Analog subsystems are needed to interface microcomputers with the real world of analog signals. In process control, transducers for temperature, pressure and flow cannot be directly connected to a microcomputer. The interface board for data acquisition must bridge the gap. But will the cost be compatible? Plug in on p. 26.
Any way you look at it, there's beauty and reliability at a low cost in our new Model H-1400 turns-counting dial. From the smooth, high impact tapered plastic design... to the big, bold legible numbers... this dial will add to the aesthetics of any control panel. But, with beauty being only skin deep, we've put durable long-lasting metal inside where it counts — including the gears and set-screw thread insert. And, the price is just as attractive — only $4.26* in production quantities!

Send today for complete technical data and discover a beautiful new angle in turns-counting dials — from Bourns, naturally!

Direct or through your local distributor.

TRIMPOT PRODUCTS DIVISION, BOURNS, INC. 1200 Columbia Ave., Riverside, CA 92507 Phone: 714 781-5123. TWX: 910 332-1252

*Domestic U.S.A. price only, H1411, without brake.
High Reliability Optoelectronic Products!

Hermetic lamps, displays and isolators from Hewlett-Packard. That's our family of high-reliability optoelectronic products. These devices are ideal for ground, airborne and shipboard equipment, medical instrumentation, fire-control and space flight systems. Lamps are available in high-efficiency red, yellow and green.
Our isolators offer high speed.
And displays come with a built-in decoder, driver and memory.

In the U.S., contact Hall-Mark, Schweber, Wilshire or the Wyle Distribution Group (Liberty/Elmer) for immediate delivery.
In Canada, contact Bowtek Electronics Co., Ltd., Schweber Electronics or Zentronics, Ltd.

HEWLETT PACKARD

Sales and service from 179 offices in 85 countries.

CIRCLE NUMBER 2
The Relay of Tomorrow is here today: the Centigrid.

Out of Teledyne's TO-5 relay technology has evolved the Centigrid® — the ultimate subminiature relay. It combines the proven TO-5 relay design concept and internal construction into an even more compact package. Low profile height — just .230" (5.84mm) — with terminals spaced on a .100" (2.54mm) grid permitting direct pc board mounting without the need for lead spreading.

Add to this the same low coil power consumption as the TO-5 relay, with obvious thermal and power supply advantages. And for RF switching, the Centigrid's low inter-contact capacitance and contact circuit losses provide high isolation and low insertion loss up through UHF frequencies.

To top it all off, the Centigrid is qualified to levels "L" and "M" of MIL-R-39016, including the internal diode suppressed versions.

For complete specification data on the Relay of Tomorrow, contact Teledyne Relays, the technology leader in the relay industry.

TELEDYNE RELAYS
3155 West El Segundo Boulevard, Hawthorne, California 90250, Telephone (213) 973-4545

CIRCLE NUMBER 3
Analog boards for microcomputers: It’s a case of not always getting what you want—A special report

Home computers: from a bag of parts to a system you simply plug in.

Distributed processing spreads computer intelligence around

Washington Report

Microprocessor Basics: Part 19
Exploit existing Nova software by designing computer systems around the microNova. The microprocessor gives you minicomputer performance from a 40-pin package.

Mate microprocessors with CRT displays but make sure you know enough about the displays. Raster-scan systems are simple and can be easily interfaced.

Speed up digital processors by not using shift registers to do data scaling. Specialized scaling circuits can do the job faster and simpler.

Memory Technology: Part 2
When testing 16-k dynamic RAMs, keep your eye on the temperature and your finger on your pattern generator. Minding both gives more accurate results.

Consider piezoelectric ceramics: Easily formed into complex shapes and chemically inert, they provide stable piezoelectric characteristics up to 180°C.

Predict system dependability with a pocket calculator. A programmable unit speeds computations of reliability and maintainability models.

Fred Bucy of TI Speaks on Managing Innovation

Ideas for Design:
Three-digit bipolar voltmeter built with v/f converter and BCD counters. Synchronous counter also shifts for serial/parallel conversions. Demand power supply draws low standby current. Add missing segments to 6 and 9 on standard seven-segment decoders. Interface slows visual-display data for driving data-recording peripherals.

International Technology

Products

Modules and Subassemblies: Analog I/O cards for industry plug into M6800

Instrumentation: Calibrator stores tolerance limits

Instrumentation: Programmable source spans 1 mHz to 50 MHz

IC's and Semiconductors

Data Processing

Components

Micro/Mini Computing

Packaging & Materials

New Literature

Bulletin Board

Vendors Report

Departments

Editorial: Down with Professionalism

Across the desk

New Literature

Bulletin Board

Vendors Report

Advertisers' Index

Product Index

Information Retrieval Card

Cover: Cover design by Art Director, Bill Kelly.
Dual op amps were a great idea—less space, less cost. But **matched performance duals** make much more sense. And only PMI has them.

A matched performance dual op amp puts into the designer's hands a pair of gain blocks that function in sync. They track each other—making them useful for any number of applications calling for a pair of matching outputs.

To put it another way, matched performance makes the dual op amp concept a truly practical one for the first time. In aerospace, instrumentation, process control—think of how useful matched performance could be. And PMI **guarantees** the match.

Of course, matched performance is no good if the **specs** aren't good. Ours are.

### MATCHING CHARACTERISTICS

<table>
<thead>
<tr>
<th>Parameter</th>
<th>OP-14A/OP-04A</th>
<th>OP-14/OP-04</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Offset Voltage Match</td>
<td>ΔV&lt;sub&gt;os&lt;/sub&gt;</td>
<td>V&lt;sub&gt;CM&lt;/sub&gt; = ±CMVR</td>
</tr>
<tr>
<td>Common Mode Rejection Ratio Match</td>
<td>ΔCMRR</td>
<td>V&lt;sub&gt;CM&lt;/sub&gt; = ±CMVR</td>
</tr>
<tr>
<td>Test Conditions</td>
<td>Min</td>
<td>Typ</td>
</tr>
<tr>
<td>Min</td>
<td>0.3</td>
<td>1.0</td>
</tr>
<tr>
<td>Typ</td>
<td>1.0</td>
<td>—</td>
</tr>
</tbody>
</table>

These specifications apply for V<sub>in</sub> = ±15V, T<sub>A</sub> = 25°C, R<sub>in</sub> ≤100Ω, unless otherwise noted.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>OP-14E/OP-04E</th>
<th>OP-14C/OP-04C</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Offset Voltage Match</td>
<td>V&lt;sub&gt;os&lt;/sub&gt;</td>
<td>V&lt;sub&gt;CM&lt;/sub&gt; = ±CMVR</td>
</tr>
<tr>
<td>Common Mode Rejection Ratio Match</td>
<td>CMRR</td>
<td>V&lt;sub&gt;CM&lt;/sub&gt; = ±CMVR</td>
</tr>
<tr>
<td>Test Conditions</td>
<td>Min</td>
<td>Typ</td>
</tr>
<tr>
<td>Min</td>
<td>0.5</td>
<td>1.5</td>
</tr>
<tr>
<td>Typ</td>
<td>1.5</td>
<td>—</td>
</tr>
</tbody>
</table>

These specifications apply for V<sub>in</sub> = ±15V, –55°C ≤ T<sub>A</sub> ≤+125°C for OP-14A and OP-14, 0°C ≤ T<sub>A</sub> ≤70°C for OP-14E and OP-14C, R<sub>in</sub> ≤100Ω, unless otherwise noted.

### OP-04 and OP-14: the pin-compatibles

The OP-04 and OP-14 are monolithic chips, each containing a pair of matched-performance op amps. The OP-14 is the best dual you can buy that fits standard 1458/1558 sockets; the OP-04 is just as good, but fits 747 sockets and can be nulled.
OP-10:
the only precision dual

The OP-10 is a nullable precision device consisting of two discrete chips in a single 14-pin DIP. Think of it particularly for instrumentation, where its extremely high performance is of greatest value. You could look at the OP-10 as two OP-05’s in a single package. Military standard models are available.

The OP-10 will save you costly and laborious selection and matching of discrete amplifiers. Matching specifications include $V_{os}$, $I_B$, $I_{os}$, CMRR, PSRR; drift for $V_{os}$, $I_B$ and $I_{os}$ match with temperature.

When you think of matched-performance duals, remember: either they’re unavailable or they’re PMI parts. And ours are available now—on your distributor’s shelf. Write on your letterhead for samples and applications notes.

Precision Monolithics Incorporated
1500 Space Park Drive, Santa Clara, California 95050.
Telephone: (408) 246-9222. TWX: 910-338-0528.
Cable: MONO.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Test Conditions</th>
<th>OP-10AY Min</th>
<th>OP-10AY Typ</th>
<th>OP-10AY Max</th>
<th>OP-10Y Min</th>
<th>OP-10Y Typ</th>
<th>OP-10Y Max</th>
<th>Units</th>
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<tbody>
<tr>
<td>Input Offset Voltage Match</td>
<td>$\Delta V_{os}$</td>
<td>–</td>
<td>0.07</td>
<td>0.18</td>
<td>–</td>
<td>0.12</td>
<td>0.5</td>
<td>mV</td>
<td></td>
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<tr>
<td>Average Non-Inverting Bias Current</td>
<td>$I_{o+}$</td>
<td>–</td>
<td>$\pm 1.0$</td>
<td>$\pm 3.0$</td>
<td>–</td>
<td>$\pm 1.3$</td>
<td>$\pm 4.5$</td>
<td>nA</td>
<td></td>
</tr>
<tr>
<td>Non-Inverting Offset Current</td>
<td>$I_{o+}$</td>
<td>–</td>
<td>0.8</td>
<td>2.8</td>
<td>–</td>
<td>1.1</td>
<td>4.5</td>
<td>nA</td>
<td></td>
</tr>
<tr>
<td>Inverting Offset Current</td>
<td>$I_{o-}$</td>
<td>–</td>
<td>0.8</td>
<td>2.8</td>
<td>1.1</td>
<td>4.5</td>
<td>nA</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Common Mode Rejection Ratio Match</td>
<td>$\Delta CMRR$</td>
<td>$V_{CM} = \pm CMVR$</td>
<td>114</td>
<td>123</td>
<td>–</td>
<td>106</td>
<td>120</td>
<td>–</td>
<td>dB</td>
</tr>
<tr>
<td>Power Supply Rejection Ratio Match</td>
<td>$\Delta PSRR$</td>
<td>$V_{s} = \pm 3V$ to $\pm 18V$</td>
<td>100</td>
<td>112</td>
<td>–</td>
<td>94</td>
<td>110</td>
<td>–</td>
<td>dB</td>
</tr>
<tr>
<td>Channel Separation</td>
<td>–</td>
<td>–</td>
<td>126</td>
<td>140</td>
<td>–</td>
<td>126</td>
<td>140</td>
<td>–</td>
<td>dB</td>
</tr>
</tbody>
</table>

These specifications apply for $V_{s} = \pm 15V$, $T_{A} = 25^\circ C$, unless otherwise noted.
INTERESTED IN HIGH EFFICIENCY POWER SUPPLIES?

ABBOTT HAS THE ANSWER

Abbott Transistor Laboratories manufactures three complete lines of hermetically sealed, switching regulated power supplies. These rugged and dependable power modules have already found wide use in many military, aerospace and industrial applications. All units are designed to meet the EMI requirements of MIL-STD-461 and the environmental requirements of MIL-STD-810.

77% EFFICIENT
60 Hz to DC model VN

70% EFFICIENT
400 Hz to DC model UN

70% EFFICIENT
DC to DC model BN

Abbott's Model VN series converts 47 to 440 Hz AC lines to any DC voltage between 4.7 and 50 VDC at output powers of 25, 50 and 100 watts. Line and load regulation are controlled to 0.4% with a peak-to-peak ripple of 100 mV. Efficiencies of 77% are achieved with power densities of greater than 1 watt per cubic inch.

Designed to operate from 360 to 420 Hz AC lines, Abbott's Model UN series offers output powers of 25, 50 and 100 watts at all popular voltages between 5 and 50 VDC, including ±12 and ±15. The full load operating temperature range is −55°C to +100°C. Peak-to-peak ripple of 100 mV and load regulation of 0.5% are just a few of the standard features of this line of 70% efficient power modules.

Wide range DC inputs of 20 to 32 VDC can be accommodated by Abbott's BN line of high efficiency DC to DC converters. All popular output voltages between 5 and 50 VDC, including ±12 and ±15, are available at output power levels of 25, 50 and 100 watts. 0.5% line and load regulation, 100 mV peak-to-peak ripple and −55°C to +100°C operating temperature range are a few of the standard features of the BN line.

Complete electrical specifications, size charts and prices for these units are listed in our new 60 page free catalog. Also listed are 12 additional line of power modules, including:

- 60 Hz to DC model VN
- 400 Hz to DC model UN
- DC to DC model BN

For immediate complete information on Abbott Modules, see pages 1037-1056 Vol. 1 of your 1975-76 EEM Catalog or pages 612-620 Vol. 2 of your 1975-76 GOLD BOOK.

Send for our new 60 page FREE catalog —

"SEE US AT WESCON/77 SHOW IN SAN FRANCISCO, BOOTH NO.'S 710-712"

CIRCLE NUMBER 4
Across the desk

A baby trolley?

Your news story on the mother and baby elephants in the Rose Bowl parade (ED No. 2, Jan. 18, 1977, p. 15) evoked memories of a similar “float” on Engineers’ Day at Ohio State University in the spring of 1940, which I attended as a high school senior from London, OH.

Electrical engineering students had built a battery-powered model of the Toonerville trolley from which they controlled (or tried to!) a baby trolley by radio. Straight-away control was O.K., but the baby usually ended up against the curb when the parade turned a corner.

William P. Reid
Staff Engineer
Otis Elevator Co.
Engineering Center
440 Franklin Turnpike
Mahwah, NJ 07430

When in Germany...

In “IR-Activated Headphone Works without A Cord” (ED No. 3, Feb. 1, 1977, p. 13), you described a device that I saw and tried out in a hi-fi store in Germany in the summer of 1975.

I don’t know if Sennheiser Electronics Corp. was aware of the existence of the German device, but let’s give credit where credit is due. The address of the German maker is Loewe Opta GmbH, Berlin Kronach, Germany.

Wolfgang Fischer
Project Engineer
Kepco, Inc.
131-38 Sanford Ave.
Flushing, NY 11352

About our counter...

I was very interested in Stan Runyon’s review of all the frequency counters (ED No. 11, May 24, 1977, p. 54), but was sorry to see that our AIM-1005 did not get a mention. Maybe because it does not have a display for humans to read but is intended to be read by a microcomputer? It has gate times from 10 µs to one hour, which give it greater dynamic range than all the eight-digit counters, and at a fraction of the cost.

E. Barry Hilton
President
Automated Industrial Measurements Inc.
P.O. Box 125
Wayland, MA 01778

Viva second sources

After reading the article, “8080As Are Not All Alike” (ED No. 2, Jan. 18, 1977, p. 41), I couldn’t help but make (continued on page 16)
5.3 mW

PLANAR GAS DISCHARGE DISPLAY

LED DISPLAY

100 mW
You can see the difference

...in the brighter, more readable Beckman PGD displays. But, what about the other advantages... the non-visible benefits that shine just as bright... like:

- Lower power consumption.
- Lower-cost designs.
- Smaller (less expensive) power supplies.

You may want to look a little further. For example:

**PGD uses less power than LEDs**

LEDs consume more power than PGD displays of similar character size. That's fact. Look at the power-consumption comparison chart that follows. Among others, it compares the Beckman SP-350 display with the efficient Litronix 747. Both are essentially half-inch displays. Both were measured at factory-recommended, typical current levels.

In this case, specified voltage drop across the LED is 3.4 volts. When it's driven from 5 volts, total power consumption for the LED and driver is 100mW per segment. That's 800mW for a complete figure "8". Conversely, total segment power consumption for the SP-350 is 54mW; or, 415mW for a figure "8"... about one-half that of the LED.

And, that's only part of the story. Check the chart and compare the resulting, readable brightness figures for three different sizes of Beckman PGD displays with those of comparable LEDs.

As you know, for equal power consumption, high voltage means low current. More importantly, high voltage is easy and inexpensive to handle with Beckman adjustable, UL-listed converters, and DD-700 Decoder/Drivers. As a result, you can save money on your designs; and, use smaller, less expensive power supplies, too.

**PGD and RFI**

Beckman PGD displays are being used in many aircraft applications — with no RFI shielding. The Pulsed-DC Technique makes it possible to dim from Sunlight Brightness to easy-on-the-eyes night viewing without annoying buzz. They're used also in a full line of automotive aftermarket products — speedometers, tachs, fuel-flow meters, rally clocks. And, they're used in other consumer products, like clock-radios, as well as in sophisticated counters and scientific instruments — with no fear of RFI from the display itself, when DC-driven.

**PGD is reliable**

No other display manufacturer offers a warranty that is equivalent to that of Beckman's Information Displays Operations.

In fact, Beckman is so confident of the reliability of its display products that, almost two years ago, we invented "Warranty Plus".

Simply stated, Warranty Plus means that Beckman warrants its raised-cathode display for the period the customer warrants its product in which the display is employed. We're with you all the way!

How do we do that? With great care.

Every Beckman display undergoes 100% burn-in before it goes to market. As a result, infant mortalities are eliminated; and, so are all visually unacceptable products.

**PGD is MOS-compatible**

Hook up any Beckman raised-cathode display to one of the off-the-shelf AMI, EA, or National MOS chips — for example, the 40-pin, S1998 and, watch it operate without any components between it and the MOS part.

**PGD is most things to most engineers**


A designer's joy!

**PGD is bright**

The bottom line. Superior readability, any way you look at it. An even glow, segment-to-segment... digit-to-digit. And, brightness uniformity from unit-to-unit. Clarity and visibility of Beckman PGD displays provide The Visible Edge. That's what makes the difference between a winner and a washout; and, that's just what other displays do — in competing environments.

For discussion of features important to you, request Beckman application notes on: "Display Power Supply Requirements" and "DC Clock Application"; the data sheet on DD-700 Decoder/Drivers; or, the Short Form Catalog. Write: Beckman Information Displays Operations, P.O. Box 3579, Scottsdale, AZ 85257. Phone (602) 947-8371.

Spec-for-spec, eyeball-to-eyeball, Beckman Planar Gas Discharge displays are better. And, brighter.

As anyone can see.

---

**LED vs. PGD Power Comparison**

<table>
<thead>
<tr>
<th>Segment Current</th>
<th>Litronix 747</th>
<th>IEE 1720</th>
<th>Monsanto MAN6160</th>
<th>H-P 5082-7650</th>
<th>SP-101</th>
<th>Beckman SP-350</th>
<th>SP-330</th>
</tr>
</thead>
<tbody>
<tr>
<td>Forward Voltage Drop</td>
<td>20mA</td>
<td>20mA</td>
<td>20mA</td>
<td>20mA</td>
<td>700mA</td>
<td>330mA TYP</td>
<td>180mA TYP</td>
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<tr>
<td>Power Per Digit (1-DP)</td>
<td>540mW</td>
<td>495mW</td>
<td>280mW</td>
<td>336mW</td>
<td>730mW</td>
<td>350mW</td>
<td>190mW</td>
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<tr>
<td>Power Per Digit (2-DP)</td>
<td>800mW</td>
<td>800mW</td>
<td>800mW</td>
<td>800mW</td>
<td>870mW</td>
<td>415mW</td>
<td>230mW</td>
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<tr>
<td>Efficiency (F.L./mW)</td>
<td>.04</td>
<td>.02</td>
<td>.08</td>
<td>.16</td>
<td>.26</td>
<td>.51</td>
<td>.90</td>
</tr>
</tbody>
</table>

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**Beckman Displays. The visible edge.**
It's amazing how an easy mind enhances your hobbies

We're the easy mind people. TRW Capacitors. You can rely on us to choose the best raw materials.

Our X363 metallized polypropylene line is a perfect example. We spent several years making sure we had chosen precisely the right dielectric. And simultaneously making sure our technology was precisely right, too. The results were worth it.

The line features excellent electrical properties—high IR, low DF, and dielectric absorption that's even better than polystyrene—to minimize offsets and errors in slope integrators and sample and hold circuitry.

The line features low dissipation factor (High Q) in a small package, for pulse, low level RF or filter applications. And it features high stability—for the long term shelf life and resistance to severe environments that's important for time base generators, integrators and filters. The specs are unique. And impressive. So are our engineering services. So relax and give us a call. Or write: TRW Capacitors, An Electronic Components Division of TRW, Inc., 301 West "O" St., Ogallala, Nebraska 69153 • Tel: (308) 284-3611.

TRW Capacitors
Another Product of a Company Called TRW

Circle Number 7
TAKE A CLOSE LOOK AT THESE BURROUGHS PLASMA DISPLAY BREAKTHROUGHS.

The new Burroughs SELF-SCAN® II single register gas plasma panels are breakthroughs in visibility and readability, making them ideal for all types of applications — from audience information displays to instrumentation applications. They are digitally addressed to interface easily with microprocessors and computers.

Only 15 connections are required. These new units complement Burroughs' standard line of single register 16 and 32 character plasma displays.

The Burroughs SELF-SCAN II 1 x 20 and 1 x 40 displays. Certainly worth looking into.

Burroughs Corporation, Electronic Components Division, P.O. Box 1226, Plainfield, New Jersey 07061. Telephone (201) 757-5000. SELF-SCAN displays are available nationwide through our distributors, Hamilton/Avnet and Cramer Electronics.

You can see the difference

Burroughs

ELECTRONIC DESIGN 19, September 13, 1977

CIRCLE NUMBER 8
Circuits for systems that count.

Save space, time and system cost with Intersil counting and timing microcircuits.

For event timing, unit counting and frequency generation, Intersil has a line of circuits second to none. You get solid state reliability and size reduction, plus the time- and money-saving benefits of just the right product for your job... from Intersil.

Intersil stocking distributors: Advent Electronics, Inc. (Indianapolis); Arrow Electronics; Century Electronics; Components Plus (N.Y.); Diplomat (Fla., N.J.); Elmar/Liberty Electronics; Harvey (Upper N.Y.); Intermark (San Fran.); Kierulf Electronics; L Comp (Mo.); R.A.E. Ind. Elect. Ltd. (Van. B.C.); RESCO (Raleigh, N.C.); Schweber Electronics; Sheridan Assoc.; Zentronics (Canada).
Versatile low power counter.

7208 is a 7-digit frequency, unit or period counter which directly drives an LED display. For a unit counter, add a display, 2 resistors, a capacitor and control switches.

CMOS quartz crystal frequency generators.

7207 Frequency Counter Timebase (.01 and .1 second count window) or the 7207A Frequency Counter Timebase (.1 and 1 second count window) provide all the gating, store and reset signals necessary to expand the 7208 into a frequency counter.

7209 is a versatile high frequency clock generator with a divide-by-8 output stage for a 5 Volt system.

7038A is a micropower oscillator, frequency divider and output driver for 3 Volt synchronous motors. The 7038B is designed for 1.5 Volt synchronous motors.

7213 is a versatile oscillator, divider and waveshaping circuit providing various outputs including 1-second and 1-minute pulses.

7049A and 7050 are oscillator circuits which include a divider chain, output one-shot and output buffer for 1.5 Volt stepper motors.

7051A is a clock circuit for 12 Volt synchronous motor applications.

Battery operated CMOS counter/timers.

7215 industrial counter/timer has four functions (start-stop, split, taylor and time-out) and times up to 59 minutes, 59.99 seconds.

7205 has split, taylor and reset functions for timing to 59 minutes, 59.99 seconds.

7045A times up to 23,9999 hours. All the above counters directly drive an LED display.

Externally settable counter/timer circuits.

8240 is one of a family of programmable counter/timers which generate long pulse widths with inexpensive RC components. Each circuit contains an oscillator and divider flip flops. Pin connections on the 8240 select an output pulse width from 1 RC to 255 RC.

8250 can be used with thumbwheel switches to count from 1 to 99.

8260 counts 1 to 59 for timing seconds, minutes or hours.

Low cost precision timers.

555 generates time delays from microseconds to hours, with the addition of only one resistor and a capacitor.

556 contains two 555s in a single package.

Custom circuits also available.

We can develop custom CMOS LSI circuits for your special counting and timing applications. Consult your local sales office listed below for information.
Your best source for SCRs is one you may never have heard of.

Would you believe Teccor? That's right. Teccor. We're not a small components company. In fact, with over 1,000 employees, 3 plants, and over 16 million dollars in sales, we're not small at all.

Our reputation for dependable quality is known around the world. Has been for 13 years.

To give you the design flexibility you want, we offer the widest selection of SCR package designs in the industry.

At the same money you're paying now — maybe less.

Contact your local Teccor representative or call us at 817-267-2601. Tell us about your specific SCR applications. We'll get you the information or samples you need for evaluation.

You may not know us, but we figure it's only a matter of time.

Just think of us as the world's largest unknown source for SCRs.
New from Centralab...

IMPS PUSHBUTTON SWITCHES

A new miniature modular building block system that offers microprocessor control designers more of what they need.

To meet the special digital and analog needs of today's μP-based controls, Centralab offers design engineers a whole new system of modular pushbutton switch building blocks. We call it IMPS — Integrated Modular Panel System. IMPS saves PC board and panel area, simplifies front panel design, cuts assembly costs, reduces back-panel space requirements, and meets the digital-analog needs of μP-based controls. Check these space saving, cost-cutting features.

Simplify front panel interface.
All IMPS switches regardless of function, are uniform in size, simplifying design and selection of front panel hardware. They have high volumetric efficiency, occupying 0.505" x .388" PC board area and require only .608" of space between PC board and front panel.

Meet analog and digital needs.
IMPS switches are available with momentary, push-push and interlocking actions, with a long-life contact system that switches both digital and analog signals. To accommodate critical signal requirements, housings are high-insulation molded plastic with UL 94V-0 rating.

Available options.
Optional installations include ganged assemblies, front-panel mounting and wire-wrapping.

Cut assembly costs.
IMPS switches may be mounted on the front panel, and are designed for automatic wave soldering installation and PC board cleaning. Insert molded terminals prevent flux and solder wicking and contact contamination. Integral PC board stand-offs provide for efficient board cleaning.

Built To Centralab Quality Specs.
IMPS Pushbutton Switches combine compact size, low cost and highest quality throughout.
- Silver or gold inlay wiping contacts for long-life and low-contact resistance.
- Less than 2 milliseconds contact bounce.
- SPST, SPDT, DPST, and DPDT switch contacts.
- Printed circuit, DIL socket or wire-wrap terminations available.
- 2.5 to 3.5 oz. actuation force (momentary).
- Choice of button interface — square or blade shaft (shown) — permits use of a variety of Centralab and industry standard buttons and keycaps.
- 10, 15, 20 or 25mm center-to-center spacing.
I've read several of your editorials. I agree with the first paragraph of this one. I couldn't believe the rest of it! It is a disgrace the way you wrote about a subject you know nothing about!

Anonymous

My first reaction to your editorial was that it was extremely unprofessional and that you made some pretty sweeping accusations. I am convinced you would not be able to substantiate these if you took time to re-read your own editorial.

I am not sure why you should assume such a vitriolic attitude towards the medical profession. Do you think it is fair in your position to air these opinions if they are not well founded?

I am fortunate in the field of orthopedics not to have to treat many people with cancer. Each such encounter is a painful and difficult task, which usually involves a considerable amount of soul searching. To read that anybody would specifically try and prevent a patient from receiving a cure is to gloss over the whole issue. I have seen people who have been treated with laetrile and it is a very distressing negative result.

Your reference to the various vitamins is inappropriate and I think you should fudge up your knowledge on the history of vitamin deficiency. Just remember why a limey was called a limey, and remember it was not the medical profession, it was the seafaring people who objected to carrying excessive lime.

Your editorial on laetrile shows the great distance between the heart and the head. The most generous explanation I can give for your unfortunate stand is that you have allowed your human feelings of compassion for the victims of cancer to over-ride your professional judgment.

A careful reading of the history of

(continued from page 7)
Who can meet your greatest needs in D Subminiatures?

Cannon can!

Six decades on the leading edge of interconnect technology.

Cannon ITT
**PRODUCT LINE SUMMARY**

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<tr>
<th>SERIES</th>
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<td>D*</td>
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<td>ORIGINAL-D</td>
<td>Two-piece white Nylon</td>
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<tr>
<td>D*P</td>
<td>All-plastic 90° p.c.b. D Subminiature</td>
<td>BURGUN-D (Mark IV)</td>
<td>Black glass-reinforced thermoplastic, UL rated 94V-O (flame retardant)</td>
<td>Stamped printed circuit</td>
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<td>D Subminiature connector for more critical applications conforms to MIL-C-24308</td>
<td>GOLDEN-D (Mark I)</td>
<td>Monobloc, dark green, Diallylphthalate glass-filled</td>
<td>Solder, printed circuit, Wire-Wrap, Coaxial, high power and high voltage</td>
</tr>
<tr>
<td>D*MA</td>
<td>D Subminiature with LITTLE CAESAR® contact retention system conforms to MIL-C-24308</td>
<td>ROYAL-D (Mark III)</td>
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<tr>
<td>D*SP</td>
<td>Mass Terminated D Subminiature pin &amp; socket connector</td>
<td>Mas/Ter-D (Mark V)</td>
<td>Black glass-reinforced thermoplastic, UL rated 94V-O (flame retardant)</td>
<td>Non-removable insulation displacement termination.</td>
</tr>
</tbody>
</table>

**BROADNESS OF LINE**

Welcome to the ITT Cannon Electric D Subminiature store... Feel free to look around among one of the broadest lines of high quality, high reliability subminiature rectangular connectors found anywhere. Our store has been around for 60 years, serving industry worldwide. During that time customers have used billions of Cannon® D Subminiature connectors, contacts, and associated accessories and tooling. Why billions? Because people appreciate quality, and that's the concern of everyone in the ITT Cannon family. From the president to the assembly worker, we've a dedication to doing things right the first time. That's why our Quality Assurance department guarantees the high reliability of our products in meeting industry standards and MIL-Spec demands. And we're proud that this dedication is reflected in the numerous customer awards for excellence that we've received.

The versatile D Subminiature connector series is designed for applications where space and weight are prime considerations. Often the most economical solution to any interconnect problem, they accommodate a great number of circuits in relation to their size and weight. D series connectors can be adapted for cable attachments by use of one of the many accessory junction shells.

All seven of our D Subminiature connector types are fully intermateable, each accommodating up to 50 contacts in standard arrangements as well as high-density Double-D arrangements. Also available are combination arrangements with provision for coaxial, power, high voltage and printed circuit contacts. The versatility of D Subminiature connectors is enhanced by a variety of finishes and a complete line of accessories, most of which are UL-recognized.
With manufacturing facilities on several continents and a global network of more than 200 distributors, ITT Cannon is geared to supply interconnect products to customers around the world. In North America most distributors are also Cannon Authorized Plug Specialists (CAPS). Besides maintaining comprehensive off-the-shelf inventories, CAPS distributors operate local assembly centers set to our factory standards of stringent quality control. The combination of a vast distributor network and local and district sales offices gives you ready access to the Cannon storehouse of products.

No matter where you are, no matter what your needs, the Cannon capability means on-time delivery of the product you want, in the quantities you want, and at the right price.

At the heart of our organization are our technical sales offices, all equipped to provide you service equal to that available from our home office. Our technical specialists have been thoroughly trained and can help you select the Cannon products that will meet your needs.

Shop at the Cannon store, and you'll find our product support doesn't stop when an application is implemented; field service personnel are available to study the changing requirements of your operation, and provide you with cost-effective solutions to your needs.

All Cannon interconnect devices—catalog or custom—are supported by the necessary termination tooling to speed production and lower your total installed costs.

As a product is being designed for your application, our engineering department is working with our customer tooling group to develop the insertion, extraction and crimping tools necessary for proper implementation. Standard customer tools available with every ITT Cannon product include a full range from simple hand tools to crimp machines, and both automatic and semi-automatic strip-and-crimp machines that can terminate up to 2,400 contacts per hour.

Six decades on the leading edge of interconnect technology.
MAS/TER-D MASS TERMINATED D SUBMINIATURE
Cannon Mas/Ter-D pin-and-socket D Subminiature connectors provide reliable high-speed mass termination at a lower total installed cost than conventional techniques. Fully intermountable and intermateable with all Cannon D Subminiature types, Mas/Ter-D connectors are terminated at one time with no insulation stripping or complex tooling. Cables may be terminated or used in daisy chain configurations with no cable breaks. Each contact size terminates two wire gages, solid or stranded, utilizing round conductor flat cable or individual wires with most standard insulation materials.

D SUBMINIATURE ALL-PLASTIC 90° D*P
This high performance, low cost D*P all-plastic 90° PCB connector is fully intermateable with all D Subminiatures, and can be mounted over PC patterns without causing short-circuits. It can replace other D Subminiature-type 90° PC connectors without board redrilling. A special contact retention technique holds pins precisely aligned for easier assembly to the PC board. The D*P offers lower total installed cost as well as improved performance and reliability in interconnect systems in such applications as telecommunications, computer and industrial control.

QUICK ACTION GETS YOU ALL THIS...
Got an interconnect problem? Let us help you solve it. Send today for complete product information and a Cannon Quick Action card. Once you've returned it to us, we'll send you a free old fashion apothecary jar filled with Cannon Candy. So take action today and send for our Quick Action card. And see for yourself that Cannon can! ITT Cannon Electric, 666 E. Dyer Road, Santa Ana, CA 92702. Toll-free, 24-hr. (800) 854-3573; in CA, (800) 432-7063. (And be sure to check the EEM Directory for all your Cannon Connector needs.)
Overspecifying your cermet trimmer needs?

Why use multiturn trimmers when CTS single turns provide settability accuracy of .03%...approaching that of a 20-turn trimmer. Compactness, economy and excellent performance add up to a lot of efficiency in product design. You get all these benefits when you rely on CTS single turn cermet trimmers.

For example, the \( \frac{3}{8} \)" diameter Series 375 is available in six popular terminal styles. And they're priced as low as 25¢ each in production quantities.

The CTS Series 345 is a "mini" \( \frac{3}{8} \)" round design featuring low .180" profile, sealed construction and production priced at just 70¢ each.

The \( \frac{3}{8} \)" square Series 360 satisfies a wide range of critical OEM applications. Eleven popular grid spacings include both top and side adjust .100", .125", .150" and TO-5 centers. Low priced, too. Under 40¢ each in production quantities.

All available off the shelf from CTS Industrial Distributors. CTS single turns handle nearly every trimmer application...economically! You be the judge. Call for your Free Sample. CTS of West Liberty, Inc., 6800 County Road, West Liberty, Ohio 43357. Phone (513) 465-3030.

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A world leader in cermet and variable resistor technology.
We've combined refresh with storage in a new modular graphics display.

You build from there.

Suddenly state-of-the-art display technology comes built for the OEM. Tektronix' new GMA display modules let you integrate into your system our most impressive display capabilities ever. Including refresh and storage graphics in one tube. Complete character and vector generators. Big 19" screen and fine resolution.

It's exactly what you need, because you can specify exactly what you want. Order CRT and power supply only, or select from a range of performance and packaging options in our extensive product line.

You can integrate other products from our graphics family, like hard copy modules. Or talk to us about other special product configurations, like our 11" storage-only components.

No other package lets you pick such comprehensive graphic display capability at anywhere near the price. It figures, because Tektronix has been the worldwide low-cost graphics leader for years. No matter what unique and unusual systems you're working with, we can help with manufacturing flexibility, engineering assistance, and a passion for excellence.

Get capability you can build with. From a supplier you can work with. Get your Tektronix OEM Sales Engineer on the phone today. Or write us for more information.

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Information Display Group
OEM Components
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Beaverton, OR 97077

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Tektronix
OEM components:
the perfect fit.

Ship hull display courtesy of University of Arizona

Tektronix
COMMMITTED TO EXCELLENCE

CIRCLE NUMBER 13
You Can Do More with HP Microprocessor Power Supplies...

BECAUSE YOU GET TRIPLE OUTPUT!

for the design stage...

of your microprocessor system, HP's compact, low cost lab power supplies offer more. For example, Models 6236B and 6237B offer three adjustable output voltages. Model 6236B covers 0 to 6V at up to 2.5A. Model 6237B is 0 to 18V at up to 1A. Both have plus and minus outputs of 0 to 20V that track within 1%, or you can switch to a variable tracking mode which allows the negative output to be separately set lower than the positive providing three different output voltages. There are no turn-on/off voltage transients so your circuit is protected against damage. Both models are designed to make development work with microprocessors easier.

for the end product...

where you can feature a triple output OEM Modular Supply specifically designed for powering microprocessor systems. Model 62312D provides three isolated, independently adjustable outputs. The main output is rated at 4.75V to 5.25V at 3A. Two others each range from 4.75V at 0.38A to 12.6V at 0.6A. Other standard features to help optimize your microprocessor design include an internal AC line fuse, fixed foldback current limit, over voltage protection on the main 5V output, remote programming terminals for margin testing and much more. Write for complete details or contact your nearby HP field sales office.

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CIRCLE NUMBER 14
From those who brought you Wescon—here's Midcon

An electronics exposition and convention that is similar to Wescon will debut November 8 to 10 at the O'Hare Exposition Center and Hyatt Regency O'Hare Hotel, just north of Chicago.

Midcon '77 will concentrate on four product areas: production and packaging, components and microelectronics, mini/microcomputers and peripherals, and instruments and control systems.

In addition to the exposition by various manufacturers, 30 half-day technical sessions will be held in the ballrooms of the Hyatt Regency hotel.

Among the topics to be covered at Midcon are universal programming languages and universal interface ICs. The universal programming languages will be covered in Sessions 1 and 6.

In a Session 1 paper, "A Universal Language for Microcomputers," P.J. Plauger, vice president of Yourdon Inc. of New York City, will discuss the industry's need for such a language. According to Plauger, such a universal language would eliminate users' dependence on the whims of different hardware vendors and help keep down the rising cost of program development.

Programming language C, developed at Bell Laboratories, is the ideal candidate for such a task, Plauger proposes. It is high-level enough to permit machine-independent coding across a variety of architectures and close enough to real hardware operations that it can be compiled into compact and efficient code, according to Plauger.

"C is moderately reminiscent of Pascal," says Plauger, "because it is a structured language with data types." Comparing C with Fortran, he points out that anything that can be said in Fortran can be said in C. And the two statements will look similar.

C would be ideal for engineers designing systems around micros that need at least 1000 bytes of code, Plauger believes. Not only that, but the software can begin development even before a final decision has been made on which micro to use. The reason is that C can generate code for any microprocessor.

Unlike other compilers that are relatively inefficient (PL/M produces a machine language program 10 times larger than necessary), the C compiler produces very efficient code. Inefficiency seldom reaches 30% and often is equal to what an experienced programmer can do directly in machine language.

Another discussion of universal software will be given by Roy Carlson of Tektronix in Beaverton, OR. In his Session 6 paper, "Portable Software," Carlson will discuss a compiler generator that he developed that will produce object code for various microprocessors. His idea is similar to Plauger's—that is, to use one language to generate code for any micro. But while Plauger's approach requires the use of C, Carlson's approach enables the designer to make up his own language.

