning, a user lifts the 7115's cover, operates a diagnostics switch and, at the touch of a button, calls up each of the calibration constants for display on the unit's front-panel LEDs. A troubleshooting chart then directs him to a failed or suspicious board or component. Additional internal LEDs—34 of them—indicate operational status or possible failures.

**To \( \mu P \) or not to \( \mu P \)**

A microprocessor isn't mandatory for self-test, however, as Hewlett-Packard aptly demonstrated five years ago in its Model 3490A DMM—perhaps the first such instrument with extensive, built-in diagnostics. At the flip of a switch, the 3490A checks its timing signals and autoranging circuits, validates most of its logic, checks its 6-digit display, and displays results. The key? A microprogrammed, 4096-bit ROM. HP's latest systems DMM, the \( \mu P \)-based 3445A, goes even farther, with both autocal and a test function. In the 3445A, only four manual calibration adjustments are necessary—two each for dc volts and ohms. They are made on a rear-mounted plug-in reference module that can be taken to a calibration lab without disturbing the input connections.

Since the modules are interchangeable, the DMM can go right on working once a spare module is plugged in. With the new module in, the instrument proceeds to eliminate gain and offset errors from its measurement results. How often depends on the DMM's operating mode.

When the 3445A is placed in the self-test mode, it compares all its autocalibration measurements against internally stored limits. If a measurement is out of tolerance, a number between 1 and 15 is displayed to indicate the source of the problem. A troubleshooting chart then points the way to the most probable cause.

Another systems DVM—from the industry leader in DVMs, John Fluke Manufacturing Co.—offers something called calibration memory. The feature is an option in its 8500A, an advanced bus-structured instrument in which each of the various functions, or modules (dc conditioning, ohms, ac, a/d conversion, etc.) resides on an I/O bus, each with its own address. For every range and function, the calibration memory contains adjustment factors, which are obtained by taking readings at cardinal points while the instrument is in the cal mode. Once the range-cal error is in storage, the unit automatically computes the needed zero-to-end-scale correction and adds or subtracts it from the display.

When the 8500A is switched off, the cal correction can remain in storage for at least 90 days, taking power from an internal back-up battery. As a result, the unit can stay in the field longer before it is brought in for calibration certification.

Correction factors for zero drift, standard in the Fluke unit, are also stored. The zero offset in the most sensitive dc range is keyed into memory with a single stroke. Once stored, the offset disappears from the display and is automatically eliminated from all dc and ohms readings.

**Getting better**

Fluke's DVM is one example of performance being boosted by error-correcting techniques. The 8500A converts its input signals to digital form with a modified version of the company's well-known recirculating-remainder technique. The modification speeds up conversion tenfold by subtracting or adding correction values during successive steps in the conversion process. Interestingly, the 8080 \( \mu P \) in the 8500A doesn't take part in the bidirectional correction technique.

Although the 8500A doesn't carry extensive self-test features, it can show any of 10 different error codes to identify some operator mistakes or internal hangups. For instance, if the filter module doesn't complete an I/O handshake, the DVM will so indicate. If the operator selects an invalid function—for example, a current measurement without a current-shunt module
an error will be displayed and operation may be halted until a correct selection is made.

Another instrument is smart enough to test itself before it goes to work—the 4662 interactive digital plotter from Tektronix, the first one able to talk back to its host controller. When the 4662 is powered up, it automatically checks its RAM buffers and the ROM holding the controlling program. Then the pen moves automatically to the lower right corner to locate a reference, and the selected interface is enabled. Should an error be detected, the 4662 sounds a plotter bell.

Another self-test in the Tek plotter runs through a predetermined plot that lets the user examine all mechanical and electrical functions, excluding the interface.

If self-calibration makes a user more confident about an instrument's accuracy, and self-test ensures that an instrument is within specification, then the next giant step—self-diagnosis—makes life easier, if not for the user, then certainly for service personnel. This capability is demonstrated by some Hewlett-Packard logic and spectrum analyzers— instruments with perhaps the most extensive self-test and diagnostics available.

No price for self-analysis?

The HP instruments are evidence that diagnostics is not only a necessity in complex equipment, but that it is almost free if it is made part of a design right at the start.

Only 700 bytes of memory plus one I/O bit are needed for self-test in the 1602A, HP's latest logic-state analyzer. This feature costs only $20 or $30 in an instrument that goes for $1800. The 1602 runs about 35 self-tests on power up to check ROM, I/O, read/write memory and other parts. If all is OK, all the LEDs light (all segments). If a failure shows up, the 1602 takes note, completes the remaining tests, then blinks an error message—E99.

To find out what failed, the user presses the "d" key, which causes the self-test to repeat. The 1602 stops at the first failure, and displays a detailed error message along with various test parameters. Pressing any key steps the self-test to the next test segment.

The 1602's keyboard can also be tested—with the 1602's help. Power is cycled off, then on, with the "C" key depressed, and resident diagnostics are called up. Then all 35 keys are pressed in a predefined order. A failed key produces an error message.

Another HP logic-state analyzer, the 1611A, also checks itself when the power goes on. It performs a checksum to verify its ROM contents, writes a test pattern to its RAM, and reads the pattern back to check accuracy. If all's well, "SELF TEST COMPLETED" is written on the unit's CRT—all under the control of a microprocessor.

Self-test in logic analyzers was originally intended to be part of the service procedure, according to Al DeVilbiff, design engineer for HP. But so well did the feature work—and inexpensively—that it is now aimed at users as well as service people.

Hal Goldberg, president of Data Precision, a noted test-equipment vendor, considers self-test useful in complex or automatic test equipment. But in other cases, it's a marketing ploy, not worth the extra money. Goldberg, too, sees service technicians and repair shops as the main benefactors.

Bill Giles, chief engineer for DVMs at Systron-Donner, believes that self-diagnosis at least should be incorporated only where applicable and aimed at service personnel who know what they're doing, not uneducated operators who may foul up the works. Otherwise, Giles feels, self-diagnosis, too, is simply a marketing gimmick.

Although self-test appears natural for some instruments, there may be a natural reluctance to offer the feature for another reason: It may be too effective.

Too much of a good thing?

When an instrument tests itself without being asked each time it's turned on, "minor" failures may be
indicated a bit too often. An untrained operator may interpret an error message to mean that his machine is broken, whether it is or not. And one thing manufacturers don't want is an increased warranty return rate.

Of course, self-test can be aimed at the major functional blocks, and the nitpicking ones eliminated from the instrument's repertoire. But with complex equipment, defining what constitutes a failure may not be so easy. And as HP's DeVilbiff points out, self-test can be better than human observation because a human's ability to recognize patterns is limited. On the other hand, a µP may not ignore a pattern seen as innocuous by a human.

Superior or not, self-test hasn't reached the point where troubleshooters can throw away their scopes and pulse generators. Far from it. Calibration labs needn't worry, either. Standards must still be kept and equipment calibrated to those standards. And many instrument makers, Philips Test and Measuring Instruments for one, don't offer the feature.

Stu Rauch, product engineer at Phillips, puts self-test into perspective: "It's not really valid in, say, an oscilloscope unless the scope has digital data-domain techniques or storage. But with instrument systems or logic analyzers, self-check is easy to do without adding a lot of hardware. Calibration, however, is another story. That's a matter of strict design."

When asked if the recent appearance of µPs in scopes heralds the coming of self-cal in that breed of test instrument, Rauch declared that "µPs are appearing in scopes for one reason—they're a hot item, a user confusion factor, like fins on cars." Unlike scopes, however, spectrum analyzers are likely candidates for self-analysis, according to Rauch.

As a matter of fact, Hewlett-Packard has unwrapped a top-of-the-line spectrum analyzer with extensive self-cal and diagnostic features. As complex a free-standing instrument as is likely to be found, the HP 8568A sports not one but three internal processors.

**Self-improvement is the best kind**

Among the 8568A's "introspective" features are automatic calibration and correction for certain sources of amplitude and frequency uncertainty and a host of service aids that help localize hardware failures. With self-correction, amplitude uncertainties plunge from ±3.6 dB to a low ±0.4 dB. With its other inaccuracies added in, the HP unit measures down to -70 dBm with a total accuracy of ±2 dB, and to a rockbottom ±139.9 dBm, with 3-dB accuracy. These routine measurements require none of the elaborate, painstaking procedures usually associated with such signal analysis. Frequency correction is also routine.

For self-diagnosis, the HP analyzer exercises its I/O bus on turn-on, displays the status of various circuits on its CRT and offers shift-key functions for other checks. On top of these capabilities, the instrument is designed for servicing with a desktop computer and with signature analysis, an HP troubleshooting technique that is rapidly finding its way into much of the company's new equipment. The 1611A logic-state analyzer also uses it. (For a detailed description of signature analysis, see ED No. 7, March 29, 1977, p. 19).

Meanwhile, various forms of self-test or self-cal have found their way into a wide variety of products. The line-up includes counters like Dana's 9000 micro-processing counter-timer, gauging systems like Moxon's 360 multipoint gauger, component testers from GenRad and an all-in-one digital tester, the Tektronix 851 multimeter/counter-timer/logic indicator.

What's next? Taking a cue from the available bibliography on redundant circuits, and considering the ever-increasing density and continually plunging prices of ICs, it isn't too hard to envision an instrument that can repair itself.

Sounds crazy? At least one engineer, HP's Mac Juneau, doesn't think the idea is far-fetched: "With LSI chips as big as the ones now coming out, I'd be very surprised if we didn't end up with, say, voltmeter front-ends that could be switched out if tested bad, with a new front-end switched in. The instrument could change its own parts automatically—all you need are a couple of scanning switches."

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Testing circuit cards can be a ‘monstrous’ job

Don’t envy the engineer or manager responsible for circuit-card testing. Thanks to large-scale integration (LSI), today’s cards are as complex as yesterday’s complete systems. Circuits that formerly took up several complete cards are now squeezed into single chips—computers, data-acquisition systems, UARTs and phase-lock loops, to mention a few. For boards containing combinations of these IC monsters, designing efficient test systems often rivals the design effort for the board itself.

And that’s only for testing. Many boards fail—and their faults must be identified for repair.

Of course, the cost of the testing and repair must be kept low. So ideally, testing, fault isolation and repair should be done rapidly by minimally trained unskilled workers. A system that allows untrained personnel to test and repair cards efficiently must be on-line as card production starts. So, test systems have to be finalized after cards are frozen, but before production starts—usually in a few hair-raising weeks. Even after production starts, cards frequently are redesigned, so the test system must be quickly changed.

Production-test engineers are now understandably asked to look to the future as well as the present. So all hardware and software bought or developed today should, with only minor modifications, serve for years to come—hopefully.

Technology to the rescue

Dedicated testers built in-house and with limited capability were once the mainstays of every production-test department. But now commercial general-purpose machines with great power and flexibility abound. There are functional testers that check, via edge connectors, that boards perform their required system functions. And there are in-circuit testers that check individual components and connections. In fact, today’s in-circuit testers handle boards containing the most complex LSIs, including microprocessors—and at high throughput rates, too.

Unlike the dedicated testers of the past, which usually died with the product they were designed for, the versatile instruments of the present test a multiplicity of boards. There are testers, not only for analog or digital circuits, but for mixed boards as well.

The versatility of most modern card testers comes from their internal computers, which vary in size and capability from microprocessors to the largest minis.

Teradyne’s L125 Circuit Diagnostic System has two major configurations—one for digital boards, one for mixed analog-digital boards. By following instructions from the CRT, the operator works with the system’s guided probe.

Sid Adlerstein
Associate Editor
The more powerful computers enable test systems to organize test results and present them for statistical analysis. Many computer-based systems provide data logging, inspection and failure-diagnosis reports.

But you don't need a baseball bat to swat a fly. GenRad uses its 2220 Bug Hound to pick up where the automatic-test system leaves off. With the device's current-tracing probe, a technician can locate shorts, opens, malfunctioning ICs and other common PC-board faults. When tracing a fault, the probe itself guides the technician with indicating LEDs and audible tones. The Bug Hound contains a microvoltmeter with two single-point probes, a 10-mA dc source and a conductivity tester.

Also notable among the smaller testers are Testline's Short-Stop and Short-Stop II. With these off-line devices, an operator can quickly locate short-circuits for repair, or troubleshoot pesky wired-OR buses that make μC cards a minefield for testing.

First get the shorts out

But before the cards are tested, Teradyne advises that high-production runs be screened—by its L427 and L429 testers, of course—for those last few shorts that are left on a wave-soldered board after the obvious ones have been removed at visual inspection. These testers require no programming. They make contact with each circuit stripe and component pad by means of a “bed-of-nails” fixture containing “pogo” (spring-loaded) pins.

The L427 costs $13,000, and handles 60,000 boards in one shift-year. The 429 handles 240,000 boards in a shift-year and, of course, costs more.

Other testers work even earlier in the card-production cycle. The FACT system by Hughes Aircraft tests boards even before their components are inserted. The pogo-pin field of FACT's bed-of-nails test head mates with the board under test through a glass-epoxy mask. A separate mask must be drilled for each card. The bare boards are tested for continuity and leakage under automatic, semiautomatic or keyboard control.

Functionally, these testers are simple—but not cheap. Systems with 500 to 1200 terminations cost from $35,000 to $45,000. A bed-of-nails fixture with 3000 terminations (not all are used in any one test, of course) costs between $18,000 and $30,000. Test heads cost $2 to $3 per point, and product-holding plates between $300 and $1500.

But once circuit cards contain their components, testing can get complicated. So logic simulators have been developed to make it easier. These sets of computer programs can imitate a circuit's response to a set of stimuli.

Since logic simulators contain a library of device characteristics, a device familiar to the simulator need only present its designation and interconnections to...
the tester. From these simple data the programs develop the responses of the simulated unit under test (UUT).

One simulator-based system is GenRad's 1795-HD. In its learn/test mode, this system creates test programs automatically, using known-good reference boards as criteria. Once all internal nodal values of a reference board are recorded on a disc, the board becomes superfluous.

The DTS-70, a digital PC-board test system from HP, has a simulator-based test-program generator, Testaid III, which works into the system's automatic test-pattern generator. For programming ease, this tester offers three languages: Basic, Fortran and the company's own.

Simulator-based card-test systems are usually large and complex. The DTS-70 includes an HP 1000 computer that operates under a real-time-executive operating system. This multiprogramming software permits both multiple-terminal and multiple-test-station operation. The computer can also manage the test-data base.

Simulator-based machines aren't cheap. The GenRad 1795-HD, for example, starts at $50,000.

Simulators check inputs

But logic simulators can do more than just mimic circuits—they compare the simulated outputs of both good and faulty boards for a given test pattern. This way, the simulator checks the usefulness of input patterns.

During test-pattern development, the results of this simulated monitoring are fed back as a list of undetectable faults—on a CRT or as hard copy. The number of faults not subject to scrutiny is then reduced by changing the input test patterns. When the level of detectable faults is acceptable, the test pattern is frozen.

To check the testability of board designs, the simulator-based GenRad 1795-HD uses its CAPS program-preparation and diagnostic software. By simulating proposed logic, it exposes design inconsistencies and analyzes logic and test programs even before the board prototypes are available.

Automatic program generation is a feature of the Auto-Learn software for Mirco System's Series 500 testers. These instruments use time-nodal signature testing from a known-good board for initial set-up. Test execution is from a stored test program. But the system's control $\mu$P can't do all that's required by itself—a technical operator must help.

Fault simulators test testers

After initial test programs are developed, a fault-simulation program sequentially faults each IC input and output while test patterns are run. This process checks the thoroughness of the testing by seeing that errors propagate to the board-edge connector. Fault simulation, as implemented by Data Test in its 5800 Series testers, requires the operator to place the Test Clip probe in sequence on each IC of the UUT. When the test program must be changed, the operator is alerted instantly.

For microprocessors and other bus-oriented circuits, Computer Automation's Capable Model 4400 automatic test system identifies the signal bus closest to the fault, be it a component or a production defect. Then the AFR fault-resolution system, a combination of hardware and software, presents step-by-step instructions to an operator via a video-display terminal. These instructions tell the operator where to place the system's current-sensing probe while the system injects controlled-current pulses into the signal bus. Both the current pulses and the probe are software-controlled.

The operating principle of this level of fault isolation is that any defect will either source or sink an abnormal current. The controlled current pulses are injected into the circuitry via the system's clip feature, which is first used without the probe to isolate the bus carrying a fault. The AFR costs $7200 as an option to Capable Model's 4400 family of logic testers.

Hundreds of device-testing subroutines are contained in Faultfinders' Faults II software test-program generator for the FF101C and FF303 minicomputer-based in-circuit testers. Test programs generated by Faults II can isolate shorts, opens, or components that are bad, wrong, misoriented or out-of-spec.

The program-generation software, Z-Pact, for Zehntel's Troubleshooter 400 in-circuit tester, derives a fully formatted test program for cards containing both analog and digital components. The only input Z-Pact uses are a list of the components and their locations. The software interacts with the UUT to correct the test programs. To interact with the tester...
via a CRT and a keyboard, a programmer need only be able to read schematics and recognize common component characteristics.

Through the Flash software package, Mirco Systems' Series 500 testers generate test programs that produce a printout (a fault dictionary) of error signatures and their causes, and a printout of scope-trace data. Programs are also produced for developing such test statistics as

- Test-program comprehensiveness, which is the ratio of detectable failures to total possible failures.
- Average fault-isolation resolution, which is the percentage of all failures isolated to one component, two components, etc.
- Average failure-dictionary entry, which is, for example, the failure isolated to 1.7 components.
- No-find list, which identifies undetectable failures.

Time-sharing terminals can be used to prepare and edit programs for Series-500 testers. Mirco Systems' programs are available through GE's Mark III timesharing service.

Which inputs test best?

Whether testing relies on simulation or not, test-pattern inputs must be applied to the UUT. These inputs come from either hardware or software generators.

Hardware generators develop either fixed or pseudorandom patterns. The fixed patterns are usually in binary count or Gray code, and are used together with fixed-pattern-response testing, which requires no more than 16 bits per node.

Pseudorandom patterns, while statistically random during a test, are repeated in each test. A major advantage of pseudorandom patterns over fixed patterns is that they make program-preparation time shorter.

Test patterns from software generators are complex enough to check out almost any board. When software patterns are used, the UUT's responses must also be programmed. The resulting programmed-response generators can easily use millions of stored patterns to test a complex card. Naturally, an enormous memory is required. Also, testing a complex card takes many steps and thus a long time.

Hardware generators work faster than software-based systems. For hardware, there isn't as much time between steps in a sequence, because call-up from memory isn't required. Also, the bit rate for each step is usually higher with hardware.

One card-tester family that boasts both fixed and programmable pattern generation is the microcomputer-based 5800 series from Data Test. With its fixed patterns, the tester checks for transition-redundancy responses. With its programmed patterns, the tester checks for programmed responses. An option allows the three test stations in the 5800 family to perform either real-time or high-speed tests on logic boards that contain such complex LSIs as µPs, UARTs, PIAs, RAMs and ROMs.

The basic 5800 system has 128 I/O pins and is expandable to 256. Tests are performed from the card-edge connector.

Mirco's Series-500 testers also generate test patterns from their hardware—pseudorandom test patterns whose relative frequencies are software-controlled. The Series 500 testers have a repertoire of 255 different hardware-controlled patterns, and the length of test-pattern sequence can be as much as 1 \( \times 10^{12} \) bits. Either pseudorandom or programmed test patterns can be created by software at 500-kbits per second. The Series 500s have from 64 to 224 I/O pins.

Because of hardware's short testing time, high-speed signals and minimal programming, sections of a card should be checked from hardware whenever possible. So obviously the tester being used must have both hardware and software test-pattern generators.

Start with cleared logic

But before any functional-test pattern is applied to a board containing memory elements, the board must be initialized. That is, the board's sequential logic must be brought to a predetermined state.

Determining whether or not a complex board is initialized can be difficult. Software generators usually initialize the UUT to a high level of confidence.

Only edge-connector testing requires card initialization. But when the card is tested component by component by means of onboard probing, initialization usually isn't necessary.

To test without initializing—to keep programming...
simple and to locate faults for repair—in-circuit testers are often preferable to instruments that test from a card's connector. Testing to the component level requires access to each component, which can be accomplished via bed-of-nails fixtures, test clips or probes.

In addition to being accessed, the component under test must also be electrically isolated, temporarily, from the rest of the card. For isolating simple components and analog ICs, in-circuit testers use a guarding technique, which electrically isolates a component without breaking any physical connections.

The key to guarding is establishing two circuit points, a guarded node and a measurement node. An op amp forces the guarded node to the potential of the measuring node. Then, since no current passes between these nodes, the component can be measured as if the circuit between the two nodes is open. Guarding, therefore, is a form of bootstrapping.

For digital circuits, in-circuit testers use limited-energy pulsing. Superimposing the test-input state over the steady state (for microseconds, at most) isolates the device long enough for the required truth-table testing. Zehntel uses limited-current pulsing called "Isodrive," in its Troubleshooter 400, a µP-board bed-of-nails tester.

Testline Instruments has found that the average time required to program in-circuit testing is ten ICs per hour. In many cases, the job can move much faster. But inadequate or inaccurate documentation puts a heavy burden on the time required to program tests.

Once the tester has been programmed, test time depends on the operator's ability to clip onto the IC. With average density (one IC and a few passive components per square inch) a 60-IC board can be tested in 2-1/2 minutes. High-density boards can be tested at ten ICs per minute. For boards with wired-OR buses, testing is even slower.

**You can't find them all**

Testline's users report a greater than 90% confidence level for their in-circuit-tested boards. But some problems are not resolved by Testline's in-circuit testing—open etches, resin-encapsulated leads and mistimed one-shots. Where timing-flow problems stem from marginal design rather than faults, in-circuit testing is ineffective.

Faultfinders' FF303 in-circuit tests both digital and analog components on the same board. Guarding, for analog testing, is combined with limited-energy pulsing, for digital checking. Prewired for 639 points, the 6000 derives from all these interlinked processors. The power that the 6000 derives from all these interlinked processors is evident in such features as a programmable probe, a programmable overhead spot projector that guides the operator in probing, and even a computer-operated "screwdriver" option for in-circuit component adjustments.

Besides the usual programmable signal sources and measuring instruments, this tester offers waveform analysis and time-interval measurements to nanosecond resolution. Moreover, analog and digital tests can be mixed in any order. It shouldn't be surprising, then, that all this capability costs from $40,000 to $100,000.

**Where the faults lie**

The greatest bulk of faults in high-production runs are workmanship errors—components are usually 100% tested before insertion, and designs are usually proven at this stage. Such faults as solder bridges, wrong polarities, missing parts and bent pins produce the lion's share of board rejects. Teradyne has found that, after visual inspection of wave-soldered boards in these large runs, the distribution of faults is typically:

<table>
<thead>
<tr>
<th>Source Type</th>
<th>Workmanship</th>
<th>Components</th>
</tr>
</thead>
<tbody>
<tr>
<td>Visual faults</td>
<td>Shorts, opens and misplaced components</td>
<td>Damaged components (1-5%)</td>
</tr>
<tr>
<td>(80-90%)</td>
<td>(80-90%)</td>
<td>(1-5%)</td>
</tr>
<tr>
<td>Electrical faults</td>
<td>Invisible shorts, opens and plated-through holes</td>
<td>Device interactions, internal damage (5-10%)</td>
</tr>
<tr>
<td>(10-20%)</td>
<td>(5-10%)</td>
<td>(5-10%)</td>
</tr>
</tbody>
</table>

Software algorithms locate workmanship faults to a bad node on analog cards in Teradyne's L125A system. With a known-good reference board, the L125A learns and stores all the nodal impedances, which are then compared automatically to those of
the UUT. Because of the automatic operation, only minimal information is presented to the system’s nontechnical operator.

Much more information, however, is presented to the programmer. Operating software runs a CRT screen divided into three sections—one section displays the results of a specific test; another shows the ac, dc or digital signal at the probe; a third serves as the display for the command console. Any test in a program can be directly modified from the keyboard.

A digital version, the L125, detects all errors including faulty components.

Good testers get better

Unadorned, the L125 comes in two major configurations—one for digital boards and one for mixed analog-digital boards. With the system’s Guided Probe, a nontechnical operator can be instructed from a CRT. But to make the already sophisticated L125 test system faster during troubleshooting and easier to program, two levels of automation can be added. The M150 Automatic Prober eliminates the slow and error-prone operator from the probing process. The P400 Automatic Programming System works with off-line large computers. Basic device and circuit data are fed to the computer, then the P400 terminal produces a test program on mag tape.

In-circuit testers like the L125, which work with circuit impedances, can only locate faults to a bad node. Normally, several components share the same node—with buses, the number of components on a node can be staggering. For repair, then, the exact location of the trouble must be determined.

Faults on digital boards are automatically isolated to the malfunctioning component by Testline Instruments’ AFIT 3000 and 4000 systems. These in-circuit testers supply full dynamic functional truth tables to the board through either a clip or a bed-of-nails fixture.

In the AFITs, an injected pulse overrides any malfunction in an IC; however, the pulse does not override solder bridges. Nor does it override etch shorts between lands. As a result, a defect is categorized as belonging to a component or to a land. All hard shorts are indicated as the first test result, and they must be removed before testing can continue.

Testline’s AFIT 3000 is equipped with a dual-disc data base. One of them, a master library “Super Disc,” holds over 2000 truth tables for standard ICs. The other disc serves as the data base for a specific UUT. Pertinent data are transferred, under write protection, from the Super Disc to the UUT’s disc.

LSI-memory cards are trouble

The cards that are the most demanding on digital testers contain LSI-memory chips. So many locations must be exercised and, of course, the cards must ultimately work as part of a larger system.

Dynamic testing is the key to acceptable in-system LSI-memory-card performance. This testing should be done under conditions that are as close as possible to those in the system, which means testing for direct-memory-access functions and for repeated reads and writes at 10-MHz clock rates. Because of the necessary complexity, memory-card test patterns often use millions of bits. Error-detection-and-correction logic must also be tested. For ECL especially, testing must cover more than just stuck bits—propagation and termination must also be checked.

One tester specifically geared for dynamic testing of LSI-memory boards is the two-computer MD-107 Memory System Analyzer from Macrodata. Two cascaded processors provide 10-Mbyte testing and a 10-Mbyte test-pattern generator. Fast test patterns are generated without using throughput-reducing overhead cycles.

For engineering, this system can double as a characterization tool (for shmoo plotting). For production, a CRT and hard-copy point out faults to an unskilled operator.

Fault-free LSI-memory boards don’t need the detailed testing required by faulty boards. This is the philosophy behind Adar Associates’ DR 12/25 memory-board tester. To save skilled man-hours, initial dc testing from the connector separates the functionally good and bad boards. The good boards then undergo a series of high-speed functional tests conducted by unskilled operators. Failed boards undergo a sequence of diagnostic tests that require a skilled operator to interact with the test system.

During a memory-board test, the DR 12/25 stores the locations of devices found to be faulty in a fast RAM. After the test, this Board Error Map is transferred to the system’s minicomputer for display on a CRT and printout.

High-level test language plus user-oriented executives are provided by the system’s ATLS 12/25.
software. Features include provisions for multiple peripherals, statistical-data presentation, shmoo plotting, board-error mapping, error analyzing, and message processing—all under software control.

**Keep the dynamic logic alive**

Signals from known-good boards are used as test criteria by Fluke Trendar's 3040A Logictester, which runs at multibit rates to keep the dynamic logic in \( \mu \)P and shift-register memories alive under test. Testing is speedy, since the logical behavior of each IC is supplied to the tester from a reference board. Test-input sequences to this system are flexible. Merged sequencing allows engineering test codes to be mixed with machine-generated sequences.

After a board is found to be bad, the Logictester's Autotrack option provides computer-guided troubleshooting via its applications program, a troubleshooting algorithm that uses comparative diagnostics. With Autotrack, the 3040A can test and troubleshoot boards containing \( \mu \)Ps and other LSI chips.

A 3040A Logictester with 240-pin capability costs between \$60,000 and \$95,000. The 3020A, a related logic-test system for production test, costs \$32,000. The most limited tester in the series, the 128-pin 3010A, costs \$15,000.

Not only does the System 390 from Instrumentation Engineering test boards containing memories and microprocessors, it also tests mixed analog-digital boards. The minicomputer-based system's simulator, Microsim, can imitate \( \mu \)P-based assemblies down to 1-ns resolution, in real time. In addition, the usual simulator states—ONE, ZERO and UNKNOWN—are augmented by a three-state-logic D-state. With this fourth state, System 390 can simulate buses accurately—so important with \( \mu \)Ps.

Faults can be located under end-use operating conditions. Under high-speed operation, a computer-guided probe locates digital faults; under dynamic conditions, analog faults. The 390 can test complex—even \( \mu \)P-based—boards at programmable data and strobe rates.

Both the hardware and software of the System 390 can be serviced in the field via telephone-modem hookup. In testing, where minutes of tester down time can hurt, this ever-available servicing can sometimes save what could be nerve-wracking days of waiting.

**Other testers can adapt to cards**

Not all systems capable of testing complex cards are known for this ability. For example, Tektronix's S-3260 is primarily known for testing LSI chips. But this intricate machine can perform the high-level functional and parameteric tests that even complex boards require—with fixturing, it can be a powerful board tester. And in systems that cost tens and even hundreds of thousands of dollars, the cost of the required fixturing might be worth considering.

The S-3260's programming capabilities are extensive, including a disc-operating system, a high-level language, English-language hardware commands, operator interactive control, algorithmic test-pattern generation and a library of utility routines.

The system's measurement capabilities are just as impressive. Functional measurements can be made at 20-MHz clock rates. \( \Omega \)c parameters can be measured using Kelvin (four-wire) sensing, differential voltages, and nA sensing. Ac characteristics are measured dynamically and calibrated automatically.

The results of all tests are stored and can be analyzed by the system's statistical-software package, which generates reports and presents data graphically.

With infrared detection, just one sweep of the scanner performs the inspection, testing and troubleshooting simultaneously. Analog, digital or a combination of these circuits can be handled just as easily.

Infrared-scanner testers, like the Inspect System from Vanzetti Infrared, operate on the principle that a failure is just another mode of an assembly's operation. The failure mode is unwanted, but it can be readily identified by its unique infrared radiation characteristics—its signature.

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**Need more information?**

The products cited in this report don't necessarily represent the manufacturers' complete lines. For complete details, circle the appropriate reader service card number. More vendors and information may be found in *ELECTRONIC DESIGN'S GOLD BOOK.*

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Computer Automation, 18651 Von Karman, Irvine, CA 92713. (714) 833-8830. (D. Cutforth) Circle No. 476

Data Test Corp., 2450 Whitman Rd., Concord, CA 94520. (415) 689-3583. (Cal Edmonds) Circle No. 477

DIT (Q) Int'l., 5612 Brighton Terrace, Kansas City, MO 64130. (816) 444-8700. (W. C. Comer) Circle No. 478

Faultfinders Inc., 15 Avis Dr., Latham, NY 12110. (518) 783-7786. (Tom Coleman) Circle No. 479

Fluke Trendar, 500 Clyde Ave., Mountain View, CA 94043. (415) 965-0350. (Noel Lyons) Circle No. 480

GenRad, 300 Baker Ave., Concord, CA 01742. (617) 369-8770. (Robert T. Szpila) Circle No. 481

Hewlett-Packard, Loveland Instrument Div., Box 301, Loveland, CO 80537. (303) 657-5000. (Walter Skowron) Circle No. 482


Instrumentation Engineering Inc., 769A Susquehanna Ave., Franklin Lakes, NJ 07417. (201) 891-9300. (Art Desera) Circle No. 484

Microdata Corp., 6203 Varvel Ave., Woodland Hills, CA 91364. (213) 687-6550. (Alan Portnoy) Circle No. 485

Membrain Ltd., Ferndown Indl. Estate, Wimborne, Dorset, England. 0202 893535. Circle No. 486


Omnicomp Inc., 5150 N. 16th St., Suite 263, Phoenix, AZ 85016. (602) 264-2475. Circle No. 488


Technology Marketing Inc., 3170 Redhill Ave., Costa Mesa, CA 92626. (714) 979-1100. (Jan Bosboom) Circle No. 490

Tektronix, Box 500, Beaverton, OR 97007. (503) 644-0161. (Ken Hampton) Circle No. 491

Teradyne Inc., 183 Essex St., Boston, MA 02111. (617) 482-7200. (Robert Siganuk) Circle No. 492

Testline Instrument Inc., 1625 White Dr., Titusville, FL 32780. (305) 267-7212. (Tom Simpson) Circle No. 493

Vanzetti Infrared & Comp. Systems, 507 Neponset St., Canton, MA 02021. (617) 828-4650. (Dr. Riccardo Vanzetti) Circle No. 494

Zeintl Inc., 2440 Stanwell Dr., Concord, CA 94520. (415) 676-4200. (Craig Fynn) Circle No. 495
Engineers at Hughes Aircraft Company communicate with an IBM computer through nearby terminals in a programming language called APL. A powerful language that can specify extensive computation with a few symbols, APL requires little experience or training in computer programming.

Says Robert Vuilleumier, a technical staff manager in Hughes' Los Angeles-based Space and Communications Group: "APL is a particular timesaver on problems which generate big data tables. For example, to tabulate the gain of a microwave antenna against temperature typically requires a listing of 17 columns by 30 lines. Preparing this table manually can take two days; the computer takes a few minutes.

"Quite often," Vuilleumier notes, "I need to recompute a table for a slightly different parameter value. Repeating the antenna analysis at a higher frequency would be an example. It takes only a moment to type in the new parameter and re-execute the program from the terminal."

Adds George Williams, an engineering project manager who was instrumental in APL development at the group: "APL is very effective for small jobs with their own data bases, and for spur-of-the-moment programming. I have seen users arrive at the terminal and depart so quickly I thought they'd changed their minds, but they had actually finished writing and executing their programs.

"I recently watched someone define a plane on the basis of three points in space for a geometric calculation," he continues, "using only three lines of APL code. Conventional programming would have required three pages."

"In addition to engineers, managers use APL for manpower and budget planning, cost estimating for proposals, and facilities management," says Conrad Stensgaard, Jr.

Stensgaard, a senior staff engineer, helped install APL in the System/370 Model 158 in the Hughes Computation Center. "APL has brought the computer much closer to our users," he says, "lowering the 'threshold' of entrée to the machine for small tasks and making interactive computing directly available to the end user."
Simulated Spine Hastens Injury Research

The effect of a 30-mph automobile crash on the human trunk is shown by these drawings derived from a computer. A normal spine is at left; the center and right views show its position 20 and 40 milliseconds after impact.

This insight into the complex mechanics of the backbone was made possible by a mathematical model of the spine, developed on an IBM System/370 Model 158 at the Chicago Circle campus of the University of Illinois, sponsored in part by the Aerospace Medical Research Laboratory. Engineers at the university are studying the effects of injuries and disease on the back.

The potential benefit is far-reaching, since eight million people in the U.S. suffer from back problems, and half a million currently wear braces.

"We don't know much about that sophisticated structure we call the spine," says Dr. Albert B. Schultz, professor of mechanical engineering. "We're working with orthopedic surgeons to learn more, in the hope of preventing and treating back problems."

"Because we can apply engineering principles to the skeletal system," adds Dr. Ted B. Belytschko, professor of structural engineering, "we can sometimes determine in a few days responses to treatment which would take years to find by observing results of therapy."

In one experiment, the computer simulates the force applied to the spine by a therapeutic brace. "This helps show us the effectiveness of different modes of treatment," Dr. Schultz notes. "In treating lateral curvature of the spine, or scoliosis, the model has told us that applying pressure from the side will often be more effective than a stretching force."

By means of the computer model, engineers in the university group have predicted the effect of a hip-to-neck brace in a number of patients. The actual results of treatment supported the predictions in 80 percent of the cases.

Each year an additional 400,000 American workers incur back injuries; Dr. Schultz and his colleagues expect the computer model to help analyze their causes. The results will be available as guidance to therapists, orthopedists and industrial safety programs.

Models Aid Study of Continuous Systems

Simulation as a means of investigating the behavior of a complex physical system is often simpler and less time-consuming than seeking an analytical solution.

Engineers or designers can create computer models of almost any complex mechanical, electrical or other physical system—aerodynamic components, control systems or industrial processes, for example—by means of IBM's Continuous System Modeling Program III (CSMP III). It can also be used in the analysis of systems with discrete components such as digital filters, control elements or logic.

An engineer can readily describe a system to the computer in the CSMP language, which includes 42 powerful functions for performing integration, differentiation, signal and function generation, Laplace transformation, and switching and logic.

Additionally, since Fortran IV is also a subset of the language, the user can build large functions and submodels specifically suited to his application. The CSMP III Library stores these functions, as well as arbitrary or experimental data, tables and complete models—all of which can be executed alone or in combination with other simulation elements.

The system to be modeled may be entered as a set of differential equations, or as interconnected blocks, each characterized as a mathematical function. CSMP III simulates with time as the independent variable and stores the successive values of as many as 220 dependent variables. Up to 220 of these may be printed during the run, and as many as five may be print-plotted simultaneously. Trial runs quickly show which simplifications of the real system can be made with no significant loss in accuracy.

With its Graphics Feature, CSMP III can display up to four co-ordinate grids on an IBM 2250 Graphic Display Terminal, with up to four variables plotted on each grid. Experimental data can be displayed graphically and edited interactively before it is incorporated into a simulation model.
When computer-aided design of the integrated circuit chip is complete, a computer-driven plotter draws a three-color layout of the circuit in large scale.

Computer Designs and Fabricates Computer Circuits

Today's high-speed, high-capacity computer systems depend on advanced electronic devices using Large Scale Integration technology. This micro-miniaturized circuitry puts thousands of memory or logic circuits into a space a quarter-inch square or less, making possible speeds of billionths of a second.

At IBM's General Technology Division facility in Burlington, Vermont, the computer itself is instrumental in the design and production of these advanced semiconductor devices. Engineers there are using a System/370 Model 168 and IBM 2250 Graphic Display Terminals to design and produce the high-precision photo-masks that are critical to the fabrication of integrated circuit "chips." Intrinsic patterns are successively overlaid using a lithographic process to build a finished chip containing thousands of individual memory cells.

To create a tentative design for a mask, an engineer draws lines with a light pen directly on the face of a graphic display terminal connected to the Model 168. The system automatically resolves the sketch into a precise pattern of straight lines and geometric shapes.

"It's easy to move elements around on the screen, trying alternative layouts until we find the optimum use of the space available on a chip," says Paul Serednicky, manager of computer-aided graphics. "We can rapidly try so many alternatives that we are finding much more efficient layouts than we ever could manually on a drafting board.

"Since the finished device usually consists of one memory cell pattern repeated many times," Serednicky adds, "the engineer can develop it once in detail. The system then replicates it the required thousands of times, automatically rotating it, generating mirror images and adding interconnections.

"Perhaps most significant, though, is that the computer generates a tape that guides automatic production of the mask itself in the final size. Previously, we had to draft the design by hand, and then use it as a guide in the preparation—also manual—of an oversized mask.

"Any change forced us to start over again from the beginning and repeat the manual process. Now we can go back at any time and make a change or improvement in the mask design. We can accommodate an engineering change in minutes instead of weeks."

Project Management Aids

These program products are powerful aids for management of projects in many different fields.

1. Project Management System IV (PMS IV) Creates precedence diagrams, helps to optimize the allocation of resources, calculate detailed work schedules and monitor work progress.


3. MINIPERT An APL program for management of small projects. All functions are interactive and designed for use by planners and managers with little critical path experience.

For more information on these IBM Program Products, contact your local IBM branch office or write the Editor of DP Dialogue at the address on the right.

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ENCORE!

WESTON reintroduces the DMM 6000 autoranging portable

Better performance, new options, more accessories than any other low-priced field service DMM

The Weston DMM 6000 is making an encore. It was a great field service instrument when first introduced and proved itself in dozens of applications. Now it is even better. Improved circuitry has substantially reduced response time of the autoranging digital readout for faster measurements. Better contrast and longer life have been achieved for the LCD display. Brightly lit rooms or even direct sunlight do not affect readability.

New options offered with the 6000 include a manual range hold operation feature and display backlighting for easy readability in dark locations.

New accessories extend the versatility of the 6000 to cover a host of special uses and applications to make it a more valuable measurement instrument.