The universality theme is carried over into interfacing in Sessions 2 and 12.

A new universal interface chip, the 2656, will be highlighted at Session 2 by Robert Hartman of Signetics. This chip contains ROM, PROM, RAM and a programmable I/O port. Two notable features are an on-board comparator that makes it possible to place the ROM and RAM anywhere in the memory space and an I/O port that can be set up as either a bidirectional port or as chip-select lines. The chip-select capability, says Hartman, eliminates a lot of the TTL that usually surrounds μPs.

Another universal peripheral circuit, the UPI-41, will be discussed at Session 12. The UPI-41 is a single-chip slave micro that can be used to boost the processing power of other CPUs, says Don C. Phillips of Intel. The UPI-41 features a bit-oriented instruction set that performs control tasks efficiently, according to Phillips. In addition, the device is available in both a masked-ROM version and a UV EPROM version.

Long-term plans for the Midcon show call for the show to be rotated among two or three cities each year. Next year Midcon will be held in Dallas, TX.

Phase-sensing probe finds more shorts, opens

By sensing the phase as well as the magnitude of magnetic fields around current-carrying paths, a current tracer can find short and open circuits in backplanes and cables as well as in printed wiring.

The phase-sensing probe is combined with a dc microvoltmeter in the Model 2220 Bug Hound from GenRad Test Systems Division, Concord, MA. Priced under $800, the Bug Hound also has a source of 600-kHz stimulus signals that can be injected into a wire suspected to be shorted or open.

Two LED lamps are mounted near the pickup-coil tip of the current probe. One or the other lamp lights, depending on the phase of the magnetic field passing through the coil.

If the current probe were held precisely over the center of a current path, neither lamp would light. But as the probe is moved along the path, it inevitably shifts from one side to the other, and cuts through a different phase of the surrounding magnetic field, so the two lamps alternately light, explains Brendan Davis, product marketing manager at GenRad.

Earlier current-probe indicators, like those in Hewlett-Packard's Model...
547A current tracer and in Testline Instruments Inc.'s Short Stop I and II, sense the amplitude of the magnetic field surrounding a conductor, and are brightest directly over the current-carrying lead. But looking for maximum brightness to determine which lead is carrying current is much more difficult than looking for a switch from one bulb to another, according to Davis. And amplitude-sensing tracers are almost useless for checking out cables and wire-wrapped backplanes because their probes cannot be held at a constant distance from the lead. The brightness of their indicators varies even when the current does not.

In some cases, shorts can be found simply by injecting a signal across two leads and tracking current with a microvoltmeter. The Bug Hound's microvoltmeter has two ranges—50 and 500 μV full-scale. Similar voltage sensing—and nothing else—is performed by the Short-Trak from Digital Facilities Inc., Dallas, and the Model 42 Microprobe from Integral Electronics Corp., Commack, NY. While the recently introduced Microprobe is a relatively simple microvoltmeter and nothing more, it does feature the lowest price for a current-tracing instrument—$94.50.

For more information, circle the following numbers:
- GenRad 431
- Hewlett-Packard 432
- Testline Instruments 433
- Digital Facilities 434
- Integral Electronics 435

**Videocassette player handles 4-hour tapes**

Capable of recording up to four hours on a single cassette, the RCA SelectaVision color videocassette recorder has twice the capacity of previously available VCRs such as Sony Corp.'s Betamax. And with a "dealer optional" price of $1000, the SelectaVision costs also a couple of hundred dollars less.

Made for RCA by Matsushita Electric Industrial Co. Ltd. in Japan, the SelectaVision runs at 0.66 ips in the four-hour mode or 1.31 ips in the two-hour mode. The Betamax records for two hours at 0.79 ips or for one hour at 1.57 ips.

The VCR can be connected to any monochrome or color TV between the antenna lead and the TV set. Tuners for uhf and vhf stations on the VCR permit recording one program while watching another. Programs can be selected in advance and recorded automatically with the recorder's built-in digital clock/timer.

Blank video cassettes will be available from RCA in two lengths—two-hour ($17.95) and four-hour ($24.95). An optional monochrome TV camera with a flip-up viewfinder goes for $299.95, while a deluxe black-and-white camera with zoom lens and through-the-lens viewfinder is priced at $399.95.

The SelectaVision VCR is compatible with the Video Home System (VHS) cassette standard developed by JVC Corp., a Matsushita subsidiary. VHS cassette players are marketed by JVC, Matsushita (under the Matsushita brand name, Panasonic), Hitachi, Mitsubishi, and Sharp, as well as RCA.

According to RCA forecasts, nearly 250,000 VCRs will be sold this year, with sales rising to 750,000 units in 1978 and well over 1-million units the following year. By contrast, it took color TV ten years to reach the million-a-year level.

RCA earlier used the SelectaVision name to describe its videodisc player. Despite a flurry of interest in video discs two years ago and an announced intention to manufacture its own players, the RCA videodisc effort is currently described as "dormant."

**Plastic VMOS FETs vie with power bipolaras**

Thanks to plastic packaging, three vertical-channel MOSFET power FETs will be available for about one-third the price of similar devices packaged in metal. Moreover, with hundred-quantity prices of $.96 for the 40-V VN64AF, $1.00 for the 60-V VN66AF and $1.10 for the 80-V VN88AF, Siliconix expects its 2-A, 12.5-W units to make circuits that use them cost-competitive with designs using bipolar transistors.

Unlike power bipolaras, VMOS FETs can be paralleled without the ballasting resistors that are needed to prevent current hogging that occurs when bipolaras are paralleled. Negative drain current tempco provides self-regulation—as junction temperature increases, current decreases.

In VMOS FETs, a vertical current flow created by a V-shaped gate gives the devices a much higher current density than that of conventional lateral MOSFETs. In fact, the VMOS structure can handle amps in a chip area that conventional MOSFETs need for milliamps. Moreover, the VMOS structure improves switching speed, linearity, breakdown voltage and drain-source resistance.

The three Siliconix TO-202-packaged VMOS FETs have on-chip protection zeners and are produced by the deep-groove VMOS technology used by Santa-Clara-based Siliconix and its licensee, Semtech of Japan, to produce discrete devices. This process should not be confused with the shallower-groove technology that produces VMOS ICs.

Right now, small quantities of the plastic-housed VMOS FETs can be obtained for evaluation. Large quantities are expected to become available from stock in October.

**Shuttle tolerates glitch—computer gets "voted out"**

Milliseconds after the space shuttle orbiter Enterprise cut loose from its mother aircraft for its first free flight, three on-board computers sensed that a fourth was malfunctioning and immediately shut it down. The mission continued on to a textbook landing.

What's more, still another computer malfunction could have been tolerated by the ship's redundancy-management system before the crew had to switch-in a semi-automatic backup guidance and control system.

The Enterprise has a quadruple-redundant, intelligent-interactive computer network—the guts of a data-acquisition and control system so sophisticated it can guide the craft to a safe landing on Earth with less human intervention than it takes to drive a car. With most redundancy techniques a master/slave approach puts one element in control, with the others taking over in case of a failure. But not on the space shuttle orbiter.

The four computers operate in parallel from a common clock. They each acquire data from triple-redundant sources, such as accelerometers, rate gyro, and manual pilot controls and compare their inputs. Small differences aside, the four computers agree to use just one value—the median.

Each computer then makes its own calculation as to how much deflection an elevon rudder or air brake requires.

Before a control surface (or rocket thruster) is commanded to do anything, the four computers compare their outputs-to-be. Should any one computer disagree with the other three, it will be shut down by the others.
Semtech Corporation introduces "X-WAY STIC" a new series of open rectifier sticks specifically designed for X-ray power supplies.

Each X-WAY STIC utilizes hermetically sealed Metoxilite multi-chip "avalanche" rectifiers mounted on a PCB. These Metoxilite multi-chip rectifiers (technology initially developed for high reliability aerospace programs), are now available at reduced prices.

In addition to X-ray power supplies, these rectifiers can be effectively used in most standard, single and polyphase circuits. Designed for use in oil environment.

Types: X100KS, X125KS & X150KS
PfV (operating): 100, 125 & 150kV
PRV (test): 125, 150 & 175kV
Average Rectified Current @ 55°C Oil: 150mA
Reverse Current @ PRV: 1.0 µA
Recurrent Surge (10 cycles @ 60 Hz rate): 7.5A
Single Cycle Surge @ 8.3ms: 25A
Forward Voltage @ 50mA: 160, 190 & 220V

RELIABILITY COSTS LESS!

1975 NATIONAL SBA SUBCONTRACTOR OF THE YEAR
A VMOS transistor, magnified 15,500 times.
is no longer flat.

AMI creates VMOS. This revolutionary idea revolves around a three-dimensional transistor, etched into the silicon substrate.

The result? A circuit that's extremely fast, dense and inexpensive.

It isn't blue-sky theory. The first VMOS RAM, the 1K S4015-3, is in volume production now. And a reputable second source has committed to manufacture VMOS RAMs in 1978.

Our 35 nanosecond (typical, 45 nanosecond maximum) 1K static memory is pin compatible with the fast 1K NMOS and bipolar RAMs, and leads the way for the large family of VMOS products arriving soon. These will include:

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<th>NEW VMOS PRODUCTS AND TYPICAL ACCESS TIMES</th>
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<td>4K fully static RAM</td>
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<tr>
<td>80 ns</td>
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<tr>
<td>4K fully static RAM</td>
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<td>(4K x 1)</td>
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<tr>
<td>80 ns</td>
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<tr>
<td>4K fully static low power RAM</td>
</tr>
<tr>
<td>(4K x 1)</td>
</tr>
<tr>
<td>45 ns</td>
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<tr>
<td>8K fully static RAM</td>
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<tr>
<td>(1K x 8)</td>
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<tr>
<td>125 ns</td>
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<td>16K ROM</td>
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<td>(2K x 8)</td>
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<td>100 ns</td>
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<td>64K ROM</td>
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<td>(8K x 8)</td>
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<tr>
<td>250 ns</td>
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<tr>
<td>16K EPROM</td>
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<td>(2K x 8)</td>
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<td>200 ns</td>
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The density permitted by vertical short-channel FETs produces VMOS circuits that are much smaller than competitive chips, increasing the speed and lowering the cost. For example, the latest bipolar 1K size is 61% larger, and the new fast NMOS 1K is 87% larger than AMI's S4015-3. And VMOS densities are achieved without stretching feature dimensions at the sacrifice of yields, as is necessary with bipolar and NMOS technologies.

VMOS: the new technology from AMI

In short, VMOS presents the best of all possible worlds. If you want to stay up to speed at a down-to-earth price, call your nearest AMI distributor or sales office. Or write to AMI Marketing, 3800 Homestead Road, Santa Clara CA 95051. You'll be entering the MOS world of the future.

VMOS: the new technology from AMI

See VMOS at Wescon, Booth 821

CIRCLE NUMBER 17
Analog boards for microcomputers: You can’t always get what you want

Interfacing a microcomputer board with the “real world” of analog signals, such as those from thermocouples and other transducers, may prove more difficult than expected. Unless you’re using one of the most popular microcomputers—say, from Intel, Motorola, Digital Equipment, Pro-Log or Zilog—you may not be able to buy a ready-made and compatible analog-interface board. And even if you do find a compatible board, you may find it doesn’t have the specific features you need in your applications.

Worse, so much of the microcomputer’s time may be spent controlling and waiting for analog circuits that your complete system will perform at a snail’s pace. Performance may fall far short of the “megahertz” promised by the microcomputer’s clock-rate spec or the “hundreds of kilohertz” promised by the analog board’s throughput spec. Also you may have to sacrifice speed for either greater accuracy or channel capacity.

The situation is not a happy one for system designers. At this year’s Industrial Electronics Control Instrumentation Conference in Philadelphia, PA, several engineers complained that the semiconductor industry had over-sold them on microprocessors, while failing to provide compatible analog I/O circuits.

Microcomputers have appeal

Microprocessor circuits are often preferable in systems that have a dedicated application. A microcomputer is appealing here because it can be easily programmed for a specific job by changing a programmable read-only memory and a few other parts.

But if you then have to design your own analog-interface system, development costs may skyrocket—and defeat the purpose of using a microcomputer in the first place. The answer? A pre-designed analog board you can tailor to your application just as easily as you program your microcomputer.

Fortunately, several analog-interface boards are available for the more popular microcomputers. But, the choice narrows if you aren’t using a microcomputer made by the “Big Five.” For example, Data General’s microNova has a lot of appeal because of its performance and software support. Yet it has no compatible analog board. Another powerful microcomputer that lacks analog-board support is the Texas Instruments TM 990/100.

However, analog support will soon be available for both these microcomputers. Datel plans to introduce an analog board for the microNova, and both Analog Devices and TI will soon bring out boards for the TM990.

Data General does, of course, provide analog boards for its older Nova minicomputers, while TI has an analog board for the 990/4 computer (also microprocessor-based), made by its Digital Systems Division.

Too many microcomputers

The over-all problem is that microcomputers are simply introduced much faster, and in greater quantities, than analog boards. There are signs, however, that the situation will have to stabilize. Microcomputer vendors now face a “chicken-or-the-egg” dilemma. The market for a microcomputer is severely limited unless it can be designed into analog systems. Yet who
will risk introducing a compatible analog-interface system for a microcomputer that isn't being widely used?

Until recently, the traditional analog and data-conversion module manufacturers—like Burr-Brown, Analog Devices, Datel and Analogic—have been the most willing to introduce analog-interface boards. For these companies, microcomputers represented another opportunity to sell modules. Not only could they sell modules directly to engineers who were building their own interface boards, they could also sell complete boards that used modules as components.

Also among the first to offer analog-interface boards were a group of smaller companies—such as ADAC, Automated Industrial Measurements and Data Translation. These companies were often started by engineers who had left the larger data-conversion companies. The microcomputer-interface market, though small at the time was large enough for these companies to survive and grow.

Only recently have the larger microcomputer manufacturers started to sell analog-interface boards. Facing an increasingly competitive market for microcomputers, these companies now find that analog support is becoming an important factor when a system designer makes his choice.

Of course, for a microcomputer-based analog system, analog support is just as important as software support and other types of hardware support. Already, Intel, Motorola, Zilog, DEC, MIT's, Cromemco and Wintek sell compatible analog-interface boards for their microcomputers. Several others are expected to follow suit.

Where should you buy?

But which source is preferable? Provided you've chosen the right microcomputer and the right analog-interface scheme for your system, you can safely order an analog board from any reputable vendor.

However, microcomputer manufacturers argue that since they design digital systems, of course, they understand them better than do data-conversion specialists. Furthermore, they're in a better position to evaluate hardware-software tradeoffs in interface-circuitry design. Also, they say, they can test the combined analog-and-digital system completely by using computer-based equipment and an extensive diagnostics library.

Data-conversion specialists argue that they understand all the subtleties of analog and interface design—how to avoid ground loops, where to add filtering, how to minimize the many error sources and how to budget for a specified total error. Furthermore, they say, since they have extensive experience in analog-interface applications, they better understand their customers' requirements.

You don't have to go one way, however. Some microcomputer manufacturers test and resell analog boards designed by module manufacturers. For example, Motorola sells boards made by Burr-Brown. Intel's boards are developed in cooperation with Analogic and use that company's modular components.

Compatible with Intel's SBC 80 microcomputers, Burr-Brown's MP8600 analog I/O board costs as little as $198 (in quantities of 100) for a 16-channel input-only configuration.

Even when a microcomputer manufacturer designs and makes its own analog boards, it often uses components and subsystems made by analog-module manufacturers. Consequently, most critical analog and interface circuits are designed by experts. On the other side of the fence, the analog houses often perform comprehensive computer-based tests. And many of them supply diagnostic software, so that you can test an analog system with your microcomputer.

Remember, however, that a manufacturer will be more likely to help you make the right choices if the company has a broad line of products. For example, if a microcomputer manufacturer offers both 8-bit and 16-bit machines, the company will be more ready to tell you that the larger machine is better able to handle your high-level language. Similarly, a company that makes analog boards for several different microcomputers can afford to be objective when helping you decide which microcomputer will work best in your application.

Even when you consider yourself ready to select a compatible analog board, you're not out of the woods. As a first step, be sure that you and the prospective vendor agree on the meaning of "compatible."

What is "compatible"?

Some vendors may have a rather liberal idea of what constitutes a "compatible" board. At the very least, the board should be the same size as the microcomputer and have connector pinouts that conform to the microcomputer's bus standard. Further, the analog board should have the same supply voltages and logic levels as its digital partner. Unfortunately, some boards don't even meet these minimum requirements.

Most boards meet board-size and bus-compatibility requirements, but even here you run into a problem. One bus standard that's widely used by computer hobbyists, the S-100, is not really a standard at all. At best, it provides only fuzzy guidelines for designating its pins. About 15 undesignated lines are used by different manufacturers for different functions.

Because of problems with early de facto standards like the S-100, more and more manufacturers are adopting other standards, such as Intel's MDS bus. Consequently, microcomputers...
from companies other than Intel can work with analog boards designed for Intel's SBC-80 series. For example, the Analog Devices RTI-1203, though designed for the SBC-80 series, works with National's BLC80 microcomputer as well.

Unfortunately, Intel's standard also has some undesignated pins. However, analog-board manufacturers will probably work closely with Intel this time around. Intel's arrangement has eight undesignated lines right next to the 8-bit data bus. Since this configuration obviously will allow simple expansion of the data bus for 16-bit microcomputers, interface-board designers will probably steer clear of those undesignated pins.

Perhaps the most commonly violated requirement for board compatibility is the supply voltages required. Most microcomputers work from +5 V dc, while analog-interface systems usually require that and ±15-V supplies. To make the board compatible, an inverter is usually added to derive the ±15 V from the +5-V line. Unfortunately, board manufacturers often list the inverter as an option so that they can quote a more competitive price for the "basic system." So check your supply-voltage requirements before comparing prices. And while you're at it, investigate the effects of inverter noise on your low-level analog signals. You may find you're better off providing your own filtered ±15-V power, instead of taking the inverter option.

Another area of compatibility to investigate is the logic levels. Everybody talks glibly of "TTL levels." But if the fanout is only one, and the noise margin is near zero, you may run into system problems. Remember also that a microcomputer bus usually requires three-state logic, not just simple TTL.

Is performance compatible?

Even if an analog board meets the minimum requirements for compatibility, it may still be a poor match for the microcomputer. For example, a fast microcomputer may have to stop its calculations and wait for a slow analog board to deliver its data. Or the analog board may require elaborate software subroutines—which will tie up the microcomputer's time and memory—for simple tasks that could have been handled more efficiently by hardware on the analog board. The combined performance of the two boards will often fall far short of what you might expect from the individual board specifications. Synergy is rare.

If you look at the data sheet for an analog board, you'll find a bewildering array of specs. Even after you've pinpointed the key specs, you'll still have to interpret their significance to your system. And this interpretation requires an understanding of the different schemes used for interfacing with microcomputers. Often a block diagram can tell you just as much as the performance specs.

Every analog-output system requires at least one digital-to-analog converter. Similarly, every analog-input system needs some sort of a/d converter—usually, but not necessarily, implemented with hardware. Exceptions are schemes where a d/a converter, or just a comparator, is employed in a microcomputer-controlled feedback loop to perform a/d conversions. So even a basic single-channel system can have alternative schemes and hardware-software trade-offs.

In more complex multichannel systems, which employ multiplexers, registers, sample-and-hold circuits and programmable amplifiers, the possible circuit permutations skyrocket.

There are three important configurations for data-acquisition systems, according to Jim Sherwin, Data Acquisition Applications Manager for National Semiconductor:

- A "multiplexed random-channel-addressed" scheme—an analog multiplexer delivers one signal at a time to a sample-and-hold (s/h) circuit, which then stores momentary signal values for digitizing with an a/d converter.
- A "multiplexed-with-memory" scheme—the digital signals after conversion are stored in a RAM or shift registers for rapid access by the microcomputer.
- A "parallel-conversion" scheme—each analog channel has a dedicated a/d converter.

Most commercial data-acquisition boards use variations of the first and second methods. Up to now, parallel-conversion systems have been rare because of the high cost of the a/d converters for a multichannel system. However, such a scheme is becoming more and more feasible because low-cost monolithic converters with adequate performance are starting to appear.

Speed costs money

The random-channel-addressed scheme is low-cost, but tends to be slow. The microcomputer, after addressing a channel, is usually forced to wait while the multiplexer selects the channel, the s/h circuit acquires the signal, and the converter digitizes the signal and releases the microcomputer's Ready line.

The other two schemes allow the microcomputer to access the data as memory, which tends to be faster and more convenient for the microcomputer. Of course, with a multiplexed-with-memory scheme, the data will be more stale than with a parallel-conversion scheme, because of multiplexer delays. Nevertheless, both schemes can avoid tying up the microcomputer during conversions. Further speed savings can be achieved by using different interrupt techniques. But it's difficult to provide general guidelines because priorities depend on the application.

Of course, not every application requires flat-out speed. If you're digitizing slow-changing temperature signals, for example, you'd probably be happy to trade speed for accuracy. Though it's possible to achieve speed combined with accuracy where it's needed—in radar-signal processing, for example—this tends to be expensive. You're not likely to find this combination in the average microcomputer interface board.

Though the reasons for a speed-vs-channel-capacity tradeoff are quite obvious—primarily multiplexer and scanner delays—the reasons for trading speed-for-accuracy tend to be more subtle. In general, however, high-speed circuits tend to be noisy because they require that large currents be switched to charge stray capacitances. Noise, of course, can be a major contributor to system errors. Also, large currents in high-speed circuits can magnify the

(continued on page 30)
Southern Railway has a long track record of being one of the most profitable rail systems in the country. To help stay on that track, they decided to increase the speed and flexibility of their online distributed communications network. So Southern Railway is now changing dumb terminals into intelligent ones throughout its rail system, using microNOVA microcomputers.

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Some manufacturers of analog boards for microcomputers

<table>
<thead>
<tr>
<th>Company</th>
<th>Microcomputers for which compatible boards are offered</th>
</tr>
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<tbody>
<tr>
<td>ADAC Corp., 15 Cummings Park, Woburn, MA 01801</td>
<td>•</td>
</tr>
<tr>
<td>Analog Devices, Route 1 Industrial Park, Box 280, Norwood, MA 02062</td>
<td>•</td>
</tr>
<tr>
<td>Analogic, Audubon Road, Wakefield, MA 01880</td>
<td>•</td>
</tr>
<tr>
<td>Automated Industrial Measurements, Box 125 Wayland, MA 01778</td>
<td>•</td>
</tr>
<tr>
<td>Burr-Brown, International Airport Industrial Park, Box 11400, Tucson, AZ 85734</td>
<td>•</td>
</tr>
<tr>
<td>Cromemco, 2432 Charleston Road, Mountain View, CA 94043</td>
<td>•</td>
</tr>
<tr>
<td>Cybernetic Micro Systems, 2460 Embarcadero Way, Palo Alto, CA 94303</td>
<td>•</td>
</tr>
<tr>
<td>Data Translation, 23 Strathmore Road, Natick, MA 01760</td>
<td>• • • • • • •</td>
</tr>
<tr>
<td>Datel Systems, 1020 Turnpike Street, Canton, MA 02021</td>
<td>•</td>
</tr>
<tr>
<td>Digital Equipment Corp., Main Street, Maynard, MA 01754</td>
<td>•</td>
</tr>
<tr>
<td>Intel, 3065 Bowers Avenue, Santa Clara, CA 95051</td>
<td>•</td>
</tr>
<tr>
<td>MITS, Div. of Pertec, 2450 Alamo SE, Albuquerque, NM 87106</td>
<td>•</td>
</tr>
<tr>
<td>Motorola, Box 20912, Phoenix, AZ 85036</td>
<td>•</td>
</tr>
<tr>
<td>PCS Inc., 750 N. Maple Road, Saline, MI 48176</td>
<td>•</td>
</tr>
<tr>
<td>SEA, 620 S. Rangeline Road, Carmel, IN 46032</td>
<td>•</td>
</tr>
<tr>
<td>Signal Laboratories, 202 N. State College Blvd., Orange, CA 92668</td>
<td>•</td>
</tr>
<tr>
<td>Wintek, 902 N. 9th Street, Lafayette, IN 47904</td>
<td>•</td>
</tr>
<tr>
<td>Zilog, 10460 Bubb Road, Cupertino, CA 95014</td>
<td>•</td>
</tr>
</tbody>
</table>

(Note 1: Available January 1978)  
(Note 2: Available only from the microcomputer manufacturers, not from Analogic)  
(Note 3: Available later this year)

(continued from page 28)
errors caused by thermal drift.

If you don't need speed, then, it usually pays to specify a slower system. A system with an integrating a/d converter—popular for DPMs and low-cost DVMs—will tend to filter out low-frequency noise, whereas a faster successive-approximation converter will be prone to jitter of its least-significant bits in the presence of noisy analog signals. Of course, you can always ignore the last digit or two—using, say, a 10-bit converter in an 8-bit system. But why pay for more resolution than you really need?

For good accuracy and low speeds, other data-acquisition schemes may work better than those using conventional a/d converters. In industrial systems that often require long trans-
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ducer cables in a noisy environment, such techniques as voltage-to-frequency conversion and delta-sigma modu-
lation are gaining in popularity.

One advocate of voltage-to-frequency conversion is Barry Hilton, President of Automated Industrial Measure-
ments. His company makes what he calls a "microcomputer frequency meter," which is compatible with most 8-
bit microcomputers.

"The low-level signals from the transducers are converted to frequencies at the transducer location so that
analog errors and noise problems are minimized," Hilton explains. The output frequency is then transmitted over a
twisted pair which also carries the power to the voltage-to-frequency con-
verter. "To interface with the micro-
computer, Hilton continues," we use a
digital multiplexer (which includes
memory) and our frequency-meter
card. Thus we avoid having to handle
analog signals."

Hilton's scheme not only avoids the
problems involved in processing analog
signals, it also avoids the need for a
frequency-to-voltage converter to de-
code the signals after transmission. Ripple in the output of many com-
commercial f/V converters has prevented
widespread use of f/V conversion for
data acquisition.

Noise can be an especially tough
problem when you're handling low-
level signals. Though several com-
panies offer analog-input boards that
accept low-level signals of 10 mV or so,
you usually shouldn't try to do all the
amplification on the interface board. A
better approach is to amplify the sig-
als at the transducer, or, even better,
convert at the source, as with Hilton's
system. Certainly, if you choose to use
a board with low-level inputs, you
should make sure the input amplifier
has good common-mode rejection. But
even then, the approach isn't advisable
with input leads of more than a few
feet in length.

Check the options

If manufacturers don't recommend
low-level inputs for analog boards, why
do they provide boards with this capabil-
ity? The answer, of course, is
that customers have requested boards
that accept low levels. It turns out that
manufacturers can quite easily tailor
boards for a specific market because
the boards are assembled from stan-
dardized modular or IC components.
To meet a specific need, the manufacturer
merely changes a few components on
his basic board. So if a manufacturer's
catalog doesn't list a board that has exactly the features you need, don't be
afraid to ask if a certain basic board
can be modified to your custom re-
quivalencies. For example, you may
decide you don't want voltage inputs
—you prefer an isolated 20-mA current
loop. Some boards offer this feature
outright, while others can be modified.

Another area of analog-board per-
formance that can often be customized
is converter speed and accuracy. Fred
Molinari, President of Data Trans-
lation, explains how this works for his
company's boards: "Our standard
boards have a throughput specification of 35 kHz (or 28.5-µs conversion time
can be drilled out and interconnected
with hookup wire and solder.
Jumper connections allow you to
interconnect analog and digital
grounds, establish the required imput
tage, or define the clock fre-
cequency for conversions, among other
things. Several companies have ampli-
fiers whose gain can be programmed
by changing a resistor value. And some
boards—from Analog Devices and
Cybernetic Micro Systems—include
software-programmable amplifiers.

Big boards are versatile

The most versatile boards are the
larger ones, like those for the Intel,
Motorola and DEC microcomputers.
They have the most room for the vari-
ous optional circuits. However, the
smaller analog boards, like those for
Pro-Log and Wintek microcomputers,
also have advantages for breadboard-
ing. You need only buy the individual
circuits as you need them. You don't
have to start with an expensive fully
loaded board. Also, Wintek's boards
are the same size as the popular Vector
boards, which allow you to easily hook
up your own circuitry.

The larger boards have enough room
to include both an analog-input system
and an analog-output system. With
smaller boards, these are usually sepa-
rate. Larger boards can also fit in such
features as a PROM, a local controller
or a crystal-controlled real-time clock.
It's often convenient, too, to have
digital inputs and outputs on an analog
board. For example, if an analog board
is driving a chart recorder, you may
need digital signals to control pen-lift
and color-change functions.

Even with the wide range of options
available for today's analog-interface
boards, you can't interface with every
microcomputer on the market. In
many cases you'll be forced to design
your own boards. But this task is
greatly simplified by data-acquisition
modules that contain the key circuits
you'll need. Some examples of these
modules include Burr-Brown's Micro-
peripherals, a two-chip hybrid-IC set
from Micro Networks, and Datel's
MDAS and HDAS circuits (modular
and hybrid, respectively).

Finally, manufacturers are starting
to pay attention to the much neglected
area of industrial applications. For
example, Burr-Brown has just in-
vented a set of industrial boards for
Motorola's M6800. For more on this, see
p. 131.
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At Wescon '77

Home computers: from a bag of parts to a system you simply plug in

The home computer is about to become a major consumer item—like televisions, microwave ovens, and videotape recorders.

This forecast as well as the developments in the home computing field itself will be covered at Session 22 of the Western Electronic Show and Convention (Wescon) in San Francisco, September 19 to 21.

Introduced just three years ago, home-computing systems are evolving into complete, ready-to-use systems.

- Evolving into complete, ready-to-use systems.
- Declining steadily in price.
- Creating a market for software and maintenance services.

Originally, home computers were available as a bag of parts that had to be assembled. Two years ago, assembled and tested boards became available. Now, assembled systems that can simply be plugged into the wall are beginning to appear. The latest entry in the home-computing market costs $600.

Personal computers are the natural outgrowth of existing markets for programmable desk-top calculators, hobby computer kits and even programmable video games, says Robert F. Wickham of Vantage Research in "Home Computers: The Future is Here." Some of the high-priced games use microprocessors and ROMs. And the programmable games being readied for 1978 will have alphanumeric keyboards, user programmability and high-level language programming.

Another key ingredient in the growth of the personal-computer market will be the easy availability of support and maintenance services, says Wickham. Even now, several companies are offering ready-to-use software on a variety of media, such as printed paper, tape cassettes, optically encoded pages, records and telephone-accessed subscription services.

As a matter of fact, repair and maintenance will be handled primarily by the existing consumer-electronics repair shops, Wickham foresees. Like CB radios, home computers will be serviced by either independent service shops or factory-repair stations. Indeed, TV sets with integral programmable games, to be introduced next year, will pull the conventional TV repair shops into the computer age.

Noting the potential size of the market, Wickham predicts that by 1985 the market for home computers will be close to $2-billion. This includes $800-million worth of equipment that will be used by small businesses.

PETs belong at home

Several personal-computing systems will be introduced this year. One home system that has already been announced is the Personal Electronic Transactor computer (PET) from Commodore Business Machines, Palo Alto, CA. In his paper, "PET Computer," Charles Peddle of Commodore describes some of the characteristics and capabilities of this complete home system, which sells for $600.

A stand-alone computer, the PET consists of a 9-in. black-and-white CRT that can display up to 1000 characters (25 lines by 40 columns), an ASCII keyboard and numeric pad, and a cassette-tape recorder for program storage.

The PET also contains a memory-
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CIRCLE NUMBER 23
expansion bus, a port for an additional cassette recorder, a user-controllable 8-bit bidirectional parallel port and an IEEE 488 interface port.

The home system works primarily in BASIC, notes Peddle. Plugged in and powered on, it determines the amount of memory available to the user and displays the result on the CRT. At this point, the PET can accept a program from the tape cassette, keyboard or from an auxiliary storage device such as a floppy disc.

The PET was designed with consumers in mind, notes Peddle:

- It had to be priced to attract the average consumer.
- It had to be packaged and presented so that the normal retail clerk can sell it to someone who knows very little about computers.
- It had to be serviceable through normal retail service networks.

With its ability to self-diagnose and its modular design, the PET will be easy to service, notes Peddle. The main board, which would be the least familiar to TV repairmen, contains LEDs that indicate a problem immediately. The board can then be snapped out and replaced with a new one.

Another board, for the CRT, is similar to those used in conventional TVs. A third board contains the electronics for the cassette recorder. It is identical to those used in standard recorders, except that the audio section has been eliminated.

While the PET provides everything needed to get started in home computing, according to Peddle, expansion will be possible with additional peripherals, which are now being planned.

Industry uses them, too

Not all home computers will be used at home, states Don M. Muller a senior vice president at Pertec Computer Corp. In fact, by 1980 20% of the home computers sold will actually be used in business, Muller notes in "Home Computers in Small-Business Applications." Like Robert Wickham of Vantage Research, he believes that by 1985, business applications will account for $800-million—or more than 40% of the market.

Billing and office work are among the more obvious potential business applications, according to Muller. Computers can keep ledgers, make out bills and statements, flag slow-paying accounts and handle most of the number crunching required by a small business. They can also manage mailing lists and help handle word processing.

The future is bright, but...

But bright as the future may appear, Muller warns, several problems remain to be solved—and the biggest is supplying useful software, and at a low price. But, this problem is on its way to being solved, Muller points out. Many personal-computer owners are writing their own software and packaging it for sale.

In addition, manufacturers are providing ever-increasing support. MITS, for example, which started the whole home-computing market rolling just three years ago, has set up a separate subsidiary, the Altair Software Distributing Company, solely for handling software—obtaining it, refining it, licensing it and distributing it. The new company is also putting together collections of programs designed to perform such specific business functions as office accounting or handling sales data for insurance clients.

At Wescon ’77

Distributed processing spreads computer intelligence around

As the need for large, centralized computer resources dissolves and computer costs fall, computer power is finding its way into more and more areas of business. That’s the over-all conclusion of “Transition to Distributed Processing,” Session 23 at Wescon ’77.

“Integration of computers into all aspects of business is best achieved through decentralization. “The only way computers can play their proper role in business is within a decentralized structure,” says Jacob Sternberg, chairman of Session 23 and president of Conversational Systems Corp., New York. Lower cost, easier control of costs, and improved information flow are among the reasons Sternberg cites for switching to distributed processing.

Distributed processing is “an umbrella term for a variety of processing structures whose common goal is the placement of local computer power at the disposal of every unit of the business,” according to Sternberg. This dispersion should enhance each unit’s operations and control the flow of information among the units, he says.

Not so easy to implement

But breaking up the centralized computer establishment to achieve the goal of distributed processing may not be a simple task, Sternberg cautions, explaining: “The investment in a centralized facility is usually large. Disturbing the operational calm of such a facility may be disastrous. The decision of how to decentralize may be painful for top management, [which] does not really know or trust ‘those machines.’”

Andy Santoni
Associate Editor
For two-wire, full-duplex operation at 1200 BPS, Universal Data Systems proudly announces the Model 12·12, the newest addition to the UDS family of data modems. The unit operates synchronously or asynchronously over unconditioned dial-up or private telephone lines.

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$600 Single Unit Price.
A centralized data processing structure has a "social order" of users, and the conflicts that go along with such an order, Sternberg goes on. Yet, despite the expense and the problems involved in centralized processing, such facilities manage to perform their assigned role of supporting the daily operations of a business.

Centralized processing even has some advantages, says Sternberg. "Equipment breakdowns are not excessive and are handled properly. Generalized packages handle immediate problems." But one big disadvantage is that many corporate executives don't understand how a computer center operates. Besides being a problem when a centralized system is being used, this lack of understanding can hinder efforts to switch to more efficient methods, says Sternberg. "Since software is viewed as a massive and expensive effort, the obvious question of what it would take to change to decentralization brings visions of vast expense. Even though management is aware that theoretically decentralization is possible, data-processing management hasn't explained how to get there. Worse, the technologist hasn't explained why it is necessary to get there."

Lack of understanding

But management can be convinced that a change is possible and advantageous, he says, because major computer manufacturers, led by IBM, are committed to distributed processing, and can provide the education necessary for managers and technicians. In addition, successful implementations already exist, so companies won't have to be pioneers—a very costly occupation. Moreover, there are many small companies ready to augment the corporate staff in solving local and central problems, and a large pool of technically competent personnel to develop and maintain distributed systems.

Small computers improving

Engineers can now develop low-cost distributed-processing systems in part because small computers are highly reliable, and are becoming even more so—the designer needn't worry anymore that hardware placed "in the boondocks" will require excessively expensive maintenance. In addition, remote peripherals—taking advantage of microprocessors—can be as simple or complex as required, and can easily be customized by changing hardware or software. Hardware interfaces, controllers, peripherals and communications devices all have enough intelligence to enable simple hookups. And compatible software is available.

Meanwhile, economics will force the semiconductor industry to standardize parts designed for distributed-processing applications, at least at the interface, predicts Mark Levi in another Session 23 paper. And as low-cost hardware becomes more prevalent, the marketplace will cause the current mini and macrocomputer houses to take a closer look at standardization. "Perhaps IBM's active pursuit of Series 1 peripheral suppliers is a nod in that direction," says the director of microcomputer systems at National Semiconductor Corp., Santa Clara, CA.

Microprocessors improving

Microprocessors will have greater throughput, adds Levi, as cycle times improve and architectures become more efficient, and as instruction repertoires become larger and more powerful. "Processors may contain ancillary circuits, or may be microprogrammable, stack-oriented, language processors or in fact anything that has been done in the mini or macrocomputer world."

Of course, "RAMs and ROMs will continue to get larger, cheaper, and lower power," says Levi, adding that 16-byte ROMs are not far off. Peripheral control chips will proliferate and be programmable to allow wider differentiation of standard products, he adds. "All parts will be designed to allow easier interconnection, and to put the burden on hardware as much as possible. Manufacturers will tend to standardize the universal buses and avoid specialized chip families."

The number of microprocessor components to be purchased indicates the scope of the change taking place, Levi continues. "In 1980, National forecasts a consumption of 1.5-million 8080 software-compatible microprocessors. Although many will be used in dedicated and/or control applications, that is still a lot of intelligence that will be absorbed by industry."

This intelligence can best be used to displace the present centralized processors with one of two types of distributed processing systems, says Conversational Systems' Sternberg—hierarchically or nonhierarchically structured.

There's more than one way to distribute processing power through an organization. A hierarchically distributed structure (top) is simplest and easiest to visualize and expand. But some computer users, like oil companies, have systems so complex they can be represented graphically by only the most over-simplified diagram (center). Just one node of the oil company's processing system—distribution, for example—has a complex representation (bottom).
The failure. A 16 W overload causes this 1/2 W carbon film resistor to burst into flame. The initial failure mode is a short circuit, causing even more current to be drawn as shown on the meter.

The successful failure. The TRW 1 W rated BW-20F (1/2 W size) stays cool and fuses quickly and safely under identical power surge conditions. The failure mode, as shown, is an open circuit.

A failure your circuit can live with.

Failsafe, Fusible, Wirewounds Offer Built-In Circuit Protection.

Cool wirewounds like our BW failsafe series have a dual personality.
They provide stable resistance to normal operating current. But at specific overloads, they open circuit like a good fuse. So, as shown above, they'll protect your circuit from excess heat and fire in places where severe fault conditions are encountered.

The BW failsafe series, UL listed per Document 492.2, can save cost by eliminating the need for both resistor and fuse. Save space, too, because they're about half the size of standard 1 and 2 W devices.

Depending on your specific circuit parameters, other TRW film and wirewound resistors can be engineered to meet your requirements.


TRW IRC RESISTORS
ANOTHER PRODUCT OF A COMPANY CALLED TRW
CIRCLE NUMBER 25
Expand your options with Amphenol® connector systems.

You'll find more ways to get a job done fast and economically. Why settle for less?

You can get the tried and true in connectors from us. Or you can challenge us to come up with something that's right out of tomorrow's headlines. We're loaded with ideas.

In fact, there are literally thousands of different kinds of Amphenol connector products. Those are pretty good odds, whether you're looking for cost-cutting connectors for business equipment or consumer electronics. Or connectors for data or word processing or telephony. Or a full line of Mil-Spec connectors. Or connectors for aerospace and nuclear applications.

But we promise you more than an expanding product line. We'll provide proper means of terminating too. There's also our extraordinary quality. Our prompt delivery from our close-to-you distributors. Our personalized technical help. Perhaps what you need now in connectors is shown here. If it isn't, just ask.

Our ideas. Your ideas. They're right for each other. To learn why, just call us at (312) 986-2320 or write to:


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Our 32 Series Fire-Plug™ connector lives up to its name. It meets UL 94V-O flammability tests. Mounts on panels without tools. For commercial, industrial and consumer products.

Precision in coax. New subminiature APC-3.5 precision connector ensures mode-free operation through 34 GHz.

Quick change from multi-line to single-line phone service. With our modular adapters. Six-contact jack takes new plug-in cords.

A termination system that cuts assembly costs. Our 17 Series has everything you need for rear-release, input/output connectors. Reeled contacts and crimping tools, too.

Safety-first power distribution connectors. This 229 Series has integral ground, arc-quenching, and watertight seals.

Circular power connectors. The 97 Series has heavy experience in all kinds of consumer, industrial, and business equipment. It's for rack-and-panel installations and has pre-aligned contacts for quick, easy soldering. Hundreds of configurations for connecting computers, TV's, machine tools, you-name-it.

The right idea at the right time.
The KEPCO/TDK series RMT combines a logic 5 Volt ± 10%, 10 ampere output with various combinations of auxiliary voltages (see table). All outputs are stabilized by high efficiency switching circuits.

**FEATURES**

- Each output protected by overvoltage monitor.
- Each output protected by self-resetting overcurrent circuit.
- Soft start circuit reduces primary surge current.
- Remote on-off using logic level switching
- High density: more than 75 watts in less than 100 cu. in.

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<tr>
<th>MODEL</th>
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Custom volt-ampere combinations are available. Please consult the factory.

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CIRCLE NUMBER 27

ELECTRONIC DESIGN 19, September 13, 1977
Cruise-missile flyoff set for 1979

Two competing air-launched cruise missiles, the Air Force’s long-range ALCM-B and the Navy’s Tomahawk, will participate in a flyoff during 1979, with the winner to become the new strategic weapon for the B-52 bomber early the following year.

Development of both missiles was accelerated after President Carter decided against the B-1 bomber. The flyoff will include 10 launches of each cruise missile from the wings of B-52s. To simulate operational conditions, half these tests will be conducted by Air Force Strategic Air Command crews without assistance from the contractors.

The winner of the flyoff will be tested nine more times, also from a B-52, during 1980. Even before these latter tests are completed, the Defense Department expects to start producing the winning design for installation on operational bombers during the first three months of that year.

Congress has been briefed on the competition and has been advised that funds will be needed for it as soon as the new fiscal year begins Oct. 1. The funds may be slow in coming, however. In recent years, Congress has been reluctant to fund concurrent development and initial production of new weapons.

F-16 radar problems fixed in nick of time

A radar pick-up problem on an Air Force F-16 fighter was corrected during an intensive flight-test program in August at the Baltimore facilities of Westinghouse Electric Corp., prime radar contractor. The corrections came none too soon. A formal decision on production for the F-16 is scheduled for later in September by the Defense Systems Acquisition Review Council.

The radar system on F-16 No. 3 reportedly picked up false signals from ground clutter while operating in the look-down air-to-air mode. The problem was fixed by making changes in the low-power rf unit, which acts as the analog/digital interface. The No. 3 is the first F-16 to have a production-model design radar. Changes made on that aircraft will be duplicated on other flight-test aircraft.

Earlier this year, the F-16 radar passed a major milestone, the production-readiness review. The Air Force plans to order the first 105 aircraft in the fiscal year beginning Oct. 1 and another 45 the following year. In all, 1388 F-16s are expected to be purchased for use by the U.S.

Hydrofoil patrol boat reinstated

The Defense Department, following the lead of Congress, has reversed a decision to cancel the Patrol Hydrofoil Missile (PHM) program. As a result, prime contractor Boeing will build five more vessels for the U.S. Navy and may be able to sell 10 more to the West German Navy.

Defense Secretary Harold Brown decided to kill the program in April after experience with the first boat, the PHM-1 Pegasus, had indicated that the other hydrofoil patrol boats would cost twice their original price (from $20-million each in 1974 dollars to $41.4-million). He asked Congress to rescind the $272.7-million appropriated for construction, but Congress refused to act.

The vessels, which will be used for antisubmarine warfare around coastal areas,
will be armed with Harpoon antiship missiles and the Sperry Mark 92 fire-control system, which the Navy calls an Americanized version of the Dutch Mark 94 system.

Boeing will deliver five more PHMs to the Navy between January, 1, and February, 1980, four of which will be assigned to PHM squadron operating with the Sixth Fleet in the Mediterranean. The fifth will join the Pegasus for testing.

West Germany and other NATO navies have expressed interest in the PHMs, but only if the U.S. produces more than the PHM-1.

Radiographic techniques used to test jet engines

After a year of delays, an organization to coordinate procurement methods has been put into operation by the major government agencies under a regulation requiring government-wide uniformity. The institute is supposed to be the focal point for training federal-procurement officers and conducting studies of how to achieve a uniform procurement system.

The Federal Procurement Institute was established shortly after the White House put out the famous Office of Management and Budget Circular A-109 calling for the agencies to set up a single procurement system. But because of the change in administrations, no director was named and the institute consisted only of a skeleton staff housed in the Pentagon.

Then, in late August, the White House appointed a director, Dr. John Bennett, former Assistant Secretary of Defense for installations and logistics, and moved the institute to permanent facilities at the Army’s Development and Readiness Command headquarters, Cameron Station, VA.

Federal Procurement Institute activated

Radiographic techniques by Varian Associates are being used by Pratt & Whitney to measure clearances between parts in operating aircraft engines for both commercial and military jet aircraft.

The measurements are made in an attempt to improve fuel efficiency and thrust and are conducted while engines aren’t running, during steady thrust and during sudden accelerations and decelerations.

A Varian linear accelerator is mounted in a lead shield next to the engine to be scanned. Typical measurements include axial and radial clearance of seals, radial clearance of unshrouded blades, clearances in the compressor seals and component deflections due to thermal and mechanical stress.

Capital Capsules: The Air Force has put its second E-3A Airborne Warning and Control System aircraft into operation at Tinker Air Force Base, OK. The first production aircraft was delivered in March. . . . In preparation for a decision next year on whether to develop the M-X advanced intercontinental ballistic missile, guidance-system contractor Northrop has been extended through April, 1979. The firm has delivered its first advanced inertial reference-sphere (AIRS) guidance system, which is said to be far more accurate than those used on the present Minuteman ICBMs. Northrop will build and test three more. . . . The Defense Department now estimates its TRI-TAC program to replace all three services’ current analog, non secure battlefield communications with new all-digital and end-to-end secure-equipment will cost $3.1-billion, including $995-million for development. Procurement is due to begin next year. . . . British Aerospace Corp. is planning an improved Sky Flash air-to-air missile incorporating the monopulse seeker, which is reportedly less vulnerable to enemy jamming. The U.S. Air Force and Navy are interested in the concept and will test it on the current Sky Flash this year.
COMPARE YOUR IDEA OF A WORKHORSE RECORDER TO OURS.

The rugged Gould 105 General Purpose Strip Chart Recorder delivers such reliable performance, with so many unexpected features, that it goes beyond the traditional definition of a workhorse unit.

Die-cast to handle the day-to-day rigors industrial analytical instrumentation must face, the 105 still offers you a full complement of features you might not expect on such a competitively priced recorder.

Full scale accuracy is ± 0.1%. Rectilinear data presentation is available on either single or dual 10-in. channels. Response time (10% to 90% full scale) is less than 350 ms.

The Model 105 uses disposable felt tip pens available in four colors. It easily takes Z-fold or roll paper without modification. Chart speeds range from 1 in./hr. to 20 in./min. It even makes chart annotation simpler with a flatbed, "write-on" design and event marking standard.

And of course you have the Gould/Brush sales and service organization should you ever need us. Check Gould's 105 — a workhorse of a recorder with a tradition of thoroughbreds.

For a detailed brochure, contact Gould, Inc., Instrument Systems Division, 3631 Perkins Ave., Cleveland, Ohio 44114. Or call toll free at (800) 325-6400, Ext. 77.
In Missouri: (800) 342-6600.

GOULD
Meet CSC’s LP-3. The multi-family logic probe that’s as fast as a high-speed memory scope. At about 1/100th the price.

You won’t want to be without this compact, enormously versatile test and troubleshooting tool that does the work of a level detector, pulse detector, pulse stretcher and memory probe. It gives you instant, positive indications of circuit conditions — capturing one-shot and low-rep-rate pulses (down to 10nsec) that are barely visible, even on a fast scope.

**Easy to use.** No sync, polarity or circuit loading to worry about: just set a switch to the proper logic family, connect two clip leads to the circuit’s supply and touch the probe tip to the node under test. You get an instant picture of circuit conditions: Separate LED’s indicate logic “1”, logic “0” and all pulse transitions. To store single-shot and low-rep-rate pulses, simply set the PULSE/MEMORY switch to MEMORY.

At $69.95, LP-3 simplifies testing, debugging and servicing all types of digital circuits, with pulses as fast as 10nsec. See your CSC dealer today. Or call 203-624-3103 (East Coast) or 415-421-8872 (West Coast) for the name of your local stocking distributor and a full-line catalog.

**Specifications**

- **Input Impedance:** 500,000 ohms
- **Thresholds (switch selectable):**
  - DTL/TTL: 2.25V ±.10V, 70% Vcc ± 10%
  - Logic 0 thresholds (LO-LED): 0.80V ±.05V, 30% Vcc ± 10%
- **Min. detectable pulse width:** 10nsec guaranteed
- **Pulse detector (PULSE LED)** in PULSE position of PULSE/MEMORY switch. 10nsec pulse stretcher makes high-speed pulse train or single events (+ or – transitions) visible; in MEMORY position, first transition lights and latches LED.
- **Operating temperature:** 0-50°C
- **Physical size:** (L x W x D) 5.8 x 1.0 x 0.7” (147 x 25.4 x 17.8mm)
- **Weight:** 3oz. (858g)
- **Power leads:** removable 24” (610mm) with color-coded insulated clips, others available
- **Input protection overload:** ±25V continuous; 117 VAC for less than 10 sec., reverse polarity, 50V

**Logic Family Switch**
- TTL/DTL or CMOS matches Logic “1” and “0” levels
- CMOS position also compatible with TTL, HINIL and MOS logic.

**PULSE/MEMORY Switch & LED** — PULSE position detects and stretches pulses as narrow as 10 nanoseconds to 1/10 sec.; MEMORY stores single-shot and low-rep-rate events indefinitely. HI/LO LED’s remain active.

**HI/LO LED’s** — Display level (HI-logic “1”, LO-logic “0”) of signal activity.

**Interchangeable probe tips** — Straight tip supplied; optional alligator clip and insulated quick-connecting clip available. Optional input ground lead.

**Plug-in leads** — 24” supplied, with alligator clips. Virtually any length leads may be connected via phono jack.

CONTINENTAL SPECIALTIES CORPORATION

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See us at WESCON Show Booth’s #’s 1114, 1116 & 1118

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**NEW LP-3!**
We Invite You to Build Your Instrument Inside of Our Instrument...and save a bundle!

At first glance, the AN2553 is merely another superb Analogic DPI—a digital panel instrument, not a “meter”... but that’s another subject. What’s unique about this DPI is that it comes ready to take apart—with or without our help—and to be equipped with optimized plug-in interface circuitry that lets it measure virtually anything, from nanoamperes to Amperes, from microvolts to kilovolts, from degrees F or C to pounds or kilograms... and (literally) hundreds of other parameters.

How do we help? Five ways:

- **Sockets** are provided in the AN2553 for P.C. cards—front end (analog) and tail end (digital).
- We call them “Kluge Cards.” (The DPI provides them with regulated power, too.)
- Kluge Cards are available in two forms: blank (but bused and drilled, ready for your personal circuits); and loaded with proven, high-performance standard circuits for the 18 most popular analog and digital interfaces.
- **Recommended Circuits** for all 18 standard kluges, so you can build your own versions of them, if you wish.
- **Production Services**, if you develop a kluge, but want us to produce it in OEM quantities.
- **Applications Engineering** in depth, as always, from the world’s largest manufacturer of panel digitals.

With the standard digital kluges, by the way, you’ve got more than an instrument—you’ve got a pretty fair subsystem. Compatible with printers, computers, remote displays, limit comparators, and remote D/A’s, these BCD output cards give you all the required control, programming, latching, timing (and isolation if needed) that lifts the AN2553 up to the data-acquisition/logging and process-control level—“just short of a microcomputer,” we like to say... at about one-fifth the usual cost, by the way!

The AN2553 itself is worth a lot of attention, but space is tight, so here’s a quick look:

- ±1 count limit of error; very low T.C.’s, internal dissipation, and bias current; very high CMRR, CMV, NMR, line-noise rejection, and input impedance; our exclusive “universal powering” (100, 117, 220, or 240 VAC, 50 or 60 Hz, jumper selected; DIN/NEMA case (metal optional); and our famous 96-hour heat-and-stress burn-in on every unit. Value? How about a 100’s price of $99?
- Standard analog front ends include Thermocouple and RTD interfaces, current and voltage receivers, true-RMS, AC line monitors, and a microvolt receiver for load cells, strain/pressure gages, etc.

Move up to the DPEI—the Digital Panel EVERYMAN’S Instrument...and start with this data file!

Circle inquiry number 111
For Sale – 222, 221
NBS-Traceable Secondary-
Standard DC Voltage Levels
(µV to Volts)...for only $695.

The AN3100 Secondary DC Voltage Standard is not a new instrument. For seven years now, the AN3100 has been a standard of the industry. There are thousands in use worldwide. The design is, by far, still the most accurate, stable and versatile available in this price range.

Here's what we give you:
• Five Dialable, Digital Decades of DC Voltages – Two simultaneous ranges: 0-11.1110 Volts with 100µV resolution, and 0-111.11 Volts with 1µV resolution.
• Current Capability up to 50 Milliamperes – Short-circuit proof. No restrictions on load capacitance.
• Reversible Polarity, Isolated Output – Can be floated 500 Volts above or below ground.
• Very High Stability – ±2ppm/°C and ±15ppm for 60 days.
• Absolute Accuracy of 50ppm of Reading – (±50µV) for 6 months, without recalibration.
• Low Noise – less than 0.001% of reading ±50µV.
• NBS Traceability – 4 pg. Test Report and Certificate of Performance provided with each instrument specifying calibration voltages, equipment employed and final calibration accuracies to six places (±5ppm ±instrument uncertainty of 2ppm) and their direct traceability to NBS primary standards.

We've never been able to list all of the applications for this versatile box of tricks, but there must be hundreds. Here's just a sampling...
• Calibration of digital voltage instrumentation of all kinds, right up to 5 digits.
• Calibration of voltage dividers, resistance ratios, precision pots, and resistive-ratio transducers.
• Precise monitoring and measurement of regulation and stability of power supplies, D/A converters, amplifiers, and other analog-output circuits.
• Precise, absolute gain, linearity, and stability measurements of DC amplifiers.
• As the dialable reference and programmer in precision current generators.
• Calibration of analog multiplexers, log-ratio modules, and other "function generator" circuits.

One word of warning: unless you work alone, in a locked room, get more than one. The AN5100 is habit forming, and there's no cure. Beware of borrowers because they can become addicted to your AN3100. (The AN3100 fits neatly into desk-drawers and glove compartments.) By the way, it's the most portable secondary standard you've ever seen -- light, small and tough.

Get Full Specs— plus our famous Application Note: "31 Ways to Use the AN3100"

Got Your Back to the NOISE/DRIFT Wall? Here's Immediate 10:1 Relief.

Check that scope photo. It's the output of our MP221 ultra-low-noise, ultra-low-drift chopper amplifier, the best in its class by at least an order of magnitude. What's really impressive about that photo is that it was taken at a gain of 1000, and with a 10 kHz bandwidth...a "tell-it-all" test that other amplifiers costing far more will flunk miserably!

But low voltage and current noise is only a part of the MP221 story. It's stability is equally impressive: ±0.03µV/°C, <2pA/°C. Together, they make it possible to buffer and amplify any microvolt-to-millivolt-level signal source (load cells, strain gages, thermocouples, biophysical pickups, etc.) with truly impressive accuracy, without excessive tradeoffs of bandwidth or gain.

The gain linearity, by the way, is better than ±0.002%.

There are no ugly surprises lurking in the specs, nothing to constrain you to the use of weird architectures. Input impedance is 1000 megohms, the output is short-circuit protected, the output range is a full ±10V at up to ±3mA, the frequency response is ~3dB at 100 Hz, and CMRR is 140dB.

By the way, if your application lets you limit bandwidth to 1 Hz, the noise drops to a state-of-the-art 0.1µV p-p level! And that's the whole bag of worms, including flicker and Johnson-noise components. We even gold-plate the pins, so that you can use low-thermal-EMP solder, and approach ideal passivity at the input.

The MP221 is easy to use. No sandpapering the fingers, no walking on tip-toe, no muttering of incantations. Just set the gain from 10 to 10,000, select the roll-off frequency for system compatibility and you're ready to go.

Check out the specs of the MP221. And get our "31 Ways to Use the AN3100" Application Note. We've never been able to list all of the applications for this versatile box of tricks, but there must be hundreds. Here's just a sampling...

Get the File on the MP221 – for Optimum Low-Level Amplification.

From Handshake to Marriage in Less Than Two Years

For a couple of years now, our AN5400, the world's most versatile "Real-World" Data Acquisition and Distribution System, has been engaged in polite conversation with practically every mini under the sun.

From the beginning, we have always offered standard register interfaces to eight general-purpose minis, including DEC's PDP-11 family, Data General's Nova line, the Hewlett Packard HP2100, and the Texas Instruments T1860/880 family, just to mention a few. Interfacing is accomplished through a variety of simple plug-in, handshake modules that enable easy communication via the mini's parallel I/O bus. But now we've added a new dimension to that communication.

Before proceeding with the "hard news," let's briefly review the unprecedented flexibility of the AN5400, starting with the availability of the following User Modules: 13 different D/A Modules, six High Level Mux Modules, our unique line of Standard Thermocouple Amplifiers and Low-Level Isolation Amplifiers, Two Simultaneous-Sample-and-Hold Modules, as well as digital I/O capability. Combine these with over 200 different types of A/D Modules, plus the interface modules, and the ability to combine any combination of up to 16 User Modules in one chassis, and you have a truly flexible Data Acquisition and Distribution System...the world's most flexible, we call it, and no one challenges us, either.

Consider further that with combinations of the above standard modules one can configure systems with Resolutions of from 8 to 16 bits, throughput rates of up to 10kHz, and input capacity of up to 4096 High-Level, Single Ended Input Channels.
Also consider that the 16 User Modules per chassis may be virtually any combination of standard User Modules, all within the same chassis. Hence, flexibility is maximized and user investment is minimized.

Due to this unique design and total system flexibility we felt we were years ahead of the field, and you agreed. You've bought millions of dollars worth of AN5400 equipment, and the sales curve just keeps climbing.

However, nothing ever stands still in electronics, and every landmark design like the AN5400 starts generating new ideas from the day it's introduced. About a year ago, some of you began to see the potential for bigger, faster, more sophisticated computer-based systems. The result is that we've just succeeded in arranging not one, but two "marriages" between the AN5400 and the two most widely used minis: the DEC PDP-11 and the Data General NOVA.

Yes, you can now take advantage of the AN5400's 100kHz throughput we've just succeeded in arranging not one, but two "marriages" between the AN5400 and the two most widely used minis: the DEC PDP-11 and the Data General NOVA. Yes, you can now take advantage of the AN5400's 100kHz throughput.

Due to this unique design and total system flexibility we felt we were years ahead of the field, and you agreed. You've bought millions of dollars worth of AN5400 equipment, and the sales curve just keeps climbing.

Get the AN5400 Briefing — A "Short Course" in Computer Interfacing!

When There's No Room for Compromise — and No Budget for Mistakes — Think 2900 and 2700

Seasoned Analogic watchers know that we excel in providing state of the art performance and hard-nosed economic value. In fact, if price/performance juggling is what you need, then, you should talk to us.

But — sometimes there's no way to bend a requirement without breaking it. In fact, a cold, dispassionate examination of the realities of many digitizing applications would reveal that they are woefully under-implemented. The circuits used just don't hack it, and the only things that save the designer from an outright rejection are luck and user pessimism ("none of these things ever work to spec" — how often have you heard that, or said it?).

Here's one point: if you need, in one A/D converter, top speed, high resolution, fully compatible accuracy and linearity, and rock-solid temperature/time stability, we've got a design that delivers them all, simultaneously, at a price that makes good sense, even in small quantities. Our MP2900 and MP2700 series are, we believe, the only families of moderately priced successive-approximation A/D converters that don't ask for, or need, any kind of "tradeoff relief" to keep it in spec. From the 14-bit MP2914C downward (13,12,10 and 8 bits are standard), this is a no-excuses design. Check these specs — and bear in mind, when you do, that at 14 bits, the LSB represents about 60 PPM.

MP2914C — 14-Bit Premium A/D Absolute Accuracy: 0.006% NBS traceable Relative Accuracy: 0.004%
Differential Linearity: 0.004% FSR
3-Sigma Noise: 0.005% P-P (RTI)
Monotonicity: Guaranteed Perfect
T.C. of Diff. Lin.: <±3PPM/°C FSR
Gain T.C.: <±7PPM/°C Offset T.C.: <±12PPM/°C
Conversion Time: 10µsec.

*MP2714C — specs differ slightly.

That's just a quick look — but we promise you that when you've finished reading the complete data sheet, you won't have a single quibble with our claim: this is a design without compromise.

And, like all Analogic A/D converters, a 2900 or 2700-series module is shipped to you with its own individual computer print-out, recording the results of the most exhaustive tests ever applied to a product in this class — tests so comprehensive that we also furnish a four-page engineering supplement, describing them in detail! (If we didn't computer-program them, they'd cost more than the module, and take a week or more to perform.)

Do you have an A/D requirement that's tough enough to separate the grownups from the kids? We've got the MP2900s and MP2700s. Let's get them together.

Full Data-Including Our Unique Computer-Based A/D Test Procedures — FREE.
A New Twist to the "LONG DAC" Game: Real Bits!

Have you been having fun counting the pseudo-bits on those new "breakthrough" D/A converters you read about almost every month? The latest in our collection is an 18-bit wonder that works out to somewhere between 14 and 15 real, meaningful bits, when you take it out of the magazine pages and put it in even the gentlest of environments. The extra three or four bits are apparently as useful as spigots on a bull... and you can't milk a bull, nohow.

Apparently, the reasoning behind these recent 15, 16, and 18-bit fantasies is that it makes a system designer feel better to have lots of extra terminals that appear to give him higher resolution than the DAC's linearity and stability can support. But the circuits that surround the DAC can read the fine print. They can multiply so many ppm/°C by so many °C, and come up with 3 LSB's of drift over a modest range.

The most curious part of all this is that, for the same money or less, we offer true 14-bit, 15-bit, and 16-bit DAC's—with real and meaningful 14-to-16-bit performance, mind you. Our MP1900 series, for example, comes in a number of grades, of which the MP1916TC is the "top of the line," sells for about five bills (lots less in quantity), and delivers specs like these:

**MP1916TC Premium 16-Bit DAC**
- Relative Accuracy: ±0.001% FSR
- Differential Linearity: ±0.001% FSR
- T.C. from All Sources: <1PPM/°C

(That is not a misprint!)

**Current-Mode Setting Time:** 3µsec to ½LSB
**Voltage-Mode Setting Time:** 20µsec to ½LSB

And, for substantially less money, we've got 14-to-16-bit DAC's in this same 1900 series, any one of which will still outperform those unreal "lotta-bits," as we've begun to call them around our lab. We invite you to try the real thing...

Send for the Analogic File on Real LONG DAC's—Fascinating True Stories of Actual Resolutions!

---


Turn back to page 2, and read our capsule description of the AN5400. That leaves us more space to talk about one of the new optional capabilities we've developed for this continually evolving system... an asynchronous communications interface.

With this new plug-in option, you are free to locate the AN5400 Data Acquisition System anywhere...regardless of where its host computer is located. You can build the AN5400 right into the process racks—where the wiring to hundreds (or even thousands) of transducers, control relays, solenoids, positioning motors, etc., etc., can be done most easily and economically—and then link the digital traffic to and from the computer, via dedicated serial line, or even directly over standard telephone lines.

Here are the key numbers and features...
- Complete Conformance to RS-232-C
- Plug-In 4-Card Module—No Wiring
- Compatible with 20-mA Current Loops
- Compatible with Standard Modems and Dedicated Lines (RS-422)
- Baud Rates: 50 to 19,200—Switch Selectable
- Built-In Status and Error Registers for System Debugging and Diagnostics
- Choice of Protocols

With this added capability, the AN5400 becomes more than just the most flexible system to configure, but it also makes it the easiest to locate, in the application environment and master-system architecture in which you must work. Watch future issues of Enhancement for more good AN5400 ideas—we've got some beauties in final development. In the meantime, call us and discuss what you need now or will be needing. We can almost always contribute significantly to improve interface design!

Send for the Serial-Interface Specs—and We'll Include the Complete AN5400 Brochure—FREE

---

Send for the Analogic File on Real LONG DAC's—Fascinating True Stories of Actual Resolutions!
Introducing
Robert Bosch
Mini-Giants

30-amp relays with a quarter-million cycles: smallest for the price

We invite you to compare the high technology advantages of Bosch Mini-Giants to the relays you're now using. We're confident you'll find Mini-Giants hard to beat on all the important criteria.

Versatility. Bosch has engineered the Mini-Giants to be at home in any 12- or 24-volt application—remote controls, generators, automotive systems, construction machinery, marine applications, agricultural equipment, hospitals, storage systems and more.

The same Mini-Giant that can switch the low current of an alarm can also control the high 30-amp load of a heating system.

Size. Bosch technologists have designed a PC board type relay that is 1" x 8" x .7" or just over half (.56) a cubic inch. The plug-in type (not including the plug prongs) is 1" x 1" x .8", still less than a cubic inch.

Capacity. Bosch plug-in Mini-Giants cover the entire power range up to 30 amps, with a peak current capacity of 60 amps. Even the standard 15-amp PC type is available in a 30-amp version on special order.

With one group of relays covering such a range of applications, you can cut down substantially on part numbers and simplify your stocking operations.

Reliability. All Mini-Giants are good for a minimum of 250,000 cycles at the rated current. This compares with 100,000 cycles in many comparable relays from other manufacturers.

And Bosch uses the finest materials for long life (at least 10 million cycles at no load). For example, we build the leaf springs of our plug-in relays from high-grade silver and bronze.

Cost. Bosch Mini-Giants give you all these benefits combined at a surprisingly low price. You really should compare.

For more information. Fill out the coupon below and we will contact you to discuss your specific needs and answer your questions. Or call (312) 865-5200 and ask about relays. Either way, do it now.

Robert Bosch Corporation,
Department O/ESL
2800 South 25th Avenue,
Broadview, Illinois 60153

CIRCLE NUMBER 30
When the output of a 555 timer switches high, a large current spike is generated which can drag down your power supply and upset your flip-flops. One way to cure it is with several hundred µF of capacitance. But that's awkward and space-consuming. Teledyne's new 355 timer is a better way.

The 355 Timer is a pin-for-pin substitute for the 555. It is part of Teledyne’s High Noise Immunity Logic (HiNIL) family. It, too, generates a current spike — but only on the order of 1 mA, as compared to 300 mA for the 555.

Two other problems encountered with the 555 are a potential failure to reset on command, and a tendency to exceed the power dissipation ratings when running at 15V. The Teledyne 355 is designed specifically to answer these two potential problems as well.

If you'd like full technical information on our new 355 Timer — or any other members of the Teledyne HiNIL family of logic — call us at (415) 968-9241, or contact your local Teledyne Semiconductor distributor.
Editorial

Down with professionalism

I don't know if laetrile can help cancer sufferers. But I know of many who think it can. So when I wrote my July 19th editorial, “Professionalism,” I didn't intend to endorse laetrile. Rather, I wanted to urge that our industry shun the kind of professionalism we find in outfits like the Food and Drug Administration.

A storm of letters, mostly from readers who feel that laetrile is a useless fraud, showed that I wasn't clear. (We'll publish these letters in this and coming issues as space permits.)

While I dislike some laetrile supporters, I despise opponents like the FDA, who set their “professional” interests ahead of the interests of humanity. One reader hit the point precisely when, opposing my views, he wrote: “I most respect the Medical Profession for looking out for #1.”

The FDA has succeeded in banning interstate shipment of laetrile and has been battling intrastate acceptance on several grounds: It's useless. It may be toxic in large doses. It enriches profiteers. And terminal cancer patients might try it rather than listen to their physicians, who may have nothing better to offer.

Yet the FDA has sanctioned many drugs that proved useless or dangerous. When it finally bans something (like carcinogenic food additives) it tends to issue a years-later ban, so inventories can be sold off for public consumption. Almost anything is toxic in large doses including, I understand, aspirin, alcohol, tobacco and most food additives. Does the FDA ban them? As to profiteering, that's easy. Legalize laetrile and you wipe out the black market. Then the $300/gram U.S. price might approach the $3/gram Mexican price.

Whether laetrile works or not, it should not be banned by a government bureaucracy protecting the interests of one economic group while pretending, as always, to protect the public. We engineers often view the medical industry as the archetype of professionalism. But if professionalism means that we must hound and jail people who don't like our ideas and won't accept our verdict that their plight is hopeless, then I say to hell with professionalism.

GEORGE ROSTKY
Editor-in-Chief
1. You simply set two intensified markers at the desired points using the START and STOP controls.

2. For maximum accuracy, switch to delayed sweep and use the STOP control to overlap the expanded traces.
For improved \(\Delta\)-time measurements, plus autoranging AC/DC volts, amps and ohms ...

**HP's the Answer.**

Now you can choose from two new scopes with improved \(\Delta\)-time capability: The 200 MHz \textbf{1715A} priced at $3000* or the 275 MHz \textbf{1725A} for $3300*. Both offer an optional built-in DMM for direct \(\Delta\)-time readout, plus autoranging AC/DC volts, amps, and ohms.

\(\Delta\)-time measurements are now faster with the 1715A and 1725A. They're more accurate because scope and operator errors are significantly reduced. Plus you have switch selection of channel A or B as the starting point for \(\Delta\)-time measurements, often eliminating the need to move probes and simplifying trace overlap for zeroing. But you can still select conventional delayed sweep with the flip of a switch, for brighter low-rep-rate traces and convenient trace expansion.

The optional autoranging 3½ digit DMM is priced at $325* factory installed. Or, for easy field installation, there's a kit priced at $375*. Another option, HP's "Gold Button" for $150*, gives you pushbutton selection of either time domain or data domain when the 1715A or 1725A is used with HP's 1607A Logic State Analyzer.

Like all new high-frequency HP scopes, the 1715A and 1725A have switch selectable 50 ohm or 1 Megohm inputs. And the 1725A, with 275 MHz bandwidth, is the fastest 1 Megohm-input scope available. That reduces the need for active probes when working with fast logic near maximum fan-out.

The story with both of these scopes is user convenience—from front-panel controls to the minimum of adjustments for servicing. Your local HP field engineer can give you all the details.

And here's something NEW for scopes. HP's \textbf{Easy-IC Probes}. A new idea for probing high-density IC circuits that eliminates shorting hazards, simplifies probe connection to DIPs and generally speeds IC troubleshooting. The probes are standard equipment with these two scopes.

*Domestic U.S.A. price only.
Exploit existing Nova software by designing computer systems around the microNova. The microprocessor gives you minicomputer performance from a 40-pin package.

Using the existing Nova instruction set, the microNova microprocessor can help you eliminate much of the time spent developing software. And, because it's also functionally compatible with the existing Nova, you will have many design shortcuts (Fig. 1).

Like the Nova minicomputer, the microNova has a 16-bit word length and a set of 42 instructions, including multiply and divide. But the microNova is a single-chip, NMOS circuit housed in a 40-pin DIP. It operates at a typical clock frequency of 4.166 MHz.

Although the \( \mu \)P operates on 16-bit data, the addressing range is only 32-k words—not the 64-k words that would normally be expected. However, because the microNova, known as the mN601, uses a 16-bit data word, it offers many advantages generally associated with 16-bit minicomputers. For instance, in many data-acquisition systems, 12, 14 and even 16-bit data words are often used. Most \( \mu \)Ps would have to "double up" to gather in the data, with extra control circuitry and commands needed for the shorter word-size devices.

In spite of its minicomputer capability, building a processor system around the mN601 is simple (Fig. 2). And, as shown in Table 1, the mN601 needs only a handful of circuits for the basic system.

Bidirectional buses do the work

Two independent buses on the microNova are used to communicate with the memory and I/O devices (Fig. 2). The memory bus both accesses and refreshes the memory. With 16 bidirectional data lines and three control lines, this bus requires almost half the available pins of the package (Fig. 3).

The control lines on the memory bus, called the P, SAE and WE signals, are all active-High output signals. All memory cycles are controlled by the P signal—the rising edge of the P signal indicates that a valid address is on the memory bus. The selected memory should then prepare for either a read or write operation. SAE indicates a data transfer from memory (read). A WE signal indicates a data transfer to memory (write).

1. Depending upon your needs, you can purchase any form of processor you want in the microNova family—from the bare chips to a full minicomputer.

Two bidirectional data lines can handle serial data. These lines, called I/O Data 1 and I/O Data 2, are active-Low and can carry all data, address and I/O command information between I/O devices and the mN601. Information is transferred serially at the full master-clock rate of 8.3 MHz over each I/O Data line for an aggregate transfer rate of 16.6 MHz. The processor can do five types of transfers—Request enable, Data-channel acknowledge, I/O command, I/O data in and I/O data out. Each transfer is identified by the value of the I/O Data 1 and 2 lines at the first I/O clock pulse.

During a Request-enable operation, a 2-bit request-enable code is transmitted via the I/O data pins to synchronize program-interrupt and data-channel requests from peripherals. The CPU performs these operations at irregular intervals determined by the other operations it is performing. When a Data-channel acknowledge operation is being performed, the CPU also transmits a 2-bit code to indicate that it has begun a data-channel break.

For an I/O command operation, a 2-bit code and a 16-bit command are transmitted via the I/O data pins to specify a preprogrammed I/O operation that the peripheral is to perform. The CPU performs an I/O command operation whenever it executes an input/output instruction.

Daniel Falkoff, Natalio Kerllenevich and Philip Kreiker, Design Engineers, Data General, 15 Turnpike Rd., Route 9, Westboro, MA 01581
2. **There are three major buses on the processor**—the memory bus, the serial I/O bus and the control bus. And

Similarly, for an I/O data-out operation, a 2-bit code and a 16-bit data word are transmitted via the I/O data pins. This operation occurs during data-channel breaks and while I/O instructions are being executed.

When an I/O data-input operation takes place, a 2-bit code and a 16-bit data word are received from a peripheral in response to a data-acknowledge code or an I/O command. I/O operations are always preceded by a Data-channel-acknowledge operation or by an I/O command.

Besides the two normal clock inputs needed for the two-phase processor clock, a separate clock input for the I/O channels—the I/O clock line—is used to synchronize all I/O operations. An I/O input line that is active-Low is used to indicate the direction of the I/O transfer. When the line is High, the mN601 expects to receive data. When Low, it indicates that the processor is sending data on the I/O lines.

The microNova has two interrupt lines—the External I/O interrupt (EXT INT), which handles program interrupts generated by an external peripheral, and the DMA request (DCH INT), which is a data-channel break request. In this case the processor doesn't go to a program subroutine. Instead, it stops so that data can be fed directly to the memory.

Both lines are active-Low. When the EXT INT line

3. **Of the 40 pins on the microNova**, 16 are required by the memory bus, four are used for the serial I/O, eight for control, seven for power, two for the clock and three more are not connected (a). The two-phase nonoverlapping clock (b) controls all system timing.
**Table 1. MicroNova hardware**

<table>
<thead>
<tr>
<th>Model #</th>
<th>Description</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>mN601</td>
<td>16-bit NMOS microprocessor</td>
<td>$114.</td>
</tr>
<tr>
<td>mN603</td>
<td>I/O controller (IOC)</td>
<td>70.</td>
</tr>
<tr>
<td>mN606</td>
<td>4-k dynamic RAM</td>
<td>19.</td>
</tr>
<tr>
<td>mN629</td>
<td>CPU I/O transceiver</td>
<td>30.</td>
</tr>
<tr>
<td>mN634</td>
<td>Memory transceiver</td>
<td>12.</td>
</tr>
<tr>
<td>mN636</td>
<td>IOC I/O transceiver</td>
<td>10.</td>
</tr>
<tr>
<td>mN638</td>
<td>Memory clock driver</td>
<td>7.</td>
</tr>
<tr>
<td>mN640</td>
<td>CPU and I/O clock driver</td>
<td>7.</td>
</tr>
<tr>
<td>mN506</td>
<td>Sense amp/bus driver</td>
<td>15.</td>
</tr>
</tbody>
</table>

Support boards and system components $ (unit qty)

<table>
<thead>
<tr>
<th>Model #</th>
<th>Description</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>8562/63</td>
<td>CPU with 2 k/4 k of RAM</td>
<td>$800./$950.</td>
</tr>
<tr>
<td>8572/73</td>
<td>4 k/8 k RAM board</td>
<td>600./950.</td>
</tr>
<tr>
<td>8567</td>
<td>PROM memory boards</td>
<td>300. to 4096 words)</td>
</tr>
<tr>
<td>8570</td>
<td>Hand-held console subsystem</td>
<td>700.</td>
</tr>
<tr>
<td>4207</td>
<td>Asynchronous interface board</td>
<td>250.</td>
</tr>
<tr>
<td>4208</td>
<td>Console debug</td>
<td>200.</td>
</tr>
<tr>
<td>6038</td>
<td>Single-drive diskette subsystem</td>
<td>2900.</td>
</tr>
<tr>
<td>6039</td>
<td>Dual-drive diskette subsystem</td>
<td>3900.</td>
</tr>
<tr>
<td>8574</td>
<td>PROM programmer board</td>
<td>1650.</td>
</tr>
<tr>
<td>4210</td>
<td>General-purpose interface board</td>
<td>250.</td>
</tr>
<tr>
<td>2303A</td>
<td>Extender board</td>
<td>200.</td>
</tr>
<tr>
<td>4212</td>
<td>9-slot card-frame assembly</td>
<td>250.</td>
</tr>
</tbody>
</table>

is brought Low, the mN601 will execute a jump to subroutine by saving the current contents of the program counter in memory location 0, and loading the contents of location 1 into the program counter. However, if the µP’s interrupts aren't enabled, there won't be an interrupt.