These are new additions to an already proven-superior field service instrument. The standard features that contributed to making it the best buy ever in a portable DMM still support the 6000. Autoranging in a low priced portable is unmatched by any major instrument manufacturer. Low power circuitry that operates from two 9V transistor batteries with up to 350 hrs. life eliminates time consuming battery recharging. Weak battery condition is automatically indicated 8-10 hrs. in advance to eliminate lost time in the field.

Couple these major features with things such as automatic zero, automatic overrange, automatic minus polarity. Add in unusual features that include a full 10 amp AC/DC current range and a special "Hold" function for measurements in hard-to-reach locations. Package all this in a rugged, small, lightweight case. Offer it at the low price of $195* with Weston quality manufacturing and worldwide service and nobody can match it. Bravo!

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CIRCLE NUMBER 30
Precise signal sourcing

Sig gens, synthesizers—and a capable offspring

Precise signal sources are a must for sophisticated testing. From stringent measurements on radio receivers to automated testing on production lines, the test inputs will most likely come from one of three types of instruments:

- Signal generators.
- Frequency synthesizers.
- Synthesized signal generators.

Signal generators combine modulated-signal capability with low-noise content and are ideal for narrowband receiver measurements. Frequency synthesizers get the nod where stable frequency is required, as in simulating local oscillator chains. Synthesized signal generators borrow some of the best features of the other two classes of instruments: stability (like a synthesizer) and calibrated output levels plus modulation capability (like a signal generator).

However, these categories aren't rigid. Every manufacturer packs his own special set of capabilities into different models of his signal-source line.

Generators for the tough tests

For performing sophisticated receiver tests, a signal generator can't be beaten. Signal-to-noise ratio, selectivity or rejection and gain-bandwidth characteristics are some of its primary applications. These tests

Gene Heftman
Associate Editor

Boonton's 102C/D signal generators are high-performance instruments for narrowband-receiver testing. Phase-locking the 102D's output results in a frequency stability of less than 0.05 ppm/h.
require an instrument of calibrated and variable frequency range, calibrated and leveled output voltage, and one or more types of modulation capability.

A typical pair of signal generators for high-performance receiver testing are Boonton's 102C and 102D. Covering a frequency range of 0.45 to 520 MHz, their output power levels are calibrated and variable from +13 to -130 dBm. Output frequency modulation is provided in five ranges, from 3 to 300 kHz. Amplitude modulation from 0 to 100% at 400 Hz and 1 kHz rates is also built into the instruments.

An instrument similar to the Boonton pair is Hewlett-Packard's 8640B. It spans a slightly wider frequency range, 0.45 to 550 MHz, and an option can increase the frequency to 1024 MHz. The calibrated and leveled output amplitude is variable from +19 to -145 dBm. Modulation capabilities—amplitude, frequency and pulse—are built-in, with adjustable output levels ranging from 1 mV to 3 V.

Other comparable sig gens are Wavetek's 3001, Systron-Donner's 1702 and Marconi's new TF 2020.

Precise receiver measurements require an instrument that keeps the frequency from drifting. To get frequency stability, phase-lock techniques and crystal oscillators have been introduced, particularly in the newer synthesized signal generators. Locking the output to an internal, temperature-controlled crystal oscillator can produce stability figures on the order of 10⁻⁸ parts/h.

Phase-locking the output of Wavetek's 3001 synthesized generator has resulted in a frequency accuracy of 0.001% with a stability of 0.2 ppm/h. And a stability option gives an accuracy of 0.2 ppm with a stability of 5 × 10⁻⁹ parts/day.

Systron-Donner's 1702, described by the manufacturer as a synthesized signal source, uses a phase-lock method that doesn't depend on the timebase being temperature-controlled. A discriminator is summed with the modulator input to control the oscillator frequency. Frequency accuracy from this lock technique is spec'd at 0.07 ppm.

Often, a fine line separates sig-gen specs from those of newer synthesized varieties. Solid-state designs and improved oscillators, in addition to the phase-lock technique, are bringing the noise specs of synthesized generators closer to traditional sig gens.

In fact, Marconi's TF 2020, a synthesized signal generator by name, performs both as an accurate bench generator and as a programmable instrument for production testing. With an rf output level of ±1 dB total accuracy and spurious noise levels 90 dB below the carrier, it carries a sig gen's specs. And like a frequency synthesizer, the instrument is stable to ±1 part in 10⁸ per day.

**Probing deeper into data sheets**

Speaking of specs, before a sig gen can be chosen to perform such critical receiver tests as adjacent channel selectivity and usable sensitivity, some important specs need to be considered: phase noise, modulation distortion and leakage, among others.

For example, a generator used to test for adjacent channel selectivity—the ability of a receiver to differentiate between a desired signal and one in an adjacent channel—should have a low phase-noise spec. Most manufacturers specify the phase noise as a dB level at some frequency offset from the carrier.

HP and Boonton both pick the offset as a 20-kHz band around the carrier. In the HP 8640B, single-sideband phase noise is down more than 124 dB in the 460-to-900-MHz range, and 130 dB from 230 to 450 MHz.

Phase noise for Boonton's 102C and D is spec'd in dB/Hz. At 20-kHz offset, it's typically down by 125 dB. And all single-sideband noise has a typical noise floor of 135 dB/Hz.

Marconi has a guaranteed limit on phase noise. It's spec'd at -130 dB at 20 kHz in the TF 2020.

Another important receiver test, usable sensitivity, is measured by the SINAD ratio—signal + noise + distortion divided by noise + distortion at a receiver's output. The sig gen selected for this test must have low leakage and low modulation distortion.

But leakage specs can be complicated by how manufacturers make their measurements. Leakage for the HP 8660 synthesized generator is listed as a radiated and conducted limit per a MIL spec. But on the 8640B, leakage is listed as a certain voltage induced into a coil at a specified distance from the generator. Indeed, Boonton's data sheet doesn't give any numbers, but states that the companies' machines can make unrestricted measurements on very sensitive receivers close to the instrument.

What it boils down to is this: The sensitivity of a particular receiver determines how much leakage it can tolerate.

Modulation distortion, while usually easier to locate...
on a data sheet, is a more difficult concept to understand. That's because there are so many components of distortion to contend with. In addition to envelope distortion when amplitude-modulating, a small amount of FM, called incidental FM, occurs. And when frequency modulating, something called incidental AM, gets mixed in. Manufacturers list these specs individually, but the total harmonic distortion (THD) data should be checked first, to get an over-all picture of distortion.

AM distortion in Boonton's 102C and D units depends both on the percentage of modulation and the rate. With 30% modulation at a 1-kHz rate, THD is less than 1% and less than 3% at 90% modulation. FM distortion is a function of the operating frequency and decreases as frequency increases. Maximum THD at 100-kHz peak deviation is 1% in the 0.45 to 32.5-MHz band, but only 0.15% from 260 to 520 MHz.

Marconi's TF 2020 synthesized signal generator can be operated manually as a bench generator, or automatically as a programmable generator. It's a 50 kHz to 520-MHz unit with AM and FM capability.

The AM distortion numbers are very similar for HP's 8640B. From 0 to 50% modulation at 400 Hz and 1 kHz rates, distortion is less than 1%. And from 50 to 90% at the same rates, it's less than 3%. FM distortion varies from less than 1% to less than 3%, depending on the deviation of the modulating signal.

Of course, sig gens serve in all the high-performance applications, but mainly as bench instruments. However, under computer control in an automated system, a "smart" synthesized generator can perform test routines that have been programmed-in.

Between generators—and synthesizers

The new kid on the block in precision signal sources, the synthesized signal generator, packs the futures of a signal generator and a frequency synthesizer into one box. In addition, both frequency and amplitude of the output can be programmable.

Where test conditions require many repetitive measurements, the ability of an instrument to store and recall input parameters can keep the costs of production down. And for programmability, what could be better than to have that modern-day saviour built-in—the microprocessor?

An on-board processor is a primary feature of Fluke's 6010A and 6011A synthesized generators. These so-called "smart" instruments can store and recall up to 10 frequencies, modulation conditions and attenuator settings. As a bench instrument, the processor can even inform the operator that he is attempting to program a condition that the machine can't provide. And all machine functions are both front-panel and remotely programmable.

Although microprocessor-based units are a recent innovation, instruments with programming capability are not. Marconi's TF 2020, HP's 8660 and 8672A, and Wavetek's 3001 are all remotely programmable and can be used in automatic test systems.

In the TF 2020, parallel BCD instructions from a remote controller can program-in all front-panel instructions. HP offers an interface kit for the 8660A/C that provides a link-up to the company's 2100-series computers. The 8672A has programmability as a standard feature via the IEEE 488 interface bus. Wavetek's 3001 contains standard frequency programmability, with level programming available as an option. Fluke's 6010A and 6011A offer remote control via the IEEE 488 bus or the EIA Standard RS-232-C interface.

Although synthesized generators are applied in sophisticated measurements, they're a shade behind sig gens in performing the most stringent tests. That's because the broadband amplifiers, phase-locked loops and mixers used in the instruments generate noise products that appear at the output.

Any data sheet for a synthesized generator will actually define spectral purity by listing a particular synthesized generator's harmonic and nonharmonic spurious signals. Fluke's 6010A and 6011A designate all nonharmonic spurious signals as 60 dB below the carrier or -110 dBm, whichever is greater. Harmonics are spec'd at -50 dB at 1 MHz and -40 dB at 10 MHz.

The HP 8660's spectral purity also depends on the operating frequency. At 110 MHz, harmonics are 40 dB down, while at 2600 MHz they're 20 dB down. Nonharmonic spurious are listed at -80 dB at 110 MHz.

Some data sheets list spurious signals in dBc, as a power level below the carrier. Above 120 MHz, a Marconi TF 2020 has nonharmonics at least 90 dBc. The number is 80 dBc when the frequency is below 120 MHz.

In an automatic test system, it's likely that the frequency of the instrument will have to be changed for different test conditions. How long it takes to switch from one frequency to another is directly related to the way in which the generator is designed.

Indirect generators—fast switches

To generate the output of a synthesized generator, a crystal oscillator produces a reference signal that is then translated into a broad range of output
Frequency and amplitude in an HP 3335A are controlled by a microprocessor. Ten front-panel settings can be stored and recalled from the internal memory. A 200-Hz frequencies. Either direct or indirect translation are used.

The direct method yields fast switching speeds, but opens the way to spurious outputs. Switching speed is typically 20 µs.

Indirect methods, using phase-lock loops, are more popular in current instruments. Fewer spurious signals are generated because each lock loop generates only one frequency at a time. But switching speed is much slower, typically 1 to 2 ms.

Indeed, a TF 2020 with indirect translation, can take up to 50 ms before it's within 1 Hz of the final frequency value. And after 100 ms, an 8660 may still be 5 Hz from touchdown.

A microprocessor-based unit seems to have a clear advantage in switching speed. Operating on the low (10 Hz to 110 kHz) range of a Fluke 6010A, the final programmed value of frequency is within 10 Hz in less than 2 ms. In the high (10 Hz to 11 MHz) range, on the other hand, after 2 ms, the final frequency value is still 1 kHz away.

Switching time in HP's 8672A synthesized signal generator has been cut below that of the older 8660. The high-frequency 8672A has a range of 2 to 18 GHz, and switching time is spec'd in three different frequency intervals. In the highest interval, between 12.4 and 18 GHz, frequency is within 3 kHz of the final value in under 15 ms.

A candidate for the precision signal-source category is Wavetek's Model 172 function generator. It's quite different from any of the instruments discussed so far, because besides pure sine waves, it puts out such waveshapes as squares, triangles, pulses and ramps. Frequency coverage is quite broad—10⁻⁴ Hz to 13 MHz, with a synthesizer option that yields an accuracy of 0.0005% of the programmed setting. Also, a built-in microprocessor provides interactive feedback to the operator when the unit is keyboard-operated.

The modulation capability of both sig gens and synthesized generators makes receiver testing the primary application. But when receiver components like filters and crystals need testing, a highly stable frequency source with a calibrated amplitude is most often used.

The super stable frequency synthesizers

Like sig gens, frequency synthesizers provide variable and accurate output frequency, and like synthesized generators, they are programmable. While they are classified as instruments with extremely high frequency stability and accuracy, they do suffer from high spurious signal content and poor sideband phase noise.

The current crop—from GenRad, Fluke, HP and Systron-Donner—has options that make frequencies super-stable, and noise specs that make them quieter than ever.

A GenRad 1062 synthesizer has a frequency range of 10 kHz to 500 MHz and a high or moderate stability option. A crystal oscillator in a temperature-controlled oven in the high option has a stability of better than $2 \times 10^{-10}$ parts/°C over 0 to 50 C. Drift is about $10^{-9}$ parts/day after one month of continuous operation, and less than $2 \times 10^{-10}$ parts with a 10% line-voltage variation. The same option is available in the 1061, with a frequency range from dc to 160 MHz.

Noise specs for frequency synthesizers are listed in
Calibrated microwave frequencies from 2 to 18 GHz are generated by the HP 8672A synthesized generator. High stability is provided by the internal crystal time base.

the same way as for synthesized generators. Harmonic noise is listed in two bands for the HP 3335A synthesizer/level generator. From 200 Hz to 10 MHz, it's -45 dB and from 10 to 80 MHz, -40 dB. All nonharmonic spurious signals are more than 75 dB below the carrier or -125 dBm, whichever is greater.

In any synthesizer, the primary component of noise is related to phase rather than amplitude. Noise is generally specified as the maximum noise power in a 30-kHz bandwidth centered on, but excluding, the carrier. The spec sums all the random phase-modulation products generated internally.

A 1 to 40-MHz instrument, the Fluke 6039A frequency synthesizer, specs the single-sideband phase noise as a signal-to-noise ratio. At 100 Hz offset from the carrier, s/n is greater than 110 dB, while at 600 kHz, it's way down to 140 dB. For the 6160B, covering 1 to 160 MHz, s/n is 135 dB down at 600 kHz.

Systron-Donner's 1615 uses the dB-below-carrier method to spec phase noise. At 1-kHz offset, it's listed at -70 dBc, while at 100 kHz it goes down to -100 dBc.

Programmability is a feature of all synthesizers, and one, the HP 3335A, uses a microprocessor. The processor is a big help, because it allows the instrument to store front-panel settings for fast recall in repetitive tests.

BCD programming is featured in the Fluke 6039A and 6160B units. Frequency programming takes 34 parallel, TTL-compatible lines.

GenRad offers the 1167 Frequency Programmer to control its 1061 and 1062 synthesizers. The 1167 performs digital sweep in automatic test systems, whose aging rate is less than $5 \times 10^{-10}$ parts/day. All front-panel functions can be remotely programmed via the IEEE 488 interface bus.

besides providing incremental frequency stepping and synthesized search.

A synthesizer, like a synthesized generator, has a switching speed spec to tell how fast it can change frequencies. Since both instruments are often used in automatic test systems, knowing when they are close to program frequency is important, so that the system computer will know when to begin a test.

With a GenRad 1062, how long it takes to lock onto the final frequency depends on how much the frequency changes. If the frequency changes by the highest increments (100 MHz), the 1062 will be 500 Hz from the final value after 50 μs. But after 1 ms, it's only 3 Hz away. Using the lower frequency 1061, the
Frequency programmability is a standard feature of Wavetek's 3001 signal generator, and an option can provide level programming. The instrument covers a frequency range of 1 to 520 MHz, accurate to 0.001%.

highest switching increment is 10 MHz. After 1 ms, the final value of frequency is less than 0.1 Hz off. Fluke's 6039A gives just one switching time number to consider. In less than 800 µs the unit is within 100 Hz of its final value. But in the same 800 ms, the 6160B synthesizer is only 50 Hz away.

HP specs the switching and settling time of the frequency of its 3335A synthesizer as a phase angle. The frequency is within 90° of the final phase in under 20 ms. In addition, there's a switching time for amplitude—within ±0.02 dB of the final value in less than 500 ms.

Need more information?
The products cited in this report don't necessarily represent the manufacturers' complete lines. For complete details, circle the appropriate reader service card number. More vendors and information may be found in ELECTRONIC DESIGN's GOLD BOOK

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Measuring temperatures has become critical to designing today’s electronic equipment. For one thing, thermal-design calculations may not represent the real-life situation in equipment, and only by carefully measuring the temps of key elements will a designer be sure that semiconductor and other components don’t exceed their maximum allowable temperature ratings. In addition, monitoring environmental chambers and test stands that operate at elevated temperatures to accelerate early failure rates are necessary to evaluate performance and protect prototype devices and equipment against damage from excessive heat. And locating hot spots with thermometer probes can facilitate and speed troubleshooting and trouble analysis.

Fortunately, a designer can choose from a wide range of temperature indicators and thermometers. There are simple stick-on elements that change color when a specific temp has been exceeded, and there are accurate digital thermometers that can monitor from one to as many as 20 or 30 sensors. Hand probes are now appearing that can be used with standard digital and analog voltmeters. And for someone willing or able to spend as much as $45,000 on temperature analysis, thermographic systems are available to map temperature differentials of PC boards or other equipment—in color.

**Stick-on indicators cost the least**

At the low-cost end of the spectrum, temperature indicators are available in the form of stick-on labels, crayons, pellets, lacquers and inks. Not only do they cost little, they also have fast response, and don’t conduct heat away from the device being measured.

Jim McDermott
Eastern Editor

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**Adhesive-backed temperature-recording labels** by Telatemp change from white to black when a specified temperature has been exceeded. Here, labels are placed on ICs, transistors and heat sinks.

**Thermocouples, thermistors or platinum-resistance sensors** are used in these digital thermometers by Digitec. The meters display readings in °C or °F and have resolutions of 0.01, 0.1 or 1 C or F to match applications.

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**ELECTRONIC DESIGN 24, November 22, 1977**
And a 1% indication accuracy can be achieved with them.

Temp indicators that are widely used are the temperature-sensitive labels, which are composed of one or more heat-sensitive spots. They are placed on components such as transistors, ICs and heat sinks (see photo). As a specified temperature is reached, an indicator circle changes from white to black. The color change is irreversible, so it becomes a permanent record.

These labels can also be affixed to products going out into the field to indicate the highest temperature the equipment will experience.

Crayon-type indicators tell that a fusible temperature has been reached by melting or changing color. They are generally provided in about 100 temperature ratings between 100 F and 2500 F, but their ratings can go as high as 3200 F. Where a surface may not accept the crayon, a temperature-indicating lacquer can be substituted over the same temperature ranges and with the same indicating accuracy.

Fusible pellets are also available, but they are primarily useful for monitoring higher temperatures such as heat zones in furnaces.

**Thermocouples are popular sensors**

Temperature sensors used with digital or analog thermometers fall into four general classes: thermocouples, thermistors, resistance-temperature detectors (RTDs) and junction semiconductor elements exploiting the variations in junction characteristics with temperature. Thermocouples cover the widest range of temperature measurement. Thermistors have the greatest sensitivity to temp changes. And RTDs have the highest stability. Semi elements are proving particularly useful in hand-held probes used for checking the temperatures of PC-board devices. Electronic digital thermometers range in price from $250 to $800 for thermocouple units and RTDs, and $250 to $500 for thermistor instruments. Prices depend upon such factors as resolution, accuracy and packaging.

Probably the most popular thermal sensor is the thermocouple, which is rugged and low-cost—for standard probes, around $10. Thermocouples generate thermoelectricity, which was discovered by Seebeck in 1821 when he found that if two dissimilar metals are connected in a conducting loop and one end of the loop is hotter than the other, a voltage will be developed and a current will flow.

While early thermoelectric experiments were conducted with antimony, copper and lead, improved alloy-metal combinations have been developed over the years. They are identified by American National Standards Institute Type numbers (see table).

Two factors directly related to thermocouple characteristics affect the design of electronic thermometers:

- For accurate temperature measurements, the cool junction of a thermocouple loop, which is located at the instrument, must be maintained at a fixed reference temperature—usually 0 C (32 F).

  - The output of thermocouples is highly nonlinear. If the reference-junction temperature is fixed, the thermocouple voltage is nonlinear but predictable for different temperature ranges. The National Bureau of Standards has established accurate values of this voltage for standard thermocouples.

  - For many years literally baths of ice provided reference-junction temperature. But modern digital instruments use electronic equivalents. Where the
Temperature scales and an auxiliary hand probe permit the designer to measure device or component temperatures from $-55$ to $150$ C or F with this Tektronix 851 digital tester.

The instrument is designed to use one or more specific thermocouples, the cold junction is incorporated into the instrument. But if the meter has no internal cold-junction compensation, it must be provided externally.

For cold-junction compensation, Fluke uses circuitry that senses the temperature of the reference junction and generates a compensating voltage that makes the junction look to an electronic thermometer as if it were at $0$ C ($32$ F). Omega Engineering's Model CJ cold-junction compensator, for meters without internal compensation, contains a special bridge network for the same purpose; it can be used with a variety of thermocouples.

Thermocouple outputs are low, from a few microvolts to $75$ mV. Sensitive galvanometers and meter movements have been used, but digital measurement has superseded them because of higher accuracy and resolution, and faster readouts.

Accuracy is frequently specified on the order of $1$ to $2$ C or better—even as manufacturers disagree on just what constitutes accuracy and how it should be specified. Resolution is in the order of $\pm 1$ C over a few hundred degrees, and $\pm 0.1$ C or better for shorter spans.

More than a DVM

Thermocouples make selecting a digital thermometer a lot more involved than choosing a simple DVM, upon which it is based. Besides the errors inherent with digital voltmeters, there are thermocouple errors to consider, including the deviation from the NBS curve for the thermocouple used; the span of temperature being measured, which is a function of the reference voltage coefficient; the ambient temperature error; and the reference-junction temperature error, among others.

Since thermocouple output voltage is nonlinear, compensation must be made in analog and digital thermometers. Analog meters employ nonlinear scales tailored to the thermocouple used. Digital-meter designers approach the problem differently, but in any event they break the thermocouple curve into segments providing the best possible fit to the NBS curve (see figure).

Digital thermometers using thermocouples generally use 10, 20, 25 or 32 break points. Fluke's 2100A series uses 64 segments plus a $4$-k ROM that stores programs containing $256$ possible slopes for each segment.

Both the 267 and 268 series of pyrometers by Newport Laboratories have a plug-in analog linearizer for each temp range. Called the Polylog, it changes the amplification factor of the input amplifier for 20 segments. The system equals the performance of a 20-segment digital or diode-function generator-linearizer, but without the drift and other problems associated with a diode-function generator.

A microprocessor-controlled thermocouple system, the Alnor 8800, monitors temperature at 32 points. It also has a 32-segment digital-linearizing circuit that is accurate to within $0.25$ F or $0.25$ C of NBS specs.

Where accuracy and resolution substantially higher than those obtained with thermocouple instruments are required, a digital thermometer like Hewlett-Packard's Model 2804A microprocessor-controlled quartz thermometer can be used. Unlike thermocouple instruments, this one is based on the sensitivity of a quartz crystal's essentially linear change in resonant frequency with temperature. Residual nonlinearities are further rejected by a curve-fitting technique that employs a PROM programmed for each crystal.

The 2804A thermometer has an accuracy of $0.04$ C over a temperature range of $-50$ to $150$ C and a resolution of $0.0001$ C that is two orders of magnitude or better than comparable thermocouple, platinum or thermistor systems. A seven-digit readout displays

**Exceptionally high accuracy** is provided by HP's Model 2804 quartz-crystal thermometer. Temperature range is $-50$ to $150$ C and resolution is $0.0001$ C.
Thermocouples aren’t the only sensors

Another important type of sensor used in electronic thermometers, the resistance-temperature detector (RTD), is a wound resistance element fabricated from pure platinum or other metals. Resistances range from 10 to 500 Ω. These RTDs have positive temperature coefficients and offer the best inherent linearity. But their output, or change in resistance with temperature, is low—about 0.4%/°C. Prices vary from about $10 to $100 for standard RTDs. Platinum reference elements traceable to NBS may cost several hundred dollars.

RTDs are generally used to cover broad temperature ranges. For example, the Digitech 5900 PC, with a platinum sensor, operates from –100°C to 600°C with a resolution and repeatability of 1°. Platinum resistance probes also provide the greatest composite accuracy over a broad temperature range.

Still another major temperature sensor, the thermistor, is a bulk semiconductor element with a negative coefficient of resistance. Basic cold resistance is in the order of a few hundred to a hundred thousand ohms.

For protection, thermistors are usually encapsulated in glass beads. Their output is highly nonlinear, but they can have an exceptionally large change of resistance with temperature, about 4%/°C. Depending on the mounting and probe design, they go for about $5 to $50.

Digital thermometers have generally been available in either panel-meter or bench configurations, with many having provisions for battery operation. But now, hand-held, battery-powered units are also appearing.

One pocket-sized meter, Omega Engineering’s $250 Omegatemp, measures temperatures continuously over –55 to 999°C with a 1° resolution. Automatic cold-junction and linearizing circuits eliminate error due to variations in the thermocouple length and diameter. LEDs are used for the display. Accuracy is a 0.2% of reading ± one digit.

Another hand-held meter measures temperatures over the MIL-standard range of –55 to 125°C—EDC Corp.’s $239 T-Meter. Battery drain is minimized by a liquid-crystal display. Unlike other hand probes, the T-Meter uses a silicon diode as the temperature-sensing device, which minimizes the instrument complexity. The meter measures the change, with temperature, of the forward-voltage drop across the diode. Diodes are selected, and circuits inside the probe tailor the diode outputs for optimum linearity.

The standard T-Meter probe’s accuracy is listed as ±0.5°C over the MIL-standard range. For special applications covering only a 20° span in the MIL range, a special probe can obtain ±0.1°C.

Besides electronic thermometers, both analog and digital multimeters are available that, while not primarily intended for temperature measurement, do have temperature probes and temperature scales. For example, Triplette’s Model 100-T analog volt-ammeter uses a thermistor probe to check for hot spots in PC circuits. The meter has two temperature scales: –50°F to 150°F and 50°F to 300°F.

Another example of this trend to incorporate temperature-test features is Tektronix’s $1995 851 digital tester. In addition to its many digital trouble-
Sixty thermocouples, thermistors, or RTDs can be scanned by the Fluke 2240B microprocessor-controlled Data Logger without special equipment. With it, as many shooting functions, the 851 can use an optional temperature probe to display temperatures between -55 and 150 °C, with an accuracy of 2 °C and a resolution of 0.01 °C. This feature is useful for locating malfunctioning memory chips in a large memory bank or in checking power supplies for hot spots.

Tektronix's P6430 Temperature Probe can be used optionally with the company's digital multimeters. Temperature is measured by an npn transistor sensor at the voltage-probe tip. Temperature is a function of emitter-base voltage.

Probes available for standard DMMs

As a matter of fact, dc voltmeters and multimeters without temperature scales can be converted into direct-reading thermometers by probes having a linear voltage-vs-temperature output. Fluke's 80T-150 $125 universal temperature probe produces a readout of 1 mV/°C or 1 mV/°F, depending on the model used.

Temperature ranges are either -50 to 150 °C or -58 to 302 °F. DMM sensitivity of the meter scale used to read the temperature determines the resolution of the readings. A 150-mV range resolves any centigrade reading to 0.1 °. The probe output can also operate as 1000 can be scanned. Low-thermal-EMF switches permit the 2240B to measure voltages as low as 1 µV and temperatures to within 0.1 °C or °F.

chart recorders. For the heat-sensing element, a microcircuit transistor is deposited on the small aluminum probe tip.

Battery-operated circuitry in a junction box that connects the probe lead to the meter monitors the temperature coefficient of the transistor's forward voltage drop, Vbe. This is converted into a linear mV/°C or °F output.

Another universal probe that produces 1 mV/°C is manufactured by Valhalla Scientific for use with its Model 4440 Digital Multimeter Counter or any DMM having a 200-mV full-scale range. Operated by a 9-V battery, the probe incorporates a constant current bridge that monitors a solid-state sensor. Accurate to within ±2 ° from 0 to 100 °C and ±3 ° from -50 to 150 °C, the sensor is embedded in a low-mass brass tip for minimum thermal lag.

Infrared measurements count, too

One thing that the thermocouples, RTDs and other sensors discussed so far have in common is that they must touch the surface to be measured. But noncontact infrared measuring systems are proving useful for monitoring and detecting temperatures that are too high for thermocouples and RTDs—in the order of several thousand degrees.

Hand-held infrared "guns," like the one produced by Telatemp, can be pointed at a hot source to get a temperature reading. But these provide a readout of temperature integrated over a large area, and aren't useful for most electronic applications.

Meanwhile, a thermal-monitoring system with a fiber-optic probe that pinpoints areas of interest is finding considerable use. The probe by Vanzetti Infrared and Computer Systems not only helps monitor semiconductor crystal-growing processes but can also take a thermal profile of a PC board.

Infrared energy is picked up by the fiber-optic probe and fed to a high-gain infrared detector. The output
This color thermogram of a printed-circuit board reveals temperature profiles of 64 IC packages. White is hot, black is cold. The bottom scales denote the specific temperature range observed in the thermogram made by UTI-Spectrotherm's thermographic system.

of the detector can be amplified and processed for temperature, measurement or control. The readout is digital.

One application for the Vanzetti system is a digital IC component handler developed by Micro Component Technology in Minneapolis. The IC to be tested is first energized by a thermal matrix preprogrammed for it, then passed underneath the IR fiber-optic pickup head. The IC's temperature is checked and compared with the equipment's preset band limits. If the unit is within limits, a test-ready command is sent to the digital tester.

At the high-cost end of the temperature-measuring spectrum, heat from electronic circuits and components can also be vividly displayed on a TV screen by means of thermography. Systems with this capability are currently available from UTI-Spectrotherm, Barnes Engineering and AGA Aktibolag.

Running from about $30,000 to $45,000, these systems all use a slow-scan electromechanical scanning system to paint a picture of the infrared temperatures of the object being examined. Radiant energy from the object being scanned is focused onto a super-cooled detector. The detector's output is amplified and fed to a CRT-monitor screen on which varying shades of black and white represent temp differences. These differences are quantized by a color-scan converter that presents them in multiple shades of color, each hue representing a specific temperature.

The Color Quantizer used with UTI's Model 900 system, which has a 30 x 20-degree field of view, translates these grayish tones into 10 different, easily distinguishable colors. And since a standard TV signal is used, this information can be recorded on tape. In addition, Polaroid pictures may be taken of the thermograms.

Barnes's RM50 thermographic systems, on the other hand, is capable of microscopic inspection. Its lenses can magnify areas of interest three to 100 times. Polaroid pictures may also be taken of its thermogram images, and a video display and scan converter are available.

Need more information?

The companies and products cited in this report have, of necessity, received only brief coverage. They have been selected for their illustrative qualities. Their product lines are identified here. The code to these products is: ET-electronic thermometers; TI-thermally sensitive indicators; IR-infrared thermometers; EM-electronic analog thermometers; MT—digital meters with provisions for measuring temperature; TS—thermograph systems. Many companies not mentioned may offer similar products.
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The 3554 offers the best compromise when you must have top performance in these critical areas. It maintains gain accuracy with high frequency signals. Fast settling time means better system accuracy with transient signal conditions. High output current lets you drive heavy loads with good total frequency response.

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Contact Burr-Brown, P.O. Box 11400, International Airport Industrial Park, Tucson, AZ 85734, U.S.A.
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As good as the individual components are, added together they put the model 40 product line in a class by itself. For more information, write or call: Teletype, 5555 Touhy Ave., Skokie, IL 60076. Phone 312/982-2000.

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Volmeters haven't hit a dead end. While I don't foresee much significant technological advancement of the voltmeter art in the next few years, I don't foresee a dull future—far from it. Because, as with any other maturing product, technology isn't the whole story.

The excitement, the innovations, the breakthroughs that I see ahead are going to come about as we respond, not to new technology, but to new uses by new kinds of users.

We voltmeter manufacturers will invent, adapt and improve the product as always, but the focus will shift from the voltmeter's insides to its "impedance match" with the person who's using it.

We'll be using what I call an "asymptotic" technology—a rugged, low-power, lightweight, long-lived, accurate, low-cost set of solutions that are now beginning to approach the ultimate—giving the user an even better measurement tool.

To understand where this new user came from, who he is, and what kinds of instruments he needs, you have to look back. For the two decades covering 1949 to 1969, Uncle Sam was the main, most visible customer of all instrument manufacturers. As the biggest spender around, he had the most effect on directions in new products.

He almost "paid our way"—from the vacuum-tube voltmeter of the 1950s through the debut and development of the differential voltmeter, to the birth of all-solid-state DVMs.

Uncle Sam was no piker. He cared most about our top-line instruments, and even helped us get one more digit of accuracy every year—for a while.

But after the NASA, Defense Department and other cutbacks of 1969 and 1970, we had to find a new "main customer" with volume needs. And just when we needed a new customer, big industry began to need us.

Electronics had found its way into some industrial and commercial devices—copiers, coffee dispensers, numerically controlled milling machines and drill presses, among others. So meters were needed, mostly for field service, but also for production tests.

So we were ready to sell in real volume to industry. But industry didn't want or need DVMs or DMMs that had high accuracy, high prices, fancy specs, or regular recalibration procedures.

Industry wanted ruggedness and rock bottom prices. So we had to come up with both in a hurry, since there was no one else to sell to.

Ruggedness at low prices? Up to 1969, DVM manufacturers had never put out a product like that; really, they had been like spoiled kids. Electronics had grown up treating instruments as expensive laboratory delicacies; meters were sold only to other electronickers, who coddled them. In 1969, instruments simply weren't ready for rough-and-tumble industrial use.

By 1972, however, some rugged DVMs using ICs were in volume production, including our Fluke Model 8000. The new de facto standard was 3 1/2 digits, rechargeable batteries, and a benchtop case 8 or 9 inches wide. And industry has been buying ever since.

This year's hand-holdable version, the 8020, is built to do the same job as the 8000—it has 3 1/2 digits, but it is also far more rugged, and lives through 1000-
volt overloads and 6000-volt transients in a calculatorsized tough plastic case; and it uses a 9-volt transistor radio battery. Now that's a practical DMM, and that's what industrial customers steered us into.

They make no bones about the most important spec, price. The Model 8000 was startlingly low-priced in 1972 at $299, but the Model 8020, smaller, rugged, and better designed, is only $169. The point is, even with inflation against us, we're giving the industry more performance for less cost. I think that trend will continue.

In the past seven years, industry has stepped up its use of electronics to cope with rising costs. And more consumer goods are being introduced that use electronics: washing machines, sewing machines, ovens, CBs, TV games, home computers, and a raft of other things. So industry wants more meters.

In many cases, virtually untrained people are using the meters, not only in the testing and servicing of consumer items, but also in the testing and servicing of industrial equipment.

I think that's another trend that will continue. Nationally, the education level of technicians is going down as the military cuts back technical training from the year-to-two-years that it used to be. I hear that some technical schools now go for six weeks. So the low-end (bottom price and performance level) voltmeter has to be one that's right for this slightly trained tech.

*I think the manufacturer of end-user machines will take the voltmeter or multimeter and make it support the whole field-service job for his product. Possibly it'll take more function power in the digital area, maybe signature analysis or special counters.*

Don't be surprised if leading manufacturers go back to identifying faults and localizing them at the compo-
nent level. It costs a lot in inventory to have to replace modules or PC boards. Tomorrow's voltmeter will have to be failure-proof, or closer to it than today's. If you're out on a manufacturing floor turning out electronic units in real volume, you can't have production test meters go down and make any money. What do you do with the workers?

Here, easy servicing isn't the answer; and in the real world, production people have no spare meters. The answer? A DMM that simply doesn't break, mechanically, electrically, thermally or any other way.

Hopefully, we'll be learning more about the failure modes of semiconductors, so we can do a better testing job. We do well today, applying voltage extremes while slewing temperature, rapidly. This thermally stresses the chips, and weeds out the weak ones.

Don't be looking for major improvements in measurement accuracy, however, or sweeping changes in the basic functions of the voltmeter. Reliability, convenience, human engineering, and easy-service provisions will get the attention, instead, I believe.

It's now a world of replacement, not repair. But when will voltmeters get there? Not in less than five years, I'd guess.

But in the meantime, repair is easy. The 8020 has a plug-in chip, a plug-in display, a PC board, a few discretes, switches, and that's all. Not much to fail, and most of it is pluggable.

The ruggedness and serviceability just beginning to show in tough new low-end instruments will per-

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**Who is John Fluke?**

After earning a BSEE from the University of Washington and a master's degree from MIT, the man who gave his name to the digital voltmeter began his engineering career in 1936 with the General Electric Company in Schenectady, NY. Shortly afterwards, in Bridgeport, CT, Fluke won $300—a fortune during the Depression—for a resistance-welding suggestion that saved money for GE. World War II and the Navy interrupted his career, and he found ways to degauss American ships to make them difficult for the Germans to locate. A young lieutenant commander whom Fluke worked for would later become a distinguished admiral—Hyman G. Rickover.

A civilian again, Fluke devised a wattmeter based on empirical square-law operation of some silicon carbide resistors. He began producing them in 1948 in the basement of his Springdale, CT, home with the help of one employee. Four years later he moved his rather larger company to Seattle, "God's country," and became the company's president, a position he retained until 1972 when John Zevenbergen was made President and Fluke was named Chairman of the Board and Chief Executive Officer.

With all his company responsibilities, Fluke has found time to serve on the American Security Council and on the President's Blue Ribbon Defense Panel. He has worked for the Secretary of the Army and the Department of Defense. He's recently finished a two-year stint as Chairman of the Electronic Test Equipment Committee for the Deputy Secretary of Defense. His committee's recommended improved purchasing methods will save millions.

A community-minded individual, Fluke has worked for the northwestern states' Junior Achievement organization. He has also supported the Seattle Symphony as Chairman of the Endowment Fund, Vice President and member of the Executive Committee, and member of the Board of Trustees. Right now, he's on the executive committee of the Seattle Historical Society and a member of Seattle's Major League Sports Committee.

In addition to outside activities and long daily hours with his company, Fluke "putters around" in his 40 × 60-ft home workshop, collects early engineering texts, and restores selected test equipment of earlier decades. "Maybe when we tear things up again at the plant, we'll put in a little museum," he muses.

With his wife, Lyla, Fluke can look back on 40 years of marriage. They have two sons and a daughter, all in their thirties, and three grandchildren. John, Jr., another Stanford man, works for digital services in the Fluke organization. His father approves highly of John Jr.'s present assignment—cutting business costs.
meate the middle and high-end lines as well. The middle-sized, middle-priced voltmeters are the logical ones to address the digital LSI market, which suffers from a lack of tools. Five years from now, perhaps, the middle market will show some integration between the analog-input voltmeter of today and digital tools.

These voltmeters will also give technicians more messages, like “You’re hooked up OK,” or “You’re hooked up wrong.” That’s the kind of thing that will continue to generate a middle market. Then, as now, we expect the middle to be a features race, offering some neat things beyond what the low-end units can do, for a few dollars extra.

The top-of-the-line meters will be flexible microprocessor-based instruments, competing on the basis of their "smarts." The features of such a meter will include how much calculating power it brings to the job, how well it can expand on short notice to become the hub of a little measurement "system," the messages it displays, and how it prompts the production operator.

Even with the high-end voltmeter, I keep coming back to that “new kind of operator.” We’ll design so as to make it easy for that not-too-technical tech to get right answers and only right answers. The µP will be guarding him against wrong hook-ups by averaging a series of readings to cancel out noise and hum, checking all values for reasonableness, and generally keeping him out of trouble.

We already have error displays lighting up on some instruments, to send the operator back to a “prompt sheet.” This will tell him, for example, that to measure rms he has to push two buttons, not just one. In the next few years, there’ll be more of this kind of help for the operator who may be new to the specific instrument, new to his job, or even new to the electronics field.

As for serviceability features on the high-end bench instruments, you’re already seeing good modularity inside the case, and you’ll see more diagnostics, plus readiness-test minidiagnostics for the end user.

The instrument’s going to tell you where its problem is. It’s going to say, "Hey, my ac converter isn’t feeling too good." Kidding aside, the front-panel message lit up in block letters may be worded almost that plainly. The user will expect self-diagnosis in any top-of-the-line instrument, and get it.

We’ve got a start on the diagnostics already. We put a front-panel minicassette on our new 5100 calibrator, mainly to sequence calibration steps when putting another instrument through its paces. But soon you’ll also be able to put a diagnostic cassette on that little tape deck, and have the calibrator check itself out.

The bus concept of the 5100 may lead our design people to develop many more aids. Three buses are involved, the IEEE 488 bus that talks with the outside world, the 8080 microprocessor bus, and an internal analog bus.

The bus orientation lets you define limits for each measurement, but never bothers the operator with them. The microprocessor will perhaps store upper and lower limits, compare the actual reading to the limits, and send the operator whatever display words you have programmed to indicate go or no-go.

A DVM or DMM of this kind—self-explanatory, self-checking, self-diagnostic—will be welcome in all kinds of test and experimental work being done by nonelectronickers, too. New fields to conquer.

I’m a realist. If a diesel engine had been built the way we were building voltmeters even as late as five years ago, the engine wouldn’t go 10 miles. It just wouldn’t last. But today’s and tomorrow’s new meters will hold up, because voltmeter manufacturers have learned from experience. The hard way.

I’ll tell you frankly, we’ve had some disasters—every innovative company has—and every one of them can be traced back to some fault in engineering practices, or a misunderstanding of how the meter would be used, or what punishments it would have to stand.

But after seven years of really focusing on the industrial user, I think the knowledge is there. We’ve paid our dues, and we’ve learned, not just the Fluke people, but all the leading manufacturers. Competing for business tomorrow will require more engineering discipline than it did just a few years ago. Our design people, a unique breed, can deliver.

The pressure is on the design teams to foresee all the hazards, and optimize all the features. The testing people have to make sure they’ve really wrung out the new voltmeter or multimeter before it ever goes into production, and again when the first production units are made. They must make sure a new instrument is solid—in a far wider range of uses and environments than ever before. Solid, and effective.

That’s as it should be; these are the things that happen in any industry as a product matures.
Introducing the 920-D logic analyzer. Nine channels, 20 MHz and much, much more.

Don't let the low price mislead you. Biomation's new 920-D stands up to logic analyzers costing twice, even three times as much. It includes the functional features design engineers ask for most. And combines them with 9½ pound portability, making the 920-D an ideal field troubleshooting tool.

Nine channels — not just eight — give you added capability for more applications. Use the extra channel for recording data, or to mark a trigger location. And select between trigger or clock qualifier. Attach the optional Biomation 10-TC probe pod and you can select up to a 19-bit combinational trigger word.

The 920-D enables you to set a precise interval between the actual trigger and the start of recording, using either clock periods or number of trigger events. Or the pre-trigger recording mode can be selected to capture data from before the actual trigger. The logic threshold level is selectable — TTL, ECL, or variable. And you can record at rates from DC to 20 MHz.

Captured data, at 256 bits per channel, can then be displayed on any single channel scope or CRT display in timing diagram format.

Compare the 920-D with other logic analyzers, for both price and performance. Then ask yourself if you can afford to settle for less.

Don't let the 920-D's many features and high performance mislead you. It's priced less — far less — than any comparable logic analyzer.

In fact, the 920-D's $1295 price tag makes it practical to put its extensive capabilities to work wherever you design, debug or troubleshoot TTL logic.

The 920-D is a cost-effective first logic analyzer for most applications. Years of experience providing...
thousands of engineers and technicians with the industry's leading family of logic analyzers has helped us design the 920-D with proven real-world features you can put to good use.

Low price makes the 920-D a great choice for your second... or third or fourth logic analyzer. You won't need to stand in line or share your company's only logic analyzer when you have a 920-D of your own.

We built the 920-D for lightweight portability. It weighs in at under 10 pounds and connects to the nearest oscilloscope or CRT. That makes the 920-D the newest tool for field service.

Biomation has led the way in logic analyzer developments. Today there are seven Biomation analyzers, offering from 8 to 16 channels, 10 to 200 MHz capture rate, memory lengths from 256 bits to 2048 bits per channel and operating in both time and data domains.

What more can we tell you? Plenty. Ask for the 920-D product sheet. Or give us a call to arrange a demonstration. Ask for Ed Jacklitch (408) 255-9500. Or write Biomation, 10411 Bubb Road, Cupertino, CA 95014.

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Texas Instruments.

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SN54LS/74LS322 8-Bit Shift Register w/Sign Extend
SN54LS/74LS173 4-Bit D-type Register, 3-State

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CIRCLE NUMBER 37

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Attention all of you working with 2 and 4-phase logic systems, bi-polar logic, radar testing and simulation, and with complex waveforms of all types: the new S-D 110D dual-channel pulse generator is for you.

In one compact instrument, Model 110D contains two complete pulse generators with all pulse parameters separately controllable for each channel. You can also mix the channels to produce complex waveforms and delay one channel from another. That's why you can produce a true 2-phase system (4-phase with two slaved 110D's) as well as double and triple pulse pairs and controllable pulse trains for data simulation. For sheer variety of pulses, nothing today touches Model 110D.

Model 110D is the latest member of a growing family of S-D pulse generators whose distinguished ancestors — Data-pulse Models 110B, 110A, and 110 — set the industry standards in their time.

Key 110D data:
- Amplitude, ±18v into 50 ohms • DC offset to ±18v • rise/fall time variable from 5 ns to 500 millisecond • repetition rate 50 MHz • Price $2,250 (U.S. only). Get the facts on the first modern-day 2-channel pulser.

Contact Scientific Devices or Systron-Donner at 10 Systron Drive, Concord, California 94518, Phone (415) 676-5000.
Design an IEEE-488 bus into an FPLA, and speed system operation. An extra benefit: The technique allows you to interface any number of programmable instruments.

To get high speeds in a digital-bus interface, avoid a software approach and go right to hardware. One such interface, the IEEE-488 standard bus for programmable instrumentation, can be easily designed with FPLAs. Nonextended, the standard can specify a system of up to 15 instruments. But otherwise systems of any size and complexity can be accommodated.

The interface bus decodes addresses and commands, and passes information back and forth between instruments via 16 signal lines. In effect, the addressed interface is transparent. Since each component of the system contains interface functions within itself, interconnections within the system take the form of passive cabling.

Eight functions are incorporated in the interface system: Acceptor Handshake, Source Handshake, Listener, Talker, Device Clear, Device Trigger, Service Request and Remote Local. For simplicity, the system does not contain a Controller function.

FPLA combined with D flip-flops

A good circuit design for this interface system is a synchronous sequential model, in which the outputs and the next state are functions of the present inputs and state. This general circuit realization uses an FPLA as a combinational logic element, and D flip-flops as memory devices (Fig. 1).

The Signetics 82S100 FPLA offers 16 inputs and eight three-state outputs, and the 74175 Quad-D flip-flop provides the minimum number of required inputs. Knowing that a D flip-flop retains the present state for only one unit time delay (one clock period), you must modify the original state diagrams defined by the standard. Take care that the present state does not change on the next clock, unless the transition requirements are fully satisfied.

The Talker function is typical of the eight interface functions (Fig. 2) and illustrates the design procedure. Treat two parts of the Talker-function state diagram as if you are dealing with two mutually independent functions. To do this, assign states carefully. Assign states TIDS, TADS, TACS and SPAS the binary weighted combinations 0 through 3 (functions of flip-flop outputs Q0 and Q1 only). Assign states SPIS and SPMS the binary values of 0 and 1, respectively (functions of flip-flop output Q2 only).

Furthermore, giving idling states TIDS and SPIS the binary combinations 00 and 0, respectively, forces the Talker function to enter the idle state during power-on reset (pon), and simplifies the transition from the present state to the idle state when an IPC signal appears (no transitional signals are required).

In the detailed Talker-function transition table (Table 1), if the function is in the TACS state (Q1 = 1, Q0 = 0), it will stay in that state as long as excitation signal fi is true. It will enter the next state, TADS (Q1 = 0, Q0 = 1) only if excitation signal f6 is true. If at the end of any clock pulse both excitation signals (fi and f6) are false, the function will enter idling state TIDS (Q1 = 0, Q0 = 0).

From the excitation signals derived in Table 1, calculate the excitation equations (Table 2), then
Table 1. Talker function transitions

<table>
<thead>
<tr>
<th>Present state assignments Q_2, Q_1, Q_0</th>
<th>Next state Q_1, Q_0, Q_2</th>
<th>External inputs</th>
<th>Present state signal</th>
<th>Excitation signals</th>
</tr>
</thead>
<tbody>
<tr>
<td>TIDS X 0 0</td>
<td>X 0 1</td>
<td>h</td>
<td>g_1 = Q_1 \bar{Q}_2</td>
<td>f_1 = h \cdot g_1 = IFCR \cdot (ton + MTA + ACDS)</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>f_2 = i \cdot k \cdot j \cdot IFCR \cdot \bar{g}_2 = (OTA \cdot MLA + ACDS)</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>f_3 = k \cdot \bar{g}_2 = ATNR \cdot IFCR \cdot \bar{Q}_1 Q_0 = P_2</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>f_4 = j \cdot \bar{g}_2 = ATNR \cdot SPMS \cdot \bar{Q}_1 Q_0 = P_5</td>
<td></td>
</tr>
<tr>
<td>TADS X 0 1</td>
<td>X 0 1</td>
<td>k</td>
<td>g_2 = Q_1 \bar{Q}_2</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>j</td>
<td>g_3 = Q_1 \bar{Q}_2</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Q_1, Q_0</td>
<td>f_5 = IFCR \cdot ATNR \cdot g_3 = IFCR \cdot ATNR \cdot \bar{Q}_1 Q_0 = P_6</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_6 = ATNR \cdot g_3 = ATNR \cdot \bar{Q}_1 Q_0 = P_7</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>Q_1, Q_0</td>
<td>f_7 = IFCR \cdot ATNR \cdot \bar{g}_4 = IFCR \cdot ATNR \cdot \bar{Q}_1 Q_0 = P_8</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_8 = ATNR \cdot \bar{g}_4 = ATNR \cdot \bar{Q}_1 Q_0 = P_9</td>
<td></td>
</tr>
<tr>
<td>TACS X 1 0</td>
<td>X 1 0</td>
<td>IFCR \cdot ATNR</td>
<td>g_4 = Q_1 \bar{Q}_2</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_9 = IFCR \cdot ATNR \cdot ATNR \cdot \bar{Q}_1 Q_0 = P_10</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_10 = m \cdot IFCR \cdot \bar{g}_6 = IFCR \cdot (SPD + ACDS)</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_11 = m \cdot IFCR \cdot \bar{g}_6 = IFCR \cdot (SPD + ACDS)</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_12 = m \cdot IFCR \cdot \bar{g}_6 = IFCR \cdot (SPD + ACDS)</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_13 = m \cdot IFCR \cdot \bar{g}_6 = IFCR \cdot (SPD + ACDS)</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>ATNR</td>
<td>f_14 = m \cdot IFCR \cdot \bar{g}_6 = IFCR \cdot (SPD + ACDS)</td>
<td></td>
</tr>
</tbody>
</table>

Table 2. Excitation equations for T interface function

\begin{align*}
D_0 &= F_0 = f_1 + f_2 + f_4 + f_6 + f_7 + f_8 = P_0 + P_1 \\
  &+ P_2 + P_3 + P_5 + P_7 + P_9 + P_9 \\
D_1 &= F_1 = f_2 + f_4 + f_6 + f_7 + f_8 = P_0 + P_3 + P_5 + P_7 + P_9 \\
D_2 &= F_2 = f_2 + f_4 + f_6 + f_7 + f_8 = P_0 + P_3 + P_5 + P_7 + P_9 \\
\end{align*}

Table 3. State-output equations for T interface function

\begin{align*}
\text{SPMS} &= \bar{Q}_2 \\
\text{TACS} &= F_3 = Q_1 \bar{Q}_0 = P_{13} \\
\text{SPAS} &= F_4 = Q_1 Q_0 = P_{14} \\
\end{align*}

Table 4. T function program

<table>
<thead>
<tr>
<th>Inputs</th>
<th>Outputs</th>
</tr>
</thead>
<tbody>
<tr>
<td>P0</td>
<td>f_1</td>
</tr>
<tr>
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</tr>
<tr>
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<tr>
<td>3</td>
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<td></td>
</tr>
<tr>
<td>13</td>
<td></td>
</tr>
<tr>
<td>14</td>
<td></td>
</tr>
</tbody>
</table>

Active Level

\begin{align*}
H H H H H
\end{align*}
2. The IEEE-488 Standard's diagrams must be modified to accommodate the chosen model. In this particular case the model includes eight of the allowed ten functions.

and P₉ are programmed as an active HIGH. All other P terms in the F₀ output are programmed as a dot. The three unused outputs are spares for future program alterations or for new output functions.

The program for the T function is presented in Table 4 and a corresponding circuit realization in Fig. 3. The other functions—RL, SH, AH, L and SRQ—are designed similarly.

Expressions are simplified

The absence of a Controller function within the interface system simplifies certain transitional conditions containing Controller states (logical values for CACS and CTRS are always equivalent to ZERO). For example, the expression for transition from SIDS to SGNS state “a” reduces to

\[ a = \text{TACS} \lor \text{SPAS} \]

The condition for transition from SDYS to STRS,

\[ c = \text{RFD} \land T_1, \]

The absence of a Controller function within the interface system simplifies certain transitional conditions containing Controller states (logical values for CACS and CTRS are always equivalent to ZERO). For example, the expression for transition from SIDS to SGNS state “a” reduces to
Table 5. Message outputs

<table>
<thead>
<tr>
<th>Interface function state</th>
<th>Qualifier</th>
<th>Uniline remote message sent</th>
<th>Multiline remote message sent</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>DAV</td>
<td>RFD</td>
</tr>
<tr>
<td>SIDS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>SGNS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>SDYS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>STRS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>SWNS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>WIWS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>TIDS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>TADS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>TACS</td>
<td>(F)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>SPAS</td>
<td>APRS INACTIVE</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>SPAS</td>
<td>APRS ACTIVE</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>AIDS</td>
<td>(T)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>ANRS</td>
<td>(T)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>ACRS</td>
<td>(T)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>AWNS</td>
<td>(T)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>ACDS</td>
<td>(T)</td>
<td>F</td>
<td>T</td>
</tr>
<tr>
<td>NPRS</td>
<td>(F)</td>
<td>T</td>
<td></td>
</tr>
<tr>
<td>SRQS</td>
<td>(F)</td>
<td>T</td>
<td></td>
</tr>
<tr>
<td>APRS</td>
<td>(F)</td>
<td>T</td>
<td></td>
</tr>
</tbody>
</table>

is interpreted as
\[ c = RFD \land SDYS_D, \]
where SDYS_D is a \( T_1 \)-seconds-delayed state. State SDYS_D is generated with a dual monostable multivibrator, the AM26S02 (Fig. 4). In the figure, choose resistors \( R_x, R_y \) and capacitors \( C_x, C_y \) to satisfy \( T_1 \leq 2 \mu s \).

The requirement for transition from ANRS to ACRS reduces to
\[ e = ATN \lor rdy, \]
since a tcs signal is always false in the absence of the Controller function. The DAV transition from ANRS to AWNS is deleted since it never occurs during normal interfacing.

The requirement for \( T_3 \) is taken care of automatically by the nature of the interface (clocked sequential circuit), so the transition from ACDS to AWNS reduces to:
\[ P = rdy \lor ATN. \]
The transition from LIDS to LADS simplifies to
\[ a = IFC \land (MLA \land ACDS); \]
and the transition from LADS to LIDS becomes
\[ n = ACDS \land (UNL \land MTA), \]
because of the absent Controller function (note that local messages lun and ltn are omitted).

The SRQ and L functions are implemented together on the same FPLA chip. Note that timing requirements for the IFC and ATN transitions are taken care of automatically by the nature of the clocked sequen-
### Table 6. Interface Message Reference List

<table>
<thead>
<tr>
<th>Mnemonic</th>
<th>Message</th>
<th>Interface Function(s)</th>
</tr>
</thead>
</table>
| **Local messages received**  
(by interface functions) | | |
| MEMW | memory write | SH |
| MEMR | memory read | L |
| end | end | SH, AH, T, L,SR,RL |
| nba | new byte available | AH |
| lon | listen only | SR |
| pon | power on | RL |
| rdy | ready | T |
| rsv | request service | |
| rtl | return to local | |
| ton | talk only | |
| **Local messages sent** | | |
| AHINT | acceptor handshake interrupt | |
| SHINT | source handshake interrupt | |
| SPINT | serial poll interrupt | |
| DTINT | device trigger interrupt | |
| DCINT | device clear interrupt | |
| **Remote messages received** | | |
| ATN | attention | SH,AH,T |
| DAB | data byte | (via L) |
| DAC | data accepted | SH |
| DAV | data valid | AH |
| DCL | device clear | DC |
| END | end | (via L) |
| GET | group execute trigger | DT |
| GTL | go to local | RL |
| IDY | identify | L |
| IFC | interface clear | T,L |
| LLO | local lookup | RL |
| MLA | my listen address | L,RL,T |
| MTA | my talk address | T,L |
| OTA | other talk address | T |
| PCG | primary command group | TE |
| REN | remote enable | RL |
| RFD | ready for data | SH |
| RQS | request service | (via L) |
| SDC | selected device clear | DC |
| SPD | serial poll disable | T |
| SPE | serial poll enable | T |
| STB | status byte | (via L) |
| UNL | unlisten | L |
| **Remote messages sent** | | |
| DAC | data accepted | AH |
| DAV | data valid | SH |
| END | end | (via T) |
| RFD | ready for data | AH |
| RQS | request service | T |
| SRQ | service request | SR |
| STB | status byte | (via T) |
| DAB | data byte | (via T) |
| DAC | data accepted | AH |
In the Source-handshake (SH) function, SDYS₀ (delayed source-delay state) is generated by a monostable multivibrator. Resistor $R_x$ and capacitor $C_x$ are chosen so that $T_1$ is about 2 $\mu$s. Notice that SDYS₀ is reset as soon as SDYS goes LOW.

### IEEE-488-interface specifications

**Interconnection devices:** Up to 15 on one contiguous bus.

**Interconnection path:** Star or linear bus network over 20-m total transmission path.

**Signal lines:** 16 total—eight data lines and eight lines for control and status messages.

**Message-transfer scheme:** Byte-serial, bit-parallel asynchronous data transfer using an interlocked three-wire handshake technique.

**Data rate:** 1 Mbyte/s max over limited distances; 250 to 500 kbytes/s typical over full transmission path.

**Interface functions:** 10 total—five primary communication functions and five special-purpose functions.

**Address capability:** Primary addresses—31 talk and 31 listen; secondary (2-byte) addresses—961 talk and 961 listen.

**Control shift:** May be delegated, never assumed, with a maximum of one talker (up to 14 listeners) at a time.

**Interface circuits:** Driver and receiver circuits TTL-compatible.

### IEEE-488 bus signal lines

**Data lines** (DIO1-DIO8) transfer bidirectional data and other messages in a byte-serial, bit-parallel manner.

**Handshake lines** (DAV, NRFD, NDAC) regulate data and message transfer. The information transfer asynchronously adjusts itself to the slowest currently active instrument.

**Data Valid (DAV)** is a remote message generated by the talker, indicates to the listener(s) that data on the bus are valid.

**Not ready for data (NRFD)** is a remote message generated by the listener(s); When detected true, it indicates to the talker that not all listeners are ready to accept the byte of data.

**Not data accepted (NDAC)** is a remote message generated by the listener(s); When detected false, it indicates to the talker that all listeners have accepted the byte of data, and data can be removed.

**Management lines** (IFC, REN, ATN, EOI, SRQ) control bus activity.

**Interface clear (IFC)** is a control-signal line that sets the interface system in a known quiescent state.

**Remote enable (REN)** sets devices to either remote or local control, in conjunction with other coded messages.

**Attention (ATN)** is a controller command: When ATN is true, addresses and universal commands are transmitted on only seven of the data lines, using the ASCII code. When ATN is false, any code of eight bits or less understood by both talker and listener(s) may be used.

**End or identify (EOI)** indicates the end of a multibyte transfer sequence. EOI in conjunction with ATN executes a polling sequence on devices with parallel-poll capability.

**Service Request (SRQ),** when detected true, indicates to the controller that some device on the bus wants attention.
The complete interface-logic system calls for six FPLAs to hold all the state functions. The system clock is supplied by one of the instruments attached to the interface.

5. The complete interface-logic system calls for six FPLAs to hold all the state functions. The system clock is supplied by one of the instruments attached to the interface.

The interface-message reference list is shown in Table 6, and the complete interface system logic diagram in Fig. 5. Note that the system clock is provided externally.

Handling remote messages

Normal interface operation allows two devices to send opposite values of remote messages simultaneously. The standard resolves this difficulty by introducing two kinds of message transfers over the interface—active and passive. Messages transfer so that the active value overrides the passive in every conflict.

Bearing the override in mind, select the recently introduced Motorola quad-interface-bus transceivers, MC3440 and MC3441. Both transceivers provide four open-collector drivers and four receivers, with the input hysteresis tailored to meet the bus-standard's specifications. Both are electrically compatible with the IEEE interface bus.

All remote messages sent by the interface are derived from the Message-outputs table (Table 5). The "ready" message, RFD, is generated only during ACRS. Similarly, AWNS is chosen to generate a DAC message. Message DAV is generated during STRS (note that SWNS is omitted), and SRQ during SRQS. The end message originates within a device concurrently with EOS, and is sent as an END remote message via the EOI line while TACS and STRS are active.

Status Byte (STB) may be sent in conjunction with the RQS uniline remote message during the SPAS function state while SR is in the APRS state. Accordingly, the seventh bit of data byte, DO7, is gated to satisfy this condition.

The interface-message reference list is shown in Table 6, and the complete interface system logic diagram in Fig. 5. Note that the system clock is provided externally.

Bibliography

FPLA Manual Programmer, Signetics, Sunnyvale, CA.
INTRODUCING DELCO ELECTRONICS’ MONOLITHIC OPERATIONAL AMPLIFIER

If you’re now using discrete power output transistors, we’ve got an alternative that gives you design versatility. It’s the DA-101—Delco’s Monolithic Operational Amplifier—with all the circuitry you need in one compact package.

The Monolithic Operational Amplifier (MOA) has two separate gain and power stages contained in a modified dual-in-line package. The DA-101 operates from a 10- to 16-volt DC supply and can be used in an audio bridge configuration with floating speaker output, or as two separate amplifier-speaker systems.

The MOA means weight savings in more ways than one. Besides reducing the total number of components you need, the MOA has a copper mounting surface to assure ample heat transfer to the convector. The tab negative or ground connection eliminates the need for mica insulation. In fact, the design of one power megaphone showed a components weight savings of 65 per cent.

Our new MOA means added design application flexibility, too. In automotive and home entertainment systems, two-way communication systems, power megaphones, motor controls, various H switch applications, and more.

Another advantage of our Monolithic Operational Amplifier is its durability. It has integral protective circuitry for not only overvoltage, but temperature, current conditions and shorted outputs as well. And it can be mounted by either direct soldering to a printed circuit board or through the use of a suitable socket.

For more information, contact an authorized Delco distributor, your nearest Delco sales office, or return the coupon on the right.

**ABSOLUTE MAXIMUM RATINGS**

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<thead>
<tr>
<th>Parameter</th>
<th>Min</th>
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<tr>
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**ELECTRICAL CHARACTERISTICS**

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<td>4Ω Non-bridge: 3.5W</td>
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**THERMAL CHARACTERISTICS**

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<td>Thermal Resistance, Ron(Typical)</td>
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**DIMENSIONS AND CONNECTIONS**

**SYMBOL INCHES MILLIMETERS**

<table>
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</table>

**DERATING CURVE**

**AUDIO BRIDGE CIRCUIT**

**TWO SEPARATE AMPLIFIERS CIRCUIT**

112
Standardized interfaces isolate

a control computer from its remote processors. You gain
design freedom, improve reliability, and save money too.

Inexpensive microcomputers can handle many test
and control operations with fewer than a dozen chips. But when these small computers must be integrated
into a larger system, the interface with the control
computer can become expensive. For instance, a relatively simple interface with the Camac system (see box) requires at least 45 small and medium-scale ICs.

Moreover, without guidelines for the construction
of such interfaces, the proliferating designs within a
large system make maintenance a nightmare. And the
duplication of design effort is an expensive waste. A
standard interface that connects a wide variety of 8
and 16-bit µPs to the serial Camac crate\(^1\) is therefore
long overdue.

Software beats hardware

Present Camac interfaces have been accomplished
by wiring together many small and medium-scale ICs. A few programmable interface chips like the Programmable Peripheral Interface (PPI) of Intel and the Peripheral Interface Adapter (PIA) of Motorola are available, but they do not readily mate with the Camac "dataway" (bus structure), and so require a great deal of programming, even for simple data transfers.

It is much better to adopt the basic philosophy of
µPs, namely to replace hardware with software. This
calls for programmable controllers such as a micro-
programmable sequencer. In a well-structured design,
the microinstructions can directly control the in-
terface.

Some of the relatively slow instructions required
to access the Camac dataway (about 2-µs cycle time)
can then be replaced by a sequence of fast (200-ns)
microinstructions. The resulting simplification of the
µP's software interface is an additional benefit.

To accommodate the predominant 16-bit mini-
computers, the majority of data transfers in Camac
use 16 bits, and the interface can be laid out for this
word size.

In a block diagram of the standardized interface
module (Fig. 1) the main functional blocks are a

1-k × 16 bit RAM, interface to the µP, Camac interface
buffers, and an interface controller. The RAM acts
as a buffer memory between Camac and the µP—all
data transfers between the two must temporarily be
stored here. To the controller and Camac, the memory
is configured as 1 k × 16 bits, but to the µP it may
also be accessed as 2 k × 8 bits. Camac commands
coming from the µP to be executed by the interface
controller are, for instance, passed in this form.

The µP interface contains control and status reg-
isters needed by the µP to initiate the stored com-
mands, and to read the controllers' responses. These
registers can be interrupt signals that inform the µP
when a command has been executed.

Camac interface buffers, on the other hand, pass
data between the internal data/control bus and the
dataway. The controller is responsible for operating
these buffers, and for generating the two dataway
timing signals, S1 and S2.

The core of the interface module, the controller,
consists of a microprogrammed sequencer and its
associated microprogram memory. This controller
initiates dataway cycles on command from the µP,
gives the required responses to Camac commands

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Dr. Peter J. Horne, Fellow, and Dr. Olaf Kaestner, Fellow.
European Organization for Nuclear Research, Geneva, Switzerland.
issued by the central computer, and interrupts the µP when a "LAM" signal is received from a Camac module. LAM (look at me) is equivalent to an interrupt.

Organize your memories

The 1 k x 16 bits of data memory may be accessed by either the µP or the controller, because both control the address and data lines. To enable 16-bit as well as 8-bit µPs to access this memory, a 50-ns PROM (Signetics N82S123) interprets the memory as 1-k words or 2-k bytes (Fig. 2), and a set of dual in-line switches compresses the 16-bit data bus to eight bits when necessary.

When the µP is not accessing the RAM, the three-state buffers in Fig. 2 are in the high-impedance state, and isolate the µP from the memory. The controller may now access the memory without conflict between its address and data lines and those of the µP. But what if the controller wants to access the memory at the same time as the µP? Unless a transfer is already underway, the µP gets priority because whenever the µP addresses the interface memory, it generates a

What is Camac?

Camac is a modular data-handling and interface system for on-line digital computers that is being widely used in Europe for industrial-process control, medical research and other applications. The Camac standard has been specified by European nuclear research laboratories and adopted as an IEEE standard (583-1975, 595-1976, and 596-1976).

The heart of the Camac standard is a bus structure, the "dataway." Since all interface modules connect to this dataway, they are completely computer-independent.

Up to 25 such modules can be housed in a "crate," where the dataway runs in the rear. Two stations of each crate are reserved for the "crate controller," which interfaces dataway and computer.

Buses on the dataway

The most important lines of the dataway are a read and write bus, each 24 bits wide; a function bus, F, with 5 bits and a subaddress bus, A, with four bits, which together define the function to be executed by a module; a private station-select line, N, for each module; a private-alarm line, L, from each module to the crate controller; a bus line, X, to confirm "command accepted;" and a line, Q, for function and module-dependent response. Line L is often called "LAM" (look at me).

The crate controller generates a "busy" signal B, two timing signals for each dataway cycle (on bus lines S1 and S2) and the unaddressed control commands to clear, initialize or inhibit the modules on bus lines C, Z, I, respectively.

Crate controller types

Camac uses three types of crate controllers (CC):
- A "dedicated" CC that interfaces the dataway to the I/O bus of the computer.
- A "type A" CC, used with the highly parallel "branch highway," that bridges shorter crate/computer distances. The branch highway is controlled by a "branch driver" and accommodates up to seven crates. A branch driver can either be a normal Camac module in a crate or a dedicated driver that interfaces to the computer's I/O bus.
- A "serial" CC, used with the "serial highway," that bridges very large crate/computer distances. Up to 62 crates form a loop that begins and ends in a "serial driver"—the serial equivalent of a branch driver.

Command messages—either byte or bit-serial—are sent around the loop. A "demand message" is inserted by the serial CC into the loop whenever a LAM occurs in its crate. Microprocessors in a crate have access to the N lines via the serial CC. They can send demand messages to the computer by a handshake with the serial CC to ensure interference-free control of the dataway.
3. A suggested interface memory map starts at 60 k to avoid interference. DSA means data storage address.

4. The standardized interface appears to the \( \mu P \) just as another block of memory.

Camouflage the interface

To make an interface usable for many \( \mu Ps \), use only address, data, and memory read/write lines for its control. As a result, the interface module looks like a block of memory to the \( \mu P \), and all control comes from predefined memory locations (Fig. 4). Four addresses are reserved for interface control:

- Initiate command address (ICA) (address = F800\(_{16}\))
- Inhibit Camac (INC) (address = F802\(_{16}\))

Camac response address (CRA) (address = F804\(_{16}\))
Status word (STATUS) (address = F806\(_{16}\))

When your \( \mu P \) wants to initiate a microprogram stored in the controller's microprogram memory, it writes to the proper ICA. These microprograms generate data transfers on the interface and Camac commands whose variables are stored in the interface memory (Fig. 4).

To initiate a particular microprogram, you must write a data value equal to its start address to the ICA after the requisite data have been placed in the correct memory location (Table 1).

While the \( \mu P \) performs data manipulations, it needs uninterrupted access to the interface memory. To prevent Camac from accessing the interface, the \( \mu P \) sets the Inhibit Camac bit by writing a One to address F802\(_{16}\). Should the central computer initiate a Camac command to the interface module at this time, it will receive an "X" response, but no "Q" response as is normal. When the \( \mu P \) has data for the central computer, it can reset the Inhibit Camac bit to Zero, and stop execution until the data have been completely acquired.

The Camac response address (F804\(_{16}\)) holds the X and Q responses to the last dataway cycle, which has
## Table 1. Microprogram parameters

<table>
<thead>
<tr>
<th>Microprogram</th>
<th>ICA i = data</th>
<th>DSA(1) Contents</th>
</tr>
</thead>
<tbody>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>0</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>1</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>2</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>3</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>4</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>5</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>6</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>7</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Initiate Camac dataway cycle in single transfer mode</td>
<td>8</td>
<td>NAF , DATA</td>
</tr>
<tr>
<td>Generate Z, C, I</td>
<td>9</td>
<td>ZCI</td>
</tr>
<tr>
<td>Load counter</td>
<td>10</td>
<td>Count</td>
</tr>
<tr>
<td>Load MAR</td>
<td>11</td>
<td>Address</td>
</tr>
<tr>
<td>Load NAF</td>
<td>12</td>
<td>N, A, F</td>
</tr>
<tr>
<td>Initiate block transfer</td>
<td>13</td>
<td>-</td>
</tr>
<tr>
<td>Initiate transfer in scan mode</td>
<td>14</td>
<td>DATA</td>
</tr>
<tr>
<td>Initiate demand message and load LAM register</td>
<td>15</td>
<td>Demand message</td>
</tr>
</tbody>
</table>

## Table 2. Decoded Camac functions

<table>
<thead>
<tr>
<th>Command</th>
<th>Response</th>
<th>Action</th>
</tr>
</thead>
<tbody>
<tr>
<td>F(0)A(0)</td>
<td>X (Q, Note 1)</td>
<td>Read register</td>
</tr>
<tr>
<td>F(16)A(0)</td>
<td>X (Q, Note 1)</td>
<td>Write to MAR</td>
</tr>
<tr>
<td>F(16)A(1)</td>
<td>X (Q, Note 1)</td>
<td>Write to MAR, if the next command is F(16)A(0)</td>
</tr>
<tr>
<td>F(16)A(2)</td>
<td>X (Q, Note 1)</td>
<td>Write to MAR, if the next command is F(0)A(0)</td>
</tr>
<tr>
<td>F(24)A(0)</td>
<td>X (Q, Note 1)</td>
<td>Inform µP of the termination of a write-to-memory sequence</td>
</tr>
<tr>
<td>F(24)A(1)</td>
<td>X (Q, Note 1)</td>
<td>Inform µP of the termination of a read-from-memory sequence</td>
</tr>
</tbody>
</table>

Note 1: The Q-response is ONE if the Inhibit Camac bit is ZERO.

## Table 3. Sequencer control lines

<table>
<thead>
<tr>
<th>S3 S2 S1 FE PUP Bits 23 22 21 20</th>
<th>Mnemonic</th>
<th>Action</th>
</tr>
</thead>
<tbody>
<tr>
<td>0 0 1 0</td>
<td>NOP</td>
<td>Microprogram counter is used as next address</td>
</tr>
<tr>
<td>1 1 0 1</td>
<td>JSR</td>
<td>Push microprogram counter and jump to address on D bus</td>
</tr>
<tr>
<td>1 1 1 X</td>
<td>JMP</td>
<td>Jump to address on D bus</td>
</tr>
<tr>
<td>0 1 0 0</td>
<td>RTS</td>
<td>Jump to address on stack, and pop stack</td>
</tr>
</tbody>
</table>
signals. The controller also checks for the occurrence of a LAM demand in the crate, and informs the μP when it happens.

The Am2909 microprogram sequencer is most suitable for the interface application because of its simple operation, and its speed (16.6-MHz maximum clock rate). The bipolar sequencer is a cascadable 4-bit slice device, and you need two of them in parallel to address 256 words of memory.

A control bus regulates the three other main interface blocks—memory, Camac buffers and μP interface. The data on this control bus at any particular instance depend on the microinstruction word that is held in its respective register.

The sequencer contains a four-input multiplexer to select the source of the next microinstruction. It can be an address register, a direct input, a microprogram counter, or a four-word Push/Pop register file, as determined by the code (Table 3) on the S0 and S1 lines in Fig. 6. The direct inputs form the D bus and are connected to either four Camac command lines (A1, A2, F8, F16), or the four ICA data lines (Figs. 4 and 6), or an address field that contains the destination address in the microinstruction word for direct jumps. The choice is made by the Camac N line and the Start-microprogram line.

The four-word register file allows nested subroutine calls up to four levels and temporary data storage. The File Enable (FE) and Push/Pop (PUP) lines control the use of this file; however, only one level
of subroutine nesting is planned.

The microprogram counter holds the next sequential address, which in most cases will be the incremented present address on the I bus (Fig. 6). Other sources of the next microinstruction address are selected during a jump to an address on the D bus, a subroutine call or return, and a “forced” call from either Camac or the \( \mu P \) to the address on the D bus.

The microprogram sequencer is controlled by four bits—\( S_n, S_o, \) FE and PUP—which are contained in the microinstructions as bits 20 to 23. Their possible combinations are given in Table 3.

A special microinstruction set for the interface controller eases the task of writing microprograms. Each 24-bit microinstruction word is divided into a number of control fields (Tables 4 and 5), which are selected by an operational code (bits 16 to 19). There are 10 possible microinstructions for this application:

1. Move a word (MOV \( S_i, D_j \)).
2. Branch if condition is true (BRIF \( T_i D_j \)).
3. Load destination with immediate data (LDI DA\( j, D_i \)).
4. Increment or Decrement (INC \( R D_i; Dec \( R D_i \)).
5. Interrupt the \( \mu P \) (INT \( ST_i \)).
6. Camac operation (CAM \( CA_i, S_2, S_1 \)).
7. No operation (NOP).
8. Jump to subroutine (JSR \( D_j \)).
9. Unconditional jump (JMP \( D_j \)).
10. Return from subroutine (RTS).

One clock runs the show

The controller’s timing is provided by one two-phase, 5-MHz clock. Phase 1 (\( \phi_1 \)) drives the microprogram sequencer, and phase 2 (\( \phi_2 \)) the microinstruction register. Since the access time of the NS25114 PROM microprogram memory (256 \( \times \) 8) is 60 ns, and the delay time from clock (\( \phi_1 \)) to the output of the Am2909 about 40 ns, the microinstruction is strobed by \( \phi_2 \) into its register after 100-ns delay.

Because this instruction cycle relates directly to the timing of the Camac dataway, the interface controller can easily generate the 200-ns Camac timing signals (e.g. \( S_1 \) and \( S_2 \)). The \( S_2 \) signal must, however, be generated 700 ns after the start of a Camac dataway cycle, which can therefore not be on an instruction boundary (Fig. 7). The \( S_2 \) signal is therefore generated by the 4th instruction after the start of a Camac dataway cycle, and delayed 100 ns by hardware before being clocked onto the dataway.

To allow use of the Am9130 1-k \( \times \) 4-bit, 200-ns RAM memory, all read microinstructions must be repeated twice—the \( \phi_1 \) clock strobes data into the destination register, but the memory’s access time requires that the data remain valid for the next \( \phi_1 \) strobe.

Protocol may cause delay...

To transfer data between the central computer and the \( \mu P \), you need a certain protocol. If the \( \mu P \) expects

<table>
<thead>
<tr>
<th>Bits</th>
<th>Mnemonic</th>
<th>Meaning</th>
</tr>
</thead>
<tbody>
<tr>
<td>7 6</td>
<td>MEM</td>
<td>The contents of the memory location whose address is held in MAR</td>
</tr>
<tr>
<td>0 0</td>
<td>LAM</td>
<td>The contents of the LAM register</td>
</tr>
<tr>
<td>0 1</td>
<td>CNTR</td>
<td>The contents of the counter</td>
</tr>
<tr>
<td>1 0</td>
<td>MAR</td>
<td>The contents of the memory address register</td>
</tr>
<tr>
<td>5 4</td>
<td>Sources (( S_i ))</td>
<td></td>
</tr>
<tr>
<td>0 0</td>
<td>MEM</td>
<td>The memory location whose address is held in MAR</td>
</tr>
<tr>
<td>0 0</td>
<td>MAR</td>
<td>The memory address register</td>
</tr>
<tr>
<td>0 1</td>
<td>NAF</td>
<td>The NAF command register</td>
</tr>
<tr>
<td>0 1</td>
<td>SGLE</td>
<td>The SGLE register</td>
</tr>
<tr>
<td>1 0</td>
<td>CNTR</td>
<td>The counter</td>
</tr>
<tr>
<td>1 0</td>
<td>RREG</td>
<td>The CAMAC read register</td>
</tr>
<tr>
<td>1 1</td>
<td>MARB</td>
<td>The memory address register buffer</td>
</tr>
<tr>
<td>2 1</td>
<td>Test (( T_i ))</td>
<td></td>
</tr>
<tr>
<td>0 0</td>
<td>AUXLOC</td>
<td>Test the state of the auxiliary lockout bit</td>
</tr>
<tr>
<td>0 0</td>
<td>AUXREAD</td>
<td>Test the state of the auxiliary read bit</td>
</tr>
<tr>
<td>0 1</td>
<td>AUXTEST</td>
<td>Test the state of the auxiliary test bit</td>
</tr>
<tr>
<td>0 1</td>
<td>CNTRZ</td>
<td>Test the state of the counter = zero bit</td>
</tr>
<tr>
<td>1 0</td>
<td>Q</td>
<td>Test the state of the Q bit</td>
</tr>
<tr>
<td>1 0</td>
<td>DBSY</td>
<td>Test the state of the demand BUSY bit</td>
</tr>
<tr>
<td>1 1</td>
<td>X</td>
<td>Test the state of the X bit</td>
</tr>
<tr>
<td>1 1</td>
<td>LAM</td>
<td>Test the state of the LAM bit</td>
</tr>
<tr>
<td>6 5</td>
<td>Camac (( CA_i ))</td>
<td></td>
</tr>
<tr>
<td>0 0</td>
<td>MEM(R)</td>
<td>Auxiliary receive, read from the dataway to memory pointed at by contents of MAR</td>
</tr>
<tr>
<td>0 0</td>
<td>MEM(W)</td>
<td>Write to memory location whose address is held in MAR</td>
</tr>
<tr>
<td>0 1</td>
<td>MAR</td>
<td>Memory address register (write only from CAMAC)</td>
</tr>
<tr>
<td>0 1</td>
<td>RREG</td>
<td>Read the contents of the CAMAC read register</td>
</tr>
<tr>
<td>1 0</td>
<td>MEM(T)</td>
<td>Read the contents of memory location pointed at by MAR and transmit to CAMAC (auxiliary transmit)</td>
</tr>
<tr>
<td>1 0</td>
<td>NAF</td>
<td>Enable the NAF command register/buffer onto the dataway</td>
</tr>
<tr>
<td>1 1</td>
<td>ZCI</td>
<td>Generate the dataway common control signals</td>
</tr>
</tbody>
</table>
Table 5. Status field descriptions

<table>
<thead>
<tr>
<th>15</th>
<th>14</th>
<th>13</th>
<th>12</th>
<th>11</th>
<th>10</th>
<th>9</th>
<th>8</th>
</tr>
</thead>
<tbody>
<tr>
<td>ST1</td>
<td>ST2</td>
<td>ST3</td>
<td>ST4</td>
<td>ST5</td>
<td>ST6</td>
<td>ST7</td>
<td>ST8</td>
</tr>
</tbody>
</table>

- Data available (DTV)
- Data read (DTR)
- LAM demand (LAM)
- End of cycle (EOC)
- No Q response (NQ)
- No X response (NX)
- Demand busy (DBSY)
- Auxiliary lockout (AUXLOC)

---

Data from the central computer, the µP must wait until it knows that the data transfer is completed. The interface controller uses the first bit in the status field description (ST1) to signal "data available" (DTV in Table 5).