Similarly, when the DCH INT line is brought Low, the processor executes a direct-memory access. Once the line goes Low, a data-channel-acknowledge code is sent out by the processor on the I/O bus. The µP then reads the memory address and direction mode from the interrupting device. If the request was to output data, the data from the memory are sent to the device. If the request was to input data, the data are read from the device and written directly into memory.

Just three other control lines are included on the microNova—Halt, Clamp and Pause. The Halt is an active-High output signal. When the processor is stopped (idling) as a result of the execution of a Reset or Halt instruction, the Halt output will provide a stream of positive pulses.

The Clamp line, an active-Low input, is used to initialize the processor. For instance, when the µP is first powered up, it doesn't perform any operation as long as the Clamp line is held Low. When the line goes High, the processor is initialized and enters the Halt state.

The Pause line is also an active-Low signal. When Low, it indicates that the phase-A and phase-B clocks can be stopped so that the memory can be accessed by other devices sharing the same bus.

**Accessing the memory is simple**

The main memory is partitioned into 32,768 different locations, each of which can be randomly accessed. Six instructions in the microNova instruction set directly reference the memory by means of word addressing (see instruction set, p. xx). These instructions use 11 bits in the instruction word to define the address. The bits don't specify the address directly, but are used in a calculation that produces the address of the desired word. The resultant address is called the effective address, E, and the calculation is called the effective-address calculation.

As Fig. 4 illustrates, the effective address calculation is rather complex. The instruction uses bits 5 to 15 to define the effective address. Bit 5 is called the indirect bit, bits 6 and 7 are called index bits, and bits 8 to 15 the displacement bits.

During a calculation, the displacement is converted to a 15-bit intermediate result. This result is interpreted either as the indexed address without further calculation or as a number and added to the contents of the program counter, accumulator 2 or accumulator 3.

If the CPU adds the intermediate result to one of the registers, the indexed address is bits 1 to 15 of the result. Bits 6 and 7 of the instruction that the CPU is currently executing determine to what register, if any, the displacement is added—accumulator 2, accumulator 3, or the program counter.

Although bytes in the main memory cannot be directly addressed by the CPU, some programming aids ease the manipulation of byte-sized data. The microNova software makes use of a byte pointer—a word in which bits 0 to 14 are the address of a normal 2-byte word and bit 15 is the byte indicator. If bit 15 is High, the pointer indicates the lower-order byte. When bit 15 is Low, the pointer indicates the higher-order byte.

If all address locations aren't filled with RAM or ROM, and an attempt is made to retrieve a word from the nonexistent memory, the CPU functions as though the memory is there, but brings back all ONEs.

The CPU does any of four operations on the memory—Read, Write, Read-modify-write, and Refresh. During the first three, data are transferred over the 16-line bidirectional bus. A Read-modify-write operation permits a 16-bit word to be pulled from memory and a different word to be put back into the same location. During a Refresh operation, the CPU specifies a group of 512 memory locations to be refreshed but transfers no data. The 512 locations are 1/64 of the memory...
5. Housed in a 20-pin package, the 4-k dynamic RAM developed by Data General keeps the memory-support circuits needed by the processor to a minimum (a). The I/O controller circuit, housed in a 40-pin DIP, is almost as complex as the processor (b). One controller must be used with every peripheral device connected to the µP.

4. To calculate the effective address, the microNova goes through a very complex procedure. The first step in the process is to check the two index bits so that the processor knows what to do with the displacement bits in the instruction before performing the calculation.
## Table 2. Software support for microNova systems

<table>
<thead>
<tr>
<th>Program</th>
<th>Description</th>
<th>Cost</th>
<th>Media</th>
<th>Minimal system needed</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Operating systems</strong></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>DOS (Diskette operating system)</td>
<td>A subset of the company’s compatible Real-time Disc Operating System (RDOS), DOS provides operator interface features, peripheral control, and file management. Interrupt handling, physical I/O, and file processing are made transparent to the user.</td>
<td>$300 for the first system, including one year’s free software subscription service.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>RTOS (real-time operating system)</td>
<td>RTOS is a DOS-compatible runtime executive that is compact memory-resident, and has a real-time multitask capability for controlling real-time applications. RTOS provides standard interrupt servicing, device handling, and execution-scheduling functions.</td>
<td>$100 for the first system, including one year’s free software subscription service.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td><strong>Languages</strong></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Fortran IV</td>
<td>A high-level language that exceeds ANSI standards, with multitasking extensions essential for real-time applications. It supports multiple I/O formats, inline assembly language coding, and relational and logical operators. It generates re-entrant code that can be shared by multiple tasks for memory efficiency and ROM-based program storage.</td>
<td>$500 for first system, including one year’s free software subscription service.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Single-user Basic</td>
<td>An extension of Dartmouth Basic that includes string arithmetic and matrix I/O operations, user-controlled output formatting, and comprehensive access to data files.</td>
<td>$1000 for first system, including one year’s free software subscription service.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Multi-user Basic</td>
<td>Similar to single-user Basic, but having the user program area divided equally among the users.</td>
<td>Same as Single-user Basic</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td><strong>Utilities</strong></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Macro assembler</td>
<td>Macro instructions translate a single multi-argument source line into a sequence of machine instructions. Expanded expression evaluation allows Fortran-like expressions to be used with machine language efficiency.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Command line interpreter</td>
<td>An operator interface to DOS that provides extensive file maintenance capabilities, control over system utilities, and a simple way to invoke complex sequences of program executions.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Library file editor</td>
<td>Combines compiler or assembler output to form binary libraries, resulting in a set of central, updatable program libraries that eliminate program duplication.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Text editor</td>
<td>The editor combines multiple text streams, “remembers” often-used editing sequences, and even executes a “program” of conditionally-looping text modification commands.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Relocatable loader</td>
<td>Lets users combine multiple independent binary modules into an executable program. Includes automatic library search, conditional load, comprehensive load map listings, and origin definition flexibility.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Libraries</td>
<td>Data General supplies a set of libraries for complex character-formatting I/O routines, logarithmic, exponential, and trigonometric function evaluation, and comprehensive array handling.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
<tr>
<td>Symbolic debugger</td>
<td>Facilitates program debugging with symbolic designation of user labels, assembler mnemonics, and program offsets. Symbolic references allow program debugging in source-language terms that do not require cumbersome binary translation.</td>
<td>Included with DOS or charge.</td>
<td>Diskette or paper tape.</td>
<td>Any microNova CPU with 8 kwords of main memory board or packaged computer</td>
</tr>
</tbody>
</table>
Internal architecture of the microNova

Since the mN601 microprocessor is software-compatible with the Data General line of Nova mini-computers (it operates with the Nova-3 instruction set), the internal architecture is very similar to that of the Nova minis. The CPU has four general-purpose accumulators, each 16 bits wide.

The arithmetic and logic unit on the processor chip accepts any two 16-bit accumulator outputs and one bit from the carry register. Among other on-chip registers, there are three 15-bit registers—the stack pointer, the program counter and the frame pointer. There are also four more 1-bit registers—an interrupt-enable bit, a real-time-clock-enable bit, a stack-overflow-request bit and a real-time clock-request bit—as well as a 6-bit refresh address counter.

The stack pointer is a register that contains the address of the top of a stack. It is affected by operations that either push or pop data from the stack. The program counter contains the memory address of the next instruction to be executed. Somewhat like the stack pointer, the frame pointer points to the stack—but not necessarily to the top. It points to the portion of the stack storing the status information to be used in returning from a subroutine.

As can be seen from the accompanying CPU block diagram, all 15 and 16-bit registers are “paralleled” onto the main internal buses. During the execution of instructions, program interrupts and data-channel breaks, information is transferred among the registers, the memory-address/data pins and the I/O data pins. When arithmetic operations are performed on the data held in these registers, each word is interpreted as a binary number, whether it be a 15 or 16-bit register.

If the contents of a register are transmitted to the memory-bus pins as data, the contents of the register’s bit 0 are sent to bus pin MB(0), all the way up to bit 15, which is sent to the MB(15) line. When the register contents are sent as an address to the MB bus, the contents of bits 1 to 15 are transmitted as before. However, the contents of bit 0 are not transferred. The state of the MB(0) line depends on the operation that the CPU is performing on the pins of the memory port. It’s High when a refresh operation is being performed and Low for normal addressing.

To perform arithmetic and logic operations, each instruction specifies two accumulators to supply operands to the function generator (ALU). The function generator performs the operation dictated by control bits 5, 6 and 7 of the instruction. A carry bit is also generated by the function generator. This carry bit depends on three quantities—an initial value specified by the instruction, the inputs and the function performed. The initial value is often derived from the previous value of the carry bit, otherwise the instruction can specify an independent value.

The 17-bit output of the function generator, composed of the 16-bit function result and the carry bit, then goes to a shift network where it can be rotated one place left or one place right. Or the two 8-bit halves of the function result can be swapped without affecting the carry bit. A test command then permits the shifter output to be examined for a skip instruction. After the output has been tested, it can be loaded into the carry-bit register and the output accumulator (ACO), or it can be fed into any of the other registers.

To keep all the circuit operations perfectly timed, a two-phase clock is needed by the processor. The maximum frequency of the clock can reach 4.166 MHz.

and are selected by a 6-bit refresh address placed on the lower six address lines.

Other circuits help the processor

Some specialized support devices help the processor interface to the outside world. The main devices include a 4-k dynamic RAM, the mN606, and a peripheral interface and control circuit, the mN603—often referred to as an I/O controller (Fig. 5). Although other dynamic memory chips can be used with the processor, the mN606 has been specially designed to simplify the interface requirements—just two control lines (the chip-select and write-enable) and a clock are required.

The I/O controller (or IOC), on the other hand, is almost as complex as the processor. It comes in a 40-pin package. Usually, one IOC is used with every peripheral device connected to the computer system. Connecting it to the system is relatively simple. There are 16 bidirectional bus lines, five supply pins, two clock inputs, five function-control pins, four I/O lines and eight assorted control and indicator lines.

Many subsystems inside the IOC work together to coordinate the transfer of data and the control of a peripheral device by the processor (Fig. 6). The main
control element within the IOC is a programmable logic array that defines the machine states for the various control functions. The IOC also requires a two-phase nonoverlapping clock, just like the processor. However, instead of being called phase A and phase B, as on the processor clock, the phases are labeled A/B and B/A. To ensure that handshaking functions are properly executed between the CPU and IOCs, the processor is the source of timing for the entire system. The timing information is transmitted to the IOCs over the I/O bus. The I/O transceiver (mN629) used with the CPU transmits to all the other I/O transceivers (mN636s) connected to the IOCs. A differential signal called BMCLOCK is used by the IOCs to synchronize themselves to the CPU. Up to 20 mN636s plus one mN629 can be connected to the I/O bus.

Both the mN629 and 636 are very similar—their internal circuitry is identical except for one change in the signal flow in the MCLOCK, BMCLOCK and BMCLOCK lines (Fig. 7b). On the 629, the MCLOCK line is the clock input from the processor. The

6. The many registers inside the mN603 controller keep track of where data are to be sent, where data are coming from and what operation is to be performed. An internal PLA controls the operation of the mN603.

**MicroNova software and instruction set**

With a set of 42 instructions, the microNova µP can rival the performance of its bigger brothers in the Nova series of minicomputers. The basic instruction set contains commands that perform fixed-point arithmetic between accumulators, including multiply and divide; transfer operands between accumulators and main memory; perform logic operations between accumulators; transfer program control; and do all I/O operations.

The instructions are one 16-bit word long and can address memory either directly or indirectly. Chains of indirect addresses can be up to eight-levels deep. Also available is a direct-memory-access channel to help speed data transfers from peripherals to the main memory.

In one instruction, the arithmetic and logic instructions can execute a command, shift the result one bit left or right, test the result of the shift, then conditionally skip the next instruction. In addition, this entire sequence
can be done without affecting either of the operands. A last-in, first-out stack is maintained by the processor in the external memory, and up to 32-k 16-bit words can be directly addressed by the microNova. Each word is set up so that, by convention, the highest-order bit is numbered 0 and the lowest-order bit is 15.

Several addressing modes are available to the processor:

- **Direct addressing**, which is similar to direct addressing on other processors.
- **Indexed addressing**, where the effective address is calculated by the processor from the data included in bit positions 8 to 15 of the instruction plus the contents of either the program counter, accumulator 2 or accumulator 3.
- **Indirect addressing**, where the actual address of the operand and is contained in a memory location addressed by the instruction. This mode of addressing can be made eight levels deep.

Several memory locations (addresses 20s to 27s) are called auto-incrementing locations. During the calculation of an indirect address, the CPU performs Read-modify-write operations on these locations, and during the write portion increases the contents of the location by one. Similarly, other locations are used for auto-decrementing applications (addresses 30s to 37s). In this case, the data held in the location specified are automatically decremented during the write portion of the operation.

The instructions of the microNova can be split into five basic groups—Memory reference, Arithmetic and logic, Input/output, Stack manipulation, and Central processor control commands. One of the few processors to include hardware multiply and divide capability, the microNova can perform these operations in 41.3 and 59 μs, respectively, with a 4.166-MHz clock.

Four basic instruction formats used for microNova instructions permit an extensive instruction set without going beyond the one-word instruction. The four formats are:

- **No accumulator** — **effective address**. Bits 0 to 2 are 000 and bits 3 and 4 contain the operation code. The effective address is computed from bits 5 to 15.
- **One accumulator** — **effective address**. Bit 0 is 0 and bits 1 and 2 contain the operation code. Bits 3 and 4 specify the accumulator used for the operation and the effective address is computed from bits 5 to 15.
- **Two accumulators** — **multiple operation**. Bit 0 is 1, bits 1 and 2 specify the source accumulator, bits 3 and 4 specify the destination accumulator, bits 5 to 7 contain the operation code, bits 8 and 9 specify the action of the shifter, bits 10 and 11 specify the value to which the carry bit will be initialized, bit 12 specifies whether or not the result will be loaded into the destination accumulator, and bits 13 to 15 specify the skip test.
- **Input/output**. Bits 0 to 2 are 011, bits 3 and 4 specify the accumulator for operation, bits 5 to 7 contain the operation code, bits 8 and 9 specify the control signal to be used, and bits 10 to 15 contain the device code of the referenced device.

### Mnemonic Octal Operation

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<thead>
<tr>
<th>Memory reference instructions</th>
<th>Decimal</th>
<th>Operation</th>
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<tbody>
<tr>
<td>DSZ 014000</td>
<td>Decrement location E by 1 and skip if result is zero.</td>
<td></td>
</tr>
<tr>
<td>ISZ 010000</td>
<td>Increment location E by 1 and skip if result is zero.</td>
<td></td>
</tr>
<tr>
<td>JMP 000000</td>
<td>Jump to location E</td>
<td></td>
</tr>
<tr>
<td>JSR 004000</td>
<td>Load PC+1 in AC3 and jump to subroutine at location E</td>
<td></td>
</tr>
<tr>
<td>LDA 020000</td>
<td>Load contents of location E into AC</td>
<td></td>
</tr>
<tr>
<td>STA 040000</td>
<td>Store AC in location E</td>
<td></td>
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<thead>
<tr>
<th>Arithmetic and logical instructions</th>
<th>Decimal</th>
<th>Operation</th>
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<tbody>
<tr>
<td>ADC 102000</td>
<td>Add complement of ACS to ACD</td>
<td></td>
</tr>
<tr>
<td>ADD 103000</td>
<td>Add ACS to ACD</td>
<td></td>
</tr>
<tr>
<td>AND 103400</td>
<td>AND ACD with ACD</td>
<td></td>
</tr>
<tr>
<td>COM 100000</td>
<td>Place complement of ACS in ACD</td>
<td></td>
</tr>
<tr>
<td>INC 101400</td>
<td>Place ACD+1 in ACD</td>
<td></td>
</tr>
<tr>
<td>MOV 101000</td>
<td>Move ACS to ACD</td>
<td></td>
</tr>
<tr>
<td>NEG 100400</td>
<td>Place negative of ACS in ACD</td>
<td></td>
</tr>
<tr>
<td>SUB 102400</td>
<td>Subtract ACS from ACD</td>
<td></td>
</tr>
<tr>
<td>DIV 073100</td>
<td>If overflow, set Carry. Otherwise divide AC0 by AC1. Put quotient in AC1, remainder in AC0</td>
<td></td>
</tr>
<tr>
<td>MUL 073300</td>
<td>Multiply AC1 by AC2, add product to AC0, put result in AC0-AC1</td>
<td></td>
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</table>

<table>
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<tr>
<th>Input/output instructions</th>
<th>Decimal</th>
<th>Operation</th>
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</thead>
<tbody>
<tr>
<td>DIA 060400</td>
<td>Data in, A buffer to AC</td>
<td></td>
</tr>
<tr>
<td>DIB 061400</td>
<td>Data in, B buffer to AC</td>
<td></td>
</tr>
<tr>
<td>DBC 062400</td>
<td>Data in, C buffer to AC</td>
<td></td>
</tr>
<tr>
<td>DOA 061000</td>
<td>Data out, AC to A buffer</td>
<td></td>
</tr>
<tr>
<td>DOB 062000</td>
<td>Data out, AC to B buffer</td>
<td></td>
</tr>
<tr>
<td>DOC 063000</td>
<td>Data out, AC to C buffer</td>
<td></td>
</tr>
<tr>
<td>NIO 060000</td>
<td>No operation</td>
<td></td>
</tr>
<tr>
<td>SKPB 063400</td>
<td>Skip if Busy is 1</td>
<td></td>
</tr>
<tr>
<td>SKPBZ 063500</td>
<td>Skip if Busy is 0</td>
<td></td>
</tr>
<tr>
<td>SKPDA 063600</td>
<td>Skip if Done is 1</td>
<td></td>
</tr>
<tr>
<td>SKPDZ 063700</td>
<td>Skip if Done is 0</td>
<td></td>
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<tr>
<th>Stack manipulation instructions</th>
<th>Decimal</th>
<th>Operation</th>
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</thead>
<tbody>
<tr>
<td>MFFP 060201</td>
<td>Move contents of frame pointer to AC</td>
<td></td>
</tr>
<tr>
<td>MFSP 061201</td>
<td>Move contents of stack pointer to AC</td>
<td></td>
</tr>
<tr>
<td>MTFP 060001</td>
<td>Move contents of AC to frame pointer</td>
<td></td>
</tr>
<tr>
<td>MTSP 061001</td>
<td>Move contents of AC to stack pointer</td>
<td></td>
</tr>
<tr>
<td>POPOP 061601</td>
<td>Move top word on stack to AC and decrement stack pointer</td>
<td></td>
</tr>
<tr>
<td>PSHA 061401</td>
<td>Increment stack pointer and move contents of AC to top of stack</td>
<td></td>
</tr>
<tr>
<td>RET 062601</td>
<td>Restore accumulators, program counter and carry from last return block on stack</td>
<td></td>
</tr>
<tr>
<td>SAV 062401</td>
<td>Push a five-word return block on stack</td>
<td></td>
</tr>
<tr>
<td>MSKO 062077</td>
<td>Set up interrupt-disable flags according to mask in AC</td>
<td></td>
</tr>
<tr>
<td>RTCEN 071077</td>
<td>Enable interrupts from CPU real-time clock</td>
<td></td>
</tr>
<tr>
<td>RTDCS 065077</td>
<td>Disable interrupts from CPU real-time clock</td>
<td></td>
</tr>
<tr>
<td>TRAP 100010</td>
<td>Software interrupt (ALC format no-skip, no-load)</td>
<td></td>
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<thead>
<tr>
<th>Central processor control instructions</th>
<th>Decimal</th>
<th>Operation</th>
</tr>
</thead>
<tbody>
<tr>
<td>HALT 063077</td>
<td>Halt the processor</td>
<td></td>
</tr>
<tr>
<td>INTA 061477</td>
<td>Acknowledge interrupt by loading code of nearest device that is requesting an interrupt into AC bits 10 to 15</td>
<td></td>
</tr>
<tr>
<td>INTDS 060277</td>
<td>Disable interrupt by clearing interrupt ON</td>
<td></td>
</tr>
<tr>
<td>INTEN 060177</td>
<td>Enable interrupt by setting interrupt ON</td>
<td></td>
</tr>
<tr>
<td>IORST 061077</td>
<td>Clear all I/O devices</td>
<td></td>
</tr>
</tbody>
</table>

1 \* "location E" pertains to a location with an address computed using bits 5 to 15 of the word and either the FC, AC2 or AC3
2 ACS and ACD refer to source and destination accumulators, each selected by a 2-bit section of the instruction.
BM CLOCK lines provide a differential clock signal for the I/O transceivers. Two other clock outputs from the 629 or 636—the \( \phi A \) and \( \phi B \) lines—are designed to feed the clock drivers for the CPU and IOCs.

The other lines on the transceivers are used to buffer the I/O Data 1, Data 2, input and clock lines from the processor. Not only are the lines buffered, but they are designed to handle data differentially so that line-driving up to 100 feet is possible without any other drive circuits.

One unusual feature of all the microNova circuits is the capability to clear the system under the control of the mN629 and mN636s. When the Clear line on the 629 or any 636 is brought Low, it pulls Low the buffered I/O clock lines in the mN603s and mN601s for a comparatively long time—milliseconds instead of microseconds. All circuits connected to the I/O clock lines have special detection circuits built in that can sense the longer shut-off of the signal and, in turn, signal each circuit to reset itself.

**Put together a working system**

Getting all the components to work together requires that you connect a two-phase clock to the processor, buffer the I/O data lines with an mN629, buffer the address bus with mN634s and connect the power supplies (Fig. 8a). Shown in Fig. 8a is a complete processor (CPU module) that can be used in a minimal system configuration with static memory or in larger systems with dynamic memories.

A typical 4-k x 16 memory board can be built from the mN606 memories, the mN634 address drivers, the mN506 sense amp/bus driver and some simple control logic. The wiring interconnect is mainly a mass of bus interconnects, since all the address lines as well as the supply and control lines are paralleled (Fig. 8b).

The last board, or circuit section, that must be added can drive up to 20 mN636s. For every I/O controller circuit, there must be one mN636.
8. **By combining a processor chip**, two mN634 buffers, an mN640 clock driver and an mN629 transceiver, you can build a complete CPU module (a). Data General also has available a 4k memory card (b) and an IOC card (c).
to form a working system is the I/O control board. A typical I/O module consists of the mN603 controller, the 636 transceiver, a 4 to 16-line decoder, and line buffers and control logic (Fig. 8c). The decoder section of the I/O module decodes the 16 possible function codes delivered by the mN603 over the F bus. These signals indicate, among other things, whether the IOC module is transmitting or receiving data via the device data signals and, if so, the nature of the data.

Connected together, the three basic modules can form a powerful computer system with the software capability of the larger minicomputers. Data General has combined some of the functions on single circuit boards that form part of the support products available for the microNova. For example, the CPU and 2-k/4-k RAM board measures just 7.5 × 10.4 in., yet contains the central processor as well as circuitry for a real-time clock, power-fail/auto restart, auto program load and all support and interface circuits for connecting the board to external I/O and memory buses. Also built onto the board are either 2048 or 4096 words of RAM (960 ns cycle time).

To get data into or out of the processor board without building a large system, Data General offers a hand-held console. When used with standard console software, the hand-held subsystem provides all the functions normally found on a minicomputer’s front panel. It can be used for simple programming, troubleshooting and program debugging. The portable console consists of a 20-key keypad and six-digit readout, and is housed in a 1.2 × 3.3 × 4.85 in. case. The console is based on one of the mN603 controller circuits.

Full-duplex communication between a microNova and an asynchronous terminal is easily provided by an asynchronous interface board with either a 20-mA loop or RS-232 interface at rates ranging from 50 all the way to 19,200 baud. Also, character formats can consist of one start bit and five, six, seven or eight data bits, even, odd or no parity, and one or two stop bits. All the features are jumper-selectable.

For low-cost mass storage, the microNova system also has available a floppy-disc subsystem that can pack up to 157,696 words onto a single disc. Over 300-k words of on-line storage is provided because each subsystem controller can handle two disc drives.

Even a PROM programming board is available to microNova users. Based on the IOC circuit, it can program the Signetics 82S126 and 82S130 PROMs mounted on boards in use in an on-line mode, and zaps ONEs at a rate of one every 20 ms.

Program development has abundant support

Since the microNova family of products is compatible with all the other Data General Computer products, a great deal of development software is readily available (Table 2). A basic development system, consisting of the microNova, a diskette sub-system and an ASCII terminal, comes with all development software. For larger development systems, the Nova-3 minicomputer that supports up to 128-k words of memory can be used to develop software.

The basis for most microNova development software is the disc-operating system. The diskette-based DOS provides a smooth flow through varying development phases to completed production software. It provides operator-interface features, peripheral control and file management. Interrupt handling, physical I/O and file processing are transparent to the user.

A command-line interpreter provides a simple interface to the DOS. It gives the operator extensive file-maintenance capabilities, control over the system utilities and a simple way to invoke complex sequences of program executions. As part of the program-entry system, a text editor program combines multiple text streams, remembers frequently used editing sequences, and even executes a program of conditionally looping text-modification commands.

Both Fortran IV and full Basic are available to those who want to work in higher-level languages. The Data General version of Fortran IV exceeds ANSI standards and offers multitasking extensions that are essential to real-time applications. It supports multiple I/O formats, in-line assembly-language coding, and relational and logic operators. The program also generates re-entrant code that can be shared by multiple tasks for memory efficiency and ROM-based program storage.

Available on diskette, full Basic, with extensions for string arithmetic and matrix I/O operations, can be used in conjunction with the DOS. It is available in single and multi-user versions and can run on all Data General computer systems from the microNova to the Eclipse C/330.

Other software for the microNova system includes a macro assembler, a library-file editor, a relocatable linking loader, a symbolic debugger and an extensive set of program libraries from the users’ group.

With machine-language efficiency, the macro assembler permits expanded expression evaluation via Fortran-like expressions. Extensive listing-control directives generate self-documenting programs with little help from the programmer. The library-file editor lets users combine compiler or assembler outputs to form binary libraries.

The relocatable linking loader lets you combine multiple independent binary modules into an executable program. Capabilities include automatic library search, conditional load, comprehensive load-map listings and flexible origin definition. A symbolic debugger helps simplify program troubleshooting by designating user labels, assembler mnemonics and program offsets. Multiple-format printout directives let data be listed as characters, half-words, or symbols, or in octal format.

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but make sure you know enough about the displays. Raster-scan systems are simple and can be interfaced with little extra circuitry.

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In general, a CRT-based display system is the most flexible display you can interface with a microprocessor. Under program control, the CRT’s electron beam can be made to form any character or pattern desired. Highly reliable, a CRT offers the lowest cost per character for displays of 50 or more characters.

Raster scanning works like this. . .

The image on raster scanned CRT displays is built up by generating many lines across the face of the CRT. Typically, the electron beam starts in the upper left corner of the display, moving from left to right and top to bottom, to “paint” a series of zig-zag lines on the screen (Fig. 1a). Two independent circuits, operating simultaneously, control the horizontal and vertical movement of the beam.

As the electron beam moves across the face of the screen, a third circuit controls the intensity of the beam so that the phosphors can be made to light in any desired pattern—from a simple on/off dot pattern to either a complex grey-scale arrangement for black-and-white displays or multicolor variations for color displays.

1. Both a non-interlaced video display (a) and an interlaced display (b) generate images on a CRT screen. But, the interlaced display effectively provides double the resolution of the non-interlaced version.

When the beam reaches the end of a line, it is brought back to the beginning of the next line faster than it moved to generate the line. Usually during this “retrace” period, the electron beam is shut off (blanked) so the retrace line doesn’t appear.

As the beam is moved horizontally, it is also moved slightly downward. As a result, each successive line starts below the previous line. When the beam reaches the bottom of the screen, it retraces vertically at high speed back to the first line. The network of lines that are traced on the CRT screen is called a raster.

Although manufacturers have standardized at a frequency of 15.7 kHz for the horizontal sweep frequency (63.5 µs/line), this can vary by 10% for most display systems. Vertical sweep will usually be between 45 and 65 Hz. However, in many CRT display systems, the power supplies are poorly filtered and shielded, which causes some line-frequency modulation of the raster. Ideally the sweep rate should be equal to the power-line frequency for the best display. If the sweep isn’t synchronized, the raster will appear to move or “breathe” at the difference of the two frequencies. If the two frequencies are equal, this motion cannot be noticed because a stroboscopic effect freezes the motion.

For 60-Hz line frequencies, there are normally 262 lines per complete raster scan (often referred to as a field); for 50-Hz systems, normally 312 lines. In many applications, though, neither line count provides enough resolution. But you can effectively double the number of lines (Fig. 1b) by inserting a second set of lines between the first set (interlacing). However,
the line sets aren't generated simultaneously. For a 60-Hz system first all the even-numbered lines are scanned: 0, 2, 4, ..., 524. Then all the odd-numbered lines: 1, 3, 5, ..., 525. Each set of lines (field) usually contains different data.

However, interlacing has some disadvantages. First of all, the circuitry necessary for scanning is more complex than noninterlaced display circuits. Second, the over-all vertical refresh rate is half that of noninterlaced units. As a result, the display can flicker when a CRT screen has fast reacting phosphors.

For the best viewing, use CRTs with P33 or P39 high-persistence phosphors. In most TV receivers, the flicker cannot be noticed, since both fields contain almost identical information.

Of course, another way to get good resolution is to use a special CRT system that operates at a higher horizontal sweep frequency. These systems are more expensive than TV monitors and use nonstandard horizontal scanning components.

**Several signals control the display**

The internal sweep circuits of most CRT-display systems are free-running—that is, they aren't synchronized to any master timing circuit. However, to obtain a meaningful display, the sweep must be sync'd to an external controller (Fig. 2a). This is done by horizontal and vertical sweep signals generated by the controller (Fig. 2b). Lower-cost CRT monitors usually require one signal source for horizontal sync, one for vertical sync and one for the data.

Many TV monitors accept one signal that combines all three signals into a composite video signal (Fig. 2c). Circuits inside the monitor separate the composite signal into its component parts. The major advantage of a composite video signal is that it can be sent over long distances on a single 75-Ω coaxial cable.

The main part of any CRT-monitor control system is its sync generator, which provides all the sync and timing signals necessary to control the display. There are several approaches to designing one. To provide the proper signals in the simplest way, first the CRT screen is divided into tiny cells. Then the beam's position is controlled by keeping track of the cell number where it is positioned.

Cells are also handy for generating characters, since each character can be defined as requiring one cell. For alphanumeric displays, cells usually correspond to character positions. In graphic displays, a cell can be a single dot or a group of dots.

In the case of alphanumeric displays, characters are generated by lighting up the proper combination of dots in a $5 \times 7$ or a $7 \times 9$ dot matrix that makes up each cell (Fig. 3a). The patterns for each character are often stored in a character-generator ROM. For the CRT display, the ROM should be row-addressable not column-addressable (Fig. 3b). The cell on the CRT screen must also allow for horizontal and vertical-row spacing—usually one extra row or column of unlit dots is used for the space between characters and rows. Then the cell is either $6 \times 8$ or $8 \times 10$ dots. Some of the ROMs also include the blank lines of dots, so the external circuits can be simplified even further.
ROW OUTPUTS OF ROM PROVIDE ONE SLICE THROUGH CHARACTER

ROM ROW ADDRESS SELECTS ROW WHICH IS OUTPUT

ROM CHARACTER ADDRESS SELECTS CHARACTER TO BE DISPLAYED

PARALLEL CLOCK
LATCH
SHIFT REGISTER
CHARACTER GENERATOR ROM

3. **Standard 7×9 and 5×7-dot matrix displays** can be generated from ROM-based data (a). To actually form the characters, a line-by-line slice is read out from the row-addressable character generator ROM (b).

4. **Inside the sync generator** many counters are used to generate all the various timing signals and provide the addresses for the RAM where the displayed data are temporarily stored.

5. **A video RAM circuit** combines the sync generator with all the counting circuits, the character generator and the necessary memory pages to form an almost complete video display system.
ROMs require two sets of input addresses - one for the character to be addressed and one for either the row or column of the character to be displayed. The ROM inputs are usually ASCII-encoded so that a keyboard's output can be fed directly to the ROM.

In a CRT display, the electron beam provides slices of the characters, one row at a time, as it scans a line. The row outputs of the ROM are usually held in latches, which are transferred to a parallel-input shift register, then shifted into the video-generation circuits via the shift register's serial output.

Inside a video display, the character generator receives stable row and character addresses to determine which character is to be displayed. Then the output of the generator is latched into a shift register and clocked out to form the video signal (Fig. 4). So a master clock is needed to do all the timing.

The clock that drives the sync generator and video-shift register operates at what is called the dot frequency, which can be calculated by:

$$f_{dot} = f_{line} \times \text{number of lines} \times \text{number of cells per line} \times \text{number of horizontal dots per cell}$$

Number of lines = number of character lines \times number of lines per cell.

The dot frequency is fed into a counter that divides by the number of dots per cell. Logic circuits driven by this counter control the flow of data to the shift register delivering the serial video data. The final output of the dot counter drives another counter that keeps track of the number of cells on the current line.

Make allowances for the number of displayed cells along with the necessary retrace time. Typically, an 80-character line should have at least 104 cells (retrace should have at least 25% of the total number of displayed cells).

Logic circuits connected to the cell counter can generate the necessary sync and blanking signals during the nondisplay portion of the line. And the outputs of the cell counter can also be used to drive some of the address lines of the display memory.

The output of the cell counter also feeds to another counter that keeps track of the number of lines displayed for a particular cell. This cell-line counter feeds its outputs directly to the row-address lines of the character generator.

One more major counter is used in the system — a character-line counter. Fed by the final output of the cell-line counter, it keeps track of how many character lines are being displayed. To permit enough time for the vertical retrace of the beam, the count value must be 20 to 25% more than actually needed.

The logic that generates the vertical sync and blanking signals is controlled by this counter. What's more, some of the outputs can be used to drive the remaining address lines of the character memory.

Since a CRT doesn't hold data on the screen indefinitely, all video data must be refreshed, every 1/30 of a second at least. To hold all the data that must be displayed, a block of fairly fast RAM must be used for temporary storage. Each full screen of data is often referred to as a page, and the minimum storage usually included for a display is one page. However, some monitors that are designed to handle large amounts of data, can often store several pages of data.

**Hold the pages in memory**

The type of memory page used is governed by the type of memory circuit and the method of interface. Almost any kind of memory can be used in page storage—circulating memories, such as CCDs and other shift registers, or static or dynamic RAMs. Since RAMs are the easiest memory to use, let's confine this...
discussion to RAM systems.

The sync-generator circuit, besides supplying the timing necessary to provide the horizontal and vertical sync, scans the memory page and can also perform the refresh of dynamic RAMs. However, the timing of these RAMs with, say, a microprocessor that isn’t synchronized with the sync generator creates limitations. Interrupting the refresh cycle can cause data loss. Static RAMs eliminate this problem.

But in systems that need a great deal of memory, such as graphics displays, the lower cost of dynamic RAMs outweighs their disadvantages.

The total system revolves about the sync generator. All necessary timing is generated by decoding appropriate counter states. Note that the sync pulses should be positioned in the middle of the retrace interval. The row addressing of the character generator comes from the cell-line counter. Memory addressing comes from the cell counter and the character line counter.

Building the character’s screen image begins with the electron beam writing a slice through a series of characters as it scans a line. The column address of the memory is controlled by the cell counter. On the next line, a different slice of the same characters is scanned through since only the address to the cell-line inputs of the character-generator ROM has changed. This continues until the cell-line counter resets, and increments the character-line counter. Note that the cell-line counter is interpreted as the row address of the page memory. Thus, the beam then starts to slice through another set of characters on the new line. The video RAM organization (Fig. 5) is a typical interface arrangement between a sync generator and the page memory.

Start your actual design by selecting a screen format and a character generator. Assuming a 24-line x 80-character format with a 5 x 7-dot matrix character, the number of dots per line will be 80 x 6, or 480 (remember, the cell is 6 x 8). However, one line must consist of the 80 cells plus another 24 to handle timing overhead. Thus, the cell counter must divide by 104. The number 104 is an easy one for binary counters to handle (64 + 32 + 8).

Since there are eight lines per cell, the cell-line counter must divide by 8. A minimum 24 character lines are required, but 9 additional line-time periods should be included to permit vertical retrace. So, a divide-by-32 counter will do the trick.

For every frame, then, there are eight lines per character and 32 character lines, for a total of 256 dot lines. This is well within 10% of the 262 lines desired.

The dot frequency can now be calculated from the formula described earlier:

\[ f_{\text{dot}} = 60 \text{ Hz} \times 256 \text{ lines} \times 104 \text{ cells/line} \times 6 \text{ dots/cell} = 9.58464 \text{ MHz}. \]

You can vary the aspect ratio of the characters by varying the intercharacter spacing. In this example the character can be made narrower by using seven or eight dots per cell.

8. To control the timing all that’s needed is a single-phase clock. When High it lets the sync generator feed into the multiplexer. When Low, it lets the processor control the display memory through the multiplexer.

9. By using a DMA interface between the processor and the video display, the main system memory can be constantly updated then transferred to the display’s buffer in one operation every time the display wants an update.

10. Connecting the video RAM to either the 8080A or 6800 is easily done with some gates and the µP’s read/write line. The video RAM can be located anywhere in the computer’s memory space and is, in fact, addressable just like any random-access memory.
11. **Building an intelligent terminal** with a video RAM is as simple as adding some more RAM. Just connect the

Speed is important, especially when a large number of characters must be put on a screen. The greater the number of characters on the screen, the higher the dot-clock frequency. However, the CRT monitor itself is often the limiting factor (many monitors are limited to 5 or 10 MHz).