If the data are located in a contiguous block of memory, it is necessary that one of the following three conditions be satisfied:

1. The data block's start address is known to the µP beforehand.
2. The MAR, having been loaded by Camac, is pointing at the start address.
3. The start address is stored in memory at DSA (11) and is ready for a load MAR command from the µP.

The second and third cases occur when the data in memory are to be written immediately to another module in the Camac crate. The first case, however, will probably be used most often, with the data block's size and start address specified in advance for any particular application.

While the µP uses the interface, the central computer must be prevented from interrupting. This is achieved when the µP sets the Inhibit Camac bit. With this bit set, the interface module gives X responses to all Camac commands, which signals that these commands have not been executed. Before the central computer can load a second block of data into the memory, it must repeat the initial command until it receives both X and Q responses.

When the central computer expects data from the µP, the µP writes the data into the interface memory and informs the central computer of that by either transmitting a demand message or "dropping" the Inhibit-Camac bit. Transmitting a demand message is more efficient because the central computer then does not have to keep on testing the state of the interface module.

The data block's start address must either be known to the central computer beforehand, or the MAR must point at it. If the address always remains in the MAR, the central computer need not load this register prior to reading the data. It must, however, inform the µP that the data have been read, by sending the Camac command F(24)A(1).

...and barricade the dataway

In a serial-crate controller, you may have to deny auxiliary controllers (interface and µP) access to the dataway, by setting an "auxiliary lockout" bit (ACL). When a crate controller recognizes its address in an incoming message, it sets this bit automatically (Ref. 1, p. 81) and keeps it "on" until the required dataway cycle terminates or an error is detected in the message.

The interface controller tests the condition of the ACL line before each µP-requested dataway cycle. If ACL is active, the interface controller doesn't start the cycle but informs the µP by sending an interrupt, and setting the AUXLOC bit in the status register (Fig. 4).

In a 5-MHz byte-serial crate system, the maximum time that the ACL bit can be set is 4.7 µs; thus, the µP should wait that long before reinitiating the Camac command. In systems that use the bit-serial mode, or have slower clock rates, the delay will be proportionately longer, and the µP will spend more time waiting for Camac commands to be executed. However, with an intelligent auxiliary controller in the system, the central computer should access the crate infrequently, and minimize µP delays. ■

Acknowledgement

The authors wish to thank the CERN fellowship program for support of this work.

References

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- Tune the VCO frequency coarsely with the channel information along with frequency lock-in by the loop.

Fast lock-up—increasing the speed at which a digitally programmed frequency source moves between channels—is important, for instance, when a synthesizer generates both transmitter driver and receiver local-oscillator signals, and when the output must change by the i-f frequency of the receiver (when switching from transmit to receive).

Fast PLLs are also important in scanning receivers in which preprogrammed channels—perhaps widely spaced in frequency—are scanned, and receivers that time-share local-oscillator frequency. In each of these cases the maximum scanning or sharing rate is determined by how quickly the loop dynamics will allow the synthesizer-output frequency to change and stabilize between acceptable limits.

**Analyzing the PLL**

A typical PLL is composed of a phase detector, loop filter and VCO (Fig. 1). Since the detector is a digital, three-state circuit, its output is a pulse that lasts as long as the phase difference of the input signals—provided the input frequencies (more accurately, repetition rates) are identical. When the input rates differ, the output-pulse width changes between limits at a rate equal to the difference of the input rates.

A useful approximation relates the average output voltage to the input phase difference. If the frequencies are locked and the phase difference is 180°, you get the waveform in Fig. 2. If the height of the output is $V_p$, the average voltage is, of course, $V_p/2$. Since a three-state phase detector is linear from $-2\pi$ to $+2\pi$ radians, the average voltage relative to the phase difference is $V_{av} = V_p\phi/2\pi$, which yields a gain constant of $K_\phi = V_p/2\pi$ volts/rad.

---

C.A. Sharpe, Project Engineer, Bendix Avionics Division, 2100 Northwest 62nd St., Fort Lauderdale, FL 33310.
When the input frequencies differ, the gain constant (not the same as the phase gain constant) may again relate the average output voltage to the frequency difference. The second PLL element, the loop filter, is often called a low-pass filter because of its general transfer function.

However, in the synthesizer of Fig. 1, the filter serves as an integrator that accepts the phase-detector pulse and raises or lowers a control-line voltage until there is zero phase error or no further input pulse (Fig. 3). The transfer function of the loop filter-integrator is given by $(sCR_2 + 1)/sCR_1$.

The VCO is specified in units of $f_l/V$, since the frequency usually varies about a value far removed from zero. In this case, the actual VCO frequency is $\omega_K + K_{vco}(V - V_K)$. To get the transfer function, the most useful quantity in loop analysis, run through the following operation:

$$\frac{\omega_{vco} - \omega_K}{V - V_K} = \frac{\Delta \omega}{\Delta V} = K_{vco} \frac{\text{rad/s}}{V}.$$ 

Since phase is the integral of frequency,

$$K_{vco}(\theta) = \frac{1}{s} K_{vco}(f).$$

In most analyses, the VCO-gain constant is taken to be

$$K_{vco} \text{ rad/s/volt.}$$

In Fig. 4, assume the two inputs have the same repetition rates, but that input 1 leads input 2 in phase. That is, switch S connects to $V_p$, with each positive transition of input 1, and opens with a positive transition of input 2. Note that the phase detector now alternates between a "pump" state in which the output equals $V_p$, and a high-impedance state, in which the output line floats (see Table).

(A similar analysis holds if input 1 lags input 2. The output line alternates between open circuit and ground, for example, in a three-state phase detector: $V_{p\text{na}},$ open circuit, $-V_p$.)

While the output line is high, the filter integrates the input voltage, and lowers the control-line potential to that of the VCO. The equation for this mechanism is

$$V_{\text{control line}} = V_{\text{initial}} - V_p \left[ R_2 + \frac{1}{R_1C} \int_0^T \text{dt} \right]$$

or

$$\Delta V = \frac{V_p}{R_1C} t.$$ 

The result of this last equation can be considered the control-line slew rate—the maximum speed at which the control line can move to the new required voltage. Multiply the slew rate by the VCO-gain constant and the result is the maximum rate at which the VCO frequency can change:

$$S_{vco} \text{ Hz/s}.$$ 

When shifting from receive to transmit, the VCO frequency must change by 10.7 MHz. The time(T) required to do this is the fastest rate you can get and is found from

$$T = \frac{10.7}{S_{vco}} \text{ MHz}.$$ 

But since the average input to the loop filter is less than $V_p$, the actual time required will be longer than the calculated value. However, you can determine a worst-case lock time by assuming that $V_p$ has the lowest possible average value with a frequency difference and that the lock-up transient occurs after the VCO frequency reaches the proper value. Thus,
Time (worst case) = lowest slew rate of VCO + lock-up transient
\[ \Delta f_{VCO} + \frac{4}{2S_{VCO} \omega_n} \]
where \( \omega_n \) = the natural frequency.

The actual time required falls between the best and worst-case values and depends upon the damping factor and the type of phase detector. With a quad-D detector, the average output voltage is very close to \( V_p \) and produces a much faster slew rate.\(^1\)

**Speeding the slew rate**

The analyses show that using the normal loop dynamics to get a large VCO slew is slow. What you need is a mechanism that gets the VCO frequency to the right vicinity immediately and then lets the loop lock itself.

The simplest way to get a fast transition is to switch between two VCOs in the loop. If, for instance, two VCOs are tracked with the same control voltage between separate frequency ranges (Fig. 4), no major control-voltage transition is required for a large frequency change.

When transmitting, VCO 1 is active and tuned by the control line. When receiving, VCO 2 is active and requires the same tracking voltage to generate a frequency that is 10.7 MHz lower than VCO 1 (in this example). The time required for lock, therefore, is the time required for the control line to compensate for any tracking error plus the regular lock-up transient of approximately four \( \omega_n t \) units from the second-order curves.

You may want to simplify Fig. 4 when you can switch one VCO in range—add capacitance to the tank circuit (Fig. 5). Normally, the circuit is designed for a certain tracking response in the transmit mode. In keeping with Fig. 4, select values so that 2 V tunes the tank to 150 MHz and 8 V to 160 MHz. Energize the receive line to switch \( C_x \) in parallel with the tank and to lower the resonant frequency.

Next, adjust \( C_x \) so that the output frequency is exactly 10.7 MHz lower with the same control-voltage input. Now when the device switches from transmit to receive, you don't require much more control voltage than is needed for a single-channel change.

However, the techniques in Figs. 4 and 5 are very restrictive—you must know the exact frequency shift beforehand. This requirement is no problem for simple \( R_x = T_x \) operation, but when the frequency shift continually changes, it can be.

**More sophisticated approaches**

In the optimization approach, the constraints on the loop's natural frequency and the damping factor define the lock-in performance for small frequency changes and determine the spectral purity of the VCO output. However, in any system using a three-state phase detector and an integrator, both \( \omega_n \) and \( \gamma \) are free variables that can be specified by \( R_1, R_2 \) and \( C \) in the integrator for any combination of \( N, K_v \), and \( K_\phi \). Thus,
\[ \omega_n^2 = \frac{K \phi K_v}{N R_1 C} \]
and
\[ \gamma = \frac{R_2 C}{2} \]

Usually, you must decide whether to use an offset oscillator with a mixer, a fixed prescaler, or do direct counting. To decide, consider the usual tradeoffs: cost, space or availability. See if any of the loop constants can be optimized for slew rate:
\[ T_L (approx) = \frac{16}{\omega_n^2} \] (from second-order curves),
where \( T_L \) equals the lock time.

From your analysis of absolute maximum slew rate,
\[ \Delta V_{VCO} = \frac{V_{p(max)} T_s}{R_1 C} \]
and
\[ T_s^2 = \frac{\Delta V_{VCO}^2 R_1^2 C^2}{V_{p(max)}^2} \]
where \( T_s \) equals the slew time and \( V_{VCO} \) equals the voltage change required to slew the VCO from one end of the band to the other. However, \( V_{p(max)} = 2 K_\phi \pi \),
\[ T_s^2 = \frac{V_{VCO}^2 R_1^2 C^2}{4 \pi^2 K_\phi^2} \]
and
\[ T_s^2 = \Delta V_{VCO}^2 R_1^2 C^2 \times \frac{\omega_n^2}{16} \]
Substituting for $\omega_n^2$

$$M = \frac{T_s^2}{T_L^2} = \frac{(\Delta V_{VCO})^2(R_1^2 C^2 K_\phi K_v)}{(4\pi^2)(K_\phi^2 16NR_1 C)} = \frac{(\Delta V_{VCO})}{R_1 CK_v \phi 64\pi^2 N}$$

with $T_s/T_L$ representing a measure of slew rate vs lock time.

Now examine the equations for $M$ and $\omega_n$. You can readily see that to minimize $M$ and keep $\omega_n$ constant, the confining variables are $N$ and the $R_1C$ product. If $N$ is made very large to reduce $M$, $\omega_n$ can be kept constant by reducing the $R_1C$ product—which further reduces $M$. Since $\omega_n$ determines the adjacent-channel lock time, selecting the system with the largest $N$ results in the minimum slew rate. Note that the damping factor has not been mentioned. It is a free variable, a function of $R_2$, and can be left for last.

Consequently, the slew rate in a direct counting system with a large $N$ is greater than in a system designed around an offset oscillator. With an offset oscillator, the arrangement feeding the highest-difference frequency into the logic (requiring a larger $N$ than with counting) will be the fastest. If the slew speed is still not fast enough, look into changing the loop dynamics.

Since $\omega_n$ and $\gamma$ are constrained, by tradeoffs of spectrum purity and lock time, a combination of $R_1$, $R_2$, and $C$ is specified at lock. However, while the loop is slewing to a new frequency, spectral purity is unimportant and $\omega_n$ can be raised to a higher value. This operation is quite simple. See Fig. 6.

Select $R_1$ and $R_2$ to give the desired $\omega_n$ and $\gamma$ when the system is locked. Then select $R_{1s}$ to give a much higher $\omega_n$ when the system is slewing. Finally, select $R_{2s}$ to give an acceptable $\gamma$ when $R_{1s}$ is switched in. The switches can be FETs or inexpensive CMOS.

To determine when and how long to activate the switches, monitor the channel lines and detect any change occurring above a selected value. Or, for $R_x = T_x$ switching, use the key line. Either method can filter a one-shot for a fixed interval that you determine:
1. Select $R_1$ and $R_2$ for desired $\omega_n$ and $\gamma$ when the PLL is locked.
2. Select $R_{1s}$ and $\gamma_{1s}$ to give the desired slewed time.
3. Fire the one-shot to activate the switch for slightly less than $T_s$.

When the PLL is out-of-lock, use the $R_{1s}$ and $R_{2s}$ constants for $\omega_n$ and $\gamma$. To use them, activate the one-shot with an instantaneous loss-of-lock detector. If the one-shot period is slightly greater than that of the reference, $R_{1s}$ and $R_{2s}$ will switch-in as soon as lock is lost and out when it is re-established.

Finally, should you decide to coarse-tune the VCO, set the VCO frequency approximately at the correct frequency with an analog voltage determined by the selected channel. The control voltage supplied by the integrator maintains phase lock but only over a restricted range. The primary advantages of coarse-tuning are that you can set the frequency instantly to anywhere in the range with the coarse tuning, and the lock-up time becomes essentially the same as that of the adjacent-channel case. Two ways to coarse-tune the VCO are shown in Fig. 7a and 7b.

The summing circuit in Fig. 7a can be a passive resistor network or an op-amp configuration. If in the PLL of Fig. 1 the 150 to 160-MHz spread must be divided into 1-MHz increments on the coarse-voltage generator, the advantages of coarse-tuning become apparent. And since the dynamic range of the control line—hence the varactor-capacitance change—is much smaller than a direct method (which covers the full 10 MHz), VCO-temperature drift (encountered with offset mixing) is easily controlled.

Using two varactors as in Fig. 7b will usually save some space. Regardless of the method, however, take care to keep the coarse-voltage line as noise-free as possible. Any garbage on the line will directly modulate the VCO and substantially decrease spectrum purity. Of course, if you want FM (as in the case of an FM transmitter), it's easy to couple-in audio through a capacitor. 

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Conventionally, scope rise time is determined by watching the output of a fast pulse generator on the scope and assuming that the observed delay time is the desired rise time. This method is costly and faulty because you need an expensive pulse generator and because you have to assume that the rise time of the pulse generator is many times faster than that of the scope—often an unwarranted assumption.

An equivalent circuit illustrates a scope's bandwidth limitation and points the way to measuring its $t_r$ (Fig. 1). With most scopes, the input impedance given includes the probe's. An impedance of $10 \, \Omega$ in parallel with $10 \, pF$ is quite common. With the scope driven from a voltage source (zero impedance), the result is similar to a Bode plot (Fig. 2).

Working out the math

In Fig. 2, point $f_1$ represents the corner frequency associated with $R$ and $C_2$. With $R$ equal to $10 \, \Omega$, the problem is to find that value of $C_2$ that limits the bandwidth and increases the rise time. Start by finding the output voltage, $e_o$ (Fig. 3):

$$e_o(s) = \frac{e_i(s)}{R C_2} \left[ \frac{1}{s^2 + s(C_2 R + R C_2 + R C_2) + \frac{1}{R C_2}} \right]$$

with $C_T \gg C_2$,

$$e_o(s) = \frac{e_i(s)}{R (R C_T C_2)} \left[ \frac{1}{(s + \frac{1}{R C_2})(s + \frac{1}{R C_T})} \right]$$

Let the input voltage, $e_i(s)$, be a step function. Then $e_i(s) = e_i/s$, and using partial fractions,

$$e_o(s) = \frac{e_i}{R (R C_T C_2)} \left[ \frac{A}{s} + \frac{B}{s + 1} + \frac{C}{s + \frac{1}{R C_T}} \right]$$

where

$$A = R C_T R C_T, \quad B = R C_T R C^2, \quad C = \frac{R C^2 R C_T}{R C - R C_T}$$

After simplifying those equations, and taking the inverse Laplace transform, then the partial of $e_o(t)$ with respect to $C_T$,

$$\frac{ae_o(t)}{aC_T} =$$

$$\frac{(R C_T R C_T + t R C_T - t R C_T) e^{-t}}{C_T(R C_T - R C_T)^2} \left[ \frac{-1}{C_T(R C_T - R C_T)^2} \right]$$

Now take the partial derivative of $e_o(t)$ with respect to $t$. At the moment the measurement is made, $e_{id}(t)$ can be considered constant (Fig. 4):
2. The frequency response of a scope's input circuit resembles that of a low-pass filter when the scope is driven from an ideal voltage source.

3. A complete scope circuit includes source and probe impedances (a). For calculating, the circuit is reduced to a generalized, equivalent form (b).

4. This voltage waveform of the scope calibrator shows that $e_{in}(t)$ is constant at the moment of measurement.

\[ \frac{ae_0(t)}{ae_0(t)} = \frac{e^{\frac{-t}{R_sC_T}} - e^{\frac{-t}{RC_2}}}{R_sC_T - RC_2} \]

Since

\[ \frac{ae_0(t)}{ae_0(t)} \times \frac{aC_T}{ae_0(t)} = \frac{aC_T}{\text{at}} \]

inverting Eq. 1 and multiplying the inverted equation by Eq. 2 yields an expression for $\frac{aC_T}{\text{at}}$:

\[ \frac{R_sC_T - RC_2}{C_2R_sR} \left[ e^{-\left(\frac{1}{R_sC_T} - \frac{1}{RC_2}\right)} - 1 \right] \]

Now,

\[ aC_T = \Delta C_T \quad \text{if} \quad C_T >> \Delta C_T \]

and

\[ \Delta t = \text{at} \quad \text{if} \quad t >> \Delta t \]

where $t$ is the point at which the measurement is made.

Therefore,

\[ \frac{\Delta C_T}{\Delta t} = \frac{R_sC_T - RC_2}{C_2R_sR} \]

Using L'Hospital's rule to evaluate Eq. 3 at $R_sC_T = RC_2$, you get

\[ \frac{\Delta C_T}{\Delta t} = \frac{2C_T}{t} \]

Not much equipment is needed

To obtain the scope's rise time, set up the equipment as shown in Fig. 5a. Select $C_1$ to be 200 pF, and $t$ to
5. A rise-time-measurement setup consists of just a few circuit components (a). Resistor \( R_s \) is varied to get a predetermined trace displacement on the CRT (b).

Let \( \Delta t = 10 \mu s \). Make \( \Delta t \) equal to 1 \( \mu s \). Then,

\[
\Delta C_T = \frac{2}{t} \left( \frac{C_T (\Delta t)}{t} \right)
\]

\[
\Delta C_T = \frac{2(200 \times 10^{-12})(1 \times 10^{-6})}{10 \times 10^{-6}}
\]

\[
= 40 \times 10^{-12}.
\]

Now, vary \( R_s \) until a \( \Delta C_T \) of 40 pF produces a displacement on the CRT of 1 \( \mu s \) when measured at 10 \( \mu s \) (Fig. 5b). This value of \( R_s \), multiplied by \( C_t \), equals \( R_{C_2} \), and \( C_2 = R_s C_m / R \).

Now that you’ve determined the time constant of the oscilloscope, you can calculate the rise time and bandwidth:

\[
\text{Rise time} = k_1 R_C T_2;
\]

\[
\text{Bandwidth} = K_2 / R_C T_2,
\]

where \( k_1 \) depends on the definition of rise time and equals 1 for a \( t_r \), between 0 and the 62% point; \( k_2 = 0.33 \) for circuits with one predominate pole.

Note that the output resistance of the calibrator is part of \( R_s \).
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Of course, you can always monitor an analog signal at the converter input with a precision DVM and compare the input to the converter output. This is simple enough—but impractical, in most cases. For instance, a 10-bit converter requires the plotting of 1024 readings. Sure, you can automate the process. But you'll need sophisticated interface hardware and software routines. And automatic test equipment will run to around $10,000 for hardware and at least that much for software.

How the circuit shapes up

But in the much quicker, much less expensive alternative, a storage scope is the only external piece of equipment. A ramp generator provides a linear-output voltage over the input range of the converter being tested (Fig. 1). The analog-input range of the circuit is 0 to 10.00 V. The ramp functions as a horizontal-amplifier input to the storage scope, as a reference for the difference amplifier and as an analog input to the device under test.

Zero and full-scale adjustments make possible accurate nonlinearity measurement. A d/a converter testing an a/d converter should introduce insignificant errors relative to the device under test. A 12-bit d/a with 0.01% accuracy suffices to test a 10-bit a/d.

Time delays associated with the a/d-converter path (relative to the slew rate of the ramp generator) are not a problem for successive-approximation a/d converters when the ramp generator slews at 2 V/s or less.

The complete test circuit can "ring out" such a/d products as National Semiconductor's 8-bit ADC0800 and the 10-bit ADC1211 (Fig. 2). With a 12-bit a/d rather than a 12-bit d/a (DAC 1200), the circuit can test 8-bit or 10-bit d/a converters. Whatever converter is under test—d/a or a/d—the corresponding reference converter should be more accurate by at least two bits.¹

A buffered reference voltage (generated by the LM199) is provided for both the a/d and d/a converters, but isn't needed for converters with an internal reference. Resistor R₅ sets the reference level of the d/a, and a full-scale pot adjusts that of the a/d converter.

To generate a manual start-conversion pulse, close switch S₃. However, you won't have to do it too often because the end-of-conversion signal ties back to the start-conversion input for each a/d converter. Consequently, the converters continuously convert as long as a signal is present. Trigger switch S₄ simply causes the horizontal-output amplifier to integrate linearly up to the full-scale voltage or to range downward to zero.

Next to the converter, difference-amplifier IC₆ and its associated resistors are most important to the circuit. With 0.01% film resistors, an amplifier gain

¹ The reference voltage level is 5 V for the ADC1211.
2. **Precision amplifiers and adjustments** for zero and full scale contribute to an over-all test-system accuracy of 0.02%. Up to 10-bit units can be tested.

of 100 and a true 12-bit d/a converter, system accuracy is 0.02% or better.

A jack lets you plug in an external clock should the 660-kHz internal one prove unsatisfactory. All interfaces between components are CMOS-compatible.

**What the test results look like**

Fig. 3 shows a typical output characteristic (not to scale) obtained when testing an ADC0800. To set the reference line, switch the vertical-channel (Y-axis amplifier) to dc and trigger the ramp generator. Make the adjustment with the scope’s horizontal position-adjust. The vertical range should be set to 5 V/division to give an effective range of 50 mV/division for the channel.

Once you’ve completed the setup, you should have no problem pinning down converter errors. Zero error is simply a deviation from the reference line to the middle of the quantizing error when the input voltage is zero. All errors can be expressed as percents of full scale or in least significant bits. For a 0 to 10.24-V, analog-input, 8-bit converter,

\[
1 \text{ LSB} = \frac{10.24}{2^8} = 40 \text{ mV} = 0.39\% \text{ fs.}
\]

Scale error is similar to zero error except that it occurs when the analog-input voltage is at full scale. Both zero and scale error can be determined by leaving S₁ and S₂ open.

In most applications, linearity per se isn’t important, but rather the slope—or sensitivity—of the transfer curve. For instance, consider an a/d converter that indicates the gasoline level in a tank and computes the remaining miles that can be traveled at the current rate of usage.

A large nonlinearity slope produces what appears to be good mileage over a certain range and poor mileage over another range. Specifying both the nonlinearity error and differential nonlinearity error provides an error band around which to limit the change in slope or rate of change.

**Nonlinearity and other errors**

Nonlinearity error can be defined two ways. The conventional “best-straight-line” definition (Fig. 4) is
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3. Output characteristic for an 8-bit a/d converter exhibits the most important errors.

used for the ADC0800 because of the inherent unidirectional nature of the error. A more conservative definition, "ideal straight-line linearity," sometimes called "total error," gives a number twice as large as the best-straight-line error.

Total error can be defined as the maximum deviation from a straight line drawn between zero and full scale. The ADC1210 and ADC1211, 10-bit and 12-bit a/d converters, employ this definition of nonlinearity because the deviation can be in either direction. Regardless of the definition, linearity is the most obvious characteristic of the resulting transfer curve.

Differential nonlinearity is most noticeable in successive-approximation converters. It is the change in input voltage required to cause a change in the digital output. It shows up on the scope trace as a change in nonlinearity at one point and offers a check for missing codes. No missing codes means that over the input range, the converter provides 2^n digital-output codes, where n is the resolution of the converter.

Total unadjusted error is the maximum deviation from an ideal a/d-converter transfer function, excluding quantizing error. The nonlinearity error of an unadjusted ADC0800 is in a direction that will decrease the total error. This means that some quantizing error exists, and that output transitions occur to correct for the zero error.

As a result, the unadjusted transfer curve of the device comes closer to the reference line between zero and full scale. In general, therefore, the total unadjusted error for the ADC0800 is either the zero or the scale error, whichever is greater—a characteristic peculiar to series-resistor type, successive-approximation converters.

Quantizing error is inherent in converters. An 8-bit converter can make no more than 256 changes in the output regardless of the input-voltage range. Therefore, any converter has 1 LSB of quantizing error. Ideally, the error appears as ±1/2 LSB around a straight-line approximation of the output characteristic.

References
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Process controls are evolving fast.
In set-point systems, logic often outperforms familiar analog standbys such as comparators and conditioners.

You can choose from a variety of technologies to monitor industrial-process variables. Electromechanical and electronic controls have replaced many earlier hydraulic and pneumatic systems. And, as controls become more complex, the electromechanical approach is yielding its popularity to electronic systems—both analog and digital. But which discipline is best?

Often the system you use will depend on how much alarm capability is required. An alarm can be a simple switch closure or the incredibly complex and exact control of a set of critical process variables.

Position, pressure and temperature are typical variables that require alarms. To sense a position limit, simple set-point controls can be implemented with mechanical contacts, adjusted along the axis of motion. For pressure and temperature, gauges are available with adjustable mechanical contacts that can provide set-point alarms.

In mechanical set-point systems, output functions such as actuator solenoids, motors, clutches and brakes are usually controlled directly via the same contacts that sense the set point. But these contacts of course, have chatter, speed, and life problems—which are often bypassed by substituting solid-state devices, such as triacs.

Electronics is spreading

At the front ends of industrial-control systems, electronic devices are steadily replacing mechanical ones for threshold setting. But these require an electrical-signal input. Transducers, therefore, are an important part of electronic set-point systems.

But most transducers are nonlinear over some part of their usable range. Where linearity is needed, a nonlinear transducer output can be conditioned. Also, signals representing several variables can be combined into a single function.

Sometimes measurement isn’t enough

Another advantage of systems with electrical rather than mechanical outputs is that you can use a greater variety of alarm circuits. Some basic alarm circuits using threshold-sensitive devices are described in Fig. 3. Activated when the output is either above or below a threshold or out of a range, these set-point controls can test for size or position and can even detect defects. Other set-point arrangements can classify parts by properties and select the middle value from among several—an ability useful for monitoring.

Often, units must be sorted—that is, grouped so that a certain characteristic is between predetermined sets of values. In machining, for example, the characteristic might be size; in resistor production, resistance; and in transistor production, current gain. In Fig. 4a, the two-comparator circuit provides one output level when its input voltage is between the two set points, and another level when the input is beyond these limits.

Fig. 5 shows a circuit for classifying materials or parts. Inputs come from transducers that measure the variables in question. The comparators match the transducer signals to a graduated series of reference levels. The resulting comparator outputs are processed with logic gates that develop the required functions. The outputs control sorting machinery via motors, solenoids, clutches or brakes.

Another sorting circuit is shown in Fig. 6. This time the median value is selected from three separate transducer inputs.

Michael F. Hordeski, P.E., President, Siltran Digital, Silverado, CA 92676.
2. **Transducer outputs are linearized** in one of two ways:
A nonlinear function in which \( V_5 \), a scaling input adjusted for proper offset, is applied continuously (a) or a piecewise-linear approximation (b) in which a series of similar summing circuits generates the separate sections of the curve. These are then summed.

The sorting schemes in Figs. 4a and 5 can use analog or digital comparators. Many of the parameters that limit comparator performance are familiar to op-amp users: finite gain, limited bandwidth, input and output voltage-and-current offsets, internal impedance, and drift due to temperature changes and aging. As with op amps, you can reduce these limitations with device selection, with error compensation or with temperature-controlled environments. Of course, these alternatives will add to the cost and complexity of your system.

**Analog ICs can help**

IC analog comparators are often the answer to this cost and complexity problem. These circuits are descendants of the differential or difference amplifier, which is noted for its exceptional de-bias stability.

The basic analog-comparator circuit couples two transistors through their common emitters. The transistor bases provide the inputs.

If the transistors match, the voltage difference between the two inputs causes a current flow in the common emitters. But as this current varies, so do the junction temperatures of the transistors. And, as you know, many of the transistor parameters are affected by junction-temperature variations. Maintaining matched characteristics over a wide temperature range is difficult, so accuracy suffers.

Fortunately, IC technology can reduce many temperature-related drift problems. Because the transistors are near each other, their temperature differences are small. What's more, IC comparators use high-impedance inputs, followed by additional amplification. In this way, the signal current is kept low with respect to the dc operating current. For a moderate cost, these and other IC balancing techniques, produce analog comparators with high stability and fast response.

But whether IC, hybrid or discrete, analog comparators are necessarily high-gain devices. So take care to maintain the isolation between their input and output circuits. Since comparators can easily oscillate, with even just a little positive feedback, make sure that the inputs and outputs are isolated electrically, thermally and physically—especially at the power-input terminals.

Wherever electrical-noise level is high, as in many industrial environments, tap back part of the output to the comparator's inverting input. This negative feedback often prevents yet another potential instability—switching on noise.

**For accuracy, go digital**

But, perhaps the best solution to the accuracy problem, is a digital comparator. Such a device compares the input data to a reference on a bit-by-bit basis. In set-point control systems, digital com-
Comparators can provide better resolution, accuracy and long-term stability than can their analog counterparts.

In a digital comparator, an array of logic gates tests two words, the variable and the reference, against one another. Separate outputs indicate that the input word is less than, equal to, or greater than the reference word (Fig. 3c).

Temperature sensitivity is not a problem for digital comparators because the logic gates compare digital bits. Analog comparators, on the other hand, work with continuous levels. Furthermore, digital-logic levels provide noise immunity; and except in the fastest systems or the most complex installations, oscillation isn't usually a problem.

When a digital comparator operates from one reference, the reference word can be hardwired. When the reference is to be variable, it can be adjusted in a variety of ways. For frequent calculations, the word can be programmed by an on-line computer. For operator control, keyboards, thumbwheels or other coded switch arrays can set the reference.

Digital comparators can, of course, directly drive other digital elements. For example, a driven counter can select every Nth part that meets the criteria monitored by a set of digital comparators.

**Condition with a ROM**

Digital devices can also condition nonlinear input signals. For example, a ROM can store correction terms for the nonlinear output of a thermocouple like the one in Fig. 1. Of course, the thermocouple output must be digitized. Converting from analog to digital produces a word representing a temperature on the response curve. This word addresses a look-up table in the ROM. In this way, each input word is transformed into a corresponding output word that contains the proper correction factor.

When correction isn't needed, the inputs can come directly from a table of data points taken from the response curve. This table can also be stored in a ROM.

Even in systems requiring multipliers and dividers, digital components can replace the familiar analog workhorses—and handily. Digital multipliers and dividers can be built with available ICs. But often the carry operations are complex, which makes implementation with discrete logic both cumbersome and costly. When many systems are to be produced, a custom LSI chip can be practical. But if just a few systems are needed, use a microprocessor that can perform arithmetic operations efficiently.

Cost differences between analog and digital set-point systems are difficult to generalize. Sometimes, the lowest parts count results with an analog system, sometimes with digital. Usually, however, digital components cost less, so in all but the simplest cases, you can do more digitally for less money.

Digital systems are also more adaptable than analog. Take the digital route, and you get programmability and a variety of peripheral options. Be sure to compare the power requirements for both types, primarily:

- The number of voltages required—each voltage means, at least, another regulator.
- The total power required—this determines the supply size.
- The regulation needed.

The analog ICs used in set-point control generally require dual-polarity supplies, whereas logic ICs usually require only one voltage. Current requirements for analog systems are usually lower than those for TTL-logic systems, but higher than for MOS digital circuits. And supplies for digital systems usually need less stringent regulation.

Response times are usually not a critical factor in the analog-vs-digital choose-off. Both analog and digital comparators react in under 100 ns, typically. For very high speeds, however, you may be forced to use an analog comparator because the delays of cascaded stages add up in digital systems. A fast-logic family like ECL may prove too expensive.

**Digital systems pull ahead**

For repeatability, however, digital systems clearly outshine analog. Sensitivity (the response to small inputs) depends on easily controlled word length in digital comparators but on unyielding input parameters in analog comparators. While digital comparators are easily cascaded for increased word lengths (higher sensitivity), the transducers usually limit set-point system accuracy and sensitivity.

Safety and maintenance requirements are usually tied to individual systems. However, digital systems...
5. **Comparators match the transducer signals** to a graduated series of reference voltages. Appropriate logic gates combine the individual comparator outputs to develop the output functions needed for the desired grouping.

6. **This three-comparator scheme selects the middle value** of the three inputs. The median value is significant when transducers monitored this way are strategically located along the route of a production process.

eliminate the costly periodic adjustments common to analog set-point controls.

In set-point systems, reliability usually has but two major components: failure, which is proportional to complexity; and sensitivity to environmental factors, principal of which is temperature. Failure often results in a total loss of control whereas sensitivity to such factors as temperature usually causes drift and degraded control.

Since digital systems usually contain more stages, digital systems are more prone to permanent failure. Generally, however, a digital system failure is less likely than an analog system error. 

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CIRCLE NUMBER 55

ELECTRONIC DESIGN 24, November 22, 1977
**Technology**

**Improve your digital recorder** with a latch circuit that catches all unexpected pulses. The circuit offers a choice of operating accuracies, too.

With a new latch circuit and a “bit” more memory, it’s easy to overcome a serious shortcoming of conventional digital recorders. Many present recorder-latch modes don’t always catch short, unexpected pulses occurring between clock samples, even if the pulse width is much more than, say, 10 ns (but less than the clock cycle time).

In a conventional front-end circuit, sampled data enter the input only during a clock pulse (Fig. 1). In a latch mode, data enter between clocks, as well, through PR and C, of flip-flop FF1 in Fig. 1. The state of FF1 controls the sign of the pulse caught between clocks—negative through C, when Q1 = ONE, positive through PR when Q1 = ZERO.

In four instances, a pulse between clocks will not be caught by conventional latch modes (Fig. 2). After a latch-mode activation, the data in each memory bit indicate the state either at the time of sampling or between samples. The state between samples will indicate a pulse only when the sample states on either side differ from the in-between state.

If the states of the two samples differ, one bit of memory is not enough to distinguish whether the in-between event is a pulse or a legitimate change of state (cases S3, S4 of Fig. 2). The latch circuit itself can’t make this distinction, either—you need more memory and a different latch to solve the problem.

In cases S1 and S2 of Fig. 2, the latch circuit detects only the first of two pulses occurring between samples. In fact, with conventional latches, the detection of the first pulse inhibits the detection of the second.

**More memory is needed**

The new latch circuit uses two memory channels, one for the sample, the other for the latch (Fig. 3). State ONE in the latch memory indicates a pulse, and ZERO no pulse. By comparing the two memory channels, you can tell the pulse polarity.

The clock samples the signal, which is then stored at FF0 until the next clock. The sample state serves as the initial state of FF1, and its complement as the initial state of FF2. Flip-flop FF1 detects the first change between clocks—Q = ONE opens the NAND gate (Fig. 3).

1. **Conventional recorder-latch circuit** captures data during clock transitions (M=ZERO) and unexpected pulses that occur between transitions (M=ONE). But not all unwanted pulses are caught.

2. **Four cases occur** (S1 to S4) in which conventional latches fail to capture transients or other undesirable pulses. In S1 and S2, the latch detects the first pulse, but is inhibited from catching the second. In S3 and S4, more memory is needed to tell between valid (sampled) data and glitches.

Raphael Pesso, Head of Digital Laboratory, Department of Electrical Engineering, Ben-Gurion University of the Negev, Beer-Sheva, Israel.
gate to CL₁, Q = ZERO opens the NAND to PR₁. Flip-flop FF₁ detects the second change—Qi = ONE opens the NAND to CL₁, Qi = ZERO opens the NAND to PR₁. At the next clock pulse, the result of pulse detection is stored at FF₁, with a ONE indicating a pulse.

Pulse-detection decisions are made by the AND/OR logic at the input of FF₁. The logic uses the sample states of both the previous clock (Q) and the present clock (D) and the changes detected between clocks (Qi and Q₁) to detect a pulse (Fig. 4).

Column NOC indicates the number of changes detected between clocks, and X (don't care) indicates that Qi is detected without Q₁—an impossible situation. Previous state Q is needed because the detected changes, Q₁ and Q₂, are with respect to Q.

To understand the role of the present sample state, look at the function of C₁ (Fig. 5). Signal C₁ ends the progress of change in flip-flops 1 and 2 through the preset or clear, depending on the internal delays of the NAND and FF₁. The flip-flops must stabilize before the next sample to ensure that the correct initial states are entered.

Thus, C₁ increases the minimum detectable pulse width, a value greater than the delay in the AND/OR logic (DL₁) plus the delays of the NAND and FF₁. The value can be decreased by DL₁ if the clock to FF₁ is delayed by DL₁.

In the timing diagram of Fig. 5, the pulse between the pair of clocks is wide and the falling edge of the pulse occurs when C₁ is HIGH. So detection of the falling edge is inhibited by C₁. The present sample state (D) in the AND/OR is necessary to distinguish between when one change indicates a pulse (groups 1 and 2 in Fig. 4) and when just one change occurs (groups 3 and 4 in Fig. 4).

As seen in the truth table, the new latch takes into account all possible pulse states between a pair of clock pulses. The second memory in the latch mode ensures that a pulse is detected in all possible states.

**Better recorder flexibility**

Besides detecting unexpected pulses, the latch enables you to choose either of two accuracies. Assume a logic signal with a minimum pulse duration, Wₘᵢₙ (the time between two successive transitions), and a minimum pulse-cycle time, Tₘᵢₙ. The signal is sampled at cycle time T by a logic recorder having 256 memory bits per channel and a maximum frequency of 10 MHz.

You can distinguish two operating possibilities;
1. Wₘᵢₙ > T, that is, wide signal pulses relative to T.
2. Wₘᵢₙ < T < Tₘᵢₙ, that is, short pulses relative

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**3. The redesigned latch captures sampled data** in one memory, pulses in another. The logic at the input of FF₃ “detects” pulses based on previous sample states, present clock conditions and changes occurring between clocks.

**4. This pulse-decision truth table** accounts for all possible pulse states occurring between clocks. Column NOC indicates the number of changes between clocks (X = don't care).
5. In the redesigned latch, signal $C_1$ ends the process of change in flip-flops 1 and 2 to "make way" for the next sample. The detection of the falling pulse edge is inhibited if the edge occurs when $C_1$ is High.

to $T$ and having a low frequency with respect to the operating frequency.

In the first case, normal sampling will record all signal pulses, and the latch will catch unexpected pulses during the sampling interval. Because of the limited memory, the total sampling time is given by $256 \times T$. Decreasing $T$ improves the accuracy, but decreases the total sampling time.

In the second case, normal sampling won't detect all the pulses. Assume a signal in which $W_{\min} = 10$ ns and $T_{\min} = 1$ ms. Only if $T < 10$ ns (or $f > 100$ MHz) will all the pulses be detected. For example, if $T = 5$ ns ($f = 200$ MHz), the accuracy is 5 ns and the total sampling time is 1280 ns ($5 \times 256$).

The required 200-MHz logic recorder will be about 10 times more expensive than a 10-MHz unit. With the latch circuit and a separate memory, in addition to the normal sampling, all expected pulses will be detected at a much lower frequency ($f > 1$ kHz).

Second-case conditions ensure that no more than one pulse will be found between a pair of clock samples and that the latch circuit will detect that pulse. For example, if $T = 0.5$ ms ($f = 2$ kHz), the accuracy is 0.5 ms, and the sampling time is 128 ms ($256 \times 0.5$).

Comparing the two examples of the different $T$s, you can see that when $T = 0.5$ ms, the latch improves the frequency and the sampling time 100,000 times, but decreases accuracy by the same factor. So you have a choice between low accuracy at low frequencies and greater sampling intervals and high accuracy at higher frequencies and shorter sampling intervals.

With low accuracy, the latch detects only expected pulses, but a minor improvement solves the problem. To register the unexpected pulses, the latch of Fig. 3 must have two states: a "one pulse" state and a "two or more pulses" state. The second state, which requires a third memory channel, indicates the unexpected pulse.

To make sure unexpected pulses are detected, add two flip-flops for second-pulse detection—like FF1 and FF2 for the one-pulse—and some logic for the second-state indication—like the AND/OR/FF3 arrangement...
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Instead of complicated formulas for determining coil inductance, most ferrite magnetic-core manufacturers supply core constants and an inductance factor, $A_L$, for particular core types and dimensions (Fig. 1). The inductance of a coil wound on a core can be figured to a respectable degree of accuracy with

$$L = A_L N^2 \text{ (nanohenries)}.$$  

(1)

However, the given $A_L$ values are accurate only for the specific applications and flux densities that the core is tested and rated for—filters, pulse-transformers, power-inverters, etc.¹

So manufacturers also make it easy to calculate the operating, or effective flux density, $B$, by supplying a core’s effective area, $A_e$, as well as effective volume, $V_e$. You simply use the following equation:

$$B = E (10^6)/4.44 f N A_e \text{ (gauss)},$$  

(2)

where

- $E = \text{rms volts}$,
- $f = \text{frequency in Hz}$,
- $N = \text{number of turns}$,
- $A_e = \text{effective core area in cm}^2$.

To get the effective field strength, $H_e$, in the core or its air gap, if any, you need to know the effective length of the magnetic path, $d_e$, in cm. Use the following equation:

$$H_e = 4\pi NI/10d_e \text{ (oersteds)},$$

where $I$ is the current in amperes through the coil. Again, manufacturers make the calculation easy by supplying values of $d_e$ for their various core designs.

**Cores don’t always fit your needs**

But what if listed core dimensions don’t quite fit your needs? How can you adjust their dimensional constants to get the performance you want?

The equation for inductance also can be expressed with

$$L = 4\pi N^2 \mu_e (10^9)/C_1,$$  

(3)

where

- $\mu_e = \text{effective permeability}$,
- $C_1 = \text{a dimensional core constant}$.

Change the constant $C_1$, and you can change the inductance for a given core-material permeability. Clearly, from Eqs. 1 and 3,

$$A_L = 4\pi \mu_e (10^9)/C_1.$$

The core constant $C_1$, supplied by manufacturers for specific core sizes, can be calculated² from the summation,

$$C_1 = \sum_{i=1}^{n} d_i/A_i.$$

For a uniform toroid (Fig. 2a), then,

$$C_1 = \int_{r_1}^{r_2} 2\pi r/(h\cdot dr) = 2\pi/h\cdot \log_e(r_2/r_1).$$  

(4)

For a more complex core, say, with four identifiable sections as in Fig. 2b, you must sum the separate sections. Therefore,

$$C_1 = \sum_{i=1}^{4} \frac{d_i}{A_i} = \frac{d_1}{A_1} + \frac{d_2}{A_2} + 2 \frac{d_3}{A_3}.$$

Note that sections 3 and 4 are identical and combined in the last term.

In section 1, using the methods of Eq. 4, since

$$\frac{d_1}{A_1} = \pi/h\cdot \log_e(r_3/r_1).$$

In section 2, since $d_2 = (\pi - 2\phi) r_b$, then

$$\frac{d_2}{A_2} = (\pi - 2\phi)/h\cdot \log_e(r_2/r_1).$$

And in sections 3 and 4, to simplify calculations, since $\phi$ is relatively small, $r_2$ and $r_3$ can be averaged (Fig. 2c) and the approximate answer you obtain will cause little error. Then,

$$2 \frac{d_3}{A_3} = 20/[h\cdot \log_e(r_2 + r_3)/2r_1].$$

Changes in the core dimensions—radii $r_1$, $r_2$, $r_3$ and

---

1. **Ferrite coil and transformer cores** are usually specified in manufacturers’ catalogs with effective values for both their magnetic and dimensional constants. Effective values enable you to quickly design practical components.

2. **A simple toroid core** (a) is easily evaluated to determine its important dimensional core constants, $C$, $d$, and $A$. But more complex shapes (b) require that you sum the various sections and make approximations (c) for some of the irregularly shaped parts. Core-constant equations allow you to adjust the dimensions as needed.

---

**Core Constants**

**U Core**

<table>
<thead>
<tr>
<th>Core Constants</th>
<th>$C$</th>
<th>$d_e$</th>
<th>$A_e$</th>
<th>$V_e$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>3.55 cm$^2$</td>
<td>22.91 cm</td>
<td>6.45 cm$^2$</td>
<td>147.77 cm$^3$</td>
</tr>
<tr>
<td>$A_L$</td>
<td>13,300 (1.8 kG)</td>
<td>7970 (2.8 kG)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**E Core**

<table>
<thead>
<tr>
<th>Core Constants</th>
<th>$C$</th>
<th>$d_e$</th>
<th>$A_e$</th>
<th>$V_e$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>4.63 cm$^2$</td>
<td>15.19 cm</td>
<td>3.28 cm$^2$</td>
<td>49.82 cm$^3$</td>
</tr>
<tr>
<td>$A_L$</td>
<td>9415 (1.8 kG)</td>
<td>5860 (2.8 kG)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**POT Core**

<table>
<thead>
<tr>
<th>Core Constants</th>
<th>$C$</th>
<th>$d_e$</th>
<th>$A_e$</th>
<th>$V_e$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>5.16 cm$^2$</td>
<td>3.20 cm</td>
<td>0.819 cm$^2$</td>
<td>1.98 cm$^3$</td>
</tr>
<tr>
<td>$A_L$</td>
<td>250 ± 3%</td>
<td>103</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

---

**Electronic Design** 24, November 22, 1977
In evaluating the core constants for an E core (a), you can take advantage of its symmetry (b) and approximate the effective dimensions of the corner sections (c) to simplify the calculations.

Solving the constant for E cores

A similar procedure for E cores provides the relationship between \( C_1 \) and the core's physical dimensions. For a pair of E cores with a rectangular cross section, you need consider only five sections, since the two Es are identical. And because each E is symmetrical, the area of the magnetic path in each half-E is in parallel with the other half, but in series with its counterpart in the other section of the pair; thus,

\[
C_1 = \sum_{i=1}^{5} \frac{d_i}{A_i}
\]

In Fig. 3b, the dimensions of \( d_1, d_2 \) and \( d_3 \) are obviously the lengths as shown. However, \( d_4 \) and \( d_5 \) need some special treatment.

A good approximation for \( d_4 \) is to use one-quarter the circumference of the mean circle whose radius, \( r_a \), is the average of \( b/2 \) and \( d/2 \) (Fig. 3c); consequently,

\[
d_4 = \frac{1}{4} (2\pi) r_a = \frac{1}{4} (2\pi) \left( \frac{b/2 + d/2}{2} \right) = \frac{\pi}{8} (b + d)
\]

Similarly,

\[
d_5 = \frac{\pi}{8} (c + d)
\]

The areas, \( A_i \), associated with sections 1, 2 and 3 are clearly,

\[
A_1 = ab, \quad A_2 = ad, \quad A_3 = ac.
\]

But for sections 4 and 5, you must make another approximation: Use the average of the sections' terminating cross-section areas, so that

\[
A_4 = \frac{1}{2} (ab + ad), \quad A_5 = \frac{1}{2} (ac + ad).
\]

Now, the complete expression for \( C_1 \) can be written as

\[
C_1 = \frac{d_1}{ab} + \frac{d_2}{ad} + \frac{d_3}{ac} + \frac{\pi}{4} \left( \frac{b + d}{ab + ad} \right) + \frac{\pi}{4} \left( \frac{c + d}{ac + ad} \right)
\]

With these examples of how \( C_1 \) is related to core dimensions and geometry, you should now be able to derive your own relationships for other core shapes. Once you have determined the equation—even an approximate one—you can then decide how to adjust the dimensions to your needs, and tell a manufacturer exactly what you want.

References

You're looking at one of many different Sprague dual and quad power drivers. Each leads its category in many ways.

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SERIES UDN-3600M Dual 2-Input Power Drivers: These dual drivers complement the UDN-5700 Series and are compatible with MOS logic. They are pin-for-pin replacements for Series LM3600N. Sprague types offer reduced Icc (on) currents for lower power, reduced noise problems, lower junction temperature, and higher package dissipation capability, plus 80 V breakdown.

UDN-5790/5791 Quad Drivers for PIN Diodes: These new devices have a 120 V maximum output voltage! Each output is capable of switching 300 mA. These units are available in both plastic and ceramic DIP packages. They permit users of discrete or hybrid PIN interface drivers to replace present components with a reliable monolithic design. Both inverting (5790) and non-inverting (5791) types are available.

For application engineering assistance, write or call George Tully or Paul Emerald, Semiconductor Division, Sprague Electric Company, 115 Northeast Cutoff, Worcester, Mass. 01606. Tel: 617/853-5000.

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CIRCLE NUMBER 62
Ideas for design

Precision peak-to-peak ac-dc converter built with single-supply op-amp circuit

Overcome the forward voltage drops of the diodes in a conventional voltage-doubler circuit with two precision diodes, and the result is a fast, peak-to-peak ac-to-dc converter with wide dynamic range and bandwidth (see figure).

The peak-to-peak converter's input RC network should be chosen with a high-pass corner frequency adequate for the input frequency. And, the holding, or decay, time of the circuit is adjusted with the RC network at the output. For fast response, both input and output capacitors should be limited to about 0.02 µF maximum, and the source impedance of the input signal must be kept low—less than 1 kΩ.

Because the CA3140 has an input-voltage range 300 mV below its negative-supply rail, the circuit can operate from a single positive supply. A single supply not only reduces cost, but also speeds the response of the precision diodes, D1 and D2, as the op-amp outputs switch from saturated "negative" states to forward bias the diodes.

Note, that with the specified +15-V-dc power supply, the input voltage should be less than 11 V peak-to-peak.

Dan L. Vogler, President, Lintech Electronics, P.O. Box 25124, Albuquerque, NM 87125.CIRCLE NO. 311

Square-to-triangle-wave converter provides constant amplitude, rapid response

Convert square waves into triangle waves over a wide frequency range for many applications, such as frequency synthesis and function generation. Triangle waves can be converted directly to other desired waveforms—square waves cannot.1,2,3

Unlike most other converter approaches, the circuit in the figure
• Provides a constant output amplitude as the frequency is varied.
• Preserves a constant phase shift from input to output.

• Responds rapidly to abrupt frequency changes, with the output able to stabilize within one cycle. Furthermore, the input is TTL-compatible.

The circuit has three distinct sections: a period-to-voltage converter, an analog reciprocal generator and a ramp generator. In the period-to-voltage converter, three sections of a quad op amp, IC1, and a quad CMOS switch, IC2, generate a voltage, Vp, that is proportional to the period of the input square wave. Voltage Vp is updated every cycle. An accurate temperature-(continued on page 162)
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stable reciprocal generator formed from IC10 and transistors Q, Q1, and Q4 provides an output:

\[ I_1 = \frac{(I_{REF})^2 R_i}{V_p} \left( \frac{I_{2A} \cdot I_{3A}}{I_{2B} \cdot I_{3B}} \right) \]

The currents \( I_{2A} \) through \( I_{3B} \) are emitter-saturation currents of the corresponding transistors. Variable resistor \( R_i \) controls \( I_{REF} \), which becomes part of the constant of proportionality in the equation. The reciprocal relationship between \( I_1 \) and \( V_p \) produces proportionately slower-rising triangle ramps for longer input periods. The reciprocal function is necessary, because \( V_p \) is directly proportional to input period.

Finally, a transconductance op amp, IC6, operates as a bipolar current switch. With \( C_1 \), it forms a ramp generator whose slew rate is determined by \( I_1 \). The result is a triangle wave whose corners are synchronous with the edges of the input square wave, and whose amplitude is very nearly independent of frequency.

The output amplitude should be set to about 5 V peak-to-peak with \( R_i \). And variable resistor \( R_i \) should be adjusted for zero dc shift in the output waveform as the input frequency is varied.

With the component values shown, the circuit's frequency range starts at 100 Hz. The output amplitude holds within 2% from 100 to 1000 Hz and within 10% over from 100 to 4000 Hz. Note that the analog reciprocal generator used in the circuit can be applied to many other applications.

References

Max W. Hauser, Plasma Research Lab, Cory Hall, University of California, Berkeley, CA 94720.

CIRCLE No. 312
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The circuit is initialized by a Clear signal to the State-address register, IC5 (Fig. 2). The output of the State-address register controls the six most-significant address bits of all the PROMs, IC5, IC6, IC7, and IC8, not including address bit A7. These six state-address-register bits determine which of the 16 inputs are addressed.

Since all inputs must synchronize with the clock, flip-flops IC1 and IC2 synchronize any asynchronous inputs. The input selected appears at the W output of the multiplexers, IC3 and IC4, and becomes the least-

(continued on page 166)
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Ideas for design

2. A Clear signal starts the circuit on the next clock pulse. Thereafter, each successive clock pulse initiates another system state.

significant address bit of the state and output PROMs.
Before the falling edge of the clock pulse occurs, the addresses to decoder IC11 and flip-flops IC10 stabilize. The output selected at decoder IC12 is clocked in on the negative edge of the clock and held until the next negative edge. At the next rising clock edge, the outputs of the State PROM, IC9, are loaded into the State-address register, IC8, which initiates the next cycle.

A typical flow chart shown in Fig. 3 will help you develop the coding needed to program the controller. Note: Only half the states and addresses of the PROM memories are used. The unused address lines of each PROM, A7, can double the states from 64 to 128, but the state register must then be changed to handle seven bits.

Another potential use for the A7 address lines enables you to monitor an additional set of inputs. Merely duplicate the input section, address it with the same state bits and feed the new W output into the A7 address lines of the state and output PROMs. In this way, you can look at two inputs simultaneously and allow up to four different responses to occur.

Harold J. Alber and Nancy L. Esken, Electronic Engineers, ASD/ENA, Wright-Paterson AFB, OH 45433.
CIRCLE No. 313

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CIRCLE NUMBER 70
Modulating SAW devices is made simpler

FM-modulating surface-acoustic wave oscillators with conventional phase-shifting techniques can be complex and difficult. A simpler way is to make use of the magnetoelastic effect in a thin garnet film on which the SAW delay line is deposited. Central Research Laboratories of Thomson-CSF in Orsay, France has grown an yttrium-iron-garnet (YIG) film on a gallium-gadolinium-garnet film by means of liquid-phase epitaxy.

Gallium and gadolinium are exchanged within the YIG film to produce a Gd-Ga-YIG film 9 \( \mu \text{m} \) thick. A useful property of this film is that it can be easily saturated in the flat plane.

Next, a 1-\( \mu \text{m} \) zinc-oxide piezoelectric film is sputtered onto the magnetic film to form the SAW structure. Interdigital transducer electrodes formed on the oxide layer complete the device (Fig. 2).

When a magnetic field is applied to the delay line, the relative phase-velocity shifts, to give a modulation ratio, \( \Delta f/f \), of about \( 2.2 \times 10^{-3} \) (Fig. 1).

Acoustic attenuation is also affected. With the present garnet material a 600-kHz frequency shift from an initial value of 340 MHz has been measured for a magnetic-field variation from 3820 to 10 5 \( \text{Alm} \).

Rms voltage measured quickly and accurately

A new approach to measuring true rms voltage is said to be more accurate than the two currently used methods.

In one of the current techniques, a thermocouple is employed to measure heat generated when the measured voltage is applied to a resistive heating element. However, this method is slow, and its small output voltage requires error-free amplification.

In the second method, circuitry is used to square the input voltage, integrate the squared value and produce the square root of the integral, which is the rms value. But this method is prone to errors, and its bandwidth is limited by the performance of the analog multipliers used to form the squares and square roots.

The new rms-measuring system developed by Philips of Eindhoven contains two identical integrated circuits each containing a resistor and a heat-sensing transistor. The ICs are mounted on a small glass plate, which provides thermal insulation. The assembly is encapsulated.

With pairs of ICs from the same die, the transistors and resistors are closely matched and can be connected in a heat-balancing configuration as shown in the figure.

The voltage being measured, \( V_{\text{rms}} \), heats resistor \( R_1 \), and increases the \( T_{S1} \) collector current. At the noninverting input of the op amp, the voltage decreases, which raises output \( V_o \). This output, in turn, heats up \( R_2 \), which increases the collector current of \( T_{S2} \)—which tends to reduce \( V_o \). When \( V_o \) equals the rms value of \( V_{\text{rms}} \), a balance is reached.

The Philips circuit has 0.05\% accuracy and the bandwidth is limited only by that of the op amp, so 100 kHz can be easily achieved. The response time is typically 100 ms to 90\% of full scale deflection.

Radar calibration comes back to earth

A ground-based way to calibrate a radar in terms of a target's echo area rejects the effects of ground clutter just as effectively as suspending a sphere from a balloon—the usual calibration method.

In the new system, developed by England's Royal Radar Establishment, a pair of triangular trihedral corner reflectors rotate in a horizontal plane at about 200 rpm. The reflectors are attached to a vertical shaft with their open ends facing in opposite directions so that only the reflector turning away is seen by the radar. Towards the radar, a reflector produces a negligible signal.

When the reflector system is placed in the far field of the radar, near enough to ensure a high signal/noise ratio, audio-frequency doppler signals from in-phase and quadrature radar outputs can be derived by standard methods and recorded. These signals can subsequently be digitized and analyzed by a minicomputer to produce curves of power-spectral density against doppler frequency. The technique is particularly suitable for calibrating equipment used to track moving targets.
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THICK FILM CIRCUITS • TRIMMER RESISTORS

CIRCLE NUMBER 72
The many advantages and unique capabilities of Arrow-M's R Relays are far too extensive to be covered here. Therefore, we'd like to whet your creative appetite with a few outstanding facts:

1. Arrow-M R Relays are available in 1 Form C contacts which can carry a high current capacity of 1 Ampere 20 watts, and are capable of resisting welding at higher inrush currents. The dry circuit type which can switch current as low-level as 100uA is available in addition to the power type.

2. **High Speed**: Arrow-M R Relays can be operated at 500 cycles/sec.

3. Greater reliability and lower cost, due to simultaneous automatic fabrication of coil bobbin, contact and terminal.

4. In addition to the standard there are 1 coil and 2 coil latching types, which are useful for logic circuit design as a memory component.

5. Not only can they be automatically wave soldered on PC boards with a high density of electronic parts, but they are simple to clean with most degreasers and detergents without affecting maximum contact reliability.

6. **High Sensitivity**: Minimum operating power:
   - Single Side Stable 80 mw/Bistable 40 mw

7. **Longer Life**: Mechanical: More than $10^8$ operations.
   - Electrical: More than $10^4$ operations.
   - (1A 20vdc, 0.3A 110vac)

Hungry for more information? For exact specifications on all of our relays, write or call your nearest Arrow-M office.

**Arrow-M Corporation**
250 Sheffield Street
Mountainside, NJ 07092
(201) 232-4260

**Mid-Western Office**: 600 E. Higgins Rd.
Elk Grove Village, Ill. 60007
(312) 593-6535

**Western Office**: 22010 So. Wilmington Ave.
Suites 300 & 301
Carson, Calif. 90745
(213) 775-3512

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**Relays for Advanced Technology**

Member of Matsushita Group

The Digilin Series 7000, from Dynamic Sciences, looks much like other digital panel meters. But this DPM, called a "digital process monitor," uses a programmable read-only memory to "shape" the magnitude of nonlinear analog input signals directly into the desired engineering units.

Operating rather like indirect addressing in a computer, the PROM "buffers" the display from the analog input, and is programmed according to the nonlinearity of the function being monitored.

For example, the volume of liquid in a tank won't be directly proportional to the output from a pressure transducer mounted near the bottom of the tank. The nonlinear relationship will depend on many parameters: the size, shape and attitude of the vessel, the sensitivity and location of the transducer, the specific gravity of the liquid, and other factors. Dynamic Sciences will program the internal PROM of a Series 7000 meter to meet the specific requirements of a customer's application.

Inside the 7000, an input value is digitized to select a PROM address that holds the correct display value for that particular value. Two trip points also burned into the PROM serve as limit switches and are available on two discrete output lines.

The 7000 has three input current ranges (0 to 1, 4 to 20, and 10 to 50 mA) and three voltage ranges (0 to 1, 1 to 5, and 0 to 10 V). Its over-all accuracy is spec'd at ±0.1% ±1 bit. The 7000 provides 500-V-dc input-to-line isolation, and can be either triggered or set to sample asynchronously.

One 7000 costs $568, and delivery takes 30 days. Two options are available—a TTL-compatible, BCD representation of the displayed value for $50, and a high-intensity LED readout for $15.

By early next year, the firm expects to offer a field-programmable option so that the PROM may be burned on-site.

CIRCLE NO. 301

PORTABLE LOGIC ANALYZER IS PRIMARY/BACK-UP UNIT

Biomation, 10411 Bubb Rd., Cupertino, CA 95014. Ed Jacklitch (408) 255-9500. $1295; 6 wk.

A 9-channel logic analyzer (920 D) can be used as a medium-performance primary instrument or as an economical back-up unit. Its size is 6 × 10.5 × 17.25 in., and it weighs 9.5 lb. It has connections for plugging into any oscilloscope or CRT. Built-in are a versatile auxiliary channel, clock or event-trigger delay, a 20-MHz record rate, combinational triggering and a 10-ns glitch-detection feature. The unit has a 9-bit × 256-word memory capacity using a static RAM.

CIRCLE NO. 302

DUAL-TRACE SCOPE CHECKS LOGIC CIRCUITS

Tektronix, P.O. Box 500, Beaverton, OR 97077. Maury Floate (503) 644-0161. $1225.

Model-442 dual-trace oscilloscope provides the bandwidth (dc to 35 MHz) needed to troubleshoot most logic circuits. Its 2-mV/div sensitivity allows the user to display and measure low-level signals typical of those from magnetic storage or modems. Full X-Y capability plots Channel-1 vertically against Channel-2 horizontally. Calibrated sweep-speed range is from 10 ns/div to 0.5 s/div. The 150-mV external trigger sensitivity permits the user to trigger on TTL levels when a 10X probe is required to minimize capacitive coupling. The display measures 8 × 10 cm.

CIRCLE NO. 303
Giga-Trim® (gigahertz-trimmers) are tiny variable capacitors which provide a beautifully straightforward technique to fine tune RF hybrid circuits and MIC’s into proper behavior. They replace time consuming cut-and-try adjustment techniques and trimming by interchange of fixed capacitors.

Applications include impedance matching of GHz transistor circuits, series or shunt “gap-trimming” of microstrips, external tweaking of cavities, and fine tuning of crystal oscillators.

Weinschel Eng., Gaithersburg, MD 20870. Don Krivos (301) 948-8403. $2795; stock to 8 wks.

The range of swept and fixed frequency measurement systems, having a 1-kHz, 100% square-wave modulated source, can be extended with a precision rf attenuation controller, Model 1811. The extended range is accurate to 0.02 dB per 10 dB. The device varies the power level at the insertion point in accurate steps of 10, 20, and 30 dB. An added feature is signal-source leveling, typically 0.0005 dB/DB (steady state).

Display torque, force, power in metric/English


Digital speed/load processor, Model MP-7301, is an instrument that displays torque, force or power in metric, English or SI (Systems International d’Unites) units plus rpm. It gives a switch-selectable choice of reading torque, force or power. A simple jumper change quickly selects unit value, while rpm is displayed continuously. Interface circuitry for printers, chart recorders or other peripherals is optional.

Leader Instruments, 151 Dupont St., Plainview, NY 11803. Patrick Redko (516) 822-9300. $200.

One-button, semi-automatic range switching which facilitates fast and accurate measurements and eliminates time-consuming “knob-twisting” is among the features of the LDM-851. It is a battery operated 3-1/2 digit LED-display multimeter with crystal-controlled signal generator. Range coverage is from 1 mV to 1000 V in 16 ranges, ac/dc volts, dc current, plus fully automatic 20-MΩ resistance range.
Don't ask. This man isn't going to compromise. He knows that the pushbutton speed, high accuracy (0.1%), compact size and versatility (0.1 pf to 0.2 farads) make him faster on the draw than any reactionary still shaping up circuits by measuring resistors.

With the C-Meter®, you'll measure capacitors as standard operating procedure. You'll waste no time twiddling and nulling, and you'll cut the need for costly tight-tolerance capacitors or tweak pots. You'll be as speedy as Gonzales... and popular too. People just can't keep their hands off the C-Meter. You owe it to yourself to try one. Our reps are friendly and stock them at $289.

Capacitors supplied by Apollo Electronics, Inc.

ECD CORP.
196 Broadway, Cambridge
Mass. 02139 (617) 661-4400

CIRCLE NUMBER 75

SALES OFFICES: AL, Huntsville (205) 533-5896; AZ, Scottsdale (602) 947-7841; CA, Costa Mesa (714) 540-7160, CA, Sunnyvale (408) 733-8690; CO, Denver (303) 759-1222; FL, Winter Haven (813) 294-5815; GA, Chamblee (404) 457-7117; IL, Elk Grove Vill (312) 593-0282; IN, Indianapolis (317) 293-9827; MD, Silver Spring (301) 622-4200; MA, Wakefield (617) 245-5940; MN, Minneapolis (612) 781-1611; MO, Kansas City (816) 358-7272; NJ, Philadelphia (215) 674-9600; NM, Albuquerque (505) 299-7658; NY, Great Neck (516) 482-3500, (516) 895-7177, Syracuse (315) 446-0220; NC, Raleigh (919) 787-5618; OH, Centerville (513) 433-8171; TX, Houston (713) 688-9971; TX, Richardson (214) 231-2573.
INSTRUMENTATION

Current gun-probe tests without contact

(614) 888-7501. $165.

A noncontact “current-gun” probe permits current measurements, from dc to 1 kHz, of zero to 200 A with any voltmeter, multimeter or scope. The probe has three controls: a range selector (to set the instrument for 1 V per 10 A or 1 V per 100 A); a zero adjustment (with or without a current being measured); and a push-to-read or lock-on switch. Self-contained batteries power the unit which has an accuracy of 2.5%.

F.W. Bell, 4942 Freeway Drive East, Columbus, OH 43229. Chet Mitchell

CIRCLE NO. 308

If you have trouble isolating your inputs from your outputs read this book.

This FREE book shows you how to stay out of trouble with low cost Analog Devices isolation amplifiers. Including our latest version, the 286J which offers improved performance for applications in instrumentation, industrial and bio-medical applications. This new design features multi-channel capability for applications in multi-channel data acquisition systems ranging from 2 to over 1000 isolated data points. ($37 in 100’s)

Please send me your FREE “Isolation and Instrumentation Amplifiers Designers Guide” and 286J data sheet.

Name ___________________________ Title ___________________________ Telephone ___________________________

Company ___________________________ Address ___________________________

City ___________________________ State ___________________________ Zip ___________________________

ED1122

CIRCLE NUMBER 76

Electronic Design 24, November 22, 1977
From a single CPU board

to a half million word super computer

That's the selection you get from ROLM's AN/UYK-19 family. It's the most complete line of Mil-Spec computers in the industry. And every piece is backed by extensive, updated, upward compatible software.

Delivery? 30 days or less because they're all standard products in continuous production. Plus they follow a modular concept for interchangeability, compatibility and upgrading.

Rolm completes the package with full nomenclature and an integrated line of both military and commercial peripherals.

In just seven years we've been able to put together a family plan that lowers your programming costs, reduces hardware costs, cuts out your risk and gives you quicker reaction time.

That's Why We're #1 in Mil-Spec Computer Systems

ROLM MIL-SPEC Computers

4900 Old Ironsides Drive, Santa Clara, CA 95050. (408) 988-2900. TWX 910-338-7350.

In Europe: 645 Hanau, Muehlstrasse 19, Germany, 06181 15011, TWX 418-4170.

CIRCLE NUMBER 77
Digital multimeter reads ac and ac ratios

Dana Laboratories, 2401 Campus Dr., Irvine, CA 92715. N. Laengrich (714) 833-1224; 83105; 12 wk.
The Model 5940, 5½-digit ratiometer, features four ranges of ac reference and four ranges of ac signal input (1, 10, 100, 1000 V). The instrument also features switchable front and rear input and switchable ac or dc coupling on the ac converters. Both the input and coupling configurations are front-panel switchable and/or remotely programmable. In addition to the ac/ac ratio capability, it has five de ranges with accuracies of ±0.001% of full scale (10 ppm), eight ranges of resistance, and 4-wire/4-quadrant dc ratio.

CIRCLE NO. 314

Testing low ESR Capacitors at 10 kHz/20 kHz

assures low “switching” power.

Due to its remarkable versatility, ESI’s Model 296 Automatic LRC Meter now measures capacitors at 10 kHz or 20 kHz. You can quickly and accurately verify ESR to assure low power switching regulator power supplies. (As a dual frequency instrument the Model 296 is available with either of those higher frequencies, plus 1 kHz or 120 Hz as the second frequency.) ESI’s premier LRC tester gives you everything you could want—for now or the forseeable future: Wide ranges, choice of any loss parameters—R, G, D or Q—with either L or C, direct reading or deviation display and field installable options. Options include dc resistance measurements and interfaces for GPIB, 11-bit serial bus, card readers and automatic handlers. Basic price (in the U.S.A. only) is $5700.

LRC, G + D/Q.
% and units deviation.
multiple limits.
2 farad range.
dual frequencies.
dual displays.
dual voltages.
active guard.
6 terminal connections.
high accuracy.
high speed measurement.
programmable settling time.
digital averaging.
interface options.

CIRCLE NUMBER 78

Compact color generator subs for TV tuner

Science Workshop, P.O. Box 393, Bethpage, NY 11714. Murray Barlowe (516) 731-7628. $89.95.
A two-in-one instrument, with a size of 2 × 2-3/4 × 6-3/4 in., acts as a TV tuner and 16-pattern color-dot/bar generator. The tuner-subber provides continuous electrical channel tuning. The color generator uses a MOS-LSI chip to provide 16 stable patterns—including rainbow, color bars, noise-free raster (for purity and gray scale), plus dots, lines and crosshatches. Composite video output is 1.5 V pk-pk and rf output is adjustable from channels 2 to 4. The unit has crystal-controlled master and color oscillators.

CIRCLE NO. 317
Berg Tri-Socket™ takes leads of all sizes in Modcomp Minicomputer Family

Berg Electronics' Tri-Socket is a .025" square wire-wrapping or solder-tab design which accommodates a variety of lead sizes. Its tri-cornered fins retract upon staking, providing gentle entry into the board. A solder rivet (precisely positioned above the fins) is ready for reflow.

Modular Computer Systems appreciates the reliability of the one-piece, Tri-Socket design and uses this socket in virtually all of its minicomputer models. Modcomp has found it can rely on Berg Electronics... to supply the terminals and the application machines that precisely meet its interconnection needs.

Berg is experienced. We read interconnection needs like Modcomp reads compatibility requirements. We have the products, the background and the back-up to do the job. Your job. Let's work on it together. Berg Electronics Division, E. I. du Pont de Nemours and Company, New Cumberland, PA 17070 Phone 717-938-6711.

We serve special interests—yours!
Now... the next generation of bench DMMs!

Two New Keithley Models offer uncompromising performance and outstanding value.

- Accuracy 3½'s can't match: 0.04% + 1 digit on dc volts and ohms.
- Large, bright, 20,000-count LED display that's quick and easy to read.
- Convenient bench size that won't get "lost" yet doesn't crowd.
- Exceptional reliability.

Model 178 offers functions and ranges for most measurements: 100µV to 1200V dc, 100µV to 1000V ac, 0.1Ω to 20MΩ. At $199* it is a remarkable value!

Model 179 is a full-function, multi-feature model offering the same.

Both models feature designed-in reliability.

Rugged circuits use a minimum of parts - high quality, off-the-shelf parts - carefully assembled and tested by Keithley (we've been making sensitive laboratory instrumentation for more than 30 years.)

Outstanding overload protection and rugged mechanical design keep both units going even after severe abuse. One-year accuracy specifications minimize recalibration costs. Local assistance keeps downtime to a minimum should service ever be needed.

A battery option, user installable, gets you off "line" for critical measurements or for field use. Nine other accessories add versatility.

Keithley's 178 and 179 are designed, built and supported to provide continuous usability at the lowest total cost of ownership.

Need autoranging, more accuracy or sensitivity? See Keithley's complete line of DMMs.

For complete specifications and immediate delivery on the 178 and 179, call your local Keithley representative (see adjoining list). Or, call or write: Keithley Instruments, Inc., 28775 Aurora Road, Cleveland, Ohio 44139. (216) 248-0400. In Europe: D-800 München 70, Heiglofstrasse 5, West Germany. (089) 7144065.

*U.S. domestic price only.
# MICRO/MINI COMPUTING

## Static memory has wide range of capacity

Intel Memory Systems, 1302 N. Mathilda Ave., Sunnyvale, CA 94086. Connie Magne (408) 743-7120. See text; 12-24 tek.

The in-7000 static semiconductor-memory system has a range of memory capacity of 16 to 256 kwords and 6 to 96 bits word size. The basic in-7000 card is available in four 16-k configurations: 16 k × 12, 20 or 24 bits. In each case, the user may change the card to the corresponding 32 k × 6, 8, 10 or 12 bits configuration by operating the byte-control input line. Read and write cycle times are 250 ns (7000 version), 350 ns (7001) and 500 ns (7002). Card is 8.175 in. and can be mounted on 1/4-in. centers. Cards of 16 k × 24 bits are priced from 0.28¢/bit. Complete systems cost less than 0.5¢/bit.

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### Digital output boards are for Motorola µCs

Burr-Brown, P.O. Box 11400, Tucson, AZ 85734, C.R. Teepel (602) 294-1143. $295 to $475; stock.

Users of Motorola Micromodule and EXOCRISR µC systems can obtain a plug-compatible 16 or 32-channel isolated digital-output system that is memory mapped. The MP701 (16-channel) and MP702 (32-channel) systems provide all necessary control and timing circuitry and include contact-closure outputs rated at 28 V and 0.5 A. They are treated as memory by the CPU, for ease of programming. Eight output channels occupy one memory location.

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## To order your Keithley DMM:

**ALABAMA**: Huntsville, (205) 863-0660

**ARIZONA**: Phoenix, (602) 944-9185

**ARKANSAS**: (214) 231-9489 (Dallas, TX)

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**COLORADO**: Denver, (303) 789-0055

**CONNECTICUT**: (800) 272-5300 (Philadelphia, PA)

**DISTRICT OF COLUMBIA**: (703) 573-8787 (Arlington, VA)

**FLORIDA**: Ft. Lauderdale, (305) 776-4800

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**MARYLAND**: Baltimore, (301) 321-1411

**MASSACHUSETTS**: Boston, (617) 944-6660

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**NEW JERSEY**: South, (201) 368-0123

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**PENNSYLVANIA**: Pittsburgh, (412) 729-2222 (Cleveland, OH)

**RHODE ISLAND**: Providence, (401) 234-8993

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**SOUTH CAROLINA**: North, (803) 796-3297

**SOUTH CAROLINA**: South, (803) 796-3297

**TENNESSEE**: Memphis, (901) 520-0099

**TEXAS**: Austin, (512) 451-7463

**TEXAS**: Dallas, (214) 231-9489

**UTAH**: Salt Lake City, (801) 263-0099

**VERMONT**: Burlington, (802) 234-8993

**VIRGINIA**: Arlington, (703) 573-8787

**WASHINGTON**: Bellevue, (206) 454-3400

**WISCONSIN**: Milwaukee, (414) 464-5454

**WISCONSIN**: Madison, (608) 262-0099

**WOODS HOLE**: (508) 799-0250 (Cleveland, OH)

**CANADA**

**BRITISH COLUMBIA**: Vancouver, (604) 734-7317

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**FRANCE**: Paris, (01) 302-00-48

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**WEST GERMANY**: Munich, (089) 7144065

Or call Keithley’s Toll Free DMM Hot Line (800) 321-0560

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**KEITHLEY**

The measurement engineers.
Floppy disc reduces µP assembly time

Formulator FD is a floppy-disc operating system for the F8 and F8870 µP design aids. It reduces the time required to write, edit, assemble, execute and debug the µP programs. The system has features such as batch or interactive operation, relocating assembler, linking loader, virtual I/O, string editing, and real-time symbolic debugging. When fully configured, the system consists of a Formulator, one or two dual-drive floppy-disc cabinets with intelligent controllers and a CRT or printing terminal.

Is there a recorder just for spectrum analyzers?

The new 19" rack-mounting SPECTRUM ANALYSIS RECORDER from Raytheon. It's the first dry paper line scanning recorder specifically developed for direct plug-in operation with commercially available spectrum analyzers.

Any new or existing spectrum analyzer equipped with the SAR-097 will have a lot more going for it. Like infinitely variable 100:1 speed range - 5 sec/scan to 50 milliseconds/scan...stylus position encoder...automatic recorder synchronization...computer/ analyzer compatibility...high resolution and dynamic range... all-electronic drive. And more.

If you design and build - or buy and use - spectrum analyzers, you don't have to settle for multi-purpose recorders any more. The SAR-097 is here. For full details write the Marketing Manager, Raytheon Company, Ocean Systems Center, Portsmouth, Rhode Island, 02871. U.S.A. (401) 847-8000.

Diskette storage units are IBM compatible

A series of IBM compatible mass storage systems for minicomputer applications has formatted data capacities to 1 Mbyte. The systems use the Model 277 dual diskette drives and are available in a variety of configurations: a one or two drive system complete with µC-based controller, power supply and cabling; a one or two drive system with power supply and cabinet but without controller; a "slimline" system, 4.5 in. wide when vertically mounted, using a dual drive and a power supply in a table-top chassis. The 1070 controller, which can be used in the two-drive system, is also available for mounting in a host system. An "intelligent" controller, the 1070 includes an 8080 µP and has an internal disc operating system in firmware. The systems are available with interfaces to most µCs.
THE SWEETEST AM/FM MODULATION METER
This Side of Heaven.