Display performance can be affected by the access time of the memory system (the cell-to-cell spacing in time). In the example shown, this time can be calculated as

\[
t_{\text{cell}} = \frac{1/f_{\text{dot}}}{\text{(number of dots/cell)}} = 626 \text{ ns} \approx \frac{1}{9.58464 \text{ MHz}}.
\]

This is the total time available for both the page memory access and the ROM lookup. A pipeline organization of the two elements, as shown in Fig. 6, reduces the cell's time requirements to the greater of either the page memory or ROM-access speed.

**Interface the memory to the display**

Ideally, the RAM used in the display system should be accessible from two sources—the sync generator and an external device such as a microprocessor. Three alternative approaches can be used to do the job simply: a video RAM interface, an interlaced memory interface and a direct-memory-access interface.

Of these easy methods, the video-RAM interface is probably the easiest. It uses a memory-mapped addressing technique to access the characters. And access to the memory is controlled by a two-input multiplexer (Fig. 7).

Normally, the sync-generator's address outputs control the memory. The address lines of the memory can thus be switched between two sets of address data. The switching is controlled by a single line that is treated much the same way as a chip-select line.

The memory output and input buses can also be connected to the external system's data bus via three-state transceivers. The transceivers are, in turn, controlled by a \( \mu \text{P's} \) read/write and chip-select lines.

By activating the chip-select line, the external system can take control of the RAM. This organization creates a display interface that looks like a RAM to the computer. Similar approaches are used by Matrox and other companies to form low-cost display modules for CRT display systems.

One disadvantage is that the computer interrupts the normal scanning of its memory whenever a read/write operation is attempted. Moreover, this interruption can be seen as streaks or flashes on the CRT screen. This problem usually doesn't matter if memory accesses occur in infrequent bursts for updates. Still, the problem can be eliminated if memory accesses are confined to the video-blanking intervals.

The interlaced memory interface is similar to the video RAM interface, except that the memory is
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regularly and systematically made available to both the microcomputer and sync generator. Access to the memory is still controlled by a multiplexer. However, the multiplexer is alternated between the address bus and sync generator no matter what. Switching is controlled by the microprocessor's state sequencer. Thus, the memory is almost transparent to both the sync generator and the μP.

Another way to interlace the memory is to permit the processor to access the memory only during the "vacant" period immediately after each sync-generator access (Fig. 8). A handshake-control block helps the processor coordinate its access to the RAM so that it doesn't interfere with the sync generator.

Many variations of the interlaced memory scheme are possible. However, it is particularly suited for dynamic RAMs since refresh can always be included in the memory cycle.

The third approach, direct-memory access, can eliminate the problem of CRT memory scanning. Here, the page memory is part of the computer system's memory. When the display must access the memory for refreshing the data on the screen, it can stop the processor so the μP releases control of the address and data buses to an external device, called a DMA controller. This in turn is controlled by the display sync generator (Fig. 9).

The sync generator requests data from the system RAM in bursts via the DMA controller. The controller transfers information from the RAM to the CRT display's buffer memory, which can then be read out by the sync generator and put on the screen.

While this method avoids the interference problem of the video RAM, it is more complex—and more expensive to put into use. What's more when a DMA occurs, the processor must stop, thus slowing down any calculations or stopping any control functions the processor is doing.

Naturally, weigh the advantages and disadvantages of these three video-interface methods when you design a display system. And remember: There are other ways to do the job that haven't even been touched upon. Also, many other features can be added to the display system—scrolling, cursor generation, and multipage storage, to name just a few.

Connecting a circuit such as the video RAM into a processor system is relatively simple. Fig. 10 shows the interface necessary to connect the Matrox MTX-1632 VRAM to either the 8080A or 6800 microprocessor-system buses. The MTX-1632 provides a 16-line x 32-character display and can be located anywhere in the processor's memory.

You can also build an intelligent terminal around a video RAM (Fig. 11). The unit must be connected in the terminal system so that it becomes part of the memory. The intelligence of the terminal depends completely on the program stored in ROM. Typically, keyboard entries are read by the μP via the parallel-interface port. After processing the data, the information can be displayed by writing it into the RAM.
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Data shifting, an integral part of digital multiplication, division and scaling, is usually done with
a straight shift register. Data are entered in parallel,
shifted left or right, and outputted in parallel. However, these registers usually require one clock period
for every position shifted, which makes complex
calculations time-consuming. In the same clock period,
a specialized scaling circuit, such as the Am25S10, can
shift four bits of data 0, 1, 2, or 3 places (Fig. 1).
The high speed shifting of data is critical in many
floating-point processors and data recorders, where
real-time calculations must be performed on incoming
data. By normalizing the data before performing
calculations, many an algorithm can be accelerated.
With the right interconnections, the 25S10s can be
cascaded for any word length and shift the word any
number of places left or right. Shifting can be logical,
with ZEROs pulled in at either or both ends;
arithmetic, with the sign bit repeated during a shift
down; or end around, with the data word forming a
continuous loop.

Get to know the Am25S10

Working with the scaling circuits such as the 25S10
developed by AMD and second sourced by Signetics
is relatively simple. Housed in a 16-pin DIP, the
Schottky MSI circuit has seven data inputs, I_0, I_1, I_2,
I_3, I_4, I_5, and I_6; four three-state outputs, Y_0, Y_1, Y_2 and Y_3; one output enable line, OE; two
control lines, S_0 and S_1; and two power pins.
The three-state outputs allow several 25S10s to be
bus-organized for shifts of more than three places,
with only a single-level gate delay of less than 20 ns.
In addition, input loading due to current sharing is
usually only 1.5 standard Schottky loads—not up to
four as might be expected with the internal gate
arrangement.
The OE line is an active-Low control—when Low,
the data outputs follow the selected data inputs; when
High, the outputs present a high impedance to the
data bus. Under control of the two S lines, the I input

derived from

John Mick, Engineering Manager, Digital Bipolar Products,
Advanced Micro Devices, 901 Thompson Place, Sunnyvale,
CA 94086.

1. Under the command of two control lines the input word
to the 25S10 can be shifted 0, 1, 2 or 3 places during
a single cycle. It takes less than 20 ns for a signal to
propagate through.
2. The four shift positions of the 25S10 depend on just the \( S_0 \) and \( S_1 \) control lines (a). By representing the 7-bit input as a single word, \( A_0 \) to \( A_6 \), the function table showing the next output can be drawn up (b).

3. Shifting a 16-bit word up to four places, the scalers can be cascaded for almost any word length. When the data word is shifted, the most significant bits are discarded and ZEROs entered for the LSBs.

Another circuit that uses 25S10s can perform a complete end-around barrel shift of 0, 1, 2, 3, 4, 5, 6 or 7 places on an 8-bit input word by manipulating three control lines—\( S_0 \), \( S_1 \) and \( S_2 \) (Fig. 4a). Again four 25S10s are necessary; however, with the three-state capability on the outputs, only two circuits are actually used at one time.

In this barrel configuration, the \( S_2 \) and \( S_3 \) select...
4. An end-around barrel shifter built from four scalers can handle an 8-bit data word and shift it 0, 1, 2, 3, 4, 5, 6 or 7 places, as shown in the function table (a). An equivalent wired shifter (b) has double the circuitry.
5. Performing a 16-bit, two-level barrel shift requires just eight 25S10s. By using a two-level approach, four control inputs determine which pair of 25S10s is selected. When $S_2$ is Low, IC$_1$ and IC$_2$ are on the bus and when High IC$_1$ and IC$_2$ are enabled.

Larger word lengths can be handled by using several 25S10s on each bit line and one-of-four or one-of-eight decoders to control the enable lines. If dedicated, hardwired multiplexers are used to perform the same function as shown in Fig. 4b, at least double the hardware would be necessary.

Another way to perform end-around shifting involves more than one level of shifters. A two-level, 16-bit barrel shifter can be built from eight 25S10s,
6. To do 2's complement arithmetic, a 13-bit scaler can be built from three shifters. Scale factors of \( \frac{1}{8} \), \( \frac{1}{4} \), \( \frac{1}{2} \) and 1 can be set by the two control lines. Either a 0 or 1 can be shifted into vacated places.

Software commands for 2901A/25S10 network

<table>
<thead>
<tr>
<th>2901A Source select</th>
<th>2901A ALU function</th>
<th>2901A Destination</th>
<th>25S10 Shift control</th>
<th>Function performed</th>
</tr>
</thead>
<tbody>
<tr>
<td>Function Octal code</td>
<td>Function Octal code</td>
<td>Function Octal code</td>
<td>Function Octal code</td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 1 Rotate register</td>
<td>1 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 2 Rotate register</td>
<td>2 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 3 Rotate register</td>
<td>3 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 4 Rotate register</td>
<td>4 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 5 Rotate register</td>
<td>5 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 6 Rotate register</td>
<td>6 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 7 Rotate register</td>
<td>7 position</td>
<td></td>
<td></td>
</tr>
<tr>
<td>D, 0 7 OR 3 RAM A</td>
<td>2 8 Rotate register</td>
<td>8 position</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

which are connected to give four control lines, \( S_0 \) to \( S_1 \) (Fig. 5). The one-level method used in Fig. 4 would require 16 circuits to build a 16-bit barrel shifter.

If 2's-complement numbers have to be scaled, as in many mini or microcomputer applications, a 13-bit scaler can be built with just three 25S10s (Fig. 6). The sign bit is pulled in at the most significant end, and the least significant bits are truncated. Thus, a 13-bit number can be scaled to 1, \( \frac{1}{2} \), \( \frac{1}{4} \) or \( \frac{1}{8} \) its input value by shifting it 0, 1, 2, or 3 places.

Bit-slice processors take the best advantage of the improved speed contributed by the 25S10. Connecting an 8-bit barrel scaler as shown in Fig. 4 to a processor built around the 2900 series of bit slices is relatively straightforward (Fig. 7). The I lines connect to the 2901A output bus, and the Y-output lines connect to the data bus. The scalers are controlled by the microprogram memory directly or by one of the other control registers used in the processor.

Sample microinstructions for firmware control are shown in the table for shifting a word in any of the sixteen 2901A internal registers.

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TM 500...designed for configurability.

FOR TECHNICAL DATA CIRCLE 40
FOR DEMONSTRATION CIRCLE 41
When testing 16-k dynamic RAMs, keep your eye on the temperature and your finger on your pattern generator. Minding both gives more accurate results.

Test a 16-k RAM inadequately, and you're on your way to a migraine headache. Two ways to get into big trouble: Forget about temperature effects, and ignore important test-pattern sequences. Analyze both, and you'll save your aspirins for later. Storage time is a case in point.

Charge storage on a 16-k MOS RAM is, of course, dynamic in nature, since the charge on the MOS capacitor eventually will leak off. Storage time is an intrinsic device parameter. Refresh time—more properly, refresh interval—specifies a maximum allowable interval. The interval separates two operations (on the same storage location) that will re-establish the full charge on a partially decayed HIGH level.

Performance varies with temperature

But remember: Storage time depends on temperature:

\[ T_s = A \exp(-BT) \]

where \( T \) is the junction temperature in °C, \( B \) is a variable relating the magnitude of the generation-recombination current to the junction temperature (units of 1°C), and \( A \) is a scaling constant reflecting such variables as junction area, bulk-defect density, and sense-amplifier design.

Note that \( B \) is not a constant. Normally, it is assumed that the storage time doubles for every 10°C decrease in junction temperature—which is equivalent to assuming that \( B = 0.069 \). Data show that 0.055 is a typical value for \( B \)—but the number varies at least ±30% from the typical (Fig. 1).

The storage time at \( T_J = 25 \) °C for the hypothetical device of Fig. 1 will lie somewhere between 50 and 381 ms. If room-temperature testing is to be attempted, the refresh interval should be set at 381 ms, since any lesser value won't guarantee the assumed minimum storage time of 2 ms at 100 °C. Devices failing such a test won't necessarily be failures at 2 ms and 100 °C, and would therefore have to be rescreened at 100 °C.

The efficiency of the procedure depends upon the number of good devices found by the first screen, but in general the number of units requiring a second test is so great, you may as well go ahead and eliminate the first screen in favor of a 100% screen at the maximum-junction temperature.

Besides storage time, access time, power dissipation, and input/output levels all need to be verified over the temperature range. Access time and power dissipation are functions of transistor gain, which is temperature-dependent (through carrier mobility) and about 25% lower at 100 °C than at 0 °C. Therefore, access takes longer at elevated temperatures. The memory will dissipate more power at low temperature. However, note that much of the power required is capacitive and thus related to frequency rather than temperature.

![Storage Time vs Junction Temp Graph](image)

1. Storage time doesn't necessarily double for every 10°C decrease in junction temperature, as the "conventional wisdom" states. Setting the correct refresh intervals during testing requires an accurate knowledge of the minimum storage time for the memory.

Robert W. Owen, Product Engineer-Mostek Corp., 1215 W. Crosby Rd., Carrollton, TX 75006.
Signal levels are functions of transistor-threshold voltage, which decreases about 2 mV for every 1°C increase in temperature. Input HIGH levels and output HIGH and LOW levels are normally the worst at low temperature and must be guardbanded if you test only at high temperature. (One 16-k RAM, the Mostek MK 4116, incorporates an integrated reference voltage for address and data inputs—which removes the threshold-voltage dependence and the temperature dependence along with it.)

A few timing parameters become worst-case as the memory becomes faster, and you must guardband these if you test only at high temperature. On balance, however—primarily because storage time varies radically with temperature—it is best to conduct tests at the maximum junction temperature only and guardband parameters that aren’t worst-case.

Calculating temperature rise

The two junction temperatures singled out in Fig. 1 are not chosen at random. The equation describing temperature rise over an ambient is given by:

\[ T_J - T_A = \Delta T = \theta_J A P_D, \]

where \( \theta_J A \) is the junction-to-ambient thermal resistance (for a 16-pin ceramic DIP mounted in a socket on a double-sided PC board, the most widely accepted value is 70 C/W), and \( P_D \) is the power dissipation of the device under the conditions of interest.

To get \( \Delta T \), assume the following specified values

- \( I_{DD} \) (active) = 35 mA,
- \( I_{DD} \) (stand-by) = 1.5 mA,
- \( V_{DD} \) (maximum) = 13.2 V,
- \( t_{cycle} \) = 375 ns.

Assume that the refresh test writes 16,384 bits at the 375-ns cycle rate, pauses in the stand-by condition for the refresh interval, then reads all bits again at 375 ns. With \( t(\text{refresh}) = 2 \) ms, calculate the rise in junction temperature as follows:

\[
\text{duty factor (DF)} = \frac{2 \times 16,384 \times 375 \text{ ns}}{2 \times 16,384 \times 375 \text{ ns} + 2 \text{ ms}} = 0.86.
\]

Therefore:

\[
\Delta T = \theta_J A \left[P_D (\text{active}) \times (DF) + P_D (\text{stand-by}) \times (1 - DF)\right] = 70 \text{ C/W} \left[0.035 \times (13.2) \times 0.86 + 0.0015 \times (13.2) \times (1 - 0.86)\right] = 28 \text{ C}.
\]

With \( t(\text{refresh}) = 381 \) ms,

\[
(DF) = \frac{2 \times 16,384 \times 375 \text{ ns}}{2 \times 16,384 \times 375 \text{ ns} + 381 \text{ ms}} = 0.03.
\]

Therefore:

\[
\Delta T = 70 \text{ C/W} \left[0.035 \times (13.2) \times 0.03 + 0.0015 \times (13.2) \times (1 - 0.03)\right] = 2.3 \text{ C}.
\]

The junction temperature of a device undergoing a 381-ms refresh test at \( T_A = 25 \) C will rise only 2.3° to 27.3°, while the same device executing a 2-ms refresh test at \( T_A = 70 \) C will rise to a whopping 98 C.

Strictly speaking, the foregoing calculations are true only if you allow the junction temperature to stabilize by running the refresh test in a continuous mode. The thermal mass of the device is not negligible. In fact, \( \theta_J A \) is a function of time and has a time constant of approximately 60 s in most test situations.

Is it the pattern or the temperature?

Interestingly, much of the effectiveness of the \( N^2 \) pattern test is attributed to elevated junction temperatures occurring during the test interval. An \( N^2 \) pattern, with \( N \) equal to 16,384 and a cycle time of 375 ns, requires 100 s. The value of \( \theta_J A \) after 100 s
## Possible minimum test sequence for 16-k RAM

<table>
<thead>
<tr>
<th>Test Description</th>
<th>Data Pattern</th>
<th>Function</th>
<th>Power Supplies</th>
<th>Cycle Count</th>
</tr>
</thead>
<tbody>
<tr>
<td>Maximum cycle</td>
<td>Diagonal</td>
<td>Functionality</td>
<td>13.2 -4.5</td>
<td>2N (t_cyc = 10 Ms)</td>
</tr>
<tr>
<td></td>
<td>Diagonal</td>
<td></td>
<td>13.2 -5.5</td>
<td>2N (t_cyc = 10 Ms)</td>
</tr>
<tr>
<td></td>
<td>Diagonal</td>
<td></td>
<td>10.8 -5.5</td>
<td>2N (t_cyc = 10 Ms)</td>
</tr>
<tr>
<td></td>
<td>Diagonal</td>
<td></td>
<td>10.8 -4.5</td>
<td>2N (t_cyc = 10 Ms)</td>
</tr>
<tr>
<td>Load read</td>
<td>Parity and Parity</td>
<td></td>
<td>10.8 -5.5</td>
<td>2N</td>
</tr>
<tr>
<td>Load read</td>
<td>Checkerboard</td>
<td>Bit Interactions</td>
<td>10.8 -4.5</td>
<td>2N</td>
</tr>
<tr>
<td>Load read</td>
<td>Checkerboard and Checkerboard</td>
<td></td>
<td>13.2 -5.5</td>
<td>2N</td>
</tr>
<tr>
<td>Walking diagonal</td>
<td>Diagonal</td>
<td>Functionality</td>
<td>13.2 -4.5</td>
<td>2N</td>
</tr>
<tr>
<td>Dynamic refresh</td>
<td>Alternate Rows</td>
<td>Data retention</td>
<td>10.8 -5.5</td>
<td>1N + 2 ms</td>
</tr>
<tr>
<td>Dynamic refresh</td>
<td>Alternate Rows</td>
<td>Data retention</td>
<td>10.8 -5.5</td>
<td>1N + 2 ms</td>
</tr>
<tr>
<td>Still refresh</td>
<td>All Highs</td>
<td>Data retention</td>
<td>10.8 -5.5</td>
<td>2N + 2 ms</td>
</tr>
</tbody>
</table>

T of testing is about 80% of its final value. The junction rise for $P_D = 462$ mW is

$$
T = \theta_{JA} P_D = (0.8) (70 \text{ C/W}) (0.462) = 26 \text{ C},
$$

and this rise occurs during the test.

The storage time of the device may be reduced by as much as a factor of six, with the device speed approximately 10% less. You can attain these benefits, of course, without resorting to $N^2$ patterns: pre-calculate the final junction temperature and set the temperature chamber accordingly—an approach not without pitfalls.

If the test chamber is so constructed that heat is maintained throughout the test, you must consider the self-heating. If you hold the device in an elevated ambient before testing, then remove it and insert it into the test socket, you must then characterize the combined effects of heat loss in the socket and self-heating during the test.

The device itself can act as a temperature reference to accurately measure junction temperature. All signal inputs connect to $p_n$ diodes, which can easily be calibrated. Notice that if diode current is held constant, diode voltage is linearly proportional to temperature. Calibrate an input on a reference device by stabilizing the device at an accurately measured reference temperature, injecting a constant current, and measuring the diode drop (from the input to the $V_{BB}$ pin).

When you do so at several temperatures, you can construct a calibration curve of diode voltage vs temperature, then use the device to measure unknown temperatures by injecting current, measuring the diode voltage, and referring to the calibration chart.

Once calibrated, the device can profile either heat loss at the test site or junction-temperature rise during operation—and very accurately. Some tips: A good value for the current is 100 $\mu$A; the voltage measurement requires millivolt accuracy; the measurement cannot be made while the device is operating because of noise in the substrate (operate the device, then switch out the functional inputs and switch in the measurement circuitry). You must calibrate each device separately, since the magnitude and slope of the relationship are variable.

Once you’ve sweated through the heating tests, turn your attention to other possible memory imperfections. Selection of the right test pattern can ferret out any hidden gremlins.

### Tune in to sensitive patterns

Analyzing and using test sequences that exploit possible memory weaknesses is necessary to keep test times for 16-k RAMs within practical bounds. (The following information, although believed to be general, applies specifically to the Mostek design.)

The 16-k is basically a synchronous machine built around a rectangular memory array, the coordinates of which are rows and columns (Fig. 2). The synchronous machine provides the timing control for
the input latches, row decoder, sense amplifier, column decoder, write circuitry, and output latch.

Unlike earlier, asynchronous, RAMs, the 16-k nearly always fails digitally. That is, if a problem exists with the input latches, the wrong output will be generated (but not a "late" output, which is correct but delayed, for example, by poor input levels). Since there is no worst-case pattern for access time, the time is controlled by internal clock generators—which greatly simplifies the testing of gross functionality. This testing ensures cell uniqueness and output validity over the specified timing and power-supply ranges.

On the other hand, you must still check the memory array and sense amplifiers for pattern sensitivities. Consider the signal-detection capabilities of the sense amplifier and its precharge requirements. A probable worst-case pattern for a sense amplifier consists of a single bit of DATA in a field of DATA.

If you run such a pattern in a "row-fast" mode, each sense amplifier will be required to perform some number of DATA reads and a single detection of DATA, and complete the scan by reading DATA.

If the DATA bit occupies, at some time, each of the locations along the digit line, you will have checked the ability of the sense amplifier to pick a signal out of noise and to dispel completely any influence of preceding cycles on the present cycle. Note that this pattern requires only as many scans as there are bits per sense amplifier, and that you can check all columns simultaneously.

When considering the row-select function, here, too, noise-coupling considerations indicate that a worst-case pattern might be either a single DATA bit in a field of DATA or a solid field. Here also the word "field" has restricted meaning, applying only to all cells connected to a single row-select line.

**Which pattern?**

Several patterns check the fore-mentioned failure modes efficiently. One pattern, the $2N^{3/2}$ "moving-diagonal," requires 128 read-write scans through the entire array.

On the first scan, all bits are written to DATA, except for the 128 bits along the major diagonal, which are written to DATA. The read scan verifies the correct operation of the array under these conditions.

On each succeeding scan, the position of the diagonal of DATA is shifted until, on the 128th scan, it has occupied every possible position in the array. Thus, each cell has been the only DATA cell in a row and column of DATA. This pattern proves to be quite effective in screening the 16-k.

Refresh tests can be classified as either still or dynamic. For still tests, write all locations, pause for the refresh interval with RAS and CAS inactive (HIGH), and read all cells. The pause allows the cells to leak LOW, but also allows internal nodes (which are bootstrapped above $V_{dd}$ by the trailing edge of RAS or CAS) to decay so that you end up testing both the cells and the dynamic periphery.

Unfortunately, such a test normally isn't the worst case for the cell, for noise generated during active cycles can contribute to the loss of data in the cell.

The dynamic-refresh tests write data into some subset of the cells (normally half the cells). Then, during the refresh interval, they perform either read or write cycles on the cells not being tested to couple charge-degrading noise onto the unaccessed test cells. Both tests are necessary to guarantee functionality.

Be careful: Testing at maximum cycle time gives noise an opportunity to couple onto the row-select lines (which should be off to prevent a partially selected transfer gate), allowing cell data to leak onto the digit lines.

This test might perform a write scan with minimum precharge times ($t_{pp}$), and maximum active time ($t_{RAS}$), followed by a "read-modify-write" scan under the same basic timing conditions, which is then followed by a read scan to verify the "modify write" operation. This important test is often overlooked but is, in fact, the worst case for many of the internal circuits.

The patterns discussed provide a basic but adequate test sequence, a good starting point. The table summarizes a sequence that should provide a reasonable degree of confidence in any RAM that passes. Special timing modes and certain timing parameters are left unchecked, but you can easily add if desired.

The sequence requires $2N + 4N^{3/2}$ cycles, of which all but $8N$ can be at the fastest allowable cycle rate. The $8N$ are at the slowest allowable cycle rate (maximum cycle length). If the fastest cycle is 375 ns, and the slowest is 10 µs, then the sequence executes in just over 4.5 s, excluding tester overhead and powersupply settling times. **

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**Bibliography**


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Consider piezoelectric ceramics:
Easily formed into complex shapes and chemically inert, they provide stable piezoelectric characteristics up to 180°C.

Piezoelectric properties of ceramic titanates make possible many new applications. Piezo-ceramic materials offer distinct advantages over other piezo-active substances. They are:

- Chemically inert in most environments,
- Processable by standard ceramic technology,
- Formable into complicated shapes with uniform piezoelectric properties, and
- Operable at high temperatures because of a high Curie point.

These superior properties allow you to apply piezoelectricity not only to such narrow uses as instrument force transducers and crystal-controlled oscillators, but also to industrial applications such as ultrasonic cleaning, gas igniters, audible alarms, keyboard switches, and even advanced medical electronics.

The piezoelectric phenomenon isn’t new. Discovered by the Curies in the late 1800s, a number of materials have been found capable of producing piezoelectricity. The most important include the two forerunners of ceramic titanates—Rochelle salt (sodium potassium tartrate) and natural crystalline quartz.

Single-crystal quartz, because of its high-temperature tolerance (usable to 573°C), stability, chemical inertness and physical ruggedness, is ideal for stable control of oscillator frequencies. However, to provide piezoelectric action, single quartz crystals must be oriented precisely, and thin platelets must be cut from the bulk crystal. Only untwinned, nearly perfect crystals can be used, and the world supply is limited. Material waste is high and only simple geometries—plates and discs—can be produced.

Rochelle salt (KNaC\textsubscript{3}H\textsubscript{4}O\textsubscript{7}·4H\textsubscript{2}O) has a much higher piezoelectric voltage output. However, Rochelle salt’s piezoelectric properties are sensitive to temperature. Water soluble, it can be destroyed in humid atmospheres—and its melting point is only 55°C.

Generator or motor action is produced

A piezoelectric material develops an electric charge that is proportional to a mechanical stress. Conversely, the material can convert an electrical field into a dimensional change.

For a stress, \( T \), in Newtons/meter\(^2\) (N/m\(^2\)) the material’s generator action produces a field strength, \( E \), in volts/meter, measured as an open-circuit voltage that is linearly dependent on stress (within limits)

\[
E = -g \cdot T,
\]

where \( g \) is the material’s piezoelectric voltage constant measured in volt-meters/newton. Typical absolute values of “\( g \)” for piezo ceramics range from \( 14 \times 10^{-3} \) to \( 44 \times 10^{-3} \) V·m/N.

Dimensional change or motor action—also a linear relationship—is

\[
S = d \cdot E,
\]

where \( S \) is strain in m/m and \( d \) is the piezoelectric charge constant, with the dimensions of m/V (or Coulombs/Newton). Typical absolute values lie in the range \( 200 \times 10^{-12} \) to \( 600 \times 10^{-12} \) m/V (or C/N) for piezo-ceramic materials.

Piezo-ceramic material has no piezoelectric properties when first fabricated, because the electric-dipoles within grains are randomly oriented. The material must be polarized to align the dipoles in a “poling” operation. The polarization is done with an electric field of 10 to 30 kV/cm at an elevated temperature, but below the ferroelectric Curie temperature.

Because of the high voltage, the material is poled while immersed in silicon oil. The poling axis is in the direction of positive polarization (Fig. 1). The voltage is applied via electrodes of evaporated gold or silver, fired-on silver paint or electroless plated nickel, depending on cost and performance requirements. While poling makes the material behave like a single crystal, the piezo properties of bulk polycrystalline material are somewhat poorer than a true single crystal’s.

Piezoelectric constants \( g \) and \( d \) are directionally dependent. Since the poling axis (direction 3) can differ from the direction of applied stress or applied field, you must employ a convention for describing this directional dependence. For example,\( g \) can have three values—\( g_{33} \), \( g_{31} \) and \( g_{15} \) (Fig. 1). The first subscript is the direction of the generated electric field; the second, the direction of the applied mechanical stress. Since in ceramics, directions 1 and 2 are equivalent,

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Electronic Design 19, September 13, 1977
1. **The piezoelectric constants and the stress and voltage axes are directionally dependent.** Therefore they are indexed relative to the poling axis, which is by convention only subscript 1 is used for both. And where shearing stress is involved, subscripts 4, 5 and 6 represent shear about the three axes.

**Avoid depolarization**

Any stress that tends to destroy polarization must be guarded against—thermal, electrical or mechanical. Heat causes the ceramic’s electric dipoles to return to their previously unaligned states. As the temperature approaches the Curie point, $T_c$, the material becomes completely depolarized and piezoelectric properties disappear. Prudent design thus requires that the continuous operating temperature of piezoceramic material should not exceed about 0.5 $T_c$, which limits operating temperatures to between 130 and 180 °C.

Understandably, a large electric field opposite the direction of the original poling field can degrade the piezoelectric properties and even reverse the polarization. Depending on the material, duration of application and temperature, experience shows that 500 (PXE-5) to 1000 (PXE-43) V/mm is a safe upper limit for applied long-term fields.

Indeed, when applied mechanical stress becomes high enough, it too can cause depolarization. Again, depending on the material, temperature and the nature of the stress, the safe range is from $30 \times 10^6$ N/m² (4351 lb/in.²) for a static load on a piezo-ceramic material such as PXE-21 to $130 \times 10^6$ N/m² for a dynamic load on PXE-4. (The PXE materials have been developed by N.V. Philips Gloeilampenfabrieken, the Netherlands. And, Vernitron Piezoelectric Division, Bedford, OH, makes a similar line of piezoceramic materials, designated PZT, as do many other companies.)

High electric-field generation for spark ignition of gases, flash bulbs or even gasoline engines usually depend on the $g_{33}$ voltage constant.¹

2. **The flexure mode, as in this bimorph configuration, is used where larger deflections and smaller forces are involved than are possible with rings or discs.**

For spark generation, therefore, use the following equations:

$$V_3 = -g_{33}T_3L_3,$$

(3)

where

- $V_3 = \text{voltage developed (V)}$,
- $g_{33} = \text{piezoelectric voltage constant (Vm/N)}$,
- $T_3 = \text{mechanical stress (N/m}^2\text{)}$,
- $L_3 = \text{length along E axis (m)}$.

The electrical energy density, $W$, available for the spark is given by

$$W = \frac{1}{2} \varepsilon_{33} g_{33} T_3^2,$$

(4)

where $\varepsilon_{33}$ is the permittivity (dielectric constant = $\varepsilon_{33}/8.85 \times 10^{-12}$ F/m) of the unstressed ceramic. The energy density, $J/m^3$, is the energy available per unit volume of ceramic and includes the additional electromechanical energy released when the spark gap becomes conductive and discharges the electric field.

When an applied mechanical-stress pulse is measured in microseconds, apply the linear stress equations
Eqs. 3 and 4. For long pulse durations—a squeezing action rather than an impact—complicated nonlinear effects must be taken into account. And though offering some advantages of higher output, such quasistatic loading requires materials with high resistance to mechanical depolarization.

But no matter how the stress is applied, choose a material with both a high $g_{33}$ and high $\varepsilon_{33}$, and able to withstand high stress levels ($T_3$) without mechanical depolarization.

A material at first might appear suitable because it has a high $g_{33}$; however, because of a low $\varepsilon_{33}$, the available electrical energy per unit volume of ceramic for a given stress could end up low.

If the safe dynamic stress for a particular ceramic (PXE-21) is $50 \times 10^6$ N/m$^2$, $g_{33}$ is $25 \times 10^{-3}$ Vm/N and the unstressed relative permittivity is 1750, the following maximum voltage and energy values can be attained:

$$V_3 (\text{max}) = 1.25 \times 10^6 \text{ V/m of ceramic length},$$
$$W (\text{max}) = 12.1 \text{ kJ/m}^3.$$

Clearly, PXE-21 is recommended for impact mechanisms. For example, a cylinder of the material 6.35 mm (0.25 in.) in diameter and 16 mm (0.630-in.) long yields an open-circuit output voltage of 20 kV.

You can solve Eq. 3 with Nomogram 1. Output voltage, $V_3$, is determined in two steps. Draw a line between the material's $g_{33}$ value and the applied stress, $T_3$. The intersection of this line with the $g_{33}T_3$ scale is a transfer point, or intermediate solution. Connect the transfer point with the desired voltage to determine the length, $L_3$, of material needed.

Since $W$ is proportional to $(g_{33}T_3)^2$, for maximum energy density, the intermediate solution should be as close to the top of the scale as is consistent with the material's $g_{33}$ and stress limits.

Small movements easily performed

For small-displacement actuator devices, Nomogram 2 solves Eq. 2 for the "33" mode. Applications built with a stack of ceramic discs or rings include actuators for fuel metering and the positioning of optical components.

Consider a material with $d_{33}$ of $384 \times 10^{-12}$ m/V (PXE-5), which is readily available in many standard shapes and sizes. If the application requires a displacement ($\Delta L_3$) of +20 $\mu$m, draw a line on the nomogram between $d_{33}$ and the 20-$\mu$m displacement. The line intersects the voltage scale ($V_3$) at 53 kV. Choose a field strength, $E_3$, for the material—about 900 V/mm—and connect this value with $V_3$ to determine the total length of the ceramic element—about 60 mm.

Note that since the electric field is applied in the same direction as the polarization, a field as great as 2500 V/mm may be applied before encountering dielectric breakdown problems in the ceramic. How-

3. A multimorph flexure configuration, for piezo ceramics (a), is simpler to fabricate than a bimorph. Such a piezo element can be used to build a snap-action switch, when bonded to a cantilevered spring of special design (b). The spring's snap action provides a step-voltage output (c) and also a tactile feel.
ever, since you must take care to prevent flashover along the ceramic's exposed surface areas, the applicable field is limited to approximately 900 V/mm. For an applied field opposite the poled direction, the maximum field is about 450 V/mm for PXE-5 to prevent depolarization.

The thickness of the individual ceramic discs can now be determined, depending upon the available voltage supply. Draw a line between $E_3$ and the voltage supply, or voltage level per disc, to obtain the disc thickness "t." For a 400-V supply, a stack of 130 elements, each 0.45-mm thick and operating at 400 V, will provide a 20-µm displacement.

A second example (solid lines) on Nomogram 2 shows the solution for a displacement of ±10 µm. However, note that since the supply voltage now opposes the polarization for negative displacements, the field is kept at 450 V/mm (for PXE-5). Consequently, the ±10-µm displacement can be obtained from a power supply of ±400 V with a stack of 65 elements, each 0.9-mm thick.

**Piezo ceramics can be bent**

For applications such as high-voltage generation you use high impact forces on ceramic discs or rings, which in compression or tension have high elastic stiffness. Conversely, such stiff structures can supply large forces for small displacements when high voltages are applied. However, for small forces and large displacements flexure elements must be used.

The simplest flexure element—a bimorph (Fig. 2)—consists of two thin strips of piezo-ceramic material bonded together, each strip operating in the "31" mode. With the two strips poled in opposite directions, one portion expands and the other contracts when a voltage is applied. The cantilevered structure bends to produce a relatively large displacement.

A similar structure—a multimorph (Fig. 3a)—is made of one monolithic ceramic element. Holes through the ceramic's center are silvered and serve only to pole the element. Silvered electrodes on the top and bottom surfaces enable the upper and lower portions to be polarized in opposite directions. The electrodes on the top and bottom surfaces then become the input or output ports.

Although performance may be slightly less than with an equivalent bimorph, the unit is much simpler to produce, and the problem of establishing a good, rigid bond between layers is eliminated.

Typical applications that employ flexure elements include sound-generation devices and microphones; small vibratory motors and fine-movement actuators; instrument transducers such as accelerometers, stress and strain gauges, and liquid-level sensors; and circuit components such as switches.

Because of low elastic stiffness, flexure elements can have very low resonant frequencies. Elements 80-mm long can resonate as low as 60 Hz. But how they are mounted, and how rigidly, strongly affect the resonance frequency and output of flexure elements.

To aid in designing for "motor" applications, Nomogram 3 provides output force (N/V) or output deflections (mm/V) as a function of the mounting method and the active length (L) of the element. As illustrated by the example sketched on the nomogram,
for an active length of 50 mm with a cantilevered configuration, you can obtain a deflection of $1.8 \times 10^{-3}$ mm/V. With a supply voltage of 20 V applied to the outer electrodes a deflection of 0.04 mm (0.0015 in.) can be obtained. Higher drive levels can produce larger displacements, and nonlinear effects tend to increase the displacement.

However, an ends-pinned configuration reduces the deflection to $0.45 \times 10^{-3}$ mm/V: For maximum deflection, therefore, with no applied force, the cantilevered approach is more desirable. On the other hand, for a force output the ends-pinned configuration is better—about $4 \times 10^{-4}$ N/V vs $1 \times 10^{-4}$ N/V for the cantilever.

For generator applications, work with Nomograms 4 and 5. Use Nomogram 4 for force inputs. For example, the open circuit output of a 50-mm multimorph operating as a cantilever is 710 V/N. With an upper safe limit of 0.034 N, an open-circuit output voltage of 24 V can be obtained.

For larger forces, the ends-pinned configuration offers mechanical advantages. Although the specific output drops to 180 V/N, the maximum allowed force is a much higher 0.13 N, so the maximum output voltage force is still approximately 24 V.

Use Nomogram 5 for deflection-input designs. The procedure is similar to that of Nomogram 4.

Note that the actual output voltage available from a piezo element depends on the capacitance of the piezo-ceramic material, $C_t$, and the shunt capacitance of any associated circuitry, $C_s$:

\[ V = \frac{q}{C_t + C_s}, \]  

where "q" is the charge output per unit of input (force or deflection). The parameters for Eq. 5 and their application are explained on Nomograms 4 and 5.

**Piezo ceramics function as switches**

The flexure mode can be applied to designing keyboard switches. A piezoelectric keyboard switch can eliminate the problems of contact resistance and bounce-in conventional contact switches, while provid-
The tactile feedback not usually found in capacitor-type switches.

Designed properly, a piezoelectric switch can generate a substantial voltage, about 5 V, which is compatible with high-impedance circuitry. The switch consists of a piezoelectric element bonded to a monostable spring. An extruded ceramic multimorph element (Fig. 3a), when flexed, operates in a "31" mode, with longitudinal tensile strain on the upper and compressive strain on the lower section. Voltage appears between upper and lower silver electrodes.

References
The choice of a protective device for any application involves voltage, current, trip time delay, and short circuit ratings. Such mechanical variables as number of poles, termination, mounting, size, and type of actuation are also involved. Before final selection is made, however, be sure to consider applicable U.L., C.S.A., and military requirements. Chances are that Airpax has the magnetic breaker you need...qualified, recognized, or listed for your specific requirements.

Other Advantages. Airpax magnetic circuit breakers have accurate trip currents. They are not sensitive to ambient temperatures, can be used as ON-OFF switches, and come in single or multipole packages. Some even have a pilot light in the handle and snap-in mounting.