...with features that are simply unavailable on competing units at any price.

Like a digital display for better accuracy on either AM or FM than any other meter; like built-in post-detection Butterworth filters; and the ability to be controlled and talk to your system through the IEEE-488 Bus.

Even more, the 82AD combines the “easy on the mind” features of automatic tuning and leveling found in the latest service-type modulation meters, with the versatility and accuracy of high-quality lab-type manual meters.

Music to your ears? Well listen to this:
Carrier Range: 10 MHz—1.2 GHz Sensitivity: 10 mV to 520 MHz, 30 mV to 1.2 GHz FM Deviation: 10, 100, 300 kHz fs FM Accuracy: 2% of reading at rates from 30 Hz to 100 kHz AM Range: 10, 100% fs AM Accuracy: 2% of reading from 10 to 90% AM, 30 Hz to 100 kHz BW Options: IEEE-488 Bus Interface, battery supply

Ask your nearest Boonton rep to let you see the 82AD, and he'll also bring along a free record album containing hits of the Big Band Era. The record is yours to keep. But we're betting you'll want the 82AD, too. Write or call Boonton Electronics, Rt. 287 at Smith Rd., Parsippany, N.J. 07054; (201) 887-5110.

BOONTON
Editype, 26 Just Rd., Fairfield, NJ 07006. (201) 227-1141. See text.

With the introduction of an "in-between" package, Editype has broadened its Selectric-conversion offers. A kit ($395) contains all parts to mechanically convert IBM Selectrics into input/output terminals. The new package includes the mechanical conversion and control electronics, installed, for parallel ASCII, at $795. Full conversion to a TTY-like serial format still costs $1455. Most Selectric models with serial numbers over 9,000,000 can be converted.

Texas Instruments, P.O. Box 53, Attn: Leisure Library, Lubbock, TX 79408. $35.

The Leisure Program library for the TI Programmable 58 and 59 calculators contains 20 different programs. They are useful to golfers, bowlers, chess players, football fans, bridge players, photographers and others interested in using the calculator for entertainment. In two of the programs, the alphabetic character and plotting capabilities of the calculators and PC-100A print unit can be used to create computer-type art or store and write out messages. Other diversions in the library are programs to calculate biorhythms, land a spacecraft on Mars, simulate sea battles and play Blackjack, Acey-Deucy, Craps, Nim, and other games.

CIRCLE NO. 326

I/O boards are for use with 8080-based µCs

Analog Devices, P.O. Box 280, Route 1 Industrial Park, Norwood, MA 02062. Russ Ver Nooy (617) 329-1700. $835 to $330 (unit qty); stock.

A 16-channel data-acquisition board with eight or 12-bit resolution and a four-channel analog output board are both functionally, electrically, and mechanically compatible with Pro-Log's 4 and 8-bit µCs. The RTI-1220 data-acquisition and RT-1221 analog-output boards provide complete analog signal handling capability. They can function with 8080 and 6800 based µCs. The RTI-1220 accepts up to 16 single-ended or eight differential channels. On the RT-1221 are four analog output channels, each with 10-bit resolution. The board contains double-buffered registers, four 10-bit resolution, four-quadrant multiplying d/a converters, output amplifiers and two precision references.

CIRCLE NO. 327

8-bit analog I/O system ties into Motorola µCs


MP7400 Analog I/O System is an 8-bit plug-compatible system offered for Motorola's Micromodule Monoboard Microcomputer and EXORciser development system. It contains both analog input and output on a single board. Each board handles up to 64 single-ended or 32 differential input channels and two output channels. A high-gain instrumentation amplifier handles input levels as low as 10 mV FS. A basic 8-channel input-only board (or 16 channel single-ended) costs $295. A fully-loaded board with 32 differential channels, or 64 single-ended, plus two output channels and de/de converter costs $595.

CIRCLE NO. 328
No one has ever seen a lamp like this. It's our bright, new, revolutionary rectangular LED

OUR “LEGEND LAMP” PUTS LIGHT UP FRONT, WHERE YOU NEED IT.

The MV57124 rectangular LED from Monsanto gathers light from a high brightness chip and focuses it on a flat front surface. The shape of the lamp and the uniform illumination across a large emitting area (.15”x.25”) makes the “legend lamp” an exciting, aesthetically pleasing element in your modern industrial panel design. It's available now in high brightness red and will soon be available in other colors.

STACKABLE: SIDE-BY-SIDE, OR END-TO-END.

The unique design of the MV57124 utilizes a special plastic to house the LED assembly, so that no light is emitted from the sides or edges of the unit. All of the light is concentrated on the viewed surface. This means that lamps can be stacked, side-by-side in an X or Y direction, without light interference between units.

4 MCD BRIGHT. UNIFORM.

The MV57124 “legend lamp” uses Monsanto’s high efficiency red emitter. The carefully engineered package makes maximum use of that emitted light, minimizing unusable light. Light output is a very bright 4 millicandelas at 20 mA forward current. That’s up to 3 times the output of other rectangular lamps. So you can use the MV57124 as a legend backlight, a panel indicator, or a bargraph meter.

ANOTHER PERFORMANCE PRODUCT FROM MONSANTO.

This unique new product is a development from the technology and experience that is Monsanto. Our history as being one of the first suppliers of LED’s has led to the features and characteristics of the “legend lamp.”

FREE SAMPLE.

Write today, on your company letterhead, for a free sample. We'll also send you full specifications on our new MV57124.

Synthesizer can be programmed to speak


A phoneme synthesizer kit, the Votrax VSK, when used with a µP, combines unlimited vocabulary, operational simplicity, and low data requirements. It can be programmed to speak, based on phonetic coding principles, producing all combinations of words and phrases. The use of phonetic coding permits the production of speech at low data rates, offering continuous speech at 20 characters/s and easy interfacing to any µP system with an 8-bit parallel output. Fully assembled, the single circuit board measures less than 36 sq. in. It uses +5 and ±12-V supplies.

CIRCLE NO. 329

High-speed I/O expansion card based on 8080 µP

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. Don Schare (408) 737-6597. $189 (100 qty).

The BLC 508 I/O expansion card is based on the 8080 microprocessor and provides eight 8-bit parallel ports, four input and four output. The board can transfer data at rates as high as 1.3 Mbytes per port, the practical limits set by the peripherals of I/O handling software. The board connects to the system bus through an 86-pin card-edge, and has a 100-pin edge connector for parallel I/O. Data, address, and control signals are TTL compatible, and the board operates on +5 V dc. The four output ports have a variable width strobe available for peripherals, which is set in a range from 100 to 1600 ns by a plug-jumper on the board.

CIRCLE NO. 330

PDP-8 processors have up to 128-kword memory

Digital Equipment, Maynard, MA 01754. John Bond (617) 897-5111. See text.

Three PDP-8 processors and three options permit memory capacities up to four times the previously available maximum. The PDP-8/205, 425, and 625 incorporate the KT8-A memory management option in all configurations employing more than 32 kwords of core, to the maximum 128 kwords. This option allows up to 128 kwords of memory to be addressed and the memory can be core, MOS, or mixed core and MOS memory modules. Also available is a MOS memory module, MS8-C. It comes in both 16 and 32-kword configurations and uses 4-k RAMs for high density memory. The KT8-A and MS8-C modules permit upgrading of current PDP-8As to 128-kword capacities. Prices range from $3900 for a 16-kword PDP-8/205 to $18,050 for a 128-kword PDP-8/625. 16-kword and 32-kword MS8-C modules are $1900 and $3100, respectively.

CIRCLE NO. 331
Our new J1P-based interface couplers will link virtually any programmable instrument to the IEEE 488 bus even though their input and output is not bus compatible.

RS-232 TO BUS
Here's a new, inexpensive way to convert your teletype to a 488 bus printer. For about $900, the Model 4884 will provide a bi-directional data link between the parallel IEEE 488 bus and the RS-232 serial data path. And it's not limited to teletype. The 4884 will make any 20mA device such as printers and recorders bus-compatible.

DVMs AND COUNTERS TO BUS
Building an ATE system? You may have a pool of older instruments, but the DVMs and counters aren't 488 compatible. For about $800 you can buy a Model 4881 that will take data from any DVM, counter, or other instrument and put it on the bus.

BUS TO FREQUENCY SYNTHESIZERS AND PULSE GENERATORS
Want to control stimulus devices? For the same $800, a Model 4882 can control any programmable instrument from the bus. Or, use it to just output parallel data. It responds to a status request from the controller and passes all data without alteration.

HOW ABOUT A BI-DIRECTIONAL COUPLER
For about $900, the 4884 combines capability and operational features of the 4881 and 4882 in one unit. It can be used to control or take data from a measuring device, accept program commands from the bus, pass the commands on to a DVM's control inputs, initiate readings and output data when addressed. You can even reduce it to "talk-only" or "listen-only" by setting the mode switches.

AND THERE'S MORE TO THE FAIRCHILD LINE
Fairchild also offers other instruments. The 6600 takes paper tape input and interfaces to CRTs, modems or remote CPUs. The 1700 takes BCD output and interfaces with TTYs, CPUs modems and paper tape punches. Write: Fairchild Instrumentation, a unit of Fairchild Camera and Instrument Corp., 1725 Technology Drive, San Jose, CA 95110. Phone (408) 275-6600 or (408) 998-0123.

CIRCLE NUMBER 87
Some of these components will probably never
The others will just come close.

Snap-action V3, SM and SX switches offer
wide variety of actuators, electrical capacity and
termination.

Mercury switches offer hermetic sealing, a
variety of electrical capacity and broad temperature
ranges at a low cost.

AML manual devices for
low installed cost,
electrical flexibility and attrac-
tive panel appearance. Series 8
miniature manual switches provide small size and
wide variety of operators. DM offers inexpensive
snap-in panel mount design.

Solid state keyboards provide high reliability no mechanical keyboard can offer. Panel sealed
versions also available.
The solid state keyboard, AML lighted push-buttons and sensors you see here will probably never wear out. Because they’re all solid state.

Each is based on a Hall-effect integrated circuit. A circuit that’s been tested through billions of operations without failing. And proven by performance in thousands of applications.

The precision electromechanical components you see here come close. Simply because of the careful way they’re designed and put together.

Like the long-life versions of our snap-action V3, SM and SX precision switches. Available in a wide variety of sizes, electrical ratings, terminals, actuators, contact forms and operating characteristics—some tested to a mechanical life of over 10,000,000 operations.

MICRO SWITCH will provide you with field engineers for application assistance and a network of authorized distributors for local availability. Write us for details or call 815/235-6600.

And find out how you can get a component that goes on forever. Or at least comes very, very close.

MICRO SWITCH
FREEPORT ILLINOIS 61032
A DIVISION OF HONEYWELL

MICRO SWITCH products are available worldwide through Honeywell International.
Low-level logic turns on optically-coupled triac

Motorola, P.O. Box 20912, Phoenix, AZ

An optical coupler, the MOC3011, provides 115-V-ac full-wave switching and isolation equivalent to an electromechanical relay—at the command of a low-level dc source such as IC logic. Used alone, the MOC3011 switches power-line loads up to 7.5 W. Kilowatt loads can be switched with a power triac driven by the MOC3011. The 6-pin coupler uses a GaAs LED that is driven by input currents of 10 mA at voltages as low as 2 V.

CIRCLE NO. 337

Epox y pack age op amp sports lower price tag

Precision Monolithics, 1500 Space Park Dr., Santa Clara, CA 95050. Donn Soderquist (408) 246-9222. $2 (100 qty); stock.

Packaged in an epoxy “B” mini-DIP, the PM725CP precision op amp gives a 35% savings compared to TO-99 packaged devices, plus compatibility with automatic insertion devices. The unit is directly interchangeable, mechanically and electrically, with Fairchild’s 725PC and National’s LMT25CN. Typical specs are input offset voltage drift of 2 µV/°C, open loop gain of 3 X 10^6, and input differential voltage protection of 30 V.

CIRCLE NO. 338

Log-amps are for wideband i-fs

Plessey Semiconductors, 1641 Kaiser Ave., Irvine, CA 92714. Dennis Chant (714) 540-9979. $42 (100 qty).

Two wideband logarithmic amplifier ICs are intended for receiver i-f’s in the 30 to 240-MHz range. The SL1522 contains two SL1521 log-amplifier chips and a resistive divider to increase i-f strip dynamic range, while the SL1523 contains two SL1521 chips in parallel. Specifications are: 12-dB voltage gain; 300-MHz upper cut-off frequency; 3-dB noise figure; 1-mA maximum rectified video output; and operation over the full MIL range of -55 to +125 C. Up to five SL1521 stages can be cascaded with no external resistors, discretes, or interstage filters for 60 dB of compression from 60 to 240 MHz. The units are packaged in 8-lead TO-5 cans.

CIRCLE NO. 339

Small rectifier bridge operates at 6 A

Electronic Devices, 21 Gray Oaks Ave., Yonkers, NY 10701. Dennis Dean (914) 945-4400.

The Model PM minibrige rectifier assemblies are designed for 6-A operation. They are available for 50, 100, 200, 400, 600, and 800 peak reverse voltage operation with surge current ratings of 100 A. Dielectric strength is 1.5 kV rms. Units have diameters of 0.89 in. and come with 1-in. leads. They can be chassis or heat-sink mounted.

CIRCLE NO. 340
The Anaren Digital Frequency Discriminator (Digital IFM) is a crystal video detection system which measures the frequency of an RF signal on a single-pulse basis without knowledge of time of arrival or frequency of the signal. The DFD behaves like a synthetic channelized filter dividing the RF frequency band into 1024 (10 bit) or 2048 (11 bit) contiguous channels or cells. Ten models are available. Series 182105-182109 has 10 bit capacity; Series 182135-182139, 11 bit. All models achieve fine frequency accuracy and resolution with wide unambiguous bandwidth. Typical cell crossing error distributions for L and Ku band models are illustrated. This is a measure of frequency accuracy. Either automatic or external override mode operation is available to allow flexibility in differing signal environments.

**Electrical Specifications**

<table>
<thead>
<tr>
<th>Model No.</th>
<th>182105</th>
<th>182106</th>
<th>182107</th>
<th>182108</th>
<th>182109</th>
</tr>
</thead>
<tbody>
<tr>
<td>Operating Frequency (GHz)</td>
<td>1.0 to 2.0</td>
<td>2.0 to 4.0</td>
<td>4.0 to 8.0</td>
<td>8.0 to 12.0</td>
<td>12.0 to 18.0</td>
</tr>
<tr>
<td>Mean Frequency Resolution (MHz)</td>
<td>0.25</td>
<td>0.625</td>
<td>1.25</td>
<td>2.5</td>
<td>5.0</td>
</tr>
<tr>
<td>RMS Frequency Accuracy (MHz)</td>
<td>0.5</td>
<td>1.0</td>
<td>2.0</td>
<td>4.0</td>
<td>10.0</td>
</tr>
<tr>
<td>Input Power Levels (dBm)</td>
<td>-1 to +7</td>
<td>-110 to +7</td>
<td>-110 to +7</td>
<td>-110 to +7</td>
<td>-110 to +7</td>
</tr>
<tr>
<td>RF Pulse Width (ns)</td>
<td>150 to CW</td>
<td>100 to CW</td>
<td>100 to CW</td>
<td>100 to CW</td>
<td>100 to CW</td>
</tr>
</tbody>
</table>

**Typical Cell Crossing Error Distribution**

**L-Band Models, 1-2 GHz Operating Frequency**

- T = +25°C
- Temp. (°C) | MHz | MHz
- 25 | 0 | 0.15
- 0 | -0.02 | 0.15
- 10 | -0.15 | +0.05
- 70 | +0.15 | +0.05

**Ku Band Models, 12-18 GHz Operating Frequency**

- T = +25°C
- Temp. (°C) | MHz | MHz
- 25 | +0.25 | 2.5
- 0 | -0.4 | 2.5
- 10 | +0.25 | 2.5
- 70 | 0 | 2.5

These DFD's are capable of handling up to 5 million pulses per second.

**Applications**

- Radar pulse train de-interleaving
- Radar test range monitoring
- Measurement of frequency agile sources

Contact your local Anaren Technical Representative for a copy of the DFD Technical Manual, Pub. M1804-77, or write/phone below.

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- quick deliveries; most modules stocked

KSC offers you a CAMAC-to-488 interface as well as a 488-controlled CAMAC system. Write or call for more information.

*IEEE-583 Modular Interface Standard for Computer Automated Measurement And Control

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Dept. ED11227 11 Maryknoll Drive Lockport, Illinois 60441 Phone (815) 838-0005

CIRCLE NUMBER 91

Now measure AC and DC on any voltmeter with the NEW CURRENT GUN™
from F.W. Bell

The all-new Current Gun is a clamp-on instrument that lets you read AC and DC from 0 to 1 kHz and from 0 to 200A quickly, easily, safely — without breaking the connection. Use with any voltmeter... or get a reproduction of the wave form on a scope. Two ranges, 0 to 10A and 0 to 100A with 100% overrange. Only three controls: zero, range selector and press-to-read button.

Less than $200

Accessories available to greatly expand ranges — higher and lower.

CIRCLE NUMBER 92

---

ICs & SEMICONDUCTORS

LSI is floppy-disc formatter & controller

Western Digital, 3128 Red Hill Ave., Newport Beach, CA 92663. George Gregoire (714) 557-3550.

Model FD1781, an NMOS device, performs the functions of a floppy-disc controller/formatter. Features include: automatic track-seek with verification; selectable track to track stepping, head settling and engage times; double buffering of data; 8-bit bidirectional bus for data, control and status; and flexible formatting, including full compatibility with IBM 3740 data entry systems. It also provides data, data strobe and address mark input/output for reading and writing data. The controller can accommodate MFM, M'FM, group coding or other double-density encoding methods. All lines are TTL compatible.

CIRCLE NO. 341

FET-input op amps span wide range of specs


Thirteen devices are offered in the BiFET II family of op amps. Devices fall into four groups, based on price, offset voltage range, package and temperature range. LF351 is a low cost series of plastic single units with voltage offsets of 10 mV, 5 mV and 2 mV priced at $0.39, $0.67 and $1.66 in 100 quantity. LF353 is a series of dual op amps with the same characteristics priced at $0.70, $1.30 and $3.06. LF347 series are quad units with the same characteristics priced at $1.25, $1.95 and $5.99. LFT156 units are high performance single op amps in TO-5 packages featuring 0.5-mV and 1-mV offsets and are priced at $18, $10, $12 and $7.50.

CIRCLE NO. 342
When you need LEDs or more than LEDs...

Dialight is the first place to look. We can help you do more with LEDs...because we've done more with them.

Discrete LEDs come in a variety of sizes, shapes, colors (red, yellow, green in clear or diffused), with or without built-in resistors.

Low cost logic state fault indicators for trouble shooting complex circuits. Designed for close density PC board mounting.

High-brightness bi-color LEDs (red/green) suitable for go/no-go situations. Designed with unique lenses for the extra visibility you'll want for your most critical applications.

Snap-in mounting LED indicators reduce labor cost. Available in red, yellow or green with or without built-in resistors.

Whatever you need in LEDs, Dialight's probably got it already. For your free 60-page selector guide and listing of our nationwide stocking distributors, contact us today.

Dialight meets your needs.

Dialight, 203 Harrison Place, Brooklyn, N.Y. 11237 (212) 497-7600

CIRCLE NUMBER 93
ICs & SEMICONDUCTORS

Single chip makes 3-3/4 digit panel meter

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. Bob Bennett (408) 737-5720. $11.95 (100 qty); stock.

The ADD3701 CMOS IC requires only a display, an external voltage reference, a few passive components and a digit-driver to form a 3-3/4 digit DVM system. It uses a 5-V supply to drive a multiplexed seven-segment output, and features differential input protection to 200 V. Overrange condition is displayed by “+OFL” or “-OFL.” The DVM also includes autopolarity and an on-chip clock that can be set by an external RC network, or can be driven from an external source. The segment output drivers can deliver up to 40 mA each, thus permitting direct drive of LED displays.

CIRCLE NO. 343

Here’s a Paktron® Capacitor with a ONE...TWO...THREE punch!

- 1. Latest Type DVL Capacitor is three units in one
- 2. U.L. listed and C.S.A. approved
- 3. Three applications
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CIRCLE NUMBER 94

Single-chip µC serves as high-speed counter/timer

Rockwell International, 3810 Miraloma Ave., Anaheim, CA 92803. Scotty Maxwell (714) 632-2321. $9.30 (1000 qty).

The PPS-4/1 Model MM76C µC can “crunch numbers” or control functions and simultaneously count inputs, events, perform timing, program fixed intervals, and generate variable-duty square waves. The device has five input control lines and 32 I/O ports, which include serial I/O capabilities that in combination with an on-chip clock circuit enable it to be synchronized with or by another µP system. The on-chip counter functions as either a single 16-bit reference or as two independent 8-bit counters. It can count inputs ranging from 2 MHz to days-long frequencies. The processor comes in a 52-pin STM plastic package.

CIRCLE NO. 344

Frequency prescaler is a power saver

Plessey Semiconductors, 1641 Kaiser Ave., Irvine, CA 92714. Dennis Chant (714) 540-9979. $5.50 (100 qty).

Divide-by-100 prescalers, the SP8627, 28 and 29, consume only 1/4 the power of previously available units. The SP8629 is a divide-by-100 counter with a minimum toggle frequency of 150 MHz from 0 to 70 C; the SP8628, the same circuit with reset; and the SP8627, the same circuit with a divide-by-80 output. All three devices have a power consumption of 170 mW, typical, and feature ECL/TTL inputs and TTL outputs. They may be positive or negative edge-triggered in single-ended or differential input modes.

CIRCLE NO. 345

Electronic Design 24, November 22, 1977
How fast can you measure rise time, fall time and pulse width?

Your way.
(About 5 minutes.)
1. Connect signal to scope.
2. Adjust trace intensity.
3. Adjust focus.
4. Select VOLTS/DIV range.
5. Select TIME/DIV range.
6. Adjust vertical gain to fill screen for location of 10% & 90% points.
7. Locate 10% point.
8. Locate 90% point.
9. Determine horizontal displacement between 10% & 90% points.
10. Multiply displacement by horizontal scale factor.

That's RISE TIME. Only 9 more steps and you've got PULSE WIDTH and FALL TIME.

Our way.
(About 5 seconds.)
1. Connect signal.
2. Push button for RISE TIME.
3. Push button for PULSE WIDTH.
4. Push button for FALL TIME.

The rest is automatic.

Your move.
Give us a call and we'll tell you how the Dana 9000 Microprocessing Timer/Counter can solve your measurement problem the easy way.

Others measure by us.
Dana Laboratories, Inc., 2401 Campus Drive, Irvine, CA 92715
Phone: 714/833-1234
Plastic 8-k PROM is thrifty sub for EPROM

Motorola, 3501 Ed Bluestein Blvd., Austin TX 78721. (512) 928-2600. $9.95 (100 qty); stock.

The silicon-gate PROM, MCM2708P, is a 1024 X 8-bit memory and is a low-cost alternative for EPROMs. Its operation and programming are identical to the MCM2708L EPROM and is pin-for-pin compatible with 2708 type EPROMs and the MCM65308, MCM68308, and 2308 mask-programmable ROMs. Maximum access time is 450 ns, power supplies are +12 and ±5 V. The unit comes in a 24-pin plastic DIP.

Static n-channel ROM has 4096 words

Rockwell Electronic Devices Div., 3310 Miraloma Ave., Anaheim, CA 92803. Scotty Maxwell (714) 632-2321. $20.10 (100 qty).

A completely static n-channel ROM, organized as 4096 words by 8-bits, features a typical access time of 250 ns and uses 350 mW of power. The R2332 requires just a +5-V supply. Inputs are TTL compatible and have a 400-mV minimum noise immunity on both the HIGH and LOW levels. Each of the eight outputs have three-state drivers capable of driving 100 pF and a TTL gate. Two mask-programmable chip-select inputs allow four 32-k ROMs to be OR-tied without external decoding. Programming allows selection when the input is HIGH or LOW, or in a don’t care mode. Both chip-select and chip-deselect delays are 100 ns.
Introducing the PMUX

The world's first programmable multiplexer

THE 29693 IS:

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- A sign extender
- A programmable data flow control
- A buffered programmable diode matrix
- A digital crosspoint array
- Easily programmed
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350 Ellis Street, Mt. View, CA 94042

Raytheon
SEMICONDUCTOR DIVISION

Electronic Design 24, November 22, 1977
COMPONENTS

Reed triggers hybrid ac-input relay

Potter & Brumfield, 200 Richland Creek Dr., Princeton, IN 47671. Bill Skidmore (812) 386-1000. $11.40 to $15.92 (100 qty); stock.

Each relay in series Type ECT is a medium power, 120/240-V-ac, 50/60-Hz, SPST-NO solid-state switch controlled and isolated by a self-contained 120-V-ac-input reed relay. Operate time of the ECT is 50 ms max, and expected life at rated load is at least 10-million operations. Load ratings are 2, 4, 5, or 7 A at 0.4 pF when the relay is fastened to a 10 × 10 × 0.062-in. aluminum heat sink. A 9-A model also is offered, whose rating increases to 32 A when used with a heat sink.

CIRCLE NO. 353

Interface easily with display-only DPM

Datel Systems, 1020 Turnpike St., Canton, MA 02021. Gene Murphy (617) 828-8000. $29 (100 qty); 6 to 8 wk.

Digital panel meter, DM-3100L, is for display-only applications featuring differential inputs and autozeroing. The interfacing task is eased with simple input configurations and the input can also be operated single-ended. Common-mode voltage range is ±2 V at 80 dB CMR. Temperature drift is 50 ppm/°C, with a displayed accuracy of 0.2% of reading, ±1 count at +25 C. The DPM accepts input voltages from −2 V dc to +2 V dc, with an internal pad area left for input voltage divider resistors. Input impedance is 100 MΩ and protection circuits withstand 150 V. Size is 3 × 1.8 × 2.2 in.

CIRCLE NO. 354

Keyboard family has one for each requirement

Grayhill, 561 Hillgrove Ave., La Grange, IL 60525. (312) 354-1040. $6.30 to $8.05 (100 qty).

A keyboard family offers choice of 12 or 16-button arrays plus choice of circuitry, mounting means, and legend. Circuity options include matrix coding, single-pole/commonbus switching, 2-out-of-7 code or 2-out-of-8 code. Either the 3 × 4 or 4 × 4 array is available with post or screw-type flange mount. Legend choices include standard keyboard arrangements with molded-in legends, hotstamped legends to order, and snap-on caps for self-legending of prototypes.

CIRCLE NO. 355
From the people who brought you IDIOM *
United States Instrument Rentals introduces...

Unemployment Insurance
(FOR TEST INSTRUMENTS)

Does it break your heart to see your test instruments just standing around idle while you’re kept busy paying for them? Look around on your shelves... Are your test instruments not working to their full capacity because you don’t need them all the time?

Well, U.S. Instrument Rentals believes that you shouldn’t have to worry about paying or caring for instruments that are not working for you all the time. USIR feels that your valuable capital should be spent for equipment that can be employed all the time.

So, U.S. Instrument Rentals offers you Unemployment Insurance.

Unemployment Insurance means that by renting your test instruments from USIR only when you need them, you’re protected against paying for idle equipment. You pay for our instruments *only* when they are working full-time for you. And when the job is finished, you simply return the equipment to USIR until you need it again.

In addition, by renting from USIR, you’re protected against those expensive calibration, maintenance and repair cost worries. We take care of all our instruments’ needs.

And to insure that you get the equipment you need, USIR has thousands and thousands of instruments that are seeking gainful employment, giving you a better chance of finding the instrument that is just right for your needs.

So for a list of instruments you might like to employ and suggestions for solving your test equipment unemployment problems, send for our Unemployment Insurance Booklet... The USIR Rental Catalog. It’s your best guide to full employment for test instruments.
COMPONENTS

Keyboard seals out dirt, dust and liquids

Datanetics, 18065 Euclid St., Fountain Valley, CA 92708. Darrel West (714) 549-1191.

Dataseal eliminates malfunction of keyboards caused by the environment. Dust, dirt and liquids are totally sealed out below the key caps. Only the key cap is exposed. Also, seals can be extended to assure complete waterproofing of keyboards, including exposed electronics. The keyboard is made from polyurethane and it is impervious to most common chemicals. Custom design to fit any keyboard layout is available.

CIRCLE NO. 356

Heat sinks with winged effect have low profile

Aavid Eng., 30 Cook Ct., Laconia, NH 03246. (603) 524-4443.

Heat sinks, 5071, feature a winged effect for extra cooling surface. The low profile of these heat sinks makes them ideal for mounting on PC boards, where high-density packaging of plastic power semiconductors makes cooling a critical requirement. The heat sinks are available plain or with gold-chromate or black anodizing. For use requiring extra power, they may be stacked for multiside cooling of the TO-220 case. A sample assortment of four heat sinks is available free of charge for prototype and testing use.

CIRCLE NO. 357

Mini switches have bifurcated contacts

CW Industries, P.O. Box 96, Warminster, PA 18974. Keith Nelson (215) 355-7080.

Miniature slide switches have bifurcated contacts and provide "make-before-break" or "break-before-make" action. They are rated 0.5 A ac/dc at 125 V and are UL and CSA listed. Button height is 0.2 in. and solder or PC terminals are available.

CIRCLE NO. 358

Precision resistors meet toughest spec


S102C resistors meet or exceed all requirements of MIL-R-55182/9, characteristic Y, the most demanding resistor specification issued. A new design gives lead integrity, resistance to moisture and high-temperature exposure, and improved load-life stability. Encapsulation in a one-piece compression-molded case provides maximum physical and chemical protection under all environmental conditions. Possible thermal EMF sources are reduced to a minimum. The resistors are presently available in values from 1 Ω to 100 kΩ, and in tolerances from ±0.005% to ±1%.

CIRCLE NO. 359

Transformers handle 0.5 to 25-µs pulse widths

Magnetico, 182 Morris Ave., Holtsville, NY 11742. Harold Eicher (516) 654-1166. $3.90 (5000 qty); stock to 4 wk.

Blocking-oscillator pulse transformers, PN13020 through PN13022, operate with pulse widths of 0.5 to 25 µs and voltages to 22 V. Rise and fall times are less than 0.2 µs. They are packaged in a Grade 5 (encapsulated), 9/16-in. cube for PC mounting. Operation is from −55 to +125 C.

CIRCLE NO. 360

Tiny fan delivers air at 12 cfm

Rotron, Woodstock, NY 12498. (914) 679-2401.

Minimax is a 9-frame cooling fan for high-density electronic packages. In a 1-1/8 in. diameter and just over 1-1/2 in. thickness it packs a capacity of 12 cfm at free delivery. It can be used in ambient temperatures from −55 to 100 C with a life expectancy in excess of 20,000 h.

CIRCLE NO. 361

Slide pot uses plastic-resistance element

Dale Electronics, Dept. 860, Box 609, Columbus, NE 68601. (402) 564-3131. $1.51 (1000 qty).

A line of custom slide potentiometers for PC boards has a conductive-plastic resistance element and dissipates 1/4 W at 85 C. Available in a resistance range of 100 Ω to 1 MΩ, the slide pots have a tolerance of ±10%. Independent linearity of ±1.5% is available in values of 2 kΩ and up. Internal design provides a positive adjustment stroke of 2 in. Nominal slide-starting force is 280 gm with mechanical stops available that present a max resistance of 10 times the nominal starting force.

CIRCLE NO. 362
Six important questions to ask of any DMM that claims to be designed for field service.

At Fluke, we've been building DMMs for a long time. We're the leader.
And if there's one thing we've learned over the years, it's that what works for the bench doesn't always work for the field.
But a lot of companies don't understand that. They'd like you to believe their DMM is perfect for field service. Just because they've put it in a different case.
Here's how to tell the difference:

1) Is the size and shape designed for the field?
How do you carry your tools? We designed the 8030A/8040A DMMs into an ideal shape after we researched the requirements of field service work. It's sized to fit in a case. And it's rugged, to take the beating field instruments must survive.

2) Does it have true rms ac?
Make sure you get usable accuracy. You'll need true rms ac to eliminate errors when measuring distorted waveforms.
(And if you don't understand the importance of true rms, write for our bulletin on True RMS Measurement.)

3) Does it give full performance?
Just because it's a field instrument, you shouldn't sacrifice performance. Demand five measurement functions in 26 ranges. Top specs, like our 8040A basic dc accuracy of ±0.05% or our 8030A basic dc accuracy of ±0.1%. And the specifications are guaranteed for one year. Important extras, like diode test for measurement of semiconductor junctions in-circuit, high voltage protection, and self test feature. And a complete line of accessories: various battery options, and probes for measurement of rf voltages, high current ac, high voltage dc and temperature.

4) Do you have a choice of manual or autorange?
We offer two versions: the 8030A 3½ digit and the 8040A 4½ digit with autoranging. Because we know not all field service applications are alike.

5) What is the price?
A field service DMM is a tool, and should carry a practical price. Our 3½ digit 8030A is $250. Our 4½ digit 8040A is $440. Check around and you'll see how practical that is.

6) Do you trust the company that builds it?
We became the leader in DMMs for one reason only. We build digital multimeters that people trust and continue to use, year after year. We've sold hundreds of thousands of DMMs.
And every bit of that experience has gone into the 8030A and 8040A DMMs.
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COMPONENTS

Mini isolation Xformers are for flea power

Magnetico, 182 Morris Ave., Holtsville, NY 11742. Harold Eicher (516) 654-1166. $5.90 (5000 qty); stock to 6 wk.

Encapsulated in a cube 1/2 in. on each side, transformers are offered for power-line isolation, reference voltage reduction, or those applications where isolated zero crossover detection of the power line is required. The normal input is 115 V, 60 Hz. Part 52635 provides 0.6 V at 0.1 mA and part 52636 provides 1.2 V at 0.1 mA. The units can provide constant output for input line variations, transients and most line spikes.

CIRCLE NO. 363

Touch-sensitive keyboard uses thick film

Oak Industries, Crystal Lake, IL 60014. Didi Almerantz (815) 459-5000.

A touch-sensitive keyboard, using thick-film techniques, provides a flat, sealed data-entry surface. With a smooth Mylar surface replacing the traditional pushbutton switches, the new switching system allows unusual graphic designs. It enables any number of switches, of the same or different size, to be printed on the Mylar sheet in any configuration. Since graphics on the Mylar surface replace pushbutton caps, any pictures or symbols can replace alphanumeric characters. By use of apertures in the housing, or in a special lamp isolation mask, any of the switches can be backlit.

CIRCLE NO. 364
The Best Way to Measure
CUTOFF & BANDWIDTH
PHASEMETRICS*

Phasemetrics is the most precise technique for cutoff and bandwidth measurements. In many passive and active circuits, (amplifiers, filters, tuned circuits, etc.), it is difficult to measure the "3dB-down" frequency with better than a few percent precision... particularly because it is difficult or impossible to establish the 0dB reference level, and because subtraction is involved. But, at cutoff, the phase shift is exactly 45° per pole (by definition), and the phase is easily referenced to the input signal. Hence, with a first-class phase meter – the Dranetz 305 – you can pinpoint the 3dB point within about 0.006dB (0.2%), easily. This 10 to 1 improvement also applies to measuring bandwidth and Q of resonant circuits and resonant frequencies (φ = 0° at resonance). Neat? Neat!

The point is — a phase meter doesn’t just measure phase. As many users know, the ultra-flexible, ultra-precise, fully automated “hands-off” Series 305 design equips you to measure many other parameters, faster and more accurately, in terms of phase:

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- Distance, Directivity, and Tracking Resolution.
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- Network Impedances, Impedances, and Transfer Functions.
- Component Impedances, strays, Q, DF, AC/DC Resistance Ratios.
- Cable, Filter, Communications-Channel Group Delay and Bandwidth.

All this and much, much more is explained in our famous 24-page Applications Handbook of Precision Phase Measurement, available on request. In subsequent advertisements, we shall explore some of the other advantages of the PHASEMETRICS approach. If you don’t want to wait, write or call today for your free Handbook.

Dranetz Engineering Laboratories Incorporated, 2385 South Clinton Avenue, South Plainfield, New Jersey 07080. (201) 755-7080.

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*We invented the term "Phasemetrics" to denote the art and science of making many different kinds of measurements in terms of phase, with less effort and uncertainty, using our state-of-the-art Series 305 Phase and Gain/Phase Instruments. We also invented "Phase" (ΩφΩφΩ), the goddess of Phasemetrics.

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Affiliation with Siemens gives Litronix all you could want from an optoelectronics source.

On OCTOBER 18, 1977, Siemens A.G., an $8 billion per year firm, acquired an 80% interest in Litronix through a wholly-owned subsidiary — bringing financial stability, new technologies and dozens of new products to the American firm.

Foremost among the new technologies and products are LCD displays, high-power infra-red emitters, green, yellow and red GaP LEDs, and a full line of photo detectors. Nearly all types of optoelectronic products will now be available from Litronix.

Litronix will operate under its own name and market all products in the U.S. and abroad through the same distributors and sales representatives as before.

All resources devoted to components

Litronix ceased manufacture of calculators and digital watches in January 1977. All the design and production capability once devoted to these products is now directed entirely to components. The component portion of the company's business has always been highly successful. Now, operating from a strong financial position, Litronix will resume its place as the leading source of advanced, cost-effective optoelectronic components.

New, advanced products coming fast

Already in 1977 Litronix has developed 21 new products. With the recent affiliation, new product development is being further accelerated. The company's line of displays, lamps and other opto devices is being broadened and upgraded. Special emphasis is being placed on "intelligent" displays and indicators — devices which incorporate a display and integrated logic in the same package.

The recently introduced DL-1416 alphanumeric display, which interfaces exactly like a RAM, is an apt example. Such devices eliminate need for much associated interface and logic circuitry — simplifying design and producing a sizable net saving in the production cost of customers' products. Litronix is the uncontestable leader in this promising extension of optoelectronic integration.

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Nitron NVMs are available off-the-shelf for parallel data applications in 64x4 and 256x4 configurations; and for serial data applications in 21x16, 16x18 and 1024x1 configurations. If you don't see what you need, tell us about it. We custom design NVMs, too.

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Need information fast? Call Nitron NVM Marketing at (408) 255-7550. Or fill in the coupon below for your NVM Fact Kit.
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Dale Electronics, P.O. Box 74, Norfolk, NE 68701. (402) 371-0080. $0.40; 8 to 10 wk.

Precision metal-film resistors, PTF 55, are rated at 1/10 W at 85 C. They have a resistance range from 50 to 250 kΩ. Dimensions are 0.26 in. long by 0.094 in. diameter. Tolerances from ±1% down to ±0.05%, with TCs of ±15 ppm/°C (T-10) and ±10 ppm/°C (T-13) are available.

LED indicator lamps sealed for protection

Oxley, 3250 Wilshire Blvd., Los Angeles, CA 90010. Ray Guthrie (213) 383-8270.

Solid-state indicator lamps, type PS/LH/8, for military-style rugged mounting use high-brightness, high-reliability LEDs. Panel sealed with PTFE sealing rings, the lamps embody sealed glass lenses and black shrouds to optimize the visual effect and protect the emitter in severe environments. Their aluminum-alloy bodies are compatible with standard chassis and provide electromagnetic shielding for military applications. The lamps are available in red, yellow and green.

DIP relay has low profile

Allied Control, 100 Relay Rd., Plantsville, CT 06479. (203) 621-6771.

A low-profiled DPDT, DIP relay stands only 0.38 in. high and fits within 0.5 in. spacing when mounted on a PC board. It fits standard 16-pin IC sockets and its footprints are interchangeable with similar-but-higher profile DIP relays. The relay has a sensitivity of 200 mW at pull-in. Its rating is 1-A resistive at 28-V-de switching and 5-A carry ability. Typical operating time is 4 ms; release time is 1 ms. The relay's construction is sealed for wave soldering and cleaning.

Toggle switch can be used up to 2 GHz

Instru-Mech, 1275 Bloomfield Ave., Fairfield, NJ 07006. (201) 575-1860. $5.50/$6.50; stock.