Full Details Available. For further information on the full line of Airpax circuit breakers, plus U.L., C.S.A., and military listings, request Short Form Catalog 2013 from your local Airpax representative, or contact Airpax Electronics, Cambridge Division, Cambridge, Maryland 21613. Phone (301) 228-4600. Telex: 8-7715. TWX: (710) 865-9655. Other factories in Europe and Japan. European Sales Headquarters: Airpax S.A.R.L., 3 Rue de la Haise, 78370 Plaisir, France.
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Set up system models

Three subsystem models—Series, Parallel and Any-R-of-N configuration—have been programmed for a scientific pocket calculator (see Table 1). To use the models, you need to know the mean time between failure (MTBF) and mean time to repair (MTTR) for each system component. You can either rely on figures vendors supply or, if you have access to trouble reports for the components, you can easily compute MTBF and MTTR parameters. For MTBF, multiply the operating time period in hours by the number of units sampled, then divide this product by the total number of failures. To obtain MTTR, average the "out-of-service" times.

By applying the models, you can predict MTBF and MTTR for the total configuration, as well as for every underlying subsystem. Not only that, you can also determine availability, reliability and failure probability from MTBF and MTTR.

Availability, A, is defined as the probability of finding the subsystem working at any arbitrary future time. Reliability, R(t), is the probability of completely successful operation in time period, t. The probability of n failures occurring in t is designated P(n).

To generate a model, convert the hardware configuration into a reliability "bubble" diagram, which shows how individual elements affect a subsystem’s over-all reliability. The bubble diagram is a network of connected circles, showing MTBF and MTTR figures within the bubbles. In Table 1, Example 1, a single element has an MTBF of 500 hours and an MTTR of 3 hours. To assemble single elements into first-level subsystems, use the three types of models: Series, Parallel and Any R of N.

In a Series connection, should any one element fail, the whole subsystem will cease to function. In a Parallel connection, the entire subsystem is considered operational if any one of the elements is working. However, an Any R-of-N connection is more versatile than the Series or Parallel configurations. In an N-element arrangement, the subsystem functions as long as R or more of its elements work.

When R=1, the Any-R-of-N connection is equivalent to a Parallel connection. Only one shunted element is required to maintain an operational subsystem. In Example 8, R=1 and the results approximate those for the Parallel connection in Example 7. When R=N, "Any" and Series correspond. Example 4 produces the same results as the Series connection in Example 3. A unique example of the "Any" arrangement, where R=2 and N=3, which can’t be duplicated by either the Series or Parallel models, is illustrated by Example 9.

Proceeding in this manner, you join primary elements into first-level subsystems. Then, repeat this process, assembling these first-level subsystems in turn to form higher-level subsystems, until the reliability diagram comprises the total system. Continue the same Series, Parallel, and Any R-of-N reduction strategy through each phase of the system.

Realistic assumptions are needed

To derive equations you can solve, several realistic assumptions, which apply to most encountered systems, must be made for the three models:

1. Equipment is either up (operational) or down (failed)—No in-between condition is allowed. When any module malfunctions, repair or replace it.
2. The state of one unit is unaffected by the states of its adjacent elements.
3. Redundant elements can be switched into place as a failure occurs, before the over-all system is considered to have failed.
4. Exponential service times are assumed, as is standard in the derivation of many analytical models.

In this last case, the probability of MTBF and MTTR time periods is assumed to follow a negative exponential distribution. In other words, the number of failures and repairs occurring in a unit time obeys the Poisson distribution; therefore, the variance is equal to the mean.

Assume widely fluctuating failure and repair times, with variance commensurate with MTBF and MTTR.
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<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

These distributions help in the formula derivations because of their inherent memoryless property, since at any instant, the remaining time to failure or repair is independent of what has preceded.

To estimate total system dependability, apply the models repeatedly to primary elements, first-level subsystems, second-level subsystems, and soon. Repair and failure rates of all elements and subsystems are presumed to have Poisson distributions. But don't go overboard. Although this is a fairly good estimate, it is not always precisely the case, especially for high-level subsystems containing low levels of redundancy.

While your calculator might be accurate to 12 places, your assumptions and input data are probably not as accurate. Therefore, don't carry MTBF and MTTR figures to more than a few decimal places. Round them off.

Also, of course, while you rely on the three subsystem models, don't get carried away. Applying them demands thought and proficiency, and the resulting predictions require proper interpretation.

Equations for three models

The formulas for computing total system dependability can be solved on any scientific pocket calculator. But solving them on the SR52, or another programmable type, not only enables you to complete the analysis much faster, but also reduces the risk of error. If you use an SR52, the following material will serve as a background, since you need only to follow the “User Instructions” detailed in this article. For other programmable calculators, you have to recode the equations. Those with manual calculators will have to grind through the formulas step-by-step.

Consider the Series model first. The inverse of total MTBF is the summation of the inverses of unit MTBFs:
Table 3. SR52 user instructions

<table>
<thead>
<tr>
<th>STEP</th>
<th>PROCEDURE</th>
<th>ENTER</th>
<th>PRESS</th>
<th>DISPLAY</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.0</td>
<td>Series Connection</td>
<td>START 1.</td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.1</td>
<td>Enter MTBF &amp; MTTR for each series element</td>
<td></td>
<td>MTBF</td>
<td>MTBFs Cumulative MTBF</td>
</tr>
<tr>
<td>1.2</td>
<td>Repeat steps 1.1 &amp; 1.2 for each series element</td>
<td></td>
<td>MTTR</td>
<td>MTTRs Cumulative MTTR</td>
</tr>
<tr>
<td></td>
<td>Cumulative result is displayed after each entry. After each element is added, you may interrupt the loop to compute the following:</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1.3</td>
<td>Availability</td>
<td>A</td>
<td>Availability</td>
<td></td>
</tr>
<tr>
<td>1.4</td>
<td>Reliability</td>
<td>t</td>
<td>R(t)</td>
<td>Reliability</td>
</tr>
<tr>
<td>1.5</td>
<td>Probability of n failures</td>
<td>n</td>
<td>P(n)</td>
<td>Probability of n failures</td>
</tr>
</tbody>
</table>

2.0 Series Connection

<table>
<thead>
<tr>
<th>STEP</th>
<th>PROCEDURE</th>
<th>ENTER</th>
<th>PRESS</th>
<th>DISPLAY</th>
</tr>
</thead>
<tbody>
<tr>
<td>2.1</td>
<td>Enter MTBF for each series element</td>
<td></td>
<td>MTBF</td>
<td>MTBFs Cumulative MTBF</td>
</tr>
<tr>
<td>2.2</td>
<td>Step 2.2 must precede the first use of P(n)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>2.3</td>
<td>Availability</td>
<td>A</td>
<td>Availability</td>
<td></td>
</tr>
<tr>
<td>2.4</td>
<td>Reliability</td>
<td>t</td>
<td>R(t)</td>
<td>Reliability</td>
</tr>
<tr>
<td>2.5</td>
<td>Probability of n failures</td>
<td>n</td>
<td>P(n)</td>
<td>Probability of n failures</td>
</tr>
</tbody>
</table>

3.0 Parallel Connection

<table>
<thead>
<tr>
<th>STEP</th>
<th>PROCEDURE</th>
<th>ENTER</th>
<th>PRESS</th>
<th>DISPLAY</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.1</td>
<td>Enter MTBF &amp; MTTR for each parallel element</td>
<td></td>
<td>MTBF</td>
<td>MTBFp Cumulative MTBF</td>
</tr>
<tr>
<td>3.2</td>
<td>Repeat steps 3.1 &amp; 3.2 for each parallel element</td>
<td></td>
<td>MTTR</td>
<td>MTTRp Cumulative MTTR</td>
</tr>
<tr>
<td></td>
<td>Cumulative results are displayed after each entry. After each element is added, you may interrupt the loop to compute the following:</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>3.3</td>
<td>Availability</td>
<td>A</td>
<td>Availability</td>
<td></td>
</tr>
<tr>
<td>3.4</td>
<td>Reliability</td>
<td>t</td>
<td>R(t)</td>
<td>Reliability</td>
</tr>
<tr>
<td>3.5</td>
<td>Probability of n failures occurring in time period t</td>
<td>n</td>
<td>P(n)</td>
<td>Probability of n failures</td>
</tr>
</tbody>
</table>

4.0 ANY R-of-N Connection

<table>
<thead>
<tr>
<th>STEP</th>
<th>PROCEDURE</th>
<th>ENTER</th>
<th>PRESS</th>
<th>DISPLAY</th>
</tr>
</thead>
<tbody>
<tr>
<td>4.1</td>
<td>R elements required</td>
<td>R</td>
<td>ANY</td>
<td></td>
</tr>
<tr>
<td>4.2</td>
<td>N elements available</td>
<td>N</td>
<td>RUN</td>
<td></td>
</tr>
<tr>
<td>4.3</td>
<td>Assume all elements identical. Enter MTTR &amp; MTBF only once.</td>
<td></td>
<td>MTTR</td>
<td>RUN Cumulative MTTR</td>
</tr>
<tr>
<td>4.4</td>
<td></td>
<td>MTBF</td>
<td>RUN Cumulative MTBF</td>
<td></td>
</tr>
<tr>
<td>4.5</td>
<td>Availability</td>
<td>A</td>
<td>Availability</td>
<td></td>
</tr>
<tr>
<td>4.6</td>
<td>Reliability</td>
<td>t</td>
<td>R(t)</td>
<td>Reliability</td>
</tr>
<tr>
<td>4.7</td>
<td>Step 4.6 must precede the first use of P(n)</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Therefore,

\[
\frac{1}{MTBF_T} = \sum_{i=1}^{N} \frac{1}{MTBF_i}, \text{ for } N \text{ units.}
\]

Therefore,

\[
MTBF_T = \frac{1}{\sum_{i=1}^{N} \frac{1}{MTBF_i}}.
\]

Multiplying unit availabilities results in total availability:

\[
A_T = \prod_{i=1}^{N} A_i.
\]

And once MTBF and A are determined, total MTTR can be found from

\[
MTTR_T = \left( \frac{1 - A_T}{A_T} \right) MTBF_T.
\]

For a Parallel connection, adding the inverses of MTTR for each unit results in the inverse of total MTTR:

\[
\frac{1}{MTTR_T} = \sum_{i=1}^{N} \frac{1}{MTTR_i}, \text{ for } N \text{ units.}
\]

Unavailability (U) is 1 - A. Parallel total unavailability is the product of unit unavailabilities:

\[
U_T = \prod_{i=1}^{N} U_i
\]

\[
(1 - A_T) = \prod_{i=1}^{N} (1 - A_i)
\]

\[
A_T = 1 - \prod_{i=1}^{N} (1 - A_i)
\]

Once you know MTTR and A, you can compute total MTBF:

\[
MTBF_T = \left( \frac{A_T}{1 - A_T} \right) MTTR_T.
\]

For an Any R-of-N configuration, the entire connection is operational provided R units of the N available
are working. Assume all units have identical MTBF and MTTR values, which are indicated with the subscript \( i \). Use the following formulas to calculate total MTBF and MTTR:

\[
MTTR_T = \frac{MTTR_i}{N - R + 1}
\]

\[
MTBF_T = MTBF_i \left( \frac{MTBF_i}{MTTR_i} \right)^{N-R} \left[ \frac{(N-R)!}{(N-1)!} \right]
\]

These two equations are derived with the assumption that \( MTTR_i \) is much smaller than \( MTBF_i \), as is generally the case. Once \( MTTR_T \) and \( MTBF_T \) have been computed, solve for total availability:

\[
A_T = \frac{MTBF_T}{MTBF_T + MTTR_T}
\]

The equations for reliability and failure probabilities—\( R(t) \) and \( P(n) \)—are the same for all three models. For reliability during \( t \),

\[
R(t) = e^{-t/MTBF_T}
\]

For the probability of \( n \) failures in a time period \( t \),

\[
P(n) = e^{-N} \frac{N^n}{n!}
\]

where

\[
N = \frac{t}{MTBF_T}
\]

represents the average number of failures during time period \( t \).

To appreciate the effects various configurations have on dependability parameters, examine the reliability bubble diagrams and results for a set of 12 illustrative examples tabularized in Table 1. The period during which reliability and failure probabilities were calculated was arbitrarily selected as one year of continuous operation (365 days \( \times \) 24 hours/day = 8760 hours).

Both examples 1 and 2 may be thought of as either Series or Parallel configurations, consisting of only one element. In both cases, availability exceeds 99%. On the average, these elements will be up (available) more than 99 hours out of every 100 operating hours. However, this is not always a good indicator of dependability. The reliability and failure probabilities in Example 1 are almost zero—i.e., this element is certain to have more than two failures per year.

The element in the second example is much more dependable. It has a 37.78% probability of zero failure, a 36.77% probability of one failure, and a 17.90% probability of two failures per year. Failure probabilities higher than two can also be determined, by entering \( n \), then depressing the key labeled \( P(n) \).

Units are strung together in Examples 3, 4, and 5. Where as the Series model may always be applied to such string connections, Any \( N \) of \( N \) can only be used when all components are identical. Series dependability is always less than for the weakest link in the chain. Observe that the resulting dependability parameters in Example 5 are all less than their respective counterparts in Example 1.

Paralleled elements are represented in Examples 6, 7, 8, and 10. If they aren't all identical, you must use the Parallel model. When they are, either the Parallel or Any 1-of-\( N \) models apply. The dependability of a network of parallel elements is always greater than any one of them.

The resulting \( MTBF_T \) in Example 6 is 4.8 years. In Example 7, it is 538 years. Yet, in both illustrations, the primary elements have an MTBF of only 500 hours.

Examples 9 and 11 have been computed with the Any R-of-\( N \) model. Compare Example 9 with Example 8 and note the decreased dependability. This occurs in Example 9 because two elements are required to be operational instead of only one. The network in Example 11 is a second-level subsystem configured with the first-level subsystems of Example 5.

The reliability diagram in Example 12 is a third-level subsystem. As an exercise, you should redraw it with 17 primary elements.

Occasionally, you will encounter a configuration that cannot be accurately represented by any of the models. Consider an Any Two Required of Three Available condition, where all three elements are different. When such situations occur, the models can always be applied to determine upper and lower bounds on dependability. One assumption will be optimistic, the other, pessimistic. Carrying both limits through the remaining calculations establishes two sets of results. The system's actual dependability lies somewhere between these values.

To code the SR52 calculator, see Table 2. With this coding procedure, you can obtain a program card that, when inserted into the calculator, prepares it to perform the computations described in Table 3.

Ten user-defined functions can be executed by pressing the top row of keys on the SR52 calculator. A great deal of thought has gone into their assignment to provide for maximum user convenience. In this article user function keys are named and referenced as follows:

<table>
<thead>
<tr>
<th>Key</th>
<th>Name</th>
<th>Key</th>
<th>Name</th>
</tr>
</thead>
<tbody>
<tr>
<td>A</td>
<td>MTBF</td>
<td>A'</td>
<td>START</td>
</tr>
<tr>
<td>B</td>
<td>MTTR</td>
<td>B'</td>
<td>-</td>
</tr>
<tr>
<td>C</td>
<td>MTTR</td>
<td>C'</td>
<td>A</td>
</tr>
<tr>
<td>D</td>
<td>MTBF</td>
<td>D'</td>
<td>R(t)</td>
</tr>
<tr>
<td>E</td>
<td>ANY</td>
<td>E'</td>
<td>P(n)</td>
</tr>
</tbody>
</table>

Program the TI-58 or TI-59 calculators with the keystroke modifications listed in Table 4. ...
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To screen out "infant mortality", the diodes are deliberately stressed to accelerate aging and to force time-related failure modes to take their toll. In conventional testing or "baking", the diode does not experience anywhere near the stress encountered with the HTRB program. Hence, the ability at Mini-Circuits' to locate the potentially-unreliable diodes before they are assembled into SRA-1 units is now possible. And, with double-balanced mixers, the overall reliability hinges almost entirely on the diodes used.

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---

**MODEL SRA-1**
---

<table>
<thead>
<tr>
<th>Freq. range (MHz)</th>
<th>LO · RF</th>
<th>Conversion loss (dB)</th>
<th>Typ.</th>
<th>Max.</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>LO · RF</td>
<td>one octave from band edge</td>
<td>5.5</td>
<td>7.0</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Total range</td>
<td>6.5</td>
<td>8.5</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Isolation (dB)</td>
<td>Typ.</td>
<td>Min.</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>one decade higher</td>
<td>45</td>
<td>35</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Mid range</td>
<td>45</td>
<td>30</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Upper band edge</td>
<td>35</td>
<td>25</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>one octave lower</td>
<td>35</td>
<td>25</td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Min. Electronic attenuation (20 mA)</td>
<td>3 dB</td>
<td></td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Signal, 1 dB compression level</td>
<td>+1 dBm</td>
<td></td>
</tr>
<tr>
<td></td>
<td>LO · RF</td>
<td>Impedance all ports</td>
<td>50 ohms</td>
<td></td>
</tr>
</tbody>
</table>

---

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Fred Bucy of TI Speaks on
Managing Innovation

Like motherhood and apple pie, innovation is something everybody favors. What most people don’t know is that you can actually plan and organize for it.

But no system ever created an innovation. People make innovations. So you have to create an environment in which people will be stimulated to innovate. And that environment must pervade your company because innovators are where you find them. Your R&D organization is not the sole source.

To stimulate innovation, you need a system. But you mustn’t let it become too rigid or you’ll discourage innovation instead of encouraging it.

The system we use at TI is one we call OST—for Objectives, Strategies and Tactics. It’s designed to help us nurture and manage innovation.

It starts with the idea that innovation or invention is a very tender thing. You have to bring it up very carefully. It can starve if it isn’t quickly nourished. And innovations perish without champions.

So we make initial resources available quickly and easily. Being able to allocate resources properly is the real key to the system. When a fellow comes up with a new idea, a new product, or a new solution to something, we can get the resources to him. Nothing is more discouraging than having a good idea and not being able to get the funding for it. The best way to
motivate innovators is to provide resources to help them carry out their ideas. This is far more important than it appears. You must have a source of "strategic" funding—money that's discretionary to your current operations. Such funds must be kept separate from day-to-day business requirements.

If you leave this allocation to individual managers, you force them into conflicts between today's profitability and tomorrow's growth. For the same reason, you must segregate the reporting of strategic and operating expenses so that you don't unwittingly penalize managers who carry out strategic programs. Unlike operating expense, strategic expense is desirable in business.

Further, you have to be wary of the old problem that resources do tend to gravitate away from embryonic ideas toward well developed products. We have two basic ways to provide funds for innovations—the IDEA program and the Wild Hare program.

Under the IDEA program, we distribute modest sums of money to a large number of IDEA program representatives throughout the company.

When an engineer says, "I have an idea for doing such-and-such, and I think I can prove its feasibility in six months," he merely has to convince the IDEA man, who has authority to provide funding right away, without further approval.

The engineer will have a timetable in which to prove that he's making progress. At some point he may need an extension. And at some point he may develop his idea to the point where it enters into competition with other ideas for further funding.

In many cases the engineer who develops the original idea may continue in his own job while he's developing the idea. He may tell his boss that he has the funding to carry out a new idea and he needs some time to work on it. They'll work out a way to give him the time to work on the idea.

To help him develop his idea and for many other reasons, we challenge an ancient management principle. We believe that a man's responsibility can and should exceed his authority.

I know that many management texts take it as gospel that if you give a man responsibility, you must give him authority to go with it. Of course, that's frequently true. You can't give a man responsibility for running a production line or a lab without giving him authority over that line or lab.

But we believe deeply that if a man sees an opportunity to be pursued outside his immediate area, he has the responsibility to do something about it. Maybe he should bring it to the attention of his peers, his boss, or a committee. He should not sit back and say, "That's not my job; I'm not responsible." The same rule applies in corporate or civic ethics. If you see something wrong, you are obligated to do something about it, even if it's not in your area, and even if you don't have the authority.

So, if a man is given responsibility for developing a new idea, he may have to call on resources in other departments—where he has no authority. He may be asking for the services of people who "outrank" him . . . but I should add that rank doesn't play much of a role at TI.

We may have a situation where, so to speak, a sergeant needs services from a captain. Well, with our OST system we give him the funds to buy those services. He can say, "I need this and I have the money to pay for it." And that happens frequently.

Sometimes a man's idea is such that he can't pursue it while he's working at his regular job. He may need full time to develop the idea. In this case he obviously must be relieved of his regular duties. And this raises another question.

The normal boss wants to keep his productive people because they make him look good. He's reluctant to lose an innovative man—even for a relatively short time. He needs an inducement to support the innovator even if he'll move to a new effort.

Most of the time this isn't a problem because the innovator is in his own group and it's most likely that the idea will be in his own area of interest. So there's real incentive. He has a great deal to gain from supporting the fresh idea, as it might help him gain additional resources to make his business a success.
But if the engineer comes up with an idea that's not related to the boss's current business, the engineer may be transferred, perhaps temporarily, to, say, the Corporate Engineering Center. In the Corporate Development organization, he may work on products related to any of TI's businesses or to new businesses. If his idea proves successful, he may move with it as it goes into further development and into production. In such a case, the original boss should get the satisfaction of knowing that one of his people played an important role in helping the company grow.

In our Wild Hare system, we're looking for ideas that are more nebulous. We're working long shots. We're trying for a "hole in one."

One example is our development of charge-coupled devices. We did not invent them, but we did recognize their potential and funded them with an expectation of a payoff in several years—not immediately.

It's very difficult to set checkpoints when you're trying to get innovation. You can't command invention. So we can't have rigorous milestone reviews in our Wild Hare program. We have to give people the latitude to pursue something over an extended period.

In our Wild Hare program we may be making large investments, but they'll be spread over a long period of time. Since these are important programs, possibly with long-range impact, we don't fund them as quickly as we do the IDEA programs.

Now, as you can imagine, when thousands of people in a corporation are encouraged to innovate, we must often face the problem of deciding what business we're really in, especially when we examine some of the Wild Hare proposals. And that's precisely one of the functions of the OST system.

It turns out that we usually don't have to worry about that problem since most of the fellows working here are not likely to come up with an invention in, say, biology. But every once in a while somebody comes up with an idea that makes us evaluate the merits of entering a new business.

A new business can sometimes be an outstanding payoff of the OST system which, remember, is first and foremost a philosophy. It's a philosophy that keeps pointing to the fact that we are in the business of innovation. The philosophy is a foundation on which we build a structure to nurture innovation.

There are two critical aspects to this philosophy. First, we try to make the status quo uncomfortable. And second, we don't punish innovators for unsuccessful programs. That's very, very important.

We always stress the probability of success. IDEA projects may have one chance in, say, 20 or 25. Wild Hare projects may have even lower probabilities for success. If a program has a 50-50 chance, it will probably be supported by general OST strategic funds.

As you can imagine, the system isn't flawless. One of the problems we run into is the fact that bright innovators tend to be promoted to the ranks of management, and then get buried in administrative details. Of course we reward innovators with money and prestige. But there seems to be greater social prestige for the manager.

It's often difficult to get the innovator to realize that his biggest contribution is to remain the creative genius, rather than to get into the management progression. That idea can be frustrating to the genius because he thinks he has to carry everything all the way through.

Who is Fred Bucy?

He's very much a Texan. J. Fred Bucy, whose parents, grandparents, and great-grandparents were Texans, was born in the High Plains of Texas, in Tahoka, just south of Lubbock. His wife, Odetta, is from Grassland, a suburb of Tahoka.

He went to school in Texas, earning his BS in Physics in 1951 at Texas Tech University in Lubbock and his MS Physics, two years later when he was 25, at the University of Texas in Austin.

Then, of course, he came to work in the Central Research Lab of Texas Instruments, starting in geophysical instrumentation. He left the lab to carry one of his ideas through production at TI's plant in Houston. His responsibilities increased and in 1961 he was made general manager of the Houston operation. In 1963 he was made vice-president and put in charge of TI's military business. He continued his rise and, in 1967, he was given charge of the company's semiconductor activities; in 1972 he was made executive vice-president; then chief operating officer in 1974 and president in 1976.

Bucy is a hard worker. In his spare time he works. But he enjoys working. He started working 18 hours a day when he was 13 and he still does. But it does take work and time to manage a company that wants to keep growing from its 1976 sales peak of almost $1.7 billion. Bucy would be happier if there were more hours in the day and more days in the week.

He does unwind aboard his double-ended, gaff-rigged ketch, the "Tumbleweed." But he takes his briefcase with him. His pleasure in the boat is largely vicarious because his family is more often there without him than with him. The usual occupants include his 27-year-old son, J. Fred, III, the boat's captain when he's not operating his own business (The Car Doctor ... "I make house calls"), his wife, and his two daughters, Roxanne, 24, and Diane, 21.

Bucy does find time for other activities. He is particularly active working through the Defense Science Board on the question of export of technology. And he serves as a Regent of Texas Tech. He also spends much of his spare time reading—all kinds of things, with emphasis on political science and history, biography and autobiography, lots of technical material and some fiction.
The fellow who can generate a new idea, convert it to a product, push it through production and get it into the field—that fellow is pretty scarce. But nobody likes to give his baby away. So you have to protect the creative guy by rewarding him sufficiently so that he remains motivated to stay in his position.

The genius who comes up with the basic concept is probably not the individual who can get a product through a production line. Sometimes we let an innovator find out for himself. Then we can get him to return to what he really loves and does best.

Of course, you have to make sure that the innovator's salary, bonuses and recognition will be an adequate reward. In fact, we have what we call the TI Fellow Awards for the truly outstanding innovators. We present these at our Strategic Planning Conferences and publish them throughout the company. So our innovators do get recognition from their peers. The innovator can become a Fellow instead of a vice-president. And this is one way we cope with the fact that his neighbors don't know if he has made important innovative contributions to the corporation, but they sure know if he's a vice-president. It doesn't seem to be enough that he may make as much money as a vice-president. There's great social value in the fact that a business card says he's a vice-president.

Unfortunately, vice-presidents tend to become buried in administrative work. The OST system is dedicated in large measure to making the manager spend a lot of time thinking about the nature of our business and how to improve it instead of spending all his time on current administrative duties. We try to get all our managers to spend a significant part of their time thinking about innovation and strategic planning because that's what we're all about.

We have a "two-hat" system for our managers. A manager must be a short-term operating manager and he must develop long-term strategic skills. He should develop the self-discipline needed to divide his time wisely between today's demands and tomorrow's needs. He must not let himself be consumed by today's business requirements.

**The manager has to keep thinking about the future—about new products, new management techniques, new everything.**

Without new products, we cease to grow. Without innovation in management, our overhead continues to grow. So we always worry about how to become more productive in everything we do.

You have to realize that the OST philosophy doesn't apply only to engineering. It might involve a new product, a new process, a new marketing technique, even—and especially—a new management technique. Productivity is the key.

Here's the best example: Between 1970 and 1976 we doubled our billings with an increase of only 16% in people. We didn't do that just by making everybody work hard. It was done by people thinking about their jobs and being innovative in what they're doing. Being more productive is getting more out with less effort. And that's part of the OST system.

We have a very simple measure of this productivity. It's called the People Effectiveness Index, which is simply our billings divided by total payroll. We try to make that improve every year.

Of course, no system is perfect. It's easy to fall into the trap of thinking that a system exists independent of people. And it's easy to let the system cover too much. That can lead to a heavy paperwork burden. Or the system can become too mechanistic, giving people the feeling that the system controls events. You must continue to refine and improve any system.

OST really started in the early days of our company. When we had a sales volume of substantially less than $200 million, it was possible for the president and the vice-presidents to get together and operate the OST system among themselves. They could follow what was important and get things started.

One of the early Wild Hares—long before we invented that name—was the silicon transistor. When we introduced that in 1954 we were enjoying a volume of somewhat over $24 million.

Pat Haggerty, who was then chairman of the board, sold the board on the idea of developing the silicon transistor. We could do things very informally at that time because lines of communication were short.

But Mr. Haggerty and others like him recognized the fact that, as we got bigger, we would need a system to help us see where the new opportunities were and to allocate the proper resources to help us take advantage of them.

He wanted to institutionalize what was already being done informally. "How are we going to handle this," he asked, "when we get to be a half-billion-dollar corporation, or a billion dollar corporation?"

We started formalizing the system in the early 1960s and we've been developing it ever since. Though it's now in an advanced state, we still come up with improvements.

If we didn't do that, the system would stagnate and die. What worked well with one size corporation may not work well at another level. To be useful, OST must be a living thing, a way of life, a philosophy that's ingrained in all your people. You can't just say, "Today is OST day."

OST is not merely a way to fund new ideas—though that's an important role. It can be, and often is, a meeting on a production line, where a group of people get together and talk about how to improve an operation. We do get inputs right from the people working directly on the line.

One of the best examples of ideas from the production floor I heard recently during a visit to Italy, when a girl from the production floor came out with a better layout of the product line she worked on.

Our effectiveness depends very much on our innovative skill. We want to use every technique to improve that skill. That's our life blood.
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As for accuracy, the AD561 is guaranteed to $\pm1/2$ LSB max of 10-bits (or even $\pm1/4$ LSB — and that’s 11-bits). Monotonicity is guaranteed over the full operating temperature range. The excellent stability is made possible by a unique buried zener voltage reference and Analog Devices’ proprietary thin film resistor process. And for settling time, there’s nothing faster: less than 250ns for the worse case transition; that’s fast enough to build a 5 µsec ADC. Current-to-voltage conversion with an op amp is direct and simple: trimmed application resistors mean no calibration trimmers are needed.

How did we achieve this breakthrough? With the industry’s most advanced monolithic processing and our pioneering technique of laser wafer trimming. The kind of advances that have quickly pushed us to the top and made us the leading supplier of D/A and A/D converter components.

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CIRCLE NUMBER 51
Four ways to do 8x8 Multiplication

<table>
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<tr>
<th>Device</th>
<th>MMI 67558</th>
<th>TRW MPY-8</th>
<th>AMD 25S05 (FD 93S43)</th>
<th>TI (MSI) 74S274/5</th>
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<td>115</td>
<td>210</td>
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*300 fpm cooling required.

For more information, phone, TWX or write.

Monolithic Memories

CIRCLE NUMBER 52

(Second sourcing from ITT Semiconductor.)
An automatic RLC tester for $1085? you’ve got to be kidding!

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**Microprocessor-directed ranging** takes the guesswork out of setting the correct range. Lighted arrows on the front panel indicate which range button is to be depressed and the correct range is identified automatically.

**Three range positions** provide measurements in multiples of 100, since each range has two full decades of measurement capability, a feature made possible by automatic decimal point positioning.

**Automatic decimal point positioning** causes the measurement to be made on the lowest possible range, so maximum resolution is always achieved.

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Convert voltage in the -10 to +10-V range to a frequency, count the pulses generated and provide the sign plus a three-digit BCD output with the circuit in Fig. 1. The v/f converter is a Burr-Brown VFC15 adapted to function over the voltage range with resistors $R_1$, $R_2$ and $R_3$. A reference voltage ($V_{ref}$) of 10 V must be applied to the converter's current input.

The v/f output frequency, which covers 0 to 20 kHz, feeds into three up/down SN74190 decade counters. The polarity sign is entered into a SN7474 flip-flop.

A measuring cycle begins at the positive edge of a 100-ms pulse fed to the input labeled GT. Gate G1 allows the v/f output pulses ($F_{in}$) to enter the counter, and the pulse, LD, generated by the one-shot circuit, $G_3$/$G_4$, sets the BCD counters to 999 and the SGN output of the Sign flip-flop HIGH. A HIGH SGN sets the BCD counters to count down.

If the counters pass the 000 state, the Sign flip-flop is set LOW, and thereafter every clock-pulse increments the counters by one. After 100 ms, GT cuts off the $F_{in}$ input to the counters, which then contain the value of the input voltage, $V_{in}$, in BCD code plus the sign of the input-voltage polarity.

If $F_{in}$ is higher than the 20 kHz, the Enable signal generated via $G_5$ and $G_6$ blocks the counter at +999 and provides the OVR signal to indicate an out-of-range condition.
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CIRCLE 252 FOR FREE DEMONSTRATION
Synchronous counter also shifts for serial/parallel conversions

Many logic circuits require that the output of a counter be converted to serial format. Also, a counter often must be loaded from a serial signal. Such parallel-to-serial and serial-to-parallel conversions, usually accomplished with a shift register, can be done without a shift register, if the counter is a synchronous, preloading type, such as the 74LS163.

When the 74LS163's load control is HIGH, it operates normally as a counter. However, when LOW, the counter can progressively transfer data at its preload inputs (PA through Pn) to the outputs. Four clock cycles will load all stages of the counter with a serial input to PA, and shift each of its stages progressively to the Qd output (see figure).

Darryl Morris, Northeast Electronics, Airport Rd., Concord, NH 03301.

Demand power supply draws low standby current

The inexpensive, simple power-supply circuit in the figure draws almost zero standby current and features a low component count and no power transformer. Each positive half of a power cycle charges the storage capacitor, C1, until its voltage equals the zener-diode reference voltage. At this point, the gate of the SCR reverse-biases and the SCR turns off at the end of a cycle. When the load draws current from the storage capacitor and the capacitor voltage falls below the zener voltage, the gate is forward-biased and the SCR turns on. When no load current flows, the output capacitor stays charged—the only current drain is through R1 and the zener diode.

The circuit's relaxation-oscillator mode of regulation has one disadvantage: It imposes a low-frequency ripple on the output voltage. A large R2C1 time constant can limit this ripple. Of course, to minimize power loss, R2 should be kept as low as possible.

George W. Masters, Teledyne Microelectronics, 12964 Panama St., Los Angeles, CA 90066.

Power is supplied on demand by this simple relaxation-oscillator power supply. The zener-diode reference, D1, determines the output voltage and the time constant of R2C1 controls the amount of ripple.
New technique saves 30% to 40% on big, bright, uniformly-lit LED digits.

Through computer-aided optical design, Litronix has developed a way to make top-quality LED digits using a low-cost manufacturing technique. Our new 0.5" and 0.8" digits have unsurpassed eye appeal. They're bright. Every segment is uniformly illuminated throughout. And the digits are sharply defined.

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You can use the readout of data stored in a refresh-memory display to drive external data-recording devices such as paper-tape punches, incremental magnetic-tape recorders, impact printers and teletypewriters. But the data rate of a typical 16-character display, refreshed at 60 to 80 Hz, is 960 to 1280 char/s—too fast for such recording devices.

The timing diagram of such a refresh memory, 16-digit display (Burroughs Model SSD 1000-61) is shown in Fig. 1. To slow down the readout rate, the circuit in Fig. 2 reads out the first character from an initial frame of 16 characters, then reads the second character from a subsequent frame, and so on, until all 16 characters are clocked out.

This sampling process uses a divide-by \((16n + 1)\) circuit, where \(n\) is an integer between zero and 16 chosen to get the desired speed. For example, a divide-by-33 choice gives 29.1 to 39 char/s. In addition, the circuit provides the necessary counting, latching and gating to limit the output to 16 characters.

The refresh memory of the display, therefore, can become the storage medium for a single-task system, such as an automated weighing machine. The system can easily be constructed with a digital balance, a multiplexer to read digits from the balance into the display, a keyboard to enter identifying digits into the display, and the circuit in Fig. 2 to read data from the display to a paper-tape punch or incremental magnetic-tape recorder. Data on a tape can be processed subsequently as a batch job on a computer.

Stephen A. Oliva, Captain, U.S. Army, Armed Forces Radiobiology Research Institute, Bethesda, MD 20014.

CIRCLE NO. 314

1. The Reset and Update pulses from the timing diagram of this visual-display refresh-memory system are used to synchronize the slow-down circuit for hard-copy readout.

2. The slow-down circuit extracts one character each from one or more frames to obtain the 16 characters at a much slower rate than the original visual-refresh rate of 960 to 1280 char/s.
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Add missing segments to 6 and 9 on standard seven-segment decoders

Improve the appearance of numbers 6 and 9 on standard seven-segment LED-display decoders with half a NAND chip. With type 7446/7447 decoders, the upper horizontal bar (segment “a”) and the lower horizontal bar (segment “d”) of digits 6 and 9, respectively, do not glow.

You can add the missing segments with two circuits of an inexpensive 7401 quad NAND. Their open collectors are wire-ORed to the “a” and “d” segment outputs of the decoder as shown in the figure.

A. K. Mitra, AMICO, Electrical & Electronic Engineers & Manufacturers, 20 Strand Road, Calcutta - 700001.

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Powerful oscillators are very efficient, too

Gunn oscillators that produce a peak power of 120 W with an efficiency of 18% at 5 GHz (C band) have been developed by Standard Telecommunication Laboratories of Harlow, England.

The devices are made from indium phosphide and have an active-layer thickness of 34 µm and a low-field resistivity of about 2 Ω-cm. The substrate of the indium slice is lapped until it is about 120 µm thick. Metal contacts of 90% silver and 10% tin are then evaporated on both sides and alloyed in hydrogen at 500 C. Standard photolithographic etching forms mesa devices.

Varactor has wider capacitance range

A varactor structure that yields a much greater variation of capacitance with voltage than a conventional varactor diode has been developed at Osaka University, Japan. The device consists of alternating layers of n-type and p-type silicon as shown in Fig. 1. A pair of n and p layers forms a unit structure indicated in Fig. 1 by broken lines and shown in detail in Fig. 2.

With contact 1 biased negatively with respect to contact 2, contact 1 is reverse-biased in the n region while contact 2 is reverse-biased in the p region. By suitably choosing the electron barrier heights, most of the voltage drop will occur across the reverse-biased junctions, where the depletion widths increase with bias voltage.

Because the junction between the n and p regions in each unit structure is also reverse-biased, a widening of the depletion region also takes place perpendicular to that which occurs at the metal-semiconductor interface. This bias voltage affects the depletion region in two dimensions and the larger variation of capacitance with bias voltage occurs.

Prototype 1.25-mm long x 0.14-mm wide devices have been made having a p-n junction diffusion potential of 0.52 eV. The capacitance/voltage curves of the Osaka diode (with a linear doping profile and gold contacts) reveals that the sensitivity of the capacitance to bias voltage variations (γ) lies between 0.4 and 0.6. In the curves the capacitance was normalized to its zero bias value.

In contrast, C/V measurements from a conventional varactor diode using the same materials show a lower γ, a higher capacitance and, unlike the new device, is not symmetrical about the zero bias point.

For frequency multiplication applications, the new varactor structure is more efficient as a result of its greater nonlinearity.

Superluminescent diode has narrow line width

A superluminescent diode (SLD) for optical communication systems can be pulse-modulated up to 250 MBit/s. With a narrower spectral output than a LED, it can carry data over longer lengths of fibers.

For high-bit-rate optical systems, solid-state lasers provide the best performance because they have the narrowest spectral linewidth, but they are expensive. LEDs, on the other hand, provide a low-cost solution, but typical linewidths are only about 40 nm. The SLD, developed by researchers at the Munich University in West Germany, is an excellent compromise with its 10-nm linewidths.

The SLD is based on a mesa-type structure (Fig. 1). The substrate is n-type gallium arsenide and is 300 to 1000 µm long. It consists of four layers: (1) tellurium-doped, n-type gallium aluminum arsenide, (2) undoped gallium arsenide, (3) germanium-doped, p-type gallium aluminum arsenide, and p-type gallium arsenide.

The mesa stripe is made longer than the contact length, providing sufficient loss to prevent lasting action. Line-widths of 10 nm were obtained with current densities above 5 kA/cm². Rise times below 2 ns can be achieved above this level. The SLD light output vs drive current is highly nonlinear.
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Lillian Herold is Purchasing Manager, Kantz Electronics Industries, Clifton, New Jersey. Kantz designs and prepares prototype circuitry for printed circuit boards and provides manufacturing facilities for PC board production. Her directory? Electronic Design's GOLD BOOK.

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Ms. Herold uses the GOLD BOOK about 15 times a week. Among other purchases, she has recently ordered 300,000 resistors, 20,000 sockets, solder bars, a wave soldering machine and an axial forming machine through its use.

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CIRCLE 241 FOR DEMONSTRATION

CIRCLE 242 FOR ADDITIONAL INFORMATION

ELECTRONIC DESIGN 19, September 13, 1977
Analog I/O cards for industry plug into Motorola 6800


Burr-Brown, the first to make analog peripheral boards that are plug-compatible with Motorola's 6800 microcomputer systems, is now the first to orient such boards to industrial applications.

The MP701 is a 16-channel relay-output board, and the MP702, a 32-channel. The MP7608 is an eight-channel analog-input board. Both relay-output boards feature 300-V dc channel-to-channel isolation and 600 V dc isolation to the computer bus. All three boards operate directly from the 6800's +5 V dc and ±12 V dc power-supply buses.

Output power for both the MP701 and MP702 is rated at 10 VA per channel. A metal-oxide varistor protects the dry relay contacts when they switch inductive loads. The reeds are rated at 10⁶ operations each.

The MP7608 features 12-bit a/d conversion accuracy. Normally, it is configured to accommodate direct voltage inputs from strain gauges and resistive temperature devices (RTDs). Sensing bridges and excitation voltages are provided on board.

The bridge-reference voltage is derived from the same source as the a/d converter reference—this reduces the effects of drift with time and temperature. Each channel is overvoltage-protected to 200 V.

Input-voltage bridges are replaced with precision-dropping resistors in a current-input option, the MP7608-I, which provides input for 4 to 20-mA loop signals. Fast-acting fuses protect the 250-Ω resistors from excess current surges that might affect their 0.01% accuracy. Inputs are RC-filtered to 10 Hz.

Both series of boards are memory-mapped and assigned specific addresses at the factory. The supporting 6800 software is claimed to be simple—only two instruction steps are required to change the state of as many as eight output channels, according to Burr-Brown.

Prices of the 16-channel MP701 output board are $295 in lots of 1 to 9 and $265 in 10 to 24 lots. The MP702 costs $475 and $425 in the same quantities. Both versions of the MP7608 cost $595 and $535, respectively. Delivery is from stock.

Other firms supplying analog I/O boards for microcomputers include Analog Devices and Datel.

Analogue Devices markets its RTI-1200 and 1220 series boards for Intel and Prolog card cages. By October, Analogue Devices expects to be shipping its RTI-1230 series for the Motorola bus.

Datel manufactures an ST-800 family of analog I/O cards for Intel systems and several others for minicomputer systems. Datel, too, expects to be shipping Motorola-compatible cards in the near future.

Current monitor guards up to 50-A-ac lines

Logitek, Inc., 42 Central Ave., Farmingdale, NY 11735. (516) 694-3080. From $105; 4 to 6 wks.

Type CA and 1A ac-current-monitor modules constantly oversee ac lines and test for overcurrents in the 10-A range for military use and in the 50-A range for industrial use. Accuracies of 1% and 5% are standard. Both types feature 2 and 10-A contacts. Fixed or field-adjustable trip settings are available.
Tiny d/a converter follows A-law

Precision Monolithics, 1500 Space Park Dr., Santa Clara, CA 95050. A. Chame (408) 246-9222. From $9 (100 qty); stock.

The DAC-87, a monolithic companding d/a converter, conforms to the CCITT exponential A-law characteristic. The unit features the dynamic range of a sign-plus-11-bit converter (66 dB) in a sign-plus-7-bit format. The device may be configured as an encoder, as a decoder, or may be time-shared as an encoder and decoder. The converter is meant for European A-law pulse-code-modulation systems. Significant features include: multiplying capability, true current-source outputs with -5 to +18-V compliance, 500-ns settling time and 141-mW consumption.

CIRCLE NO. 309

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Model 203A Price $69/100 units

The most popular DPVMs become even more attractive

Newport's model 203A (3½ digits) and 2003A (4½ digits) Digital Panel Voltmeters (DPVMS) are upgraded versions of the very popular Newport models 203 and 2003. Available with bright red 0.5 inch LED display or orange LED digits optionally.

The pin connections are the same as the 203 and 2003. Full scale counts are ±1999 and ±19999 respectively. Parallel BCD outputs are standard. A choice of four voltage ranges. The standard case is high impact plastic with DIN cut out dimensions or NEMA dimensions optional. One adjustment behind the lens sets full scale. Automatic zeroing of the input is performed on each conversion.

Average value, dual slope integration prevents ambiguous readings of small signals superimposed on noise. Ratio capability is standard.

Model 2003A Price $129/100 units

Options include True RMS, screw terminal barrier strip for signal and power, and 5 volt DC power instead of normal AC line power. The 2003A has an option for buffered, isolated, gated and latched BCD outputs. Available from distributors and stocking reps world wide. Ask us about our mod centers and high volume custom engineering for your application.

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CIRCLE NO. 64

High-voltage op amp has speed, too


At a gain of 100, the 3584 op amp boasts: 20-MHz min and 50-MHz typ gain × bandwidth; 150-V/μs typ slew rate; and 12-μs settling time to 0.1%. But the TO-3 hybrid must be compensated externally. The device operates with input power ranging from ±70 to ±150-V dc and swings its dc output between ± (Vcc-5) V. The unit's FET cascode input requires only 20-pA max-bias current. Other input specs include: 3-mV offset, 25-μV/°C input offset drift and 110-dB CMR. Protected against output shorts; automatic thermal shut off.

RCA, New Holland Ave., Lancaster, PA 17604, (800) 233-0153. $265; stock.

A closed-circuit-TV splitter/inserter, the TC1470, enables simultaneous display of video from two cameras on one monitor or recording of both on a single video tape recorder. The unit features front-panel-pushbutton selection of either the split or inserted display or either camera's full screen. With simple video wiring at the monitor you get a similar selection via the video cable. Front-panel screwdriver adjustments vary the horizontal and vertical size and position of the split/insert. The split or insert is outlined with black to provide clear visual separation and a front-panel balance control permits equalization of picture brightness. The master camera needs only a simple interface because the splitter/inserter provides a vertical-drive output for the second camera.

CIRCLE NO. 309

Display two cameras on one CCTV monitor
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While the Teletype® model 40 132-column printers are rated at 300 lpm (monocase), that figure is somewhat misleading.

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Pnp transistors deliver linear outputs to 1 GHz

SGS-ATES Semiconductor, 79 Massasoit St., Waltham, MA 02154, Ruben Sonnino (617) 891-3710. $4.80 (95) $6.90 (96); samples from stock.

A pnp transistor, the BFT 96, is intended for common-emitter driver applications up to 1.5 GHz. It can deliver linear signals of up to 0.5 V across a 75 Ω load at 1 GHz. Housed in a T plastic package, the BFT 96 handles a collector-base voltage of -20 V, a collector-emitter voltage of -15 V, and an emitter-base voltage of -3 V. Total dissipation is 500 mW, max.

Power MOSFETs offer upgraded performance

Siliconix, 2201 Laurelwood Rd., Santa Clara, CA 95054, Jim Graham (408) 246-8000. From $3.33 (100 qty); stock.

The 2N6657 and 2N6660 VMOS transistors are improved replacements for the older VMP 1 and VMP 2, respectively. Both the 2N6657 and 60 have upgraded specifications and contain an on-chip gate protection zener. (The VMP 1 and 2 had a separate zener mounted in the same package.) Both new units have lower input currents and lower ON resistances than their VMP series counterparts (100 nA vs 500 nA). The lower ON resistance 2.5 Ω max instead of 3 Ω results in a lower power dissipation. The 2N6660 can handle 6.25 W in a T0-39 package and the 2N6657 handles 25 W in a T0-3 package. Other features of the 2N6657 and 2N6660 are the high current handling capability (up to 3A), 60 V breakdowns, 10 ns switching times, and a complete lack of secondary breakdown or current hogging (in parallel configurations). Both the 2N6657 and 2N6660 operate over -65 to +150 C.

Broadband power FETs operate at up to 500 MHz

Teledyne Crystalonics, 147 Sherman St., Cambridge, MA 02140. Raymond Moore (617) 491-1670. From $4.50 (100 qty); stock.

The CP640, CP650 and CP651 family of power FETs is useful at frequencies up to 500 MHz. They exhibit a third-order intermodulation intercept point greater than +40 dBm and a 50 Ω VSWR of less than 1.5:1 over the 0.5 to 50-MHz range. The smaller geometry unit, the CP643, has a gm of 25,000 µmhos at a 25 mA drain current. The CP643 is useful as an i-f preamp where it presents a good termination for double-balanced mixers because of its constant 50 Ω input impedance over 1 to 108 MHz.

At +125°C you can burn your fingers on some DAC’s our 4058 stays cool

Because this new, hybrid 12 bit DAC was specifically designed for the temperature range -55 to +125°C, it is not merely a top-end selection of commercial DAC’s, where you don’t know today what tomorrow’s yield will be.

Your application may not need the full temperature range nor the hermetically sealed metal DIP. But for a lot of industrial applications these and other features of the new DAC offer you vital safety factors. For example, it is produced to MIL Std 883 giving extremely high reliability. It has a very low temperature drift of 5 ppm/°C gain, 10 ppm/°C max. offset. And if you want to fly with it, the 4058 is shock, vibration and acceleration tested - its already being used in the new MRCA.

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CIRCLE NUMBER 66

134 ELECTRONIC DESIGN 19, September 13, 1977
MCC builds custom IC's using I^2L to provide Consumer Product Prices

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- Motor Speed Controllers
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- Timer Circuits

MICRO COMPONENTS CORPORATION

CIRCLE NUMBER 67
ICs & SEMICONDUCTORS

Speedy a/d converters provide 8-bit answers

TRW, One Space Park, Redondo Beach, CA 90278. William Koral (213) 556-1500. For 100 qty: $75 (1002J), $175 (1001J); 60 days.

Capable of operating at conversion rates of 1 μs and 400 ns, the TDC-1002J and the TDC-1001J are monolithic 8-bit a/d converters. The converters are bipolar units and are TTL compatible. Accurate within ±1/2 LSB, they require synchronizing clock signal, an accurate full scale reference voltage, and a compensating capacitor. Nine clock periods are required per conversion, with a typical clock frequency of 22.5 MHz. A status output indicates when the a/d converter is available for the next conversion. All output bits are available one clock period after the status signal indicates “ready to convert.” Fanout capability is two Schottky-TTL output transistors for high-current regulators and the TDC-1001J are monolithic 8-bit a/d converters. The regulators retain all the versatility of the SG723 but have an input voltage range of 4.5 to 50 V, and open-collector outputs on the SG1532 (cerdip package) permit use of external npn power transistors for high-current regulators with only a 2-V input-output differential. Reduction of sense voltage from 650 mV in the SG723 to 80 mV in the SG1532 can save significant power. A 10-A regulator would dissipate 6.5 W in the current sense resistor when using the SG723 while the loss is only 0.8 W with the SG1532. A band-gap reference provides both a low 2.5-V reference level, as well as a greatly reduced noise voltage over the conventional zener diode used in older designs. Line regulation for the SG1532 is 0.01%/V, max. Useful output current exceeds 100 mA. Available in 14-pin cerdip and 10-pin T0-96 cans for -55 to +125 C (SG1532) and 0 to +70 C (SG2532/3532).

CIRCLE NO. 326

Quad bus transceiver provides three-state I/O

Texas Instruments, P.O. Box 5012, Dallas, TX 75222. Dale Pippenger (214) 228-2011. From $1.76 (100 qty); stock.

Three-state outputs for both driver and receiver are included in the SN75136, a quadruple bus transceiver. The outputs of the circuit provide the high switching speeds of totempole TTL circuits while offering the bus capability of open-collector gates. Other features include party line, or data-bus operation, a single 5-V supply requirement, npn inputs for minimum input loading and a 40-mA driver sink capability. 16-pin DIP.

CIRCLE NO. 325

Get almost any voltage with settable regulators

Silicon General, 7382 Bolsa Ave., Westminster, CA 92683. J. Catrambone (714) 892-5531. From $1.10 (100 qty); stock.

The SG1532/2532/3532 series of precision but general purpose voltage regulators, provides performance improvements over the older SG723. The regulators retain all the versatility of the SG723 but have an input voltage range of 4.5 to 50 V, and open-collector outputs on the SG1532 (cerdip package) permit use of external npn power transistors for high-current regulators with only a 2-V input-output differential. Reduction of sense voltage from 650 mV in the SG723 to 80 mV in the SG1532 can save significant power. A 10-A regulator would dissipate 6.5 W in the current sense resistor when using the SG723 while the loss is only 0.8 W with the SG1532. A band-gap reference provides both a low 2.5-V reference level, as well as a greatly reduced noise voltage over the conventional zener diode used in older designs. Line regulation for the SG1532 is 0.01%/V, max. Useful output current exceeds 100 mA. Available in 14-pin cerdip and 10-pin T0-96 cans for -55 to +125 C (SG1532) and 0 to +70 C (SG2532/3532).

CIRCLE NO. 327

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ELECTRONIC DESIGN 19, September 13, 1977
INTRODUCING THE NEW "DESIGNER" SERIES OF OPTOISOLATORS FROM MONSANTO.

The new MCT270 "designer" series from Monsanto introduces a new approach to your design requirements. It lets you control the important design parameters so you can specify what you need without a special order. Standard products, off the shelf, where you have the flexibility of selecting the best product for your application.

CONTROLLED GAIN.

Choose from four ranges of Current Transfer Ratio, so that you know in advance what the gain of that design stage is going to be. Not just a "typical" rating, but a distinct "min-max" specification. From a 45% transfer ratio to a 225% minimum. All are UL recognized at 2500 volts, rms.

HIGH SPEED.

If your circuit design requires high speed in a transistor output optoisolator, you can get the MCT276. It has a gain ranging from 15% to 60%, with a fast 2.5 μseconds maximum turn-on/turn-off speed. And, you guessed it—UL recognized to 2500 volts, rms.

HIGH VOLTAGE OUTPUT STAGE (80 VOLTS).

When a high output blocking voltage is needed, specify the MCT275. Current transfer ratio is between 70% and 210%. Again, it's UL recognized to 2500 volts, rms.

TEMPERATURE COMPENSATED, TTL COMPATIBLE.

Your application may require reliable operation over a wide temperature range. If so, you need an optoisolator that’s specified that way. That’s our MCT277. It features a minimum 100% current transfer, with a 15 μsecond maximum rise and fall time. And those specifications hold from 0°C to 70°C. You can get the reliable operation you need, across the temperature range you need. It too is UL recognized.

GET OUR "DESIGNER" KIT.

You’ll want to find out more about this exciting new option for your designs. Send for our free literature kit, containing complete specifications, applications information, and ordering information. Write Monsanto Commercial Products Co., Electronics Division, 3400 Hillview Ave., Palo Alto, CA 94304. Telephone: (415) 493-3300.
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Now there are three BIFET op amp families to serve virtually all of your operational amplifier requirements. The new TL061 and TL071 families join the TL081 family to offer you the most comprehensive line of BIFET op amps available. Each family has its own identical specifications so you can standardize your requirements regardless of application.

You'll find low-cost general purpose BIFET op amps priced to replace bipolar devices. Low noise audio devices with low harmonic distortion. And a totally new concept, a BIFET op amp with low power consumption and low supply current. Four singles, four duals and four quads. Six pinouts in three series plus a whole lot more.

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amps available off the shelf from TI and your TI distributor.

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Five general purpose devices with identical specifications that allow you to standardize your op amp requirements in one family to replace such widely used bipolarics as μA741, MC1458, LM308, LM324, μA747, RC4558 and RC4136.

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Low noise and low harmonic distortion make the TL071 series ideal for high fidelity and audio pre-amp applications. Equivalent input noise voltage is typically 18 nV/√Hz with a low harmonic distortion of 0.01%.

**TL061 Series**

A totally new BIFET op amp series ideally suited for battery-powered and similar applications requiring a minimum of power consumption. Now you can get BIFET dc specs and ac specs better than μA741 and MC1458 bipolar op amps at less than one tenth the power—0.25 mA max Icc per amplifier.

**Priced to replace bipolarics.**

You'll find prices as low as 33 cents each for the TL081 in 100 piece quantities; 47 cents for the TL071 and TL061. Twelve devices in three BIFET families offering low cost, low power, low noise. To learn more about how these new BIFET devices can serve all of your op amp requirements, contact your authorized TI distributor or the leader in BIFET op amps, Texas Instruments.

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**BIFET op amp specifications.**

<table>
<thead>
<tr>
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<th>TL081</th>
<th>TL071</th>
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</tbody>
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* A & B versions available with 6 mV and 3 mV respectively for all three families.

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Isolators require only 0.5 mA for 400% CTR

Spectronics, 830 E. Arapaho Rd., Richardson, TX 75081. (214) 234-4271. From $1.65 (1000-qty); 30 days.

The 6N138 and 6N139 optoisolators feature high gain at low input currents, TTL compatible outputs and 800% current transfer ratios (CTRs). And, their input currents are only 0.5 mA while providing 3000-V-dc isolation voltages. With a CTR of 300% the 6N138 (SCH 4370) requires an input current of 1.6 mA, while the 6N139 (SCH 4371) has a 400% minimum CTR with a 0.5-mA input current. The isolators are pin-compatible with respective HP 6N138 (5082-4370) and 6N139 (5082-4371) isolators. 8-pin DIP.

CIRCLE NO. 328

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CIRCLE NUMBER 71

Power transistors handle 20-A peak current

International Rectifier, 233 Kansas St., El Segundo, CA 90245. (213) 322-3331. From $3.20 (100-qty); stock.

Six 20-A power transistors, including both npn and pnp types, are available with collector-emitter ratings of 100, 120 and 140 V. Units designated 2N5629 (npn) and 2N6029 (pnp) are rated for 100 V with a minimum dc current gain of 25; the 2N5630 (npn) and 2N6030 (pnp) are rated for 120 V and a minimum gain of 20; and the 2N5631 (npn) and 2N6031 (pnp) are rated for 140 V and a minimum gain of 15. All units offer 20-A peak collector current with junction operating temperature from -65 to +200 C. Collector-emitter saturation voltage for all six devices is 2 V at a collector current of 16 A and a continuous base current of 4 A. Maximum thermal resistance, junction-to-case for all units is 0.875 C/W. TO-3 case.

CIRCLE NO. 329

Transistors operate from 200 MHz to 4 GHz

California Eastern Laboratories, One Edwards Court, Burlingame, CA 94010. (415) 342-7744. For 10 to 99 qty: $17 (chip), $77 (packaged); stock.

A general-purpose transistor, the NE645, is designed for use from 200 MHz to 4 GHz. The NE645 has a 0.8 dB noise figure and a 21 dB gain at 500 MHz, 1.3 dB noise and 14 dB gain at 1.5 GHz, and 2.7 dB noise and 8 dB gain at 4 GHz. Ideal for i-f amplifiers, the transistors require from 1.5 to 30 mA and can meet the requirements of MIL-STD-750/883.

CIRCLE NO. 330

Electronic Design 19, September 13, 1977
Burr-Brown's new VFC32 monolithic V/F converter provides ±0.01% (12-bit) linearity, a 6-decade dynamic range, yet costs only $6.10 in 100's.

Now that precision performance and wide dynamic range are available in a low-cost monolithic V/F converter, you should take another look at this low-cost method of digitizing analog signals. The VFC32, with 12-bit linearity to 10 kHz, offers a sevenfold improvement over some units you may have considered. And its top frequency of 0.5 MHz (with 8-bit linearity) is five times higher than most competitive units, allowing faster conversion times.

You can also use the VFC32 as an F/V converter. And you'll need no external active components. Use it in tachometer applications, or combine two VFC32s and make an analog-digital-analog data link that has high noise immunity.

Three versions are available, covering the temperature ranges of 0 to +70°C (epoxy DIP package), −25 to +85°C and −55 to +125°C (hermetically sealed TO-100 packages).


See us at WESCON, Booths 1622-24.
Calibrator stores tolerance limits

The 5100A calibrator stores the tolerance limits of a unit under test and flashes its display if an out-of-tolerance voltage from the calibrator is required to correct the reading of the UUT. A single “edit” control provides continuous adjustment over the output range of the calibrator and activates all error, tolerance, and limit calculations.

The calibrator handles meters with dc accuracies specified to ±0.01% and ac accuracies of ±0.1% from 50 Hz to 50 kHz. A wideband frequency module extends frequency range to 10 Hz to 10 MHz.

Current outputs, both ac and dc, are from 5 µA to 2 A. Resistance values for ohm meter calibration are from 1 Ω to 10 MΩ in eight discrete decade sizes—no intermediate values are available.

In calibrating resistances, the 5100A can compensate for lead resistances, storing this information and subtracting it from measured data. This allows precise measurements of resistance without the inconvenience of four-wire hookups. However, four-terminal resistance measurements can also be made, if desired.

The 5100A can also be programmed for entry limits. If an operator tries to call up a voltage higher than the stored limit, the instrument indicates an error and locks at the last voltage output within limits. This prevents damage to the unit under test, as well as injury to the operator.

Additional safety features include separate low and high-voltage supplies. The high voltage supply is turned on only when necessary; lower output voltages are derived from the separate low-voltage supply instead of by division from the higher-power section.

CIRCLE NO. 307

Programmer/temperature controller in one unit


The Model 4000 is a self-contained dual-function instrument that automatically controls temperature in a continuous temperature-time program. The unit comes with a proportional temperature controller in either a horizontal or vertical configuration. A program is introduced by a 6-in. rotating cam which is easily shaped by the user to the desired configuration. Temperature control is achieved by the solid-state proportional controller which responds to the sensor and the set-point. The sensor may be either an RTD or a thermocouple, while the set-point is determined manually with a 1-k pot or by a 200-Ω slidewire which is positioned by the program cam.

CIRCLE NO. 331

Portable comparator rapidly sorts resistors

Associated Testing Labs., 23 Vincent St., Wayne, NJ 07470. (201) 473-6455

A portable, solid-state resistance comparator rapidly sorts semi-precision resistors for incoming inspection. The Model DLRC-9A comparator features analog output for recording, low test currents, two or four wire (Kelvin) measurements and four-place limit-set controls. Also, the instrument offers three state readout of limit—MIN, PASS and MAX. Strobed status-lamp outputs (TTL compatible) are included for use with automatic handlers.

CIRCLE NO. 332
There's a little tiger in every Cherry switch

Our products are tough, but our people aren't... and that's the beauty of dealing with Cherry.

You see, we can control the quality of our switches because we fabricate most of our own parts (moldings, stampings, springs, printed circuits, etc.) And we can keep the price down because we're loaded with automatic equipment to handle high volume.

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CIRCLE NUMBER 74
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Panel sealed solid state keyboards in a variety of arrays.

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SE and XE miniature basic switches are environment-proof. HM version provides hermetic sealing and larger-sized HT withstands extreme temperatures.

EN is environment-proof limit switch with variety of actuators, circuitries, and electrical ratings. HE is hermetically-sealed version.
Programmable source spans 1 mHz to 50 MHz


Capable of generating sine, triangle, and square waves from 1 mHz to 50 MHz, the 8165A can store and recall up to 10 complete instrument settings via front-panel controls or an IEEE-488 interface.

While store-and-recall of frequency and amplitude has been available in other instruments, it has not been as complete, nor available in a function generator. A similar such source, Ex­act Electronics' Model 757 (ED 10, May 10, 1977, p. 102), lacks such features, but its price is much lower ($1450), and its frequency range wider (0.1 mHz to 50 MHz).

Complete operating mode settings, function parameters, and output mode settings are recalled by pushing two buttons, or by addressing one of 10 storage registers via the interface bus.

Built-in batteries maintain data storage up to 6 months when the instrument is turned off.

Pulses or ramps with 20 to 80% duty cycles are generated from 1 mHz to 19.99 MHz, with pulse transition times less than 5 ns. Source impedance can be set at 50 or 1000 Ω.

Phase-locking to a 10-MHz crystal reference achieves output frequency stability of ±1 × 10⁻⁵ of the programmed value. Frequency resolution is four digits—1 µHz in the 1 mHz to 9.999 MHz range, for example.

Output amplitude of the 8165A can be set from 10 mV peak-to-peak to 9.99 V peak-to-peak from 50 Ω into a 50-Ω load. In the 1000-Ω, current-source mode, the 8165A can deliver 20 V peak-to-peak into a 50-Ω load. Amplitude accuracy is 2% of the programmed value.

Offset is variable from zero to ±5 V from 50 Ω into a 50-Ω load, or double that in current-source operation. Offset accuracy is within ±1% of programmed value.

In the trigger mode, a single cycle of the selected waveform is triggered with an external signal. Gating is synchronous and the waveform always begins at zero phase.

In the counted burst mode, the 8165A generates a predetermined number of waveforms from 1 to 9999, independent of the frequency of the selected waveform.

The 8165A can be swept in two modes. In the VCO mode, an external voltage from 10 mV to 9.999 V controls the internal oscillator. In the sweep mode, the internal oscillator is swept logarithmically over a selected sweep time. In either case, the sweep is over three decades from the main frequency. Triggering can be internal or external.

The carrier of the 8165A can be frequency modulated using a rear­panel BNC by an external ac or dc signal. For a change of 1% in carrier frequency, a voltage of 1 V peak-to-peak is required. Modulation can be varied from 100 Hz to 20 kHz.
Synthesizer tunes continuously
Model 1010 five-digit, bench frequency synthesizer covers 1 Hz to 10 MHz and is controlled by a single front-panel knob that provides continuous tuning like a standard dial-tuned signal source. The unit provides 1-Hz resolution to 100 kHz and 100-Hz resolution to 10 MHz, as well as a metered output leveled to 0.25 dB over the full range. It has a precision output attenuator adjustable over a 60-dB range in 10-dB steps.

CIRCLE NO. 333

Model 2240A Measurement and Control Processor allows the user to acquire a mix of both digital and analog data and to control digital and analog outputs. The unit is the first in a line of such devices using silicon-on-sapphire technology and taking advantage of the HP-IB (IEEE-488) Interface Standard. The 2240A's digital and analog capabilities include multiplexing and conversion of analog input signals, multiple analog output signals, multiple digital signal event monitoring, frequency counting, event counting, digital signal outputs and stepper motor control outputs. Analog input signals are automatically corrected for temperature offset and drift.
Booth No. 2051  CIRCLE NO. 334

LSI test system aims at high throughput
Fairchild Camera and Instrument Corp., 1725 Technology Dr., San Jose, CA 95110. (415) 962-3617. Start at $169,500 (30 pins); 60-90 days.
Sentry V automatic test system is said to increase throughput by as much as 200%. The unit handles µPs peripheral chips, bit slices, phase-locked loops, RAMs, ROMs, shift registers, universal asynchronous receiver/transmitters (UARTs) and digital hybrids in such technologies as NMOS, PMOS, CMOS, SOS, ECL, TTL and PL. Sentry V is source-program compatible with the Sentry II and VII, Sentry 600 and Sentry 610, thereby minimizing programming costs.

CIRCLE NO. 335

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CIRCLE NUMBER 76
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Services? Everything from design assistance through manufacturing to packaging. Response? Design cycle times of 20 weeks are not uncommon with us. Special capabilities? A few of immediate interest to you might be our own in-house mask making facility (utilizing chrome masking, by the way), application of ADS computer aided design to generate masks, and a new cell technology which brings the densities of Nitron's ADS circuits to within 13% of that of expensive, handcrafted layouts.

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INSTRUMENTATION

PROM programmer has slave unit capability

Sunrise Electronics, 228 North El Mulino, Pasadena, CA 91101. Anna Erickson (213) 963-8775. From $1495; 30 days.

A µP-based PROM programmer/emulator offers slave expandability, an optional cassette data storage unit, multiformat load and dump features, built in PROM simulator and a resident editor. The Smarty uses the 1802, an 8-bit CMOS µP and has a 1 k x 8 data RAM, a 128 byte scratch pad, parallel and serial data interfaces.

Handling the 2704/2708 PROMs, the unit also has a hexadecimal keyboard, display and indicators. The system software includes fault tolerant input/output subroutines for BPNF, hexadecimal, packed binary, ASCII/hex or user defined format.

The software can ignore rubouts, invalid characters and comments and permits the user to load highly flawed, first attempt tapes. Editing commands include: find, delete, move, insert and replace. To put the unit in the programming mode requires four keystrokes and when slaves are connected two additional keystrokes specify which slave and PROM type are to receive the programming.

Data in the data RAM can be dumped onto punched paper tape, cassette, disk or other media under keyboard control. The system software provides multiformat input and the parallel and serial I/O buffers permit interfacing with any kind of peripheral.

The system has sockets for 4 kbytes of program memory although only 1 k is used in the basic machine. By adding several slaves of the same type the Smarty can program large quantities of PROMs in minimum time. A Smarty and eight slaves will verify erase, program and verify programming of nine 2708 PROMs in three minutes.

Fluxmeter takes ±0.2% dc readings

RFL Industries, Boonton, NJ 07005. (201) 334-8100; $1470; stock.

Model 803 fluxmeter provides ±0.2% (dc mode) readings of both total flux and flux density of ac and dc or permanent-magnetic fields, with ranges from 100 to 200 x 10^7 Maxwell-turns. A peak-reading sample-and-hold mode is also incorporated. Manual or automatic reset is continuously variable from 1 to 10 s. An analog output is included and a BCD output is available as an option.

OEM recorder ignores battery voltage changes

Astra-MED, Atlaw-Tol Industrial Park, West Warwick, RI 02893. (401) 828-4000. $425; 30 days.

This single-channel battery-powered OEM recorder retains its accuracy of 0.5% of fs despite the drop-off of battery voltage and changes in load. The 102 XLA DCH is said to regulate chart movement to within 2% of the set speed and will control gain of the galvanometer to better than 1%. A battery output voltage from a peak of 13.9 down to 10.5 V (almost depleted) will not affect the operation of the amplifier or the chart paper speed. Weighing only 4 lb, the unit consumes only 6 W. Channel width is 50 mm, with the writing on thermal paper by a stylus that operates directly from the 12-V power source without an inverter. Dimensions are 4 x 6 x 6-3/4 in.

High-speed digitizer works on IEEE bus

Tektronix, P.O. Box 500, Beaverton, OR 97077. (503) 644-0161. 16 wks.; Approx. $22,000.

Model 7912AD high-speed waveform digitizer offers fully programmable operation and compatibility with the IEEE-488 bus. The unit captures transients to 1 GHz (fully programmable to 200 MHz) with automatic waveform digitizing. Included are built-in data manipulation and self-diagnostic capability. Operation is similar to an oscilloscope except that acquired waveforms are normally output as digital information for waveform processing.

Unit converts capacitance to frequency

Valhalla Scientific, 7707 Convoy Ct., San Diego, CA 92111. (714) 277-2732. $175; stock.

The Model 2020 provides an output frequency directly equivalent to the capacitance under test. The unit handles between 1 pF and 200,000 µF. The frequency may be displayed on any conventional frequency counter. A 4.7-µF capacitor will generate an output signal frequency of 47,000 Hz accurate to within ±2% of range. Dynamic range is 0 to 200% of full-scale range.
## Device Input Drivers per package Output Current BV \(V \) @ 100 mA Gain Stages Clamp Diodes Package

<table>
<thead>
<tr>
<th>Device</th>
<th>Input</th>
<th>Drivers per package</th>
<th>Output Current</th>
<th>BV (V )</th>
<th>Gain Stages</th>
<th>Clamp Diodes</th>
<th>Package</th>
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<tr>
<td>ULN-2061M</td>
<td>TTL</td>
<td>2</td>
<td>1.75A</td>
<td>50V</td>
<td>35V</td>
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<td>50V</td>
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<tr>
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<td>1.75A</td>
<td>80V</td>
<td>50V</td>
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<tr>
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<tr>
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<td>1.75A</td>
<td>50V</td>
<td>35V</td>
<td>2</td>
<td>No</td>
</tr>
</tbody>
</table>

*Only Sprague can supply dual and quad 1.75A, 50/80V Darlington Switches*

Sprague Series ULN-2060 and ULN-2070 offer the highest power ratings available. They have 1.75 amp 50/80 volt Darlington switches and have guaranteed \(V_{CE} \) (\(V_{CES} \)) minimums of 35/50 volts. No other IC manufacturer offers voltage-current combinations of this magnitude.

A pioneer in both high-current interface and copper alloy DIP lead frames, Sprague possesses extensive experience with plastic DIPs which offer greatly improved thermal characteristics. All quad switches in this series utilize the webbed-pin "B" DIP package. Lower thermal resistance ratings offer increased device limits, reduced junction temperatures, and improved reliability.

Many high-power interface problems are simplified and solved with Sprague Darlington switches. Typical uses include interface with solenoids, relays, motors (dc and stepping), LEDs (MUXed numeric or matrix), lamps, and other applications in search of 1.5 A IC hardware.

For application engineering assistance, write or call George Tully or Paul Emerald, Semiconductor Division, Sprague Electric Company, 115 Northeast Cutoff, Worcester, Mass. 01606. Tel. 617/853-5000.

Tracking filter goes where you go

B & K Instruments, 5111 W. 164th St.,
Cleveland, OH 44142. (216) 287-4800.
$3552; 150 days.

Type 1623 tracking filter is completely
portable, operating from internal
battery power. Specs include three
selectable filter bandwidths, 6%, 12%,
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Hz to 20 kHz. The unit is tunable from
practically any periodic signal, with
filter frequency/tuning signal-fre-
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The SD340 is equally at home with
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ranges
v 60 dB dynamic range
v FFT operation: all-digital stability
v Micro-processor based
v Built-in averaging
v Completely portable: only 30 lbs.
with carrying case

Send for complete information and
specifications.

25-MHz dual-trace scope delays sweep 1 µs to 5 s

Leader Instruments, 151 Dupont St.,
Plainview, NY 11803. (516) 822-9800.
$1400; stock.

The Model LBO-515, dual-trace, 25-
MHz bandwidth oscilloscope features a
continuously variable delay from 1 µs
to 5 s. The instrument offers 5 mV/div
ermal sensitivity and allows viewing the
leading edge of pulses. The overall
accuracy level for automatic trace and
reset modes is ±3%. Also included are
beam rotator for stray magnetic-field
correction; trigger for Channel 1 and
2 with a polarity inversion switch for
Channel 2; X10 magnification and a
rise time of 14 ns.

Sensitive DMM shows 100 nV/digit

Keithley Instruments, 28775 Aurora
Rd., Cleveland, OH 44139. (216)
248-0400. $995; 60 days.

Sensitivity is the standout feature of
the Model 174 4¾-digit DMM. Dc sen-
sitivity is 100 nanovolts/digit on a
high-resolution, 30,000-count display.
Automatic zeroing and standardiza-
tion occurs during each a/d conversion
for stable, accurate readings. Dc volt-
age measurements range from 100
nanovolts/digit to 1200 V full scale.
Choice of automatic or manual ranging
is available on most ranges.
Our R-10 series Relays will switch you 7 ways to Sunday.

Giving you more design options than any other relay.

It's about as close as one relay can get to being all things to all designs. The R10 series.

A compact, reliable multi-pole relay, the R10 is specified for a wide variety of critical applications. Business machines, computer peripherals, copiers, communications equipment, precision instruments and more.

Consider these options that are available with the R10. Ratings from dry circuit to 10 amperes. Contact arrangements to 8PDT. Six styles of contacts including bifurcated types. Sockets with solder or printed circuit terminals, including one for mounting the relay parallel to a printed circuit board. All with or without grounding provision.

Mechanical life expectancy of the R10 is to 100 million operations—except W contacts, 1 million—and is available with a voltage or current-sensitive coil. It weighs, depending on the number of contacts, from 22 to 40 grams. Pickup ranges from 2.25 to 86 VDC, 5 to 86 VAC, or 0.6 to 45 milliamp with proper power supply.

Design options by the dozen, all from a single relay. The R10. It's in stock now at your distributor. Call your P&B Representative or write to us direct for a copy of our latest catalog. Potter & Brumfield Division of AMF Incorporated, 200 Richland Creek Drive, Princeton, Indiana 47671. 812/386-1000.

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### TRANSMITTER DRIVERS:

- **CA 2818**
  - 8 mW
  - 1-200 MHz
  - 600 mW CW or PEP
  - $27.20* EACH
  - Gain = 18.5 dB
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  - 8 mW
  - 10-400 MHz
  - 400 mW CW or PEP
  - $31.25* EACH
  - Gain = 17 dB
- **CA 2840**
  - 3 mW
  - 30-300 MHz
  - 500 mW CW or PEP
  - $35.90* EACH
  - Gain = 22 dB
- **CA 2830**
  - 0.2 mW
  - 2-150 MHz
  - 600 mW CW or PEP
  - $40.00* EACH
  - Gain = 34 dB
- **CA 2870**
  - 0.2 mW
  - 10-400 MHz
  - 400 mW CW or PEP
  - $59.50* EACH
  - Gain = 33 dB

*Prices quoted in 1977.
**RECEIVER APPLICATIONS:**

40 MHz to 100 MHz IF amplifier.

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- RF → PRE AMP → CA 2875R → to signal processor
- Gain = 17.5 dB
- 2 mW
- 100 mW
- $31.50 * EACH

**HIGH PERFORMANCE IF**

- RF → L.O.
- CA 2876R → Gain = 22 dB
- BPF → Gain = 17.5 dB
- AGC
- Po = 24 dBm (Harm's -40 dB)
- Zo = 75Ω
- Output Ret. Loss = 26 dB
- Ip3 = +40 dBm
- $31.50 * EACH

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- CA 2820 → Gain = 30 dB
- 1-520 MHz Swept
- +24 V
- +26 dBm Leveled
- 1-520 MHz
- $27.93 *

These applications are only the beginning. TRW RF linear hybrids can revolutionize design after design...with incredible performance at unbelievable prices. Let us prove it. To get complete data sheets, send us the coupon. To find out how you can get a free sample and test fixture, call Dan Brayton at (213) 679-4561.
5-in. scope offers triggered sweep

EICO, 283 Malta St., Brooklyn, NY 11207. (212) 878-1100. $425.
Model 480 scope offers dc to 10-MHz bandwidth, ac and dc coupling, 11-position calibrated attenuator, 10 mV/cm sensitivity, and pushbutton operation. A built-in TV sync separator makes trouble-shooting TV receivers easier. Frame or line triggering is selected automatically by the scope in conjunction with the sweep-speed setting.