The Type 10 toggle switch has low shunt capacitance (0.4 pF), so it can be used up to a frequency of 2 GHz. It does not require shielding and is for low-energy use. The size is subminiature. Type 20 has essentially the same characteristics, but performs up to 1 GHz. The switches have Teflon bodies which minimize dissipative and dielectric losses.

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CIRCLE NO. 369

**Precision pots last longer than carbon units**

Beckman Instruments, Helipot Div., 2500 Harbor Blvd., Fullerton, CA 92634. (714) 871-4848.

Type 6180 precision potentiometers are rated at 5-million shaft revolutions, which is 50 times better than carbon composition pots. The 6180 consists of three, 7/8-in. diameter, single-turn, conductive-plastic models that differ only in bushing and shaft dimensions to accommodate mounting requirements. All provide 1-W power rating at 70°C with 125°C max operating temperature. Other features include an essentially infinite resolution, output smoothness of 0.1% max and nonflammable materials.

CIRCLE NO. 370

**Mini film capacitors offered in TO-5 size**

Inter-Technical Group, P.O. Box 23, Irvington, NY 10533. (914) 591-8822.

Subminiature film-dielectric capacitors come in sizes no bigger than a TO-5 case. The FK52, MK52 and FK02 series have polyester and polycarbonate film-dielectrics about 0.002-mm thick. Lead spacings are either 5 mm or 7.5 mm. Capacitance values range from 150 pF to 1 μF in either 63 V dc or 100 V dc ratings. The capacitors are vacuum encapsulated in epoxy for physical uniformity and resistance to environmental extremes. Operating temperatures are −55 to 100°C.

CIRCLE NO. 371

**Use RFI filters in noisy switchers**

Corcom, 2635 N. Kildare Ave., Chicago, IL 60639. (312) 384-7400. $10.80 to $33.35; stock.

SP type RFI power-line filters are for switching-type power-supply-noise suppression. They provide high insertion loss for both line-to-ground and line-to-line emissions throughout the frequency range. Filters are available in 3, 6 and 10-A versions. Max leakage current, line-to-ground, is 2.0 mA at 115 V ac 60 Hz. Size is 3.75 x 2.0 x 1.75 to 2.25 in. depending on model.

CIRCLE NO. 372

**Circuit breaker doubles as snap-action switch**

Airpax Electronics, Cambridge, MD 21613. (301) 228-4600. $5.00.

The T11 magnetic circuit breaker doubles as an up-front, high-current power switch. The UL-recognized device features fast-make, fast-break snap-action contacts that have a more than 20 to 1 increase in open-contact gap over conventional switches. The series-titp spst T11 is available in six paddle-handle colors. They can be used at dc, 50 or 60 Hz. Current ratings are from 0.1 to 20 A at 32 V dc, 15 A at 120 V ac, 50/60 Hz and 400 Hz; and from 0.1 to 7.5 A at 50 V dc, 250 V ac, 50/60 Hz and 400 Hz. Short-circuit rupture capacity is 1000 A. A number of trip delays are available.

CIRCLE NO. 373
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It's CSC's DP-1: the automatic signal source that cuts hours from
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This compact, circuit-powered unit lets you inject signals at key points to test digital circuits with fast
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Short circuits can't harm it, even over prolonged
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(West Coast) for the name of
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tor and a full-line catalog.

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reverse-polarity protection.

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LED Pulse indicator—Monitors
operating mode.

Interchangeable ground leads
connection—Provides ground-side
input connection, where desired,
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Interchangeable probe tips—
For greater versatility. Straight tip
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Plug-in leads—24", supplied with
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Specifications:

- **Tri-state output**—DP-1 is isolated from circuit under test; 2>300K
- **Auto-polarity pulse sensing**—DP-1 automatically produces proper
  polarity pulse for circuit under test: logic "0" level produces a
  "1" pulse, logic "1" level produces a "0" pulse
- **LED indicator**—Flashes once for single pulse, stays lit to indicate
  pulse train
- **Short-circuit protection**—Can pulse into short circuit continuously
- **Power**—Overvoltage protected to 25V, reverse-voltage
  protected to 50V, voltage range 4-18V, 30mA max.

<table>
<thead>
<tr>
<th>Pulse modes</th>
<th>TTL</th>
<th>CMOS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pulse width</td>
<td>15µsec ± 30%</td>
<td>10µsec ± 30%</td>
</tr>
<tr>
<td>Fan out</td>
<td>60 loads</td>
<td>60 loads</td>
</tr>
<tr>
<td>Sink and Source</td>
<td>100mA source to 3.5V, sink to 6V</td>
<td>50mA source to logic 1, sink to logic 0</td>
</tr>
<tr>
<td>T&lt;sub&gt;1&lt;/sub&gt;</td>
<td>100µsec</td>
<td>100µsec</td>
</tr>
<tr>
<td>T&lt;sub&gt;2&lt;/sub&gt;</td>
<td>one TTL load, 500µsec</td>
<td>100K load, 8µsec</td>
</tr>
</tbody>
</table>

*Note: T<sub>2</sub> is directly proportional to load resistance.

**Dimensions:** L x W x D 5.5 x 1.0 x 0.7" (147 x 25.4 x 17.8mm)

**Weight:** 3 oz (85g)

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CIRCLE NUMBER 108

208 ELECTRONIC DESIGN 24, November 22, 1977
COMPONENTS

Tilt switch mounts on PC boards


Tilt switch, TS7-1832, is an omnidirectional, mercury-switching capsule that is equipped with PC-board terminals, and is epoxy encapsulated. The switch may be mounted to a PC board and wave soldered. It is positioned normal to the board surface after soldering. Tilting the board 15° in any plane, from the horizontal, will cause the normally open contacts to close. The switch contacts are rated at 1.0 A, 115 V ac or 24 V dc.

CIRCLE NO. 374

Digital encoder eliminates noise, wear

Disc Instruments, 102 E. Baker St., Costa Mesa, CA 92626. (714) 979-5300.

A digital output signal proportional to shaft rotation from a Panelcoder can replace old style analog potentiometers and eliminate noise and wiper wear. The encoder employs solid-state, LED sources and plugs in with a circuitboard edge-connector. Adjustable torque is built-in to prevent flywheel or knob movement under vibration. The unit operates manually at speeds to 100 rpm.

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CIRCLE NUMBER 111
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San Diego, California 92123
(714) 292-5584

COMPONENTS

Keyboard switch wears booties

Mechanical Enterprises, 800 Forbes Pl., Springfield, VA 22151. Robert Twyford (703) 321-8282. $0.43 (10,000 qty).

An environmentally sealed keyboard switch, T-5Q, is for circuit-board mounted, thru-panel use, including clusters to make a keyboard array. It has a neoprene sealing-boot, made in the form of a bellows. Doubleshot molded keytops are used for legending. The plungers have a total travel of 0.17 in. and an actuation force of 3.5 to 4 oz. They are available in both momentary and alternate actions with single and double-pole contacts.

CIRCLE NO. 376

Slide switch works at right angle

Stackpole Components, Farmville, VA 23901. Steve Smith (804) 392-4111.

For use where front-panel real estate is at a premium, "Side-Slide" side-actuated mini-switches can be the answer. With a height of 0.375 in. from PC board to case top, they mount where switching must be done at right angles to the board. Capable of UL listing or CSA certification of 3 A at 125 V ac, they are available in sp, dp and sp spring-return versions.

CIRCLE NO. 377

LED indicators are tiny and fast

Chicago Miniature Lamp Works, 4433 N. Ravenswood Ave., Chicago, IL 60640. George Neeno (312) 784-1020. $0.90 (1000 qty); stock.

Astrolite indicator lights are small, inherently fast, use little power and are immune to shock and vibration. Viewing angle is 60°, and they can be readily seen across the average room. LEDs in a metallic package mount in 0.193-in. panel holes. The indicators come with 6-in. leads having 1/4-in. stripped and tinned ends, or with pin terminals.

CIRCLE NO. 378

Carbon-film resistors have dual-power rating


GPR 5000X general-purpose resistors combine tight tolerance and temperature coefficient in a dual rated 1/4 W/1/2-W package. They are 2% tolerance, ±200-ppm-TC devices in 1/4-W packages, but can also be used in 1/2-W applications. The available resistance range covers from 10 Ω to 22 MΩ, with a max of 350 working volts.

CIRCLE NO. 379

Low-profile relays mount on PC boards


Low-profile relays, Type 400, may be mounted on PC boards with spacings of 19/32 in. between boards. Contact configurations from SPDT to 6PDT have a useful life of five-million operations at 1 A, 24 V dc. SPDT-relay load ratings are 2 A; multipole relays are 1 A. Latching and sealed units are available.

CIRCLE NO. 380
One Mallory THF capacitor can replace up to four CSR types in a switching power supply.

These small, solid-tantalum capacitors give you a per-unit substitution factor as high as one for four and can bypass 4.5 amp rms at 100kHz. So by using these high-performance capacitors you save in space, weight and cost.

Specially designed for low equivalent series resistance, at frequencies from 1 kHz through 1 MHz. They’re ideal for high frequency power supply switching, for regulator switching, or for bypassing or filtering unwanted ripple currents.

Because ESR is low, power losses are low. With the solid electrolyte and hermetic seal, long life is inherent. Electrical characteristics are very stable over a temperature range of $-80^\circ C$ through $125^\circ C$. Two case sizes: .29 x .69 and .35 x .79 inches.

Mallory THF capacitors are available in a wide range of ratings: 5.6 to 330$\mu$F, 6 to 50VDC.

They’re the result of Mallory’s engineering program that’s finding ways to produce high performance type capacitors at less cost to you.

Just ask your Mallory representative. Available direct, or through authorized Mallory Distributors in U.S. or overseas. Or call Help-Force Headquarters at (317) 856-3731. Mallory Capacitor Company, a division of P. R. Mallory & Co. Inc., Box 1284, Indianapolis, IN 46206.

MALLORY
DATA PROCESSING

Terminal system has hard-copy output

Olivetti Corp. of America, 500 Park Ave., New York, NY 10022. Mike Poli (212) 371-5500. $7500 to $10,000 (5 up); stock.

TC808 terminal system is aimed at interactive or batch communications with optional hard-copy output. It is for on-line communications and remote data entry users who require limited terminal intelligence, limited peripheral connections, and printed response. Standard equipment includes a central control unit, a synchronous or asynchronous line-control unit, and a workstation with keyboard and printer. A 256-character display is available, as is an extra 8-k memory that can bring the basic memory size to 24 k.

CIRCLE NO. 381

Only two companies make 50-MHz, 16-channel logic analyzers.

Our costs less and gives you Window-Trigger Storage.

Window-Trigger Storage. WITS, for short. It’s more than a catchy name. It’s a key feature of our new 50D16 logic analyzer that will let you catch the information you want better than ever before.

WITS eliminates triggering on data you’re not interested in. Like noise, static—or even the anomalies found on computer or microprocessor buses at the time of device transfer. It works because you can insert up to three sample bits of time delay in the trigger. Along with this feature, you can count trigger events and capture data just before, or just after, the event you want.

The new 50D16 is one of only two 50-MHz, 16-channel asynchronous logic analyzers available. It’s the better one. Because of WITS, and all the more features than we can mention here, if you use logic analyzers in your lab, in field service, or in your product, we’d like to have your attention. For technical data and pricing, use the reader service number or call us today at (408) 446-4322.

MATCHING WITS WITH BITS...
BP’S 50D16 WITH DISPLAY FORMATTER—

Drum plotter zips along at speed of 2 in/s

California Computer Products, 2411 W. La Palma Ave., Anaheim, CA 92801. Carol Felton (714) 821-2541. $8220 to $11,960; 12 wk.

Model 1037, part of a new family of drum plotters, features one pen, and a plotting speed of 50 mm/s (2 in/s). Capability is field upgradeable to that of other plotters in the family—the single-pen, 112.5-mm/s (4.5 in/s), Model 1088, and the three-pen, 112.5-mm/s Model 1039.

CIRCLE NO. 382

Data concentrator claims to shatter price barrier

Micom Systems, 9551 Irondale Ave., Chatsworth, CA 91311. Roger Evans (213) 882-6590. See text; 6 wk.

Micro800 is a 4 or 8-channel data concentrator, or smart multiplexer, providing multiplexing at lower cost than with conventional time-division multiplexers. Its statistical multiplexing method provides more efficient use of the shared telephone line or digital data link. Retransmission on error end-to-end is fully automatic. The device permits up to eight asynchronous data terminals to share a single line. Price is $1870 for a 4-channel system, $2630 for 8 channels.

CIRCLE NO. 383
RF PERFORMANCE... is the most important feature in any Spectrum Analyzer. **mi** gives you the best in performance, and in value!

Save your skilled engineers for more important work with **mi** Model 2370 Spectrum Analyzer. Simplify complicated measurements such as response, level, gain, signal purity, modulation and many more. Forget everything you have heard about spectrum analyzers. **mi** Model 2370 is unique. It employs advanced technology to make it as easy to operate as a multimeter. The facts speak for themselves.

- **Flicker-free high brightness TV display** (No more storage tubes to replace)
- **Electronic graticule** can pin point position of waveform display for rapid analysis and measurement.
- **Choice of vertical scales:** linear, 10dB/div for 100dB display, and 1dB/div for 0.1dB resolving power.
- **Counter automatically** displays center frequency, identifies the frequency corresponding to the manually adjusted ‘bright line cursor’, or the difference frequency between the two. All to an accuracy of 2Hz.
- **Integral synchronous signal source** for measuring networks, filters, amplifiers, etc.
- **For comparative measurements,** memory storage can retain one display indefinitely, for simultaneous display with waveform from items under test.
- **Automatic adjustment of amplifier gain** to optimize noise performance.
- **Automatic selection of optimum sweep speed.**
- **With the 5Hz filter,** signals 100Hz from a response at 0dB can be measured to better than -70dB.

Such speed and accuracy must be seen to be believed, call us for an enlightening demonstration.
DATA PROCESSING

System samples action of computers

Tesdata Systems, 7900 Westpark Dr., McLean, VA 22101. (703) 790-5580. $115,000 to $178,000.

Alpha Series of computer-performance management systems continuously sample performance of computers. They give real-time displays and report generation as system troubles occur. Each system operates in foreground/background via a disc operating system; continuous performance measurement data are stored on disc in the foreground, while system planning and trend reports are being generated in the background.

CIRCLE NO. 384

CRT terminal is TTY-compatible

Ann Arbor Terminals, 6107 Jackson Rd., Ann Arbor, MI 48103. Sarah Freeman (313) 769-0926. $1620; 8 wk.

A TTY-compatible CRT terminal, Model 400D, is available with upper/lower-case display of double-size characters. Its refresh memory stores five pages in a 50-line by 40-character format. Ten lines of 40 characters are displayed at one time, with the remaining 40 lines accessible in either roll or scroll modes. Characters are written in a 7 x 10 dot matrix in a 10 x 12 dot field. The unit comes with RS232 data interface and RS170 video output for driving auxiliary monitors. Four case options are available.

CIRCLE NO. 385

Emulation unit allows mini to use IBM devices

Information Products Systems, 6565 Rookin, Houston, TX 77074. (713) 776-0071. $15,150; 8 wk.

The Selector Channel Emulation Unit (SCEU) increases a medium-scale minicomputer system's performance by allowing attachment of IBM (or IBM plug-compatible) peripheral devices. The SCEU generates the protocol sequences required by the IBM peripheral control unit in response to the operational commands of the minicomputer CPU. It also converts the IBM selector channel's 8-bit data path into the appropriate word-path size for its host CPU; either a 16-bit or a 32-bit word. The SCEU supports up to 255 different device control units at combined data transmission rates in excess of 2.4 Mbytes/s.

CIRCLE NO. 386

Line monitor accepts full duplex data

Epicom, Altamonte Springs, FL Roy Ostrander (305) 869-5000. $3300.

A communications line-monitor, known as EPIVIEW, accepts full duplex data in either synchronous or asynchronous modes at speeds up to 100 kbits/s. Data are CRT displayed in ASCII, EBCDIC or hexadecimal codes. Other line disciplines are optionally available. It displays data on an integral 5-in. CRT, with selected segments accented by character blinking and/or reverse imaging. The instrument will also drive an optional 9-in. or 12-in. auxiliary CRT.

CIRCLE NO. 387
Our LED lamps are brighter by design.

It's no accident that our LED lamps are as bright as incandescents. We designed them that way. We also designed them to last ten times longer. At least ten years at 20 milliamps. They're designed to use only half the power of an incandescent. To operate either pulsed or continuous without life loss. To respond to short pulses that elude incandescents. We designed them to give you a bright replacement for incandescents. In a proven solid state package. Ready for immediate delivery. From sophisticated computer control panels to simple telephone pushbuttons, our Brite-Lite® LED lamps give you high reliability and longer life. Whatever your size or display requirements, there is a Brite-Lite for you. In red, amber or green. Transparent or translucent. With built-in resistors to handle up to 48 volts. From midget flanged snap-ins to space saving T² Lites. Now's the time to switch to our super bright Brite-Lites.

Our LED lamps are the brightest. And, when you are ready to select lamps, don't select them by accident. Give us a call and you'll see why Digital Equipment Corporation, the largest minicomputer manufacturer, has switched to the brightest LED lamps in the business.

"The brightest LED lamps in the business."

DATA DISPLAY PRODUCTS

303 NORTH OAK STREET, INGLEWOOD, CA 90301
TELEPHONE (213) 677-6166 • TWX 910-328-7205
Multiplexer cuts cost of data-line use


Model DA data-acquisition system is a multichannel signal conditioner. It accommodates from four to ten information channels, providing signals for the digital indicator. An auxiliary output signal from each channel is available to drive remote devices. Each channel is provided with a single PC board that plugs into connectors, supplying transducer excitation and a continuous output of 0 to 1 V. Each board has zero and span adjustments. They also include a channel selector and a digital readout in percent of full load or appropriate engineering units.

CIRCLE NO. 391

System puts 256 kbytes into mainframe memory

Interdata, 2 Crescent Pl., Oceanport, NJ 07757. (201) 229-4040.

A 16-bit processor, Model 8/16E, addresses up to 256 kbytes with its integral memory-management hardware. It has 16 general-purpose registers, an IBM-like instruction set, list processing instructions, dual I/O bus and 255 automatic I/O channels. Memory is available in 32-kbyte increments with an access time of 275 ns and cycle time of 750 ns.

CIRCLE NO. 390

Multichannel system monitors ten transducers

System quickly finds communication problems

International Data Sciences, 100 Nashua St., Providence, RI 02904. (401) 274-5100. $9975; 8 wk.

Hawk 4000 Datatrap uses a µP, and lets you diagnose data-communication problems quickly. It is interactive and can monitor, transmit, and receive data between a modem and a terminal on a 9-in., 512-character screen. 2000 characters can be trapped and stored for later recall and study.

CIRCLE NO. 389

Acoustic coupler uses telephone handset

Anderson Jacobson, 521 Charcot Ave., San Jose, CA 95131. Wayne Seppler (408) 263-8520.

A Bell-compatible 103 and 202-mode acoustic coupler and modem in one unit, Model 1245 optimizes the transfer of low and medium speed data over normal voice-grade phone lines using an ordinary telephone handset. It will interface with any EIA terminal and communicate acoustically at 0 to 450 baud in 103 mode and 0 to 1200 baud in 202 mode. The user may switch-select between these two modes with the coupler automatically adjusting baud rate and interface protocol. It can also function as a slave unit to a remote 202 modem, and simultaneously provide a 103 half-duplex interface to the terminal at up to 1200 baud.

CIRCLE NO. 393

You can't get in without a card

Schlage Electronics, 1135 E. Arques Ave., Sunnyvale, CA 94086. (800) 538-1755.

Effective, reliable security without card slots or pushbuttons is possible with the Model-414 access control system. It operates by proximity. Credit-card-sized command cards activate access doors or gates when held within 4 in. of a concealed sensor. The system controls access for up to 8 locations, and includes control units, sensors, system programmer, command keys, and optional printer. The programming unit's memory contains more than 1000 key codes. If a key card is lost, the 414 can be quickly reprogrammed to prevent a card's future use. The system's printer logs all accesses and attempted accesses by recording the key code, date, time of entry, and door number.

CIRCLE NO. 394
Opening new frontiers with electro optics

Hi-speed IR emitters with removable caps for low-loss coupling.

With the cap off, you can bring your fiber or bundle right down into very close proximity to the 6-mil GaAlAs edge emitter to maximize coupling efficiency. Along with very high collection efficiency, you get 100 MHz min. analog bandwidth (C30119) or 40 MHz min. (C30123). Rated at up to 200 mA forward current for continuous operation and 1.5 A peak forward current for pulse operation, these devices are available from stock. Hermetically sealed version also available.

IR emitters with output "pigtails." We've done the coupling for you.

Here we've made your job even easier. You can now couple your fiber or bundle to a fiber optic cable extending 5 inches from the source. At the source end, we've already made an extremely efficient internal optical connection. Like the C30119, the C30133 emitter gives you 100 MHz min. analog bandwidth. It's rated at up to 200 mA forward current for continuous operation, 1 A peak forward current for pulse operation.

Solid-state CW lasers: high power output for better coupling efficiency.

It takes less than a watt to get at least 5 mW of continuous lasing from these breakthrough solid-state lasers, which operate at room temperature. They have a rise time of less than 1 ns—allowing modulation rates well beyond 100 MHz. This plus small source size (13 x 2 μm typical) and 820 nm wavelength make them especially well suited to single fibers as well as bundles. Choose either the C30130 (OP-12 package) or the C30127 (OP-A package).

Avalanche detectors now with integral light pipes for efficient coupling.

At the receiving end too, we make efficient coupling easy. With our silicon avalanche photodiodes you secure the fiber or bundle through a hole in a mating connector (also available from RCA) and screw down the sleeve. Our detectors C30903E through C30908E give you a choice of light-pipe diameters, .25mm to 1.25mm, providing broad spectral response ranges, 400 to 1100 nm typical. All offer fast response time (0.5 to 2 ns typical) and high quantum efficiency (typically 77% to 85% at 830 nm). Also available: detector preamp modules and temperature compensation units.

If electro optics can solve your problem, remember: EO and RCA are practically synonymous. No one offers a broader product spectrum. Or more success in meeting special needs. Call us for design help or product information. RCA Electro Optics, Lancaster, PA 17604. Phone 717-397-7661. Sunbury-on-Thames, Middlesex TW16 7HW, England; Ste. Anne-de-Bellevue, Quebec, Canada; Sao Paulo, Brazil; Hong Kong.

RCA

ELECTRONIC DESIGN 24, November 22, 1977
At Power/Mate, fast delivery of open frame power supplies is an open-and-shut case.

Power/Mate can deliver open frame supplies faster than anyone else in the business. And that’s a fact! Our Econo/Mate II series is available in single, dual and triple output models with all the built-in reliability you’ve come to expect from Power/Mate. But for all its quality features, a Power/Mate open frame supply is still, most of all, economical. We wouldn’t call it Econo/Mate if it wasn’t.

Our Econo/Mates are stocked in-depth, along with our switching-regulated, miniature, modular, sub-modular and lab supplies. All ready for immediate delivery from our East or West Coast plants. And Power/Mate stands behind each and every power supply we make. We’ve been doing it for fifteen years. So if you’re looking for a power supply today, from a company who will still be here tomorrow, look no further. Call Power/Mate.

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Wayland, MA 01778 617-358-2777

CIRCLE NUMBER 123

CIRCLE NUMBER 124

DATA PROCESSING

Film scanner/plotter has large format

Optronics Int., 7 Stuart Rd., Chelmsford, MA 01824. (617) 256-4511. $50,000; stock.

Photomation Mark II Model P-1700 is a high speed, large format, digital film scanner/plotter used for digitizing, manipulating, enhancing and reconstructing graphic/photographic imagery. It has an I/O terminal and a 17 x 22-in. format rotary-drum scanner/plotter that allows the operator to move, delete, crop, size, position and automatically align items. It can add rules, screens and other tonal effects including compensation for shade and contrast.

CIRCLE NO. 395

Dispersed processor uses two diskette drives


The Model-1500 diskette-based dispersed processor has a typewriter-style keyboard, two diskette drives, high-speed video display and integral communications facilities. The keyboard provides 76 key positions, including a basic 55-key alphanumeric group, a 10-key numeric pad and five programmable function keys. The numeric pad allows high-speed entry of pure numeric material, while the function keys provide a means of generating program-control commands. Each of the two diskette drives provides storage capacity of 250,000 characters. The processor contains 32 kbytes of RAM, with an additional 4 k of system ROM. System memory provides complete support for communications I/O, display and keyboard logic, an optional serial printer, and diskette I/O.

CIRCLE NO. 396
Correct on both counts.
More Fluke logic test systems are in production and service applications than anyone else's. And more are shipped each month. Two ways of saying we're #1.
And, our customers spent less getting us there than they could have with anyone else. That makes us #3 on average cost.
But low front-end cost is only the start. You'll get lower programming, training and start-up costs than you thought possible. The highest test rates in the business, too, because boards run at rated speeds, including dynamic μP boards at multi-MHz rates.
More importantly, you'll test with confidence. If your board passes our tester, it'll work in your system. It's that simple. And reliable; more Fluke systems sold prove it.
The heart of our 3040A is a new merged sequence technique which lets you mix your test codes with automatically-generated sequences. And the best simulator around: your own known-good board. And dynamic LSI/fault isolation, automatic, manual or both!
Fluke hasn't forgotten about the bad boards either. After the tester nails the bad ones, we automate the troubleshooting. Our Autotrack® computer-guided troubleshooting leads the operator to the fault. With the new 3041A programming station, you describe the board onto a floppy disk and the 3040A does the rest.
The 3040A, with up to 240-pin capability, is $60,000 to $95,000*, depending on option configuration.
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Call (415) 965-0350, collect. Ask for the complete story on our high-ranking Logictest® family, or the location of the closest Fluke office.
Or, write: Fluke Trendar, a subsidiary of John Fluke Mfg. Co., Inc., 630 Clyde Ave., Mountain View, CA 94043.
In Europe, write: Fluke (Nederland) B.V., P.O. Box 5053, Tilburg, The Netherlands. Phone: (013) 673-973. Telex: 52237.

*U.S. price only.

Command Performance: Demand Fluke Logic Test.
DATA PROCESSING

Controller runs CDC disc drives

Datum, 1363 S. State College Blvd.,
Anaheim, CA 92806. Bob Cohen (714) 533-6533. 4 wk.

The Model 4091, an Embedded Storage Module Disc Controller, provides an interface to the Control Data storage module series (or equivalent) disc drive from a computer. A single board and occupying one CPU slot, the controller will operate using Data General software or Datum-supplied software drivers. The controller will handle two storage module series disc drives with the capability of mixing or matching drives. The µP-based controller can monitor and control events, execute commands, perform alternate-track selection, and do on-the-fly CRC generation.

CIRCLE NO. 397

Terminal displays dual-intensity characters

Honeywell Information Systems, 200 Smith St., Waltham, MA 02154. (617) 890-8400. $1,980.

Asynchronous display terminal, VIP 7200, features a 1920-character, dual-intensity display capability. It is for use as a conversational teleprinter-compatible work station for use with Honeywell's Level-6 minis, and other Series-60 systems, for such applications as time-sharing with large Level-66 computers. In addition, it can communicate with Series-2000 and 6000 systems. Full cursor movement across 24 lines of display is provided. The keyboard includes 86 keys arranged in alphanumeric and numeric groups. They can generate 128 ASCII codes. Transmission rates vary at standard increments between 75 and 9,600 bits/s. The terminal includes both 20-mA current-loop and RS232C interfaces.

CIRCLE NO. 398

Processor has floppy software for easy growth

NBI, 5593 E. Arapahoe Ave., Boulder, CO 80303. (303) 444-5710. $11,990.

A software-based word processing system offers users application flexibility plus the performance of expensive hardware-based systems. The System I provides first-time users with an economical and easily upgradeable approach to automating the production of high-volume correspondence as well as document editing and production. It allows users to update applications by entering software changes on the system's standard diskette that stores approximately 250,000 characters, or about 50 pages of text. Hardware elements include a typewriter keyboard, a CRT display, and a high-speed “daisywheel” printer that operates at 30 char/s.

CIRCLE NO. 399

SHERLOCK OHMS & DR. WATTS

MM300 Digital Multimeter

CIRCLE NUMBER 126

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CIRCLE NUMBER 127
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POWER SOURCES

New power-supply package concept is hatched


The CM2.15.100, a ±15-V, 100-mA power supply, uses a new packaging concept—a recessed barrier strip that uses a minimum of space and also provides added protection against breakage and accidental shorting of leads. Another feature is the use of thru-holes for bolting the unit to a chassis as well as molded-in threaded inserts. Line and load regulation is 0.01%. Noise and ripple are less than 1-mV rms and the stability is better than ±0.01%/°C. Size is 3.7 × 2.7 × 1.4 in.

High-power transformers suppress noise

Topaz Electronics, 3855 Ruffin Rd., San Diego, CA 92123. (714) 279-0831.
Isolation and noise-suppression transformers, and ac regulator systems having 98% efficiency, protect sensitive equipment against line noise, transients, spikes and voltage fluctuations. A box-shielded design is used to assure maximum attenuation of power-line interference caused by switching spikes, lightning strikes and other line transients. Transformers are available for 50/60-Hz operation in power ratings of 75, 100, and 130 kVA for all standard 3/δ operating voltages. The regulators have a frequency range of 47 to 63 Hz, and less than 0.1% distortion. They are available in 50, 75, and 100-kVA ratings.
"... well-organized, extremely well written... highly recommended for practicing engineers..."

IEEE Transactions

DIGITAL SIGNAL ANALYSIS
Samuel D. Stearns
This is an ideal master handbook on today’s signal processing procedures and systems, containing recent advances, new design material, and a comparison between continual and digital systems that’s extremely helpful to newcomers to the field. Featuring a foreword by Richard Hamming, the book contains a review of linear analysis; sample-data systems; analog-to-digital and digital-to-analog conversion; the discrete Fourier transform and the fast Fourier transform algorithm; spectral computations; non-recursive and recursive digital systems; computer simulation of continual systems; analog and digital filter designs, and more. 288 pages

"Jacobi’s book is great... a new, original, readable, usable book on writing for business and professional people..."


WRITING AT WORK: Dos, Don’ts, and How Tos
Ernst Jacobi, Xerox Corporation.
This guide to better writing follows its own principles by being lively, informative, and easy to read. More than a collection of pat rules and formulas, the book is a storehouse of practical advice for business and professional people to make their writing sharper, more interesting, and more informative. It shows you how to overcome procrastination and change your entire attitude toward writing, making it easier and more enjoyable for you! 208 pages

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CIRCLE NUMBER 132

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KSW Electronics Corp.
SOUTH BEDFORD STREET, BURLINGTON, MA 01803

CIRCLE NUMBER 133

MODULES & SUBASSEMBLIES

Hi-rel d/a's multiply 10 and 12 bits

ILC Data Device, Airport International Plaza, Bohemia, NY 11716.
Myron Anatole (516) 567-5600

MDA100 and MDA120 are two high-reliability, four-quadrant, multiplying hybrid d/a converters. MDA100 is a true 10-bit unit with a full 10-bit linearity. MDA120 is a true 12-bit unit with a full 12-bit linearity. They have pull-up resistors for logic compatibility and a welded-lid package.

Ssense rf power over wide band

Olektron, 6 Chase Ave., Dudley, MA 01570. (617) 943-7440. $75; stock to 3 wk.

Model P3-PS4-1004 broadband rf power sensor has a frequency response of 30 to 400 MHz and an accuracy of power detection of ±10% of incident rf power, for a temperature span of −54 to +70 C. It produces a dc output that is proportional to the input power, and provides a dc output of 1 V across a 5-k termination for an input signal or reflected signal level of 15-W CW. It is available in octave and decade bandwidth, and its dc output can be used for feedback leveling systems. The insertion loss is 0.35 dB (max), VSWR is 1.1:1 and input/output impedance is 50 Ω.

CIRCLE NO. 405

CIRCLE NO. 406

ELECTRONIC DESIGN 24, November 22, 1977
Superb characteristics and high-density processing

TDK has a whole range of materials for ferrite cores that go into high-performance transformers and filters for communications equipment. These cores help enhance the performance of the equipment, and make it more compact. Standard materials are available in 22 kinds, and you can find superb performances in permeability, in loss or in power. These materials are formed into various shapes including TDK-developed EP cores as well as quality products that conforms to IEC standards.

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Our high-level magnetic material technology gives us a claim to world fame as a broad-line manufacturer of electronic parts and you’ll find us on virtually all of the world’s leading markets. You’ll also find our products in automobiles, medical equipment, business machines, industrial equipment and many more.
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CIRCLE NUMBER 136

MODULES & SUBASSEMBLIES

Cassette-tape transport uses ac capstan-motor

Triple I, 4605 N. Stiles, Oklahoma City, OK 73118. (405) 521-9000. $149.

A fixed-speed cassette-transport with an ac capstan-motor features four-motor control, remote-control capability, fast start/stop, less than 30-s rewind, and speeds from 1 to 10 ips. Four separate motors control take-up, rewind, play or record, and head engagement. Flutter, wow, and jitter are minimized by the capstan drive. Control boards are TTL, DTL and CMOS compatible plus they contain all circuitry for proper control.

CIRCLE NO. 407

System element improves on isolation amps

Dynamic Measurements, 6 Lowell Ave., Winchester, MA 01890. (800) 225-1151. $195; 2 wk.

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CIRCLE NO. 408

ELECTRONIC DESIGN 24, November 22, 1977
The Ansley "D" Connector...

Our new series of male and female "D" connectors offer you a cost effective external mass termination cable and connector system second to none. Its uniqueness begins with a one-piece "D" connector package that meets industry standards for size, pin spacing, and contact reliability. With no loose parts to match up, positive cable-to-contact alignment is assured. Conductors are mass terminated in seconds with our standard BLUE MACS™ hand or bench tools. The results? Faster installation, higher reliability.

Contact pins are spaced on .0545" centers — a perfect fit for any standard inter-cabinet "D" type connector application. Our new "D" connectors are designed to mate with standard .050" pitch flat cable as well as our new, improved jacketed cable — the only flexible flat cable engineered specifically for out-of-cabinet use.

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The Ansley BLUE MACS™ jacketed cable is U.L. listed for external interconnection of electronic equipment. Electrically, it outperforms standard jacketed twisted pairs in typical I/O applications. And there's no special zipper lock tubing required — reducing the need for an extra cable accessory. Installation is faster, easier. And like all Ansley connectors, you can daisy chain our "D" types anywhere in the cable — along with our DIP socket, card edge, or pc board connectors.

Cable alignment and high contact reliability is assured — because both cable and connector are grooved for absolute alignment. Our patented TULIP™ 4-point insulation-displacing contacts are permanently fixed and sealed-in to provide a reliable, gas-tight, corrosion-free mass termination.

For the full reliability/cost effectiveness story and technical data, call or write:

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The shorter units have delay time-to-rise time ratios of about 4:1; the longer
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CIRCLE NO. 410
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CIRCLE NO. 411

MODUL ES & SUBASSEMBLIES

Recorder stores 350,000 characters on one track

Columbia Data Products, 6655 Amberton Dr., Baltimore, MD 21227. Don Knight (301) 796-2800. $1295; 6 wk.

Write-only drive, Model 300W, uses a data cartridge that can store over 350,000 characters in a single track. Tapes can be written in 128 or 256-character blocks with a 16-bit CRC-check character as required by the ANSI standard. Tapes generated can be read with ANSI-compatible data cartridge readers. Input buffers will accept incremental 8-bit parallel data or asynchronous serial data via RS232 or current loop. Max speed is 2500 characters/s with parallel data, and is switch selectable up to 19.2 kbaud with serial data.

CIRCLE NO. 412

8-channel FM recorder takes dc to 100-Hz data

A.R. Vetter, P.O. Box 143, Rebersburg, PA 16872. Art Vetter (814) 349-5461. $2300.

The Model C-8 FM recorder records and plays eight channels of dc to 100-Hz analog data on a standard Philips cassette. The recorder uses the full width of the cassette tape and operates at 1-7/8 ips. The three-motor transport features a closed-loop dual-capstan drive, producing under 1% pk-pk flutter noise. Also included is a voice-override channel with microphone and built-in speaker. A VU meter monitors the voice channel and a pk-responding meter monitors the FM channels.
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ELECTRONIC DESIGN 24, NOVEMBER 22, 1977
**Analog multiplexer takes 31 signals per channel**

A µP-based analog multiplexing system (SAM) can simultaneously accommodate up to 31 independent analog signals per voice channel. Program control permits the system to send or receive signals to or from telemetry instrumentation over a single tone-transmission voice channel. Accuracy of the analog output reproduced at the receiving station is 0.35% of full scale. Although the basic unit handles up to four analog signals, it can be expanded to handle 31 separate signals per voice channel.

**CIRCLE NO. 413**

**13-bit a/d converter meets MIL STDs**

Zeltex, 940 Detroit Ave., Concord, CA 94518. R. Terry (415) 686-6660. $745 (100 qty); 30 days.

The 13-bit a/d converter, ZAD3213, meets the requirements of MIL-STD-883, Level B. The encapsulated-in-metal module is only 2.12 x 4 x 0.45 in. Four mounting ears permit attachment to bulkheads or PC boards. Features include a max conversion time of 100 µs, max differential nonlinearity of ±1/2 LSB, input range is 0 to 10 V. Output coding is unipolar binary. Operating range is −25 to +100 C; storage: −55 to +125 C. The converter withstands pk shock of 350 G's and vibration to 20 G's.

**CIRCLE NO. 414**

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Other STACO Company products: Custom Transformers, STACO, INCORPORATED, Richmond, Indiana; Variable Transformers, STACO, INCORPORATED, Dayton, Ohio.
**Motor driver/controllers operate in six modes**

The M6128 and M6128PG motor drivers, and MC6128 and MCL6128 motor controllers, are all six function units in one. Each unit features multimode excitation allowing a choice of single, dual, or half-step excitation and is capable of driving 3 or 4 phase stepper motors. They include a 24-V dc at 13-A power supply. The MCL6128 adds a control logic and an internal blower for cooling. The control logic provides for stop, forward/reverse, and speed adjustment.

**Readout assembly uses fiber optics**

Model 905-H Display Fiber Optic Readout Assembly meets MIL-STD-883 Level B, is nonencoded and features an internal decoder. Light-emitting diodes transmit through fiber-optic tubes to produce a 0.43 in. high character display on the 0.5 by 0.62-in. display screen. The screen is a 7-segment display with 0 to 9 numeric capability that also includes plus, minus, decimal point and limited alphabetical characters.

**Dot-matrix printer goes at speed of 120 cps**

The Model 702 is a 120-character-per-second, 132 column, bidirectional, logic seeking, impact, serial printer. It features a standard 7 x 7 dot-matrix pattern and offers four others (5 x 7, 9 x 7, 7 x 9, and 9 x 9) as options. Printed-data format consists of 10 characters-per-inch horizontally and operator selectable 6 or 8 line-per-in. vertical spacing with either a 2, 8, or 12-channel electronic vertical-format unit.

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<th>ROW-TO-ROW DIMENSION</th>
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<td>TC-8</td>
<td>.3 in.</td>
<td>923695</td>
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<td>TC-14</td>
<td>.3 in.</td>
<td>923698</td>
<td>$ 4.50</td>
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<td>TC-16</td>
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<td>923700</td>
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<td>TC-16LSI</td>
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<td>923702</td>
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<td>TC-18</td>
<td>.3 in.</td>
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<td>TC-20</td>
<td>.3 in.</td>
<td>923704</td>
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<td>TC-22</td>
<td>.4 in.</td>
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<td>TC-28</td>
<td>.5/6 in.</td>
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<td>TC-36</td>
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<td>TC-40</td>
<td>.5/6 in.</td>
<td>923722</td>
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Microhybrid device is two-quadrant divider.

SGR, P.O. Box 391, Canton, MA 02021. Ann Ripley (617) 828-7773. $49 to $160.

A series of microhybrid dividers that interface with µP-based systems is comprised of a transconductance dividing element, stable reference, output amplifier with specified accuracy internally trimmed for feedthrough output zero and gain trim. The 503 through 506 divide in two quadrants with a transfer function of \(-10X/Y\). They are specified for dividing errors of 1%, 0.5%, 0.25% and 0.1% at 25°C. The output provides \(+10 \text{ V at 5 mA. Small}

CIRCLE NO. 418

**Data Logger Prints 10 Channels, 4 1/2 Digits**

Datel Systems, 1020 Turnpike St., Canton, MA 02021. Gene Murphy (617) 828-8000. From $1395; 4 to 8 wk.

The 10-channel 4 1/2-digit printing data-logger, PDL-10, is miniature and inkless. The device has a crystal-controlled conversion clock for high rejection of 50 or 60-Hz line noise. A relay multiplexer and selectable-gain amplifier offer individual range settings for each channel of \(\pm1.9999 \text{ or } \pm19.999 \text{ V dc. Over-all sampling and printing occurs at } 1 \text{ sample/s. The range-selecting}

CIRCLE NO. 419

**Tickets—Labels—Multiple Forms Victor Has the Printer for You.**

Seats—Labels—Multiple Forms Victor Has the Printer for You.

A low cost, reliable printer, backed by Victor's one year warranty, offers the solution to your printing problems. The Victor line of sprocket-feed printers for labels, tickets or pre-printed forms provides outstanding legibility combined with proven reliability.

The 5000-463 series offers you three choices of interface: parallel; RS232C or TTY current loop. This allows the printer to be connected directly to most computers or microprocessors.

The printer prints 64 ASCII alphanumeric and symbolic characters. By sending the proper command code, characters can be expanded, printed in red or both for highlighting or headlining.

There are no moving parts when the unit is not printing which keeps the noise level down and increases reliability since the printer is not wearing itself out while sitting idle.

The dot matrix printing mechanism in the sprocket feed printer is similar to those used in almost 500,000 Victor print mechanisms in use today.

CIRCLE NUMBER 153
**MODULES & SUBASSEMBLIES**

**Receiver takes dual-tone and gives BCD out**

GTE Automatic Electric, P.O. Box 2059, Northlake, IL 60164. (312) 562-7100. $105.

A touch-tone calling receiver, Model WA-1490-A, accepts inputs of two out of eight standard dual-tone multi-frequency signals and provides binary-coded electronic outputs. Totally contained on an 18-pin standard-sized card, it is a stand-alone receiver, usable wherever detection of DTMF signals is required. All DTMF receiver functions are incorporated on the single PC card. Meeting standard telephone signaling requirements, the receiver can be used in computer terminals, remote control systems, or other applications using DTMF signaling.

**New CODI Precision Voltage Reference Diodes. Including a 2 mA alternative to the 7.5 mA Motorola MZ 605.**

You’re assured of prompt delivery of the CODI series of low noise, ultra-stable Precision Voltage Reference Diodes...including diodes equivalent to the Motorola MZ 605 (rated at 7.5 mA, stability 30 uV/1000 hr, and 5 PPM/1000 hr).

The CODI PRD family of diodes is more than equivalent; it’s available at either 7.5 mA or 2 mA for lower power consumption...but the price is the same. Other features of this series include guaranteed stability over one year, noise 1 PPM of output, and 1 PPM temperature coefficient (+25°C to +45°C).

When you’re looking for extremely stable, low noise reference diodes, check CODI before you select. Ask for Bill Henderson.

**Scan 10 temp sensors with a/d converter**

San Diego Instrument Lab, 7969 Engineer Rd., San Diego, CA 92111. (714) 292-0646. $595 (10 qty).

A 10-channel modular RTD scanner in a card-mounted, shielded package, the SL115 connects 10 platinum-resistance thermometers directly to a user’s high-level a/d converter. The scanner excites, lead compensates, continuity tests, linearizes, amplifies, and filters the signals. Segment-free linearization is for all platinum R-vs-T standards. Remote-calibration features give on-line calibration of the scanner at the ice point and, optionally, at any span point. DTL/TTL/CMOS compatible control logic receives commands from microprocessors, minicomputers, or toggle switches. Scan rates up to 20 channels/s are available.

**Monitor prints-out time of power-line fault**

Consultronics, 38 Le Page Ct., Downview, Ontario M3J 1Z9. (416) 630-0564.

Power Line Disturbance Monitor, Model FDM-2, monitors voltage and frequency on single or three-phase power lines and prints out exact time and duration of a fault. Features include: battery standby, adjustable thresholds, testpoints for oscilloscope display, and alarm. Also included are an optional clock display showing month, day, hour, minute and the alarm on-off and acknowledgement, nominal line-voltage selector and a self-check button to verify correct operation.
Networks Save Money
Networks are in big-volume demand for one simple reason. Compared with discretes, they save. They save on assembly costs. They save PCB board space. They save on inventory. They save on inspection and testing. They save on ratio matching. And they can save installation errors.

Centralab knows networks. We pioneered thick film networks back in 1945. Since then we've produced millions. In fact, we've delivered more than 200,000,000 units.

Now, Save More With CERBON™
Centralab SIP thick film networks are now available with CERBON™ — Centralab's patented resistor system. CERBON costs substantially less than cermet, yet it is measurably superior to carbon composition in critical areas. See chart below for some typical performance comparisons.

Give a Little — Get a Lot!
If you've wanted to use networks to enjoy their many benefits, but couldn't justify the cost, consider this: CERBON meets or exceeds the performance requirements of over 85% of all resistor applications. So, if you can give a little on the precise tolerances of cermet — which you may not need — CERBON networks from Centralab can get you all the cost-saving benefits of networks — at a price you can afford.

For More Information:
Whether your needs are for standard off-the-shelf SIP resistor or resistor/capacitor networks, or for custom hybrid designs, we will show you how you can save with CERBON. Talk to your Centralab Representative, or call (414) 228-2874, Centralab Circuit Product Sales.

**Compare CERBON Resistors With Carbon Discretes**

<table>
<thead>
<tr>
<th>Measurement</th>
<th>Typical 1/4 Watt Resistors</th>
<th>Carbon Composition (MIL-R-11F)</th>
</tr>
</thead>
<tbody>
<tr>
<td>TCR (ppm/°C)</td>
<td>Centralab CERBON</td>
<td>Carbon Composition (MIL-R-11F)</td>
</tr>
<tr>
<td></td>
<td>-250 @ -55°C</td>
<td>±800 @ -55°C</td>
</tr>
<tr>
<td></td>
<td>-350 @ +105°C</td>
<td>±625 @ +105°C</td>
</tr>
<tr>
<td>Quantec Noise (0 db = 1µV/V)</td>
<td>-7 db max</td>
<td>0 to +10 db (not specified in MIL-R-11F)</td>
</tr>
<tr>
<td>Short Term Overload (±ΔR max.)</td>
<td>+0.1</td>
<td>±2.5</td>
</tr>
</tbody>
</table>
F/v converters cover wide input range

Solid State Electronics, 15321 Rayen St., Sepulveda, CA 91343. Ed Polit (213) 894-2271.

Freqmeter is an encapsulated solid-state unit that linearly converts frequency or repetition rate of input signals to proportional dc voltages. Four standard models span an input frequency range from 0 to 100 kHz. The output is insensitive to supply voltage, temperature, input amplitude or waveforms and will function when driven with sine, square and triangle waves or pulses. These converters respond to the average frequency of random signals.

CIRCLE NO. 423

Vhf crystal osc is stable to $1 \times 10^{-9}$/day

Vectron Lab, 121 Water St., Norwalk, CT 08854. Larry Jawitz (203) 853-4433.

The Model CO-220 vhf crystal oscillator provides long-term stability of $1 \times 10^{-9}$/day at any fixed frequency to 200 MHz. This stability is achieved by the use of a crystal in the 10-MHz area, followed by internal multiplication. The oscillator generates an output level of +7 dBm with +13 dBm optional. Temperature stability to $\pm 5 \times 10^{-9}$, from 0 to 50°C, is achieved by housing the oscillator in a proportionally controlled oven. Options include operation from -55 to +75°C and voltage frequency control to permit phase locking onto an external reference or for remote frequency control.

CIRCLE NO. 424

Indicator monitors process signals

ElectroSyn, 480 Neponset St., Canton, MA 02021. Charles Earle (617) 828-2840.

Voltage or current signals from any process variable, such as pressure, flow, or level, can be monitored by the Model 9000. It remembers indefinitely the highest (peak) value obtained. Interrogation provides digital readout of the peak and present values. Peak value memory is equipped with 0 to 100% FS adjustable setpoint control.

CIRCLE NO. 425

Bulletproof!

Babcock hi-rel relays meet their specifications in practice, not just on paper. Call us on it at (714) 540-1234.

Babcock Relays
An Esterline company, 3501 Harbor Blvd., Costa Mesa, CA 92626.
- Dry reed • Mercury wets • Military/aerospace
- Ultra hi-rel • Telephone • General purpose

CIRCLE NUMBER 156
Tiny fast pulser delivers 50 V

Avtech Electrosystems, P.O. Box 11426, Stn H, Ottawa, Ontario, Canada K2H 7V1. (613) 828-4823. $398 to $498; 4 to 6 wk.

Miniature pulse generators, in the AVI Series, provide high-amplitude flat-topped-pulse outputs up to 50 V when triggered by a low-level, slow-speed trigger pulse (TTL) and biased by a +15-V supply. The rise and fall times are 1 ns max. The pulse width is variable from 1 to 100 ns. An ultraminiature version is 2.25 X 1.38 X 1.13 in.

CIRCLE NO. 426

Pocket pulser senses circuit logic state

Continental Specialties, 44 Kendall St., Box 1942, New Haven, CT 06509. (203) 624-3103. $74.95 (suggested retail).

The DP-1 digital pulser senses circuit conditions and injects the proper pulse at a desired circuit node. The hand-held unit draws power from the circuit under test and the unit’s automatic polarity pulse sensing detects the circuit’s condition—high or low state—thus triggering the unit to produce an opposite polarity pulse. Trouble-shooting is accomplished by using the pulser to inject signals at key points in TTL/DTL, CMOS and other popular circuits. Testing with a single pulse or with 100 pulses per second is possible.

CIRCLE NO. 427

Video L-C lines delay up to 2075 ns

Allen Avionics, 224 E. 2nd St., Mineola, NY 11501. Lester Jacobson (516) 248-8080. $55 up; stock.

A series of 10 variable-delay units are passive L-C lines. The shortest delay is from 0 to 10.5 ns in 0.5-ns steps. The longest delay is from 0 to 2075 ns in 25-ns steps. Amplitude is flat to 5.5 MHz. The units come with toggle or rotary switches or terminals for strap-pable delay variations.

CIRCLE NO. 429

Thermal printhead prints 10 columns

Gulton Industries, 212 Durham Ave., Metuchen, NJ 08840. (201) 548-2800. From $57.05; stock to 8 wk.

The DM-1050 thermal printhead features nonimpact printing with the only moving part being the advance mechanism. Printing 10 columns, character-line speeds through 7 lps are possible printing a full 5 X 7 matrix character on standard 90-C heat-sensitive paper. Printheads are furnished ready for mounting. They include a soldered ribbon-cable and the heat-sink mounting permits ganging to extend the number of columns.

CIRCLE NO. 428

Cue three mag-tapes simultaneously

EECO, 1441 E. Chestnut Ave., Santa Ana, CA 92701. (714) 540-1234.

Microprocessor-based MQS-100 synchronizer systems can cue and synchronize any three video, audio or mag-film tape transports simultaneously. The SMPTE/EBU edit code, used for indexing of the tapes, need not be identical and tapes with drop-frame and nondrop-frame formats can be intermixed.

CIRCLE NO. 430

Call C. P. Clare and ask them why they charge twice our prices for mercury wetted relays. If you don’t like their answers—or their prices—call us at (714) 540-1234.

Babcock Relays

An Esterline company, 3501 Harbor Blvd., Costa Mesa, CA 92626.

- Dry reed - Mercury wets - Military/aerospace
- Ultra hi-rel - Telephone - General purpose

CIRCLE NUMBER 157
let's calibrate

Model 82

PRECISION STANDARD for AC/DC Voltage and Current
- Tests a wide range of analog and digital meters
- AC and Bipolar DC voltage ranges of 100mV, 1V and 10V
- AC and Bipolar DC current ranges of 100µA, 1mA, 10mA and 100mA
- Nominal accuracies of 0.01% DC and 0.05% AC
- Percent error deviation dial
- Frequency variable from 40Hz to 1kHz
- Four fractional scale division ranges

Measure or supply with one instrument
- AC or DC voltages from 10 mV to 1400V
- Current from 10 µA to 14A
- 10 cardinal resistance values from 0.01 ohm to 10 megohms
- 5-digit readout

GTE Box & Fitting Div., 1 Stamford Forum, Stamford, CT 06904. (203) 357-2000.
A PVC sectional box can be used to make 14 different outlet box configurations. The middle section of the box, No. ES-00, mates with any two of five end sections to form a variety of combinations. Available end sections include units with one ½-in. opening, two ¼-in. openings, one ¾-in. opening, two ¼-in. openings, and one blank unit. A complete box consists of a middle section and two end sections joined by PVC solvent-cement.

Automatic tool speeds crimping of connectors

Thomas & Betts, 36 Butler St., Elizabeth, NJ 07207. (201) 354-4321.
A series of automatic strip-fed tools installs insulation-piercing magnet-wire connectors at production speeds. The tools crimp a stripped stranded lead wire to an unstripped film-coated magnet wire, or crimp two or more magnet wires together, without needing their coatings removed. The insulation-piercing connectors used in the tools are on a continuous reel-mounted strip, and are available for a range of copper magnet-wire sizes from #26 to #15 AWG. The magnet wire and lead wire are inserted in the tool which is then actuated, crimping the wires together in just one step.

COMPLETE VOLTAGE, CURRENT & WATTMETER CALIBRATOR

For calibration of wattmeters from 0.05 watt to 14 kilowatts
- Consists of two Model 829G's and a Model 5058A Wattmeter Calibration Module
- Available as individual units or, as shown, in an attractive customized enclosure with work table.

USE PVC SECTIONALS FOR VARIETY OF OUTLET BOXES

Cole-Flex, 91 Cabot St., West Babylon, NY 11704. (516) 248-8150.
TF250 tubing, made with FEP Teflon, is suited for applications that do not require 500-F operating temperature. But it still has a high enough rating (400 F) for most high temperature applications. The TF series is recommended for those jobs that require better clarity, higher dielectric strength, better cold-flow characteristics or longer continuous lengths. It is considered a Class-H insulation and is solder-iron resistant. Dielectric strength is 2100 V/mil.

Use Teflon tubing for high temperatures

Series 6337 card-edge connectors contain contacts on 0.156-in.-center spacing with 0.025-in. square wire-wrappable terminals. The sizes offered cover 20, 44, 50, 56, 72 and 86-pin configurations. The insulator bodies are made of thermoplastic polyester per UL-94VO, and the contact material is phosphor bronze per QQ-W-321. Standard contact finish is gold over nickel. Current rating is 3 A max and contact resistance is 8 mΩ max. Insulation resistance is 5 kMΩ at 500 V dc and dielectric withstand voltage is 1500 V ac between adjacent contacts at sea level.

Card-edge connector uses wire-wrap terminals

CIRCLE NUMBER 158
Device-handler sorts bulk parts


Any device which can be fed down a track by gravity can be handled by the 380 Opto-Switch device-handler. Devices are fed down the track to a bulk-sort at the output. The sort section is the same for all devices, but the input section is custom made to feed and probe a particular device. It is hand-fed, has a go/no-go section and discriminator for polarity where possible. Bowl or magazine feeding is optional.

CIRCLE NO. 435

Cable-jacket remover is fast and safe

P.K. Neuses, P.O. Box 100, Arlington Heights, IL 60006. (312) 253-6555.

N-2077 cable-jacket remover is fast, safe and versatile. It will cut wires and cables, remove plastic and rubber-like jackets from cables of all diameters. In addition, the N-2077 can easily cut off fillers, and is ideal for use on shielded and nonround cables. The special top edge serves for cutting wires and cables while the longer bottom blade serves as a cutting guide. Specially designed edges on the blade avoid possible damage to conductors and problems with varying jacket thicknesses.

CIRCLE NO. 436

Card-edge connector clips to flat cable


Card-edge connector, CF-100, is for use with ribbon cable having 10, 20, 26, 34, 40 or 50 conductors on 0.05-in. centers. It provides a rapid means of connecting and disconnecting flat cable to 1/16-in. PC boards. A built-in strain relief is maintained within the connector profile and it can be permanently locked in place when a mounting flange is used. Specifications include: temperature rating of 105 C, a 1-A current rating and dielectric strength of over 500 V de at sea level. It accepts 28-30 AWG solid or stranded conductors.

CIRCLE NO. 437
Packaging & Materials

Edgeboard connector gives design versatility

Dale Electronics, E. Highway 50, Yankton, SD 57078. (605) 665-9301.

The EB8 line of MIL-C-21097C-type dual-readout edgeboard connectors are within the standard terminal grid pattern of 0.156 × 0.200 in. and provide a number of options for matching unit cost and uses. These options include a choice of three body materials—diallyl phthalate, phenolic and valox; plating options such as gold-plate, gold-flash and tin, contact choices including solder-eyelet, DIP-solar terminations in phosphor-bronze or beryllium-copper, and seven standard mounting methods. They are available in seven body sizes with 6, 10, 12, 15, 18, 22 or 25 contacts per side.

DIP socket has pins on IC side of board

Robinson-Nugent, 800 E. 8th St., New Albany, IN 47150. (812) 945-0211.

Gone is the confusion of trying to match an IC lead to a wire-wrappin g pin on the underside of a PC board. AS/U wire-wrapping DIP sockets save a great deal of time and trouble when breadboarding prototype circuits. AS/U socket pins are bent around to face the upper side of the socket. The sockets are available in 14, 16, 20, 24, 28 and 40-pin sizes.

Strain reliefs molded over flexible cables


A semi-custom strain relief for molding over flexible cables ranges in diameter from 0.13 to 0.18 in. The vinyl relief, PH-693, accommodates two to six-conductor cables. Designed to fit a 1/4-in. split-mounting aperture, the strain relief is flat on one side to prevent rotation.

CIRCLE NO. 438
CIRCLE NO. 439
CIRCLE NO. 440

Biggest DVM news of the year

You name it, Systron-Donner has it! Bench, portable and systems models for every conceivable 4½-digit DVM application. Every model is brand new, packed with all the features you could possibly want. Do you need a battery pack or an analog meter? Do you need to make dBm measurements on tones? How about BCD outputs or complete IEEE-488 interface capability? Systron-Donner's new series of 4½-digit DVM's offers all these capabilities and much more.

Classy new portables.

These rugged performers for field or lab use come with all five functions (DCV, DCl, resistance, and true RMS ACV and ACI) plus autoranging. Choice of DC accuracy of ±0.05% or ±0.02%. Also with or without dBm. Options: Battery Pack and analog meter.

<table>
<thead>
<tr>
<th>Model</th>
<th>DC Accuracies</th>
</tr>
</thead>
<tbody>
<tr>
<td>7141A</td>
<td>± 0.05%; 7141B ± 0.02%</td>
</tr>
<tr>
<td>7142A</td>
<td>± 0.05% with dBm capability</td>
</tr>
<tr>
<td>7142B</td>
<td>± 0.02% with dBm capability</td>
</tr>
</tbody>
</table>
Plugs terminate flat ribbon-cable

Insulation-displacement plugs terminate 0.05-in.-spaced laminated and extruded flat-ribbon cable. The plugs permit mass termination in one press operation and are offered in a selection of 14, 16 and 24-pin styles. A cover allows easy and quick removal for snap-on inspection or rework.

Circuit Assembly, 3169 Redhill Ave., Costa Mesa, CA 92626. Dick Foringer (714) 540-5490.

Pin-line headers are on 0.1-in. centers

Aries Electronics, P.O. Box 23, Frenchtown, NJ 08825. (201) 966-4096. 4¢ to 7¢/pin; stock.

Pin-line headers can be mounted side-by-side or end-to-end on 0.1-in. centers. Single rows of from 1-to-25 header positions in a glass-filled thermoplastic body are available with any of five styles of screw-machine terminals. Terminal pins can be either solder-tab or wire-wrap types with gold or tin plating.

Pin-line headers can be mounted side-by-side or end-to-end on 0.1-in. centers. Single rows of from 1-to-25 header positions in a glass-filled thermoplastic body are available with any of five styles of screw-machine terminals. Terminal pins can be either solder-tab or wire-wrap types with gold or tin plating.

CIRCLE NO. 441

CIRCLE NO. 442

CIRCLE NO. 443

RFL-shielded cases are in 14 sizes


Identified as the RFT series, cases are available in 14 basic sizes from 1 1/2 in. square to 3 X 6 in. in five heights ranging from ¾ to 2 ⅝ in. Shielding effectiveness is enhanced by close spacing of screws tapped directly into extruded-aluminum sidewalls.

CIRCLE NO. 443

---

A 4 1/2-digit DVM for every application!

Powerful bench instruments.

A workhorse series with all five functions, autoranging and a neat choice of options including BCD output, IEEE-488 bus, and rack mount. DC accuracy: ±0.02%.

Model Features
7241A 5 functions, 26 ranges
7244A with IEEE-488 capability

“Thin Line” for GPIB systems—under $1,000 loaded.

Here’s the first 4 1/2-digit DVM designed around the IEEE-488 bus. Model 7344A is a full rack width, but only 1 3/4” high. Everything comes standard: IEEE-488 interface, DC volts, true RMS AC volts, and rack mount. DC accuracy: ±0.02%. There’s nothing like it!

Get the full details on S-D’s “think ahead” DVM’s. Contact Scientific Devices or Systron-Donner at 10 Systron Drive, Concord, CA 94518. Phone (415) 676-5000.

CIRCLE NUMBER 160
FERRITE CORES
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SHAPES
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CIRCLE NUMBER 801

3M Brand Light Control Film Improves Readout Readability.

Microlouvers within the film enhance contrast, screen out ambient light. Works equally well on LED and CRT displays. For information on how you can use 3M Light Control Film in your product write: Visual Products Division, Industrial Optics, 3M Center, St. Paul, MN 55101.

CIRCLE NUMBER 804

WHO MAKES WHAT & WHERE TO FIND IT

Volume 1 of Electronic Design's GOLD BOOK tells all. And, when you look up an item in its PRODUCT DIRECTORY you’ll find each manufacturer listed COMPLETE WITH STREET ADDRESS, CITY, STATE, ZIP AND PHONE. Save time. There's no need to refer elsewhere to find missing information.

IT’S ALL THERE in Electronic Design GOLD BOOK

Send for information today!
A. W. HAYDON CO. PRODUCTS

NORTH AMERICAN PHILIPS CONTROLS CORP.

FOR INFORMATION, CIRCLE 802
FOR IMMEDIATE, CIRCLE 803
Copper-clad substrate is dimensionally stable


Mykroy-clad is a copper-clad glass-bonded-mica (ceramic) material for PC boards that is dimensionally stable from -270 to +750 F. The material neither outgases nor absorbs gases, because it is inorganic. It resists nuclear, X-ray and microwave radiation and is impervious to moisture with a low loss factor. It is available in standard panels 13 x 19 in. and in thicknesses of 1/16 and 1/8 in. One or two sides are clad with all standard copper foil thicknesses. The price of a 1/16-in. thick standard-sized panel (13 x 19 in.), 1-oz copper clad on one side is $150.

CIRCLE NO. 444

Air-temp source conditions PCs or parts

Thermotron, Kallen Park Dr., Holland, MI 49423. (616) 392-1482.

The ETS-150 is a compact, portable, closed-loop air-temperature source that temperature conditions circuit boards or small components. The system is bench or relay-rack mounted and operates from a 115/1/60, 20-A receptacle. The air-flow rate is 148 cfm from -75 to +125 F with proportioning control better than ±2 C. A digital indicator with 3-position selector switch is provided for monitoring supply, return, or remote temperatures.

CIRCLE NO. 445

Connector uses crimp-pin to relieve strain

Amphenol, 900 Commerce Dr., Oak Brook, IL 60521. Bob Ashley (312) 986-2700.

Miniature "D"-shaped rear-release rack and panel connectors, Type 17, feature insulation-support crimp contacts that secure both wire conductor and insulation in place, lessening chance of strain. The pin and socket contacts can accept any conductor size from 22 to 26 AWG, and have back-end tabs to crimp insulation up to a maximum OD of 0.050 in. Finger-tip pressure is all that is needed to snap contacts into connector housings. No special tools are required. The connectors are offered in 9, 15, 25, 37 and 50-contact configurations.

CIRCLE NO. 446

As the trend for miniaturization grows, the design engineers require smaller ceramic capacitors with maximum performance. The widest range of ceramic capacitors in the industry are available from Centre Engineering.

Sub-miniature ceramic capacitors as small as .050" x .040" up to .500" x .500" with a capacity range from 1 pf to 10 mfd are available to meet your requirements.

Our ultra-reliable subminiature ceramic chip capacitor both single and multi-layer are as small as .050" x .040" and designed for extreme high capacitance-to-volume ratio.

Centre's conformal coated leaded devices are only .100" square for applications requiring accurate temperature compensation, high stability, high Q, tight capacitance-to-volume ratio.

The glass sealed multi-layer capacitors are available in reel form. The small, .170" x .100" DIA. capacitors are hermetically sealed, reliable, rugged, and are ideal for automatic insertion.

It's a small, small world and we're at the Centre. For complete information write for our free catalogue.

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814-237-0321 • TWX 510-670-3517

CIRCLE NUMBER 806
THERMISTORS

New-Low cost SensiChips® • Small size • From .020" sq. to .300" sq. • Thickness from .005 to .070 in. • Resistances from 5 K ohms to 1 meg. • Typical response time 4 seconds.

VICTORY ENGINEERING CORP.
Victory Rd., Springfield, N.J. 07081
TWX: 701-983-4430 Tel: 201-379-5900

CIRCLE NUMBER 807

The world's only single-chip LSI Universal Printer Controller is here!

The very low-cost new 40-pin CY-480 controls ANY standard 5 x 7 dot matrix printer with print speeds up to 200 cps! The new CY-480 Universal Printer Controller from Cybernetic Micro Systems is the first—and only—40-pin LSI device which will control and interface any standard 5 x 7 dot matrix printer (including those from Victor, LRC, Practical Automation and Ampere) having a print speed up to 200 cps. It operates from a single +5V power supply and will interface a printer with any microcomputer or minicomputer system through standard 8-bit ports. The CY-480 accepts either serial (RS232C) or parallel input from the host system’s data channels.

The CY-480 replaces bulky, expensive dedicated controllers. The small, single LSI package offers a 5 x 7 dot matrix character generator, full upper and lower case ASCII 96-character font, and a 45-character (expandable to 96) internal line buffer storage. Standard is 10, 12 or 16 characters/inch variable character density command, 8-color selectable print command, forward/ backward printing command, and horizontal and vertical independently expanded print command. The CY-480 provides graphics capability and includes a “lop-print” operating mode for 180° viewing. Ready lines provide full asynchronous communications with handshaking, and an optional foreign language character generator is available.

Get full details on the inexpensive new Universal Printer Controller ($92 a single unit, $30 in 5,000 quantity) right now from

CYBERNETIC MICRO SYSTEMS
2460 Embarcadero Way, Palo Alto, Calif. 94303
Phone (415) 321-0410

CIRCLE NUMBER 809

AMPERITE Thermoic
delay relays

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Hermetically sealed - not affected by altitude, moisture or climate changes... SPST only - normally open or closed... Compensated for ambient temperature changes from −55° to +80°... Rugged, explosionproof, long-lived... Standard radio octal and 9-pinminiatures.

* MINIATURESDelays: 2 to 120 seconds.

RELAY PRICES:
Standard or Miniature—Under $4.00 Each.

PROBLEM: Send for BULLETIN
No. TR-81

AMPERITE BALLAST REGULATORS
Automatically keeps current at a definite value. For AC or DC... Hermetically sealed, rugged vibration-resistant, compact, most inexpensive.

Price, under $3.00 ea.
Write for Bulletins TR-81, LO-73 and AB-51

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Canada: Atlas Electronics, Ltd., 50 Wingold Ave., Toronto M6B 1P7

CIRCLE NUMBER 810

ELECTRONIC DESIGN 24,November 22, 1977
PACKAGING & MATERIALS

Cable-tie mounts are adhesive backed

Panduit, 17501 Ridgeland Ave., Tinley Park, IL 60477. (312) 532-1800.

The ABM2S-A mount has a pressure-sensitive backing with peel-off paper. It secures small wire bundles from any of the four sides of the mount. Measuring 1 × 1 in., it supports ¼-lb weight. The mount can be used with all miniature, intermediate and standard cross-section cable ties.

CIRCLE NO. 447

Wire stripper self-adjusts

AMP, 449 Eisenhower Blvd., Harrisburg, PA 17105. (717) 564-0100.

A built-in wire sensor enables this hand tool to strip single or multiple-core cables with conductors up to 12 AWG without wire-size adjustments. Paired wires are simultaneously stripped and the front feed eases stripping of short wires. Strip length can be pre-set at up to 0.7 in. and an insulation-diameter adjustment accommodates extreme variations of insulation thickness. Stripping jaws are field replaceable, and a set of wire-cutting blades are incorporated into the tool.

CIRCLE NO. 448

Conductive epoxy resists high temps

Tra-Con, 55 North St., Medford, MA 02155. Jim Hart (617) 391-5550.

TRA-DUCT 2924 is an electrically conductive silver-epoxy adhesive for critical high-temperature (190°C) bonding and sealing. It is mixed and applied at room temperature and cures at 90°C. It can bond many dissimilar surfaces.

CIRCLE NO. 449

IC packaging panels give multi-interfaces

Gary Mfg., 1010 Jersey Ave., New Brunswick, NJ 08902. Harry Koppel (201) 545-2424. $1.00 to $2.50 per IC; 2 to 4 wk.

Universal IC-packaging panels, PS4108, provide a multiple-interface system with the flexibility of four I/O channels for segmenting logic functions. The panels contain 30 columns of 64 terminals per column on 0.1-in. centers. The IC-socket contacts feature low profiles and a closed-entry style.

CIRCLE NO. 450

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CIRCLE NUMBER 811
If capacitor performance and delivery are giving you problems, our reliable metallized polycarbonate Series 650 could be the solution. More than the 1100 miniature units, in 6 case styles, rated to 50 mfd and 600 VDC — all extremely stable over a wide temperature range. And they're available in reel and unreeled packaging. For instant relief, contact Electrocube, 1710 So. Del Mar Ave., San Gabriel, CA 91776; Tel.: (213) 573-3300.

CIRCLE NUMBER 812

Where can I get an AC-DC or DC-DC switching power supply in a modular, open frame or P.C.B. design, with a 5 year warranty at reasonable cost?

ETATECH

CIRCLE NUMBER 813

Stevron, P.O. Box 8656, Anaheim, CA 92802. $29.95; stock.

“The Beeper” continuity tester measures circuit connections point-to-point on PC cards without removal of, or damage to, any component. The Model 100 uses an audio-response technique instead of an indicator scale. This technique minimizes the possibility of error and permits faster testing. It is a self-contained device and battery operation ensures electrical isolation from the equipment being tested. Output current is 20 µA max, top output potential is 40 mV.

CIRCLE NO. 522

Wrapped-wire boards fit mini/micro units


Series CIP4 and CIP4/11 IC wrapped-wiring boards are for interfacing with the DEC LSI-11 microprocessor and DEC PDP8/11 minicomputers. The module boards plug directly into, and are bus-compatible with standard DEC Omnibus and Q-Bus systems. The boards provide 32 columns of 60 low-profile socket terminals per column with alternate rows of committed ground and voltage wrapped-wire terminals. They will accommodate up to 110 16-position IC chips or an equivalent mix of 14 to 40-position IC chips. Boards are available in dual, quad, and hex sizes. Prices are from $1.50 to $2.00 per IC position.

CIRCLE NO. 523
Application notes

4-bit bipolar µP

A 12-page bulletin includes features, block diagrams and architecture of the IDM2901A 4-bit bipolar microprocessor. National Semiconductor, Santa Clara, CA

CIRCLE NO. 524

Lead-sulfide sensors

Performance data of lead-sulfide and lead-selenide sensors, packaging information, suggested circuits and environmental effects are covered in two application notes. Infrared Industries, Waltham, MA

CIRCLE NO. 525

Switching transistors

Using high-speed switching transistors in high-energy switching environments is the subject of a new 12-page app note, and parameter trade-offs in high-voltage, high-speed, switching power transistors are discussed in a reprint of a Powercon 1976 paper. General Semiconductor Industries, Tempe, AZ

CIRCLE NO. 526

Component burn-in

“A Guideline to Component Burn-in Technology,” 38 pages, explains how to apply heat to semiconductor devices or other components for the purpose of reducing the effects of “infant-mortality” failure. Graphs, charts, tables, and photographs show quality-conditioning burn-in procedures. Wakefield-Systems, Wakefield, MA

CIRCLE NO. 527

Programmable calculators

The HP-19C and HP-29C programmable handheld calculators are described in a six-page brochure. Sections describe the advanced programming features of the two calculators, keyboard features, physical specifications, and the HP warranty. Hewlett-Packard, Palo Alto, CA

CIRCLE NO. 528

ENCLOSURES

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Overall 22" 22" 22"
Depth (opening) 19.06" 19.06" 19.06"
Overall 25.5" 25.5" 25.5"
Overall Height with caster base 72.4" 79.4" 86.4"

Frame includes: caster base, vented side and top panels, plain door (hinged right or left), door lock (optional).
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CIRCLE NUMBER 814
AUTHOR'S GUIDE

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It's easy to write for Electronic Design, but it's often hard to get started. Send for your copy of our Author's Guide today.

Circle No. 250

HALOGEN-CYCLE LAMPS

Drawings, specifications and characteristics of halogen-cycle lamps are given in a 12-page catalog. General Electric, Miniature Lamp Products, Cleveland, OH

CIRCLE NO. 529

CIRCULAR CONNECTORS

Bayonet-type connectors are described in a 20-page catalog. There are more than two dozen drawings and photographs plus standard data on materials, finishes, shell styles and sizes, and charts on electrical data. ITT Cannon Electric, Santa Ana, CA

CIRCLE NO. 530

BREADBOARDS

Over one hundred different breadboards are featured in a 32-page catalog. The catalog shows minicomputer-interface boards, which are compatible with DEC, Data General, Camac, Computer Automation, and S-100 hardware systems. Douglas Electronics, San Leandro, CA

CIRCLE NO. 531

COMPUTING REFERENCE

The "Reference Book of Personal and Home Computing" provides a single source of information on stores and companies in the field, computer clubs and newsletters, magazines and professional societies. Its index of articles for the major publications sorts over 1200 articles by their content. People's Computer Co., Menlo Park, CA

CIRCLE NO. 532
At +125°C you can burn your fingers on some DAC's our 4058 stays cool

Because this new, hybrid 12 bit DAC was specifically designed for the temperature range - 55 to +125°C, it is not merely a top-end selection of commercial DAC's, where you don't know today what tomorrow's yield will be.

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And if you want to fly with it, the 4058 is shock, vibration and acceleration tested - its already being used in the new MRCA.
NEW LITERATURE

Active filter handbook

The Design of Active Filters and Experiments, a 285-page paperback textbook, provides an introduction to theory, implementation and design of active filters. Written by Howard M. Berlin, the book combines text and experiments permitting the reader to demonstrate the concepts covered. Subjects covered include the basics of operational amplifiers and filters, first-order low-pass and high-pass active filters and second and higher order active filters. Other topics described are bandpass and notch filters as well as the state-variable filter. The book costs $8.50. E&L Instruments Inc., Derby, CT

CIRCLE NO. 533

Components

Details on a wide range of components, including wirewound and metal-film resistors, thick-film resistor networks, trimmer pots, inductors, transformers and connectors, are given in a catalog. Electrical and dimensional specifications are provided. Dale Electronics, Columbus, NE

CIRCLE NO. 534

Technical index

A six-page guide lists reprints, technical bulletins and applications data sheets available from the company. Topics include process analysis, water and air quality monitoring, source monitoring, vehicle emissions analysis, and safety monitoring programs. Beckman Instruments, Fullerton, CA

CIRCLE NO. 535

Terminal boards

An updated version of the terminal board, block and strip reference guide includes the thermoplastic series for PC, insulated feedthrough and conventional flat-mount applications. Kulka Electric, Mount Vernon, NY

CIRCLE NO. 536

Test-equipment rental

A 168-page catalog describes a broad line of test-equipment rental programs designed to fit a range of individual needs. Leasametric, Burlingame, CA

CIRCLE NO. 537

Mini-DIP switches

Dimensions, features, specifications and prices of mini-DIP switches are given in a four-page catalog. EECO, Santa Ana, CA

CIRCLE NO. 538

Switches

Photos, line drawings, specifications and ordering information on over 300 different switches are included in a 24-page catalog. Chicago Switch, Chicago, IL

CIRCLE NO. 539

Solid-state amplifiers

A 32-page catalog covers solid-state amplifiers. The catalog includes selection charts, applications information, specifications, drawings, and a glossary of terms. Watkins-Johnson, Palo Alto, CA

CIRCLE NO. 540

Radio-link test set

A 24-page brochure describes the RM-4 radio-link precision test set for the two intermediate frequencies, 70 MHz and 140 MHz. Wandel and Golterman, Livingston, NJ

CIRCLE NO. 541

Pressure transducers

A 12-page brochure describes pressure transducers, carrier demodulators and multichannel signal-conditioning systems. Validyne Engineering, Northridge, CA

CIRCLE NO. 542

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CIRCLE NUMBER 820
### NEW LITERATURE

#### Antenna testing system

Technical and application information for the series 2030 antenna data collection system are presented in a brochure. Scientific-Atlanta, Atlanta, GA

**CIRCLE NO. 543**

#### Linear and digital ICs

Linear and digital semi-custom integrated circuits are featured in a 16-page brochure. The characteristics of the various integrated components (bipolar transistors, resistors, diodes, and MOSFETs) are presented in tabular forms. Interdesign, Sunnyvale, CA

**CIRCLE NO. 544**

#### Image displays

“Screened Image Displays,” 16-pages, provides a general overview of the SP-400 screened-on-glass, planar gas-discharge displays. Beckman Instruments, Scottsdale, AZ

**CIRCLE NO. 545**

#### Capacitors

Miniature aluminum electrolytic, metalized polyester film, Mylar, polyurethane film, ceramic and tantalum capacitors are featured in a 20-page catalog. TransCap, El Cajon, CA

**CIRCLE NO. 546**

#### Cabinet blower

Included in a two-page cabinet blower-data sheet are equipment specifications, in both English and metric measurements, diagrams of the equipment, air flow and acoustic charts. Rotron, Woodstock, NY

**CIRCLE NO. 547**

#### Bandpass filters

Microwave bandpass filters in the frequency range of 30 MHz to 12.4 GHz are covered in a 16-page catalog. A comparative summary, descriptions and performance data are provided. Lorch Electronics, Englewood, NJ

**CIRCLE NO. 548**

### Bulletin board

**Motorola’s new power transistors—2N3055H, 2N3773, 2N6609 and MJ15015—combine the rugged Safe Operating Area (SOA) specified for single-diffused-base types, with the economy and complementary structures of epitaxial-base devices.**

**CIRCLE NO. 549**

**Burr-Brown’s ADC85 and DAC85 a/d and d/a converter prices are slashed up to 30%.**

**CIRCLE NO. 550**

**Major enhancements to Honeywell’s TDC 2000 process control system make complete centralized control with color-video displays a reality for both simple and complex industrial processes.**

**CIRCLE NO. 551**

**TRW Power Semiconductors has lowered the OEM prices of eight power-switching transistors and nine Darlington transistors an average of 25%.**

**CIRCLE NO. 552**

**Litronix has introduced five photo-transistor opto-isolators in the JEDEC series. Prices in 1000 qty are 4N25 and 4N25A, $0.89; 4N26, $0.88; 4N27, $0.71, and 4N28, $0.67.**

**CIRCLE NO. 553**

**Texas Instruments is offering the A78M00 and A79M00 voltage regulators in low-cost TO-202 packages.**

**CIRCLE NO. 554**

**General Electric has raised prices 4 to 9% for rechargeable nickel-cadmium batteries to original equipment manufacturers.**

**CIRCLE NO. 555**

**MFE Corp. has dropped prices up to 20% on parallel and serial I/O interfaces for a cassette transport.**

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1977 CATALOG 211

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Electronic Design 24, November 22, 1977
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