CIRCLE NO. 344

µP console controls system operation

Intel, 3065 Bowers Ave., Santa Clara, CA 95051. (408) 246-7501. $1520 io/o probe; 90 days.
The µSCOPE 820 console is designed for evaluating and troubleshooting 8-bit microcomputer systems in the lab, on production lines, or in the field. With personality probe/overlay sets, it can completely interface users with many different kinds of microcomputer systems. The panel can be used to monitor, display and alter register, memory and I/O values of the system under test. It also gives complete control over microprocessor operations including halt, single-step, run with display and run in real-time. For more rigorous diagnostic tasks, the console has a 32-bit maskable hardware breakpoint with optional courses of action after a breakpoint match.

CIRCLE NO. 345

Programmable unit drives all MOS type devices

Pulse Instruments, P.O. Box 655, San Pedro, CA 90733. (213) 541-3204. $295; stock to 4 wk.
The PI-451 Programmable MOS/CCD Driver plugs into a Tektronix TM-500 mainframe and shifts TTL signal levels to ±25-V outputs, driving practically all MOS devices and other capacitive loads. The output high and low levels are independently adjustable, by front-panel controls or input voltage program. Digital programming is available, too. Output transition times are variable from 2.5 ns/V to 2.5 µs/V. Output-polarity inversion and output pulse-width controls are also provided.

CIRCLE NO. 346

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The first major advance in magnetic shielding in 50 years.

Now in 40" widths
METSHIELD™ Fabric can help you achieve EMC in field repairs, prototype design, production equipment, and shielded rooms.

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This is the magnetic shielding product whose time has come. Increased sales of electronic equipment, a trend toward miniaturization and intensified regulatory considerations have put increased emphasis on EMC.

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☐ Fabrication
☐ Grounding and contacting
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Company _______________________________
City/State/Zip ____________________________
Mail to: Metglas Products, Allied Chemical Corporation 
7 Vreeland Road, Florham Park, NJ 07932
50-W switches take nominal 45-V-dc input

Abbott Transistor Laboratories, 5200 W. Jefferson Blvd., Los Angeles, CA 90016. A. Hilbert (213) 936-8185. $310 (unit qty); stock to 10 wks.

The DC50 series of three switching regulated power modules operate from dc input power of 41 to 52 V. A single output of 5 V dc and dual outputs of ±12 and ±15 V dc together deliver a 50-W total. Full power is available at 55-C ambients with 50% derating NCC dc d at 71 C. Line and load regulation is less than 0.5% and pk-pk ripple is less than 100 mV. Standard features include overvoltage protection, short-circuit protection, over-temperature shutdown, and remote error sensing. Efficiency can go up to 80%. 5.5 x 9.4 x 2 in.

CIRCLE NO. 349

Five small switches pour out 150 W


Two single and three triple output models in the DS series feature 150-W outputs in 90 in³. Efficiencies can go up to 90%. Single-output models pass 5 V at 30 A, or 12 V at 12 A. All three triple-output models offer 5 V at 24 A; auxiliary outputs are ±12 or ±15 V at 3 A, or +12 or -12 V at 4 A, -12 V at 1 A. All models include current-foldback short-circuit protection, overvoltage protection on all outputs, over-temperature protection, and a soft start that limits inrush current. EMI filtering on inputs and outputs is standard. Ripple and noise 50-mV pk-pk on the 5-V output and 1% on auxiliary outputs; voltage regulation is 0.1% with a transient response of 250 µs. 1.75 x 5 x 11.25 in.

CIRCLE NO. 350

Multi-output switches power loads up to 750 W

Pioneer Magnetics, 1745 Berkeley St., Santa Monica, CA 90404. A. Hagiwara (213) 829-3305. $695 (unit qty); 45-90 days.

Three families of multiple-output switching power supplies, the PM2675, PM2676 and PM2677 deliver 375, 600 and 750 W, respectively. They provide regulated output at full-rated load with inputs ranging from 92 to 138 V ac for the 115-V-ac input units, and 184 to 250 V ac for the 208/220-V-ac-input units. The supplies continue to operate for several minutes with inputs as low as 60% of nominal. If the input voltage fails entirely, the output voltage will hold up for 30-ms min. The main output delivers 250 W for the PM2675, 500 W for the PM2676 and 600 W for the PM2677. Three additional channels are also included in each unit. Channels two and three of any of the models can handle 150 W or 10 A. Channel four passes 75 W or 5 A. Outputs range from 2 to 48 V. The switches also feature isolated outputs, independent from each other except for the 50-W-min load required by the main channel. Other features include overload, short-circuit and reverse-voltage protection on each output, automatic over-temperature shutdown, an ac-input fuse, overvoltage protection on the main channel and remote sensing. The supplies operate at full power from 0 to 50 C and derated to 80% at 70 C. 5 x 8 x 11 in.

CIRCLE NO. 356

Remote operation with switching regulators

β Industries, 8811 N. 34th Ave., Phoenix, AZ 85017. B.A. Barney (602) 278-7516. $150 (unit qty).

Output voltages from 5 to 24 V dc, at efficiencies of up to 80%, can be delivered by the BPS series of Mini-Switchers. Four models, covering the input range of 15 to 40 V dc at 6 to 15 A, are available in small (3.25 x 3.5 x 4.88 in.), lightweight (2-lb) packages. Ripple and noise are typically 50 mV rms over a 30-MHz bandwidth. The output has built-in overvoltage protection and is adjustable to ±10% of the stated voltage.

CIRCLE NO. 357
Same great name. Same great color.
And now a neat new way to definitive display performance.

**DOT MATRIX**

Consider the new Noritake-Ise dot-matrix line-up—9, 10, 16, 20 and 40-character line displays. Variety aimed at giving you more design potential.

Or consider our unique 400-dot graphics display with 17m/m depth and low 35V drive rating. It's aimed at helping you think low voltage, portability and economy all at the same time.

In short, consider Noritake-Ise period for dot matrix (or segmental) displays. Itrons always help you design more competitively.

**DC209AZ**
- Dimension: 41(H) x 208(W) x 10.5(D)mm
- Character Size: 9.0(H) x 6.3(W)mm

**DC95A2**
- Dimension: 24(H) x 75(W) x 7.2(D)mm
- Character Size: 5.0(H) x 3.55(W)mm

**DM400A1**
- Dimension: 114(H) x 130(W) x 17(D)mm

**FG120S1**
- Dimension: 39(H) x 138(W) x 12.5(D)mm

**FG209M2**
- Dimension: 41(H) x 208(W) x 10.5(D)mm
- Character Size: 9.0(H) x 5.4(W)mm

**Noritake CO., LTD.**

Electronics Division
1-1, Noritake-Shinmach, Nish-ku, Nagoya-Shi, Japan
Phone: NAGOYA (052) 561-7111
Telex: J59738 NORITAKE

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Torrance California 90505
U.S.A.
Phone: (213) 373-6704
Telex: 230674910

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NEUMULLER GmbH
Muenchen 2
Karlstrasse 55
F.R. Germany
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Antony Cedex, France
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Telex: 42204391

Hong Kong
Room 1403 Shing Long Bldg.
24-26 Stanley Street, Hong Kong
Phone: 5-232320 Telex: 449375S
Telex: 666-21-10

Taipei
72-9 SEC 2, JEN AI RD., Taipeh
Phone: 351-0293 Telex: 11776

Manufacturer:
ISE ELECTRONICS CORP.
P.O. Box 46, Ise-shi, Mie Pref., Japan
Phone: (0596) 39-1111
Telex: 4969523

CIRCLE NUMBER 87
Data Processing

Battery-powered board tells time and date

Digital Pathways, 4151 Middlefield Rd., Palo Alto, CA 94306. (415) 493-5544. $325 (TCU-50), $495 (TCU-100); (1-qty).

Calendar and real-time clock functions for the PDP-11 and LSI-11 computers are provided by the TCU-100 and TCU-50 timing control units. The units keep track of the correct date and time, even when the computer’s power is turned off. A read instruction given by the PDP-11 operator allows the TCU-100 to present the date (month and day) and time (hr, min, sec). The TCU-50 performs the same function in the LSI-11 computer. Both units can operate without computer power for up to three months on their built-in rechargeable batteries. They are contained on edge-connector circuit boards that plug into one of the computer’s accessory slots. Units are shipped working and preset to the correct date and local time at the customer’s location.

CIRCLE NO. 358

Double-sided floppy stores 1600 kbytes

Gulton Industries Inc., 212 Durham Ave., Metuchen, NJ 08840. (201) 548-2800. $35.65 (100-499); stock to 8 wks.

The only moving part of the DM1050 10-column dot-matrix thermal printer is the advance mechanism. The printhead can handle speeds up to 7 lines per second with 5×7 characters on standard 90 C heat-sensitive paper. It is furnished with a soldered ribbon cable and mounted on a standard heat sink designed for ganged assembly to extend the number of columns. MTBF is rated 10 million character lines minimum at maximum rated operation.

CIRCLE NO. 359

Digitizer tracks by sensing sound

Science Accessories Corp., 970 Kings Highway West, Southport, CT 06490. (203) 255-1526. $800.

The Model GP-101 sonic digitizer package consists of a stylus or a cursor, an electronics package, and a sensor L-frame. Two sensors are mounted in the rigid L-frame, which can be as long as 60 in. The assembly can be moved without recalibration or realignment of its right angle. Output of the GP-101 is two gating signals that are true from the time the supersonic pulse is generated by the stylus or cursor until the pulse is received by each of the sensors.

CIRCLE NO. 360

Nonimpact head prints 10 columns

Gulton Industries Inc., 212 Durham Ave., Metuchen, NJ 08840. (201) 548-2800. $35.65 (100-499); stock to 8 wks.

The only moving part of the DM1050 10-column dot-matrix thermal printhead is the advance mechanism. The printhead can handle speeds up to 7 lines per second with 5×7 characters on standard 90 C heat-sensitive paper. It is furnished with a soldered ribbon cable and mounted on a standard heat sink designed for ganged assembly to extend the number of columns. MTBF is rated 10 million character lines minimum at maximum rated operation.

CIRCLE NO. 361

Stand-alone terminal is microprocessor based

Omron Electronics, 132 Toyama Dr., Sunnyvale, CA 94086. (408) 734-8400. $7200 (1-qty); 60 days.

The 8035 intelligent terminal is an 8080-microprocessor-based unit with stand-alone capability. Incorporated into the system are a CRT terminal, IBM 3740-compatible dual floppy-disc subsystem, complete operating software and an RS-232C interface. A 120-char/s printer can be added as an option. The operating system software package, called FDOS is composed of an editor, assembler and debugger. FDOS includes full file management routines to handle file creation, deletion and modification. Up to 4-Mbits of memory is provided by the dual-drive floppy-disc subsystem. In communications applications the system operates at rates up to 9600-baud.

CIRCLE NO. 362

Store video signals in graphic memory

Video, P.O. Box 25552, Portland, OR 97225. (503) 292-1104.

Analog signals are converted to digital by the Model 300-YT Graphic Memory. The digital signals are then stored in an MOS memory where they are available for continuous television display or video recording. Thirteen inputs can be accepted and displayed simultaneously by the unit. Front-panel switches allow selection of one or any combination of the inputs for immediate display. The unit provides four display modes: Store-information is continuously accumulated in memory until commanded otherwise. Auto-erase: at the end of each sweep the display is erased and a new sweep starts at the next trigger. Single-sweep: sweep will run at trigger input and lock-out until reset. Wipe: old information is cleared away as new information is written into the display. Options to meet special requirements are available.

CIRCLE NO. 363

Electronics Design 19, September 13, 1977
MALCO’S THRIFT-MATE

...cuts your price not your performance

Thrift-Mate is a high-performance, hard-shell plug and receptacle, perfect for low-cost, rapid assembly applications. You can get Thrift-Mate immediately for cable-to-cable, free hanging or panel mount applications. Also in strip form for automatic or semi-automatic crimping of wires to terminals. Thrift-Mate is intermateable/interchangeable with hard shell connectors available from other manufacturers.

Let Malco help you save money without sacrificing performance. Write Malco, 12 Progress Drive, Montgomeryville, Pennsylvania 18936. Phone: (215) 628-9800.
MEET OUR FAMILY of dip clips

Model 3916
14/16 Pin
For Ultra Dense Packaging

Model 4236
14/16 Pin
For Ultra Dense Packaging

Model 4124
24 Pin
For Ultra Dense Packaging

Model 4324
24 Pin
For Ultra Dense Packaging

Model 4140
40 Pin
For Ultra Dense Packaging

Model 4340
40 Pin
For Ultra Dense Packaging

Count on Pomona Electronics to keep pace with the industry's trend toward higher density Dual In-Line packaging. We introduced the first Model 3916 in 1972. Now there are six improved models, including three designed for ultra dense packaging.

DIP CLIPS are designed for hands-free testing of integrated circuit packages. Lower contacts are .050 wide for improved surface contact with I.C. packages. Test contacts are .025 square, and are serrated for improved connection of test clips. Molded barrier between contacts minimizes accidental shorting. Can also be used as insertion and removal tool for DIPs.

Available Through Your Favorite Electronic Parts Distributor

ITT POMONA ELECTRONICS
1500 East Ninth St., Pomona, Calif. 91766
Telephone (714) 623-3463. TWX: 910-581-3822

DATA PROCESSING

Control 32 CRT stations with PDP plug-in board

Echolab, 213 Middlesex Tpke., Burlington, MA 01803. Don Brickman (617) 273-1512. $1785 (OEM-qty).

A plug-in peripheral device, the CVD-11, allows a PDP-11 computer to handle a cluster of up to 32 remote CRT stations. Each device consists of a controller card that plugs into a hex slot and two small remote interfaces. The controller card contains the electronics to support two remote CRT stations, including independent display memories, character generators, TV sync generator, and Unibus interface. A remote CRT station, which may be up to 1000 ft away, connects to its controller with a single coaxial cable. This is made possible by the remote interface which multiplexes a CRT monitor, a parallel-encoded keyboard and a serial printer to the coax cable. The display is 1920 characters in an 80x24 format, and the 128 character ASCII set is standard, with special characters available.

CIRCLE NO. 364

Nova memory card holds all 128 kwords

Mostek, 1215 W. Crosby Rd., Carrollton, TX 75006. Jim Carver (214) 242-0444. $7275 (unit qty); stock.

An add-in memory card for the Data General Nova 3, the MK8003, provides up to 128 k X 17 bits on a 15 x 15-in. card. The memory card is compatible in both hardware and software with the Nova 3/4, 3/12, or 3/D, and allows the user to place the maximum addressable memory for the Nova 3 series in only two card slots, freeing additional slots for I/O.

CIRCLE NO. 365
DATA PROCESSING

Single line terminal can replace CRTs


A single-line, 32-character data display terminal designated the Transactor I, comes with a 53-key TTY-style keyboard. Designed for low cost, small size applications, the unit is intended to replace CRT terminals. The display is a gas-discharge type with a 5X7 dot matrix for easy reading. Interfacing to existing computers is possible through either an RS-232 or 20-mA current loop. Switches allow the user to select the following operating modes: 110-9600 baud rate, full or half duplex, even/odd/no parity, five to eight data bits, and one or two stop bits. The unit is packaged in either a 6 in. (H)X15 in. (W)X11 in. (D) aluminum case or a molded plastic case.

CIRCLE NO. 366

Flexible disc drive uses band-driven design


The band-driven design concept, similar to the type used in IBM devices, is available on the Series B82 flexible disc drive. For single density drive, the unit provides up to 6.4-Mbits per disc, and 12.8-Mbits for double density. Up to 1.6-Mbytes can be stored on an industry standard 8-in. diskette. The band-driven concept provides friction-free operation and very high head speeds. Average access time is 91 ms, and track-to-track access time is 3-ms. Both hard or soft sector format operation can be provided, allowing the user to read or write any IBM-compatible diskette having the appropriate format. Electronics for the drive is packaged on a single card and it can operate either from ac or dc.

CIRCLE NO. 367

Electronic Design 19, September 13, 1977

The stepper motor/driver duo that cuts stepper motor systems costs to the bone!

And reduces circuit complexity and space requirements.

Imagine! The major components for an incremental drive stepper system for only $12.60! That's all it costs for our K82701-P2 12-volt stepper motor and SAA1027 IC driver in 100 piece quantities. Using our 16 pin dual-in-line driver saves design time, too, since you don't need to work out the attendant electronic circuitry to operate the motor. It saves space, too.

You're not limited to just one motor, either. The SAA1027 IC is capable of driving a number of different 4-phase stepper motors offering a variety of formats and operating characteristics. They are listed in the accompanying table. Take your pick.

North American Philips Controls stepper motors provide many design advantages, particularly in analytical instrumentation, business machines and computer peripherals. Using 4-phase stators and permanent magnet rotors, they are low in cost, rugged and precise and offer long-term reliability. Size for size, pull-in rates and stepping accuracy are tops. Another advantage is a low temperature rise, considerably lower than comparable VR stepper motors operating on similar duty cycles. Gear boxes can also be furnished to meet varying torque and speed requirements.

Special offer...

FREE driver chips!

We want to make it easy for you to prototype our stepper motors. Thus, for a limited period of time, when you order any of the steppers listed below, specify a chip, "NO CHARGE", with each motor requisitioned. Limit is five chips. Write or call for details.

Offer expires November 1, 1977

USE THE SAA1027 IC DRIVER WITH ANY OF THESE STEPPER MOTORS

<table>
<thead>
<tr>
<th>Series</th>
<th>Description</th>
<th>Step Angle</th>
<th>Voltage</th>
<th>Max. Pull-in Rate (Steps/sec)</th>
<th>Max. Working Torque (oz-in)</th>
</tr>
</thead>
<tbody>
<tr>
<td>K82102-P2</td>
<td>Low-cost</td>
<td>15°</td>
<td>12Vdc</td>
<td>700</td>
<td>16</td>
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<tr>
<td>K82201-P1</td>
<td>light duty</td>
<td>7°30'</td>
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<td>540</td>
<td>67</td>
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<td>.78</td>
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<td>K82401-P1</td>
<td>low duty</td>
<td>7°30'</td>
<td>5Vdc</td>
<td>400</td>
<td>1.7</td>
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<td>K82401-P2</td>
<td>high duty</td>
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<td>12Vdc</td>
<td>200</td>
<td>2.5</td>
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<tr>
<td>K82601-P2</td>
<td>low-cost</td>
<td>15°</td>
<td>12Vdc</td>
<td>150</td>
<td>5.3</td>
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<td>K82601-P2</td>
<td>medium duty</td>
<td>7°30'</td>
<td>12Vdc</td>
<td>180</td>
<td>8.2</td>
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<tr>
<td>K82701-P2</td>
<td>industrial</td>
<td>7°30'</td>
<td>12Vdc</td>
<td>200</td>
<td>6.0</td>
</tr>
</tbody>
</table>

Send for information.

NORTH AMERICAN PHILIPS CONTROLS CORP.

Cheshire, Conn. 06410 • (203) 272-0301

CIRCLE 90 FOR INFORMATION ONLY  CIRCLE 91 FOR IMMEDIATE NEED
Now the selection, availability, price, and performance you want in Open Frame Power Supplies

- Fifty-five models; single and dual outputs.
- Seven industry-standard sizes.
- In stock.
- Full performance over a wide 100-125 or 200-250 VAC input range.

- More power per package size.
- Full rated current with 50 Hz input.
- True remote sense capabilities.
- Fully adjustable current limit.
- Overload and shortcircuit protection.
- UL recognized, standard 478.

More power conversion products:
Our Power House line includes a wide selection of encapsulated and ferroresonant power supplies as well as programmable solid state loads for testing. Write for our free master catalog.

Common Specifications:
AC Input: 100-125 or 200-250 VAC, 47-440 Hz.
Ripple and Noise: 1.5 mV RMS, 5 mV P to P.
Regulation — Line or Load: 0.1%.
Operating Temperature: 0°-60°C.
Transient Response: 50 µ sec.
Cooling: Convection.
Stability: ±0.2%.

ALM Single Output Units:

<table>
<thead>
<tr>
<th>Series</th>
<th>Price</th>
<th>A Series</th>
<th>Current Rating @ 40°C</th>
<th>Model No.</th>
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<tbody>
<tr>
<td>Nominal Output Voltage</td>
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<td>1.5</td>
<td>ALM 5-1.5</td>
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<td></td>
<td>6</td>
<td>1.3</td>
<td>ALM 6-1.3</td>
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<td>12</td>
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<td>ALM 12-0.7</td>
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<td>0.5</td>
<td>ALM 20-0.5</td>
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<td>0.5</td>
<td>ALM 24-0.5</td>
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Overvoltage Protector — OVM-1 $5.00
Overall dimensions: 3.03 x 3.78 x 1.28.

<table>
<thead>
<tr>
<th>B Series</th>
<th>Price</th>
<th>Nominal Output Voltage</th>
<th>Current Rating @ 40°C</th>
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<td>1.7</td>
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<tr>
<td>20</td>
<td>1.4</td>
<td>ALM 20-1.4</td>
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<td>24</td>
<td>1.3</td>
<td>ALM 24-1.3</td>
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</table>

Overvoltage Protector — OVM-1 $5.00
Overall dimensions: 4.00 x 4.87 x 1.76.

<table>
<thead>
<tr>
<th>C Series</th>
<th>Price</th>
<th>Nominal Output Voltage</th>
<th>Current Rating @ 40°C</th>
<th>Model No.</th>
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<tbody>
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<td>5</td>
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<td>6.5</td>
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Overvoltage Protector — OVM-1 $8.00
Overall dimensions: 4.87 x 5.62 x 2.50.

<table>
<thead>
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<th>D Series</th>
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<th>Current Rating @ 40°C</th>
<th>Model No.</th>
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Overvoltage Protector — OVM-2 $16.00
Overall dimensions: 4.90 x 7.03 x 2.78.

<table>
<thead>
<tr>
<th>E Series</th>
<th>Price</th>
<th>Nominal Output Voltage</th>
<th>Current Rating @ 40°C</th>
<th>Model No.</th>
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<td>8.0</td>
<td>ALM 15-8.0</td>
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<td>7.0</td>
<td>ALM 20-7.0</td>
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<td>24</td>
<td>6.5</td>
<td>ALM 24-6.5</td>
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Overvoltage Protector — OVM-2 $16.00
Overall dimensions: 4.87 x 9.00 x 2.75.

<table>
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<tr>
<th>F Series</th>
<th>Price</th>
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<th>Current Rating @ 40°C</th>
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Overvoltage Protector — OVM-2 $16.00
Overall dimensions: 4.88 x 4.88 x 13.75.

<table>
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<th>G Series</th>
<th>Price</th>
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<th>Current Rating @ 40°C</th>
<th>Model No.</th>
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Overvoltage Protector — OVM-2 $16.00
Overall dimensions: 4.88 x 4.88 x 16.75.

ALM Dual Output Units:

<table>
<thead>
<tr>
<th>Series</th>
<th>Price</th>
<th>Nominal Output Voltage</th>
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<td>ALM 15D-2.2 D</td>
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<td>12-15</td>
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<td>ALM 15D-3.3 E</td>
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<td>12-15</td>
<td>4.40</td>
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<td>12-15</td>
<td>8.00</td>
<td>ALM 15D-8.0 G</td>
<td>136.00</td>
<td></td>
</tr>
</tbody>
</table>

Overvoltage Protector — Two OVM-1 $8.00 Each.

Phone (716) 968-2400 TELEX 91-6451 TWX 510-245-2700
Acme Electric Corporation
Cuba, N.Y. 14727
See us at WESCON, Booth 815
CIRCLE NUMBER 92
Add-in memory provides 32 k on a single board

Fabri-Tek, 5901 S. Country Rd., Minneapolis, MN 55436. John Underwood (612) 935-8811. $1085 - 16-kword (1-qty); 10 days.

A semiconductor add-in memory for the DEC LSI-11 and PDP 11/03 microcomputers is designated the LS-IN-11. Up to 32 k words can be provided on a single board using 8 k or 16 k dynamic MOS N-channel chips. The unit is available in 8, 16, 24 or 32-k memory versions and memory segments are switch selectable in 4-k increments from 0 to 32-k. A 2-wide connector system is used, as compared to a 4-wide type employed by other manufacturers. The 8.5X 5.187X0.375 in. board plugs into a single chassis slot and is hardware and software compatible with the computer.

CIRCLE NO. 368

Single-card data set runs up to 1800 b/s


The GDC 2025/S FCC-registered data set is a single-card unit that transmits and receives asynchronous serial data at up to 1200 b/s over the switched network and up to 1800 b/s over private lines. It features local and remote diagnostics such as local self test, remote test, and analoop test, and manual or automatic answer. A 5 b/s reverse channel and local copy on the primary and secondary channels are options.

CIRCLE NO. 369

Bypass leased line with remote entry terminal

Randel Data Systems, 365 Maple Ave., Torrance, CA 90503. (213) 320-8550. $4950 (1-qty); 60 days.

Remote sites can communicate with a central computer without using leased lines, through the FDSR diskette terminal. Link 100, 200 or 500 small business computers can interface with the terminal which has a file capacity of over 311,000 characters, organized as 2431 addressable lines of 128 characters each. Information is stored during the business day on a flexible disc. As necessary, the remote site calls the Link computer's location and confers with it at high speed. Access time is typically 0.3 s, and is 0.6 s maximum from keyboard or CPU to any line.

CIRCLE NO. 370

CIRCLE NO. 371
COMPONENTS

Sealed quartz crystals have tight tolerances

Quartz crystals for use in signal generating circuits of ultrasonic and other security systems equipment have frequency tolerances of +0.01%, -0.015%. The crystal is available in the frequency range from 17 to 150 kHz. Measuring 0.5-in. long, 0.14-in. wide, and 0.173-in. high, they are coldweld sealed for reliability.

CIRCLE NO. 372

Diffuse-scan photosensor sees over 6-ft range

Micro Switch, 11 W. Spring St., Freeport, IL 60021. (815) 285-5731. $118 (unit qty).

The MLS9A, a diffuse-scan, self-contained photoreceiver works at 850 operations/min and has a 6-ft range. The target returns the light beam to the photoreceiver without the need for a retroreflector. Moreover, in a retroreflective mode, the range is 50 ft. UL-listed, the control operates on standard ac line voltage from -40 to 70 C, and is made with monolithic ICs. Operational features include adjustable sensitivity, false-pulse protection and slide-switch-mode selection for dark operate/light operate. Two optional programmable-logic cards can provide up to five additional functions.

CIRCLE NO. 373

NEW 101C PULSE GENERATOR WITH 18V OUTPUT

Back in the days of 5V logic, the Datapulse 101 was the pulse generator. Now Systron-Donner brings you Model 101C with these updated features and accessories:

- Main output variable to 18V from 50 ohms
- 20 MHz rep rate
- Two simultaneous front panel outputs:
  (1) for TTL logic level, (2) a CMOS output for driving up to 40V pulses.
- Fixed rise time less than 10 nanoseconds
- Burst Generator accessory (1-999 pulses in length)
- Code Generator accessory (up to 4096 bits long)

Like its famous predecessor, Model 101C is an economical pulser, priced at $595 (U.S. only). For bench or systems applications, it will serve you faithfully for years. It’s a family tradition.

For details, contact Scientific Devices or Systron-Donner at 10 Systron Drive, Concord, CA 94518. Phone (415) 676-5000.

CIRCLE NUMBER 94

Time-delay packaged for relays and PCs

The Icsotimer, a miniature time-delay circuit, is compactly molded and easily adapted to PC designs or readily incorporated into relay packages. Time delay is adjustable from 0.1 to 300 s. Its all-solid-state hybrid network can switch standard relays and contactors with an accuracy of ±2% under fixed conditions. The circuit is available in ON and OFF-delay timing functions for input voltages of 120, 240 V ac, and 120, 24, 48 V dc.

CIRCLE NUMBER 374

ELECTRONIC DESIGN 19, September 13, 1977
Introducing the SR series, a family of miniature high-performance, power-switching inductors.

Our SR Inductors reduce size and weight. Now you have off-the-shelf power-switching inductors with performance advantages over your in-house capabilities. Low temperature rise and low loss characteristics combine to give the SR series high performance with maximum reliability. With an inductance range of 8 to 10,000 UH, a DC current range from .8 amps to 15 amps, SR Inductors have low losses in the 3 to 100 KHz frequency range, making them ideal for use in switching regulators and AC filter-choke applications.

Compact and easy to install, the SR family has pin terminals for mounting on PC boards. Available with double windings, which when brought out to four terminals permit series, parallel, center-tapped or transformer connections.

Available from stock in three sizes. Type SRA measures 7/8-in. OD by 7/16-in. height; SRB measures 1-3/16-in. OD by 9/16-in. height; and SAC measures 1-3/8-in. OD by 3/4-in. height.

Check your authorized TRW/UTC local distributor for immediate off-the-shelf delivery or contact TRW/UTC Transformers, an Operation of TRW Electronic Components, 150 Varick Street, New York, N.Y. 10013. Area Code: 212 255-3500.
COMPONENTS

Two-piece slide switch simplifies soldering

Chicago Switch, 1714 N. Damen Ave., Chicago, IL 60647. (312) 489-5500. $0.52 (spst) in (1000-qty); stock.

Wave-soldering operations are simplified by using a two-piece switch which prevents contamination from entering the upper half. Only the exposed base half of the 24-X40 series switch is soldered to the PC board, while the upper snap-action mechanism is attached after all cleaning processes are completed. Available in spst, spdt, dpdt and form-Z configurations, they are made with contacts of hard gold over a nickel barrier. The devices are designed for low energy applications with contact ratings of up to 1-A at 125-V ac or 12-V dc. Life expectancy is 50,000 actuations at 10 mA, and the operating temperature range is −40 to 100 °C.

Booth No. 1403

CIRCLE NO. 375

New relay data sheets offer detailed info

International Rectifier, 233 Kansas St., El Segundo, CA 90245. Martin Mintz (213) 678-5281.

A new type of technical bulletin provides users of solid state relays with detailed information on thermal characteristics, repetitive surge, fuse selection and duty cycle. Bulletin 500-11 is specifically for Crydom Series 3 relays, which are 2-A, 120 and 240-V-ac PC board mount devices. One area covered in depth by the bulletin is the overload capability of the devices. Conventional surge curves show only how much current can be handled on a non-repetitive basis. The new data show a series of curves relating peak surge current and overload time to the allowable number of surges. Other curves simplify fuse selection and provide data on devices that operate with less than 100% duty cycles.

CIRCLE NO. 376

Proximity-sensor line features cost economy

Turck Multiprox, 9710 10th Avenue N, Minneapolis, MN 55441. (612) 374-5000. From 816 (OEM qty.).

Six low-cost inductive proximity sensors and switches are completely encapsulated in tubular plastic housings (0.43-in. dia) and include removable mounting brackets. Switching ranges are to 0.078 or to 0.196 in. Two lower-range units may be flush-mounted in metal. They operate at from 5 to 24 V dc. Output switches handle either 12 or 24 V dc with a normally open npn output as standard (normally open pnp is also available).

CIRCLE NO. 377

Conductive plastic improves trimmer

Bourns Inc., 1200 Columbia Ave., Riverside, CA 92507. (714) 781-5140. See text.

An open-frame trimming potentiometer, Model 3355, provides performance specifications never before available in the under 20¢ industrial market, according to Bourns. Said to be the first conductive-plastic element on a plastic substrate, the unit has a contact-resistance variation of 1%; similar carbon units have 3 to 6%. Temperature coefficient is 500 ppm/°C compared to almost 1000 ppm/°C for competitive trimmers. And the conductive-plastic greatly reduces the tendency to develop holes in frequently set spots. The new trimmer has a resistance range of 100 Ω to 5 MΩ, is made of flame-retardant materials and is board washable, despite its open frame.

CIRCLE NO. 378

Visible to infrared covered by detector

Dexter Research Center, 7300 Huron River Dr., Dexter, MI 48130. (313) 426-3921. $60 (100-qty); stock.

The lM and 2M thermopile detectors provide spectral sensitivity from the visible to the far infrared. Both devices are hermetically sealed in either argon or nitrogen gas at atmospheric pressure, in TO-5 packages. The 1M has an active area of 1-mm dia with a peak responsivity of 25 V/W. Comparable figures for the 2M are 2 mm and 18 V/W. An infrared transmitting window is incorporated into the package, providing a field of view of 98°. Operating temperature range for the detectors is −65 to +85°C, and the maximum irradiance is 0.1 W/cm².

CIRCLE NO. 379

RC network series in epoxy dipped packages

TRW, 301 W. "O" St., Ogallala, NE 69153. (308) 284-3611. 8-10 wks.

Resistance values of up to 800 Ω, and capacitance values to 1 µF come in two-lead epoxy dipped packages. Designed as contact protectors for electromechanical switching systems, the packages contain a resistor and capacitor in series. The resistors have power ratings from 1/4 to 1/2 W, with a range of 100 to 800 Ω. The capacitors are metallized Mylar with voltage ratings from 100 to 400-V and capacitance values from 0.22 to 1.0-µF.

CIRCLE NO. 380
This digital thermometer is virtually indestructible...drop proof, shock proof, water proof, chemical proof, you name it. We have hurled it against stone walls, immersed it in boiling water for an hour, and submerged it for a week in a salt water fish tank without harming it. Its electronics are cast in silicon. Its teflon-coated probes and cables resist chemicals. It is so rugged that we confidently offer a 3 Year Full Warranty.

Tough, accurate, and versatile, spanning -100°C to 200°C and -150°F to 400°F, the T-Meter (with standard probe) achieves ±0.5°C (±0.9°F) accuracy over -55°C to 125°C (−67°F to 257°F). Optional high accuracy probes for special applications achieve ±0.1°C (±0.15°F), covering the MIL range in 20°C increments. You can supplement the standard 3' probe with lengths of 10', 25', and 100'. And you can special order lengths to 3,000'!


ECO CORP.
196 Broadway
Cambridge, MA 02139
(617) 661-4400

CIRCLE NUMBER 97
COMPONENTS

Ceramic caps handle 12 kVA of rf power

JFD, 15th Ave at 62nd St., Brooklyn, NY 11219. Gerald Kron (212) 331-1000.

Small ceramic capacitors in the UFP line can handle rf power levels of 12 kVA. The power handling capability is attributed to use of Hi-Q ceramic materials, glass encapsulation and monolithic construction using high conductive noble-metal electrodes. Capacitance values of 3.5 to 3,000 pF, with tolerances of ±0.25 and ±0.5 pF in the lower values, are available. Higher value capacitors have tolerances of from 5 to 10%. Small value capacitors—up to 150 pF—can handle up to 4,200-V peak, while a 300-pF device can typically handle 2,800 V. Temperature coefficient, in the temperature range from −55 to +125°C is 90 ± 20 ppm/°C.

CIRCLE NO. 381

Radiometer Electronics
Introduces
the specific generator

Spectacular quality FM and AM signal services at your fingertips.

An unsurpassed combination for AM, FM, FM Stereo receiver testing and design in R&D, Production, QC, and Service activities. We believe this combination provides the cleanest FM Stereo with the best separation, lowest distortion and greatest flexibility available today. These are just the highlights... like to know more? Contact us for additional information or a demonstration.

RE101 — RF GENERATOR...

Specifically designed for the radio industry.
- Digital display of carrier frequency in FM and AM specific ranges of 86 MHz to 130 MHz and 150 kHz to 30 MHz plus 10.7 MHz.
- Internal or external FM and AM modulation.
- Exceptionally low distortion; 0.05% FM and 0.3% AM.
- Low leakage RF output; continuously variable 0.1µV to 1 V rms.
- Built-in Sweep capabilities.

811 Sharon Drive • Cleveland, Ohio 44145 • Telephone (216) 871-8900
See these at WESCON Booth 1858.
CIRCLE NUMBER 98

Control tape loop with pressure transducer

Gulton SCD, 1644 Whittier Ave., Costa Mesa, CA 92627. Jim Pancake (714) 642-2400. $55 (1-qty); 4 wks.

The length of the tape loop in high-speed tape transports can be controlled by a transducer that senses differential air pressure. In the GS-503 pressure transducer, high level output dc signals result from differential pressures of ±2 PSID. Holes in the "slack" tape chamber allow the pressure to be sensed as the tape moves along, and the transducer outputs a signal to control the rotation of the tape reels. A solid state dc-dc converter in the transducer allows operation from 9 to 15 V dc sources. It is constructed with a diecast case which includes pressure fittings that accept standard 1/4-in. dia. tubing.

CIRCLE NO. 382

Thumbwheel switch mounts on PC board

EECO, 1441 E. Chestnut Ave., Santa Ana, CA 92701. (714) 835-6000. $0.09 per pin (500-qty); 5 wks.

Optional pin terminals on the 1800-series thumbwheel switches allow them to be mounted on PC boards. Pin terminal models are available in the following codes: 1-pole decimal BCD, BCD with complement, BCD complement only, BCD with diode provision and special 2-pole repeating codes. Dimensions of the pins are 0.025 in. square by 0.16 in. long, and board connections can be made by either hand or flow soldering.

CIRCLE NO. 383

Electronic Design 19, September 13, 1977
COMBINATION LENS AND MOUNTING DEVICE FOR T 1½ LED

REQUIRES NO TOOLS AND . . . .

INSTALLS IN 6 SECONDS
SIMPLE TWO-STEP INSTALLATION

SNAP CLIPLITE

INSTALLATION The CLIPLITE requires no tools; just snap it into a ¼" hole and insert the LED.

DESIGN The CLIPLITE design and color have been optimized through the use of selected red, clear, yellow, green, and amber plastics to provide exceptionally high contrast and visibility.

VISIBILITY The CLIPLITE permits up to 180 degrees of viewing angle using any standard T 1½ LED.

AESTHETICS The CLIPLITE gives any display or control panel the finished appearance equal to that of the most expensive indicator light assembly.

BRIGHTNESS The CLIPLITE allows the use of the much brighter narrow beam LED. Example: HP 5082-4657, 12 mcd @ 10ma vs. current popular wide beam LED HP 5082-4650, 2 mcd @ 10ma. Correspondingly, the amber and green narrow beam LEDS typically increase brightness by a factor of 4 over the commonly used wide beam LEDS.

ORDER YOUR TRIAL SAMPLE TODAY

Special Pricing for Trial Order Only

PLEASE SHIP: □ 100 CLIPLITES $10.00 □ LITERATURE

NAME

ADDRESS

CITY STATE ZIP

VISUAL COMMUNICATIONS COMPANY
P.O. BOX 986 EL SEGUNDO, CALIFORNIA 90245 (213) 822-4727

CIRCLE NUMBER 99
Hall-effect sensors shrunk to $\frac{3}{4}$ in.

Micro Switch, 11 W. Spring St., Freeport, IL 61032. (815) 235-5731. $2.10: 3AV $2.20; 4AV (100 qty).

Vane-operated position sensors, 3AV/4AV, are now only about $\frac{3}{4}$-in. long and include a standard 0.040-in. square Hall-effect IC chip on one side of the gap and a powerful rare-earth magnet on the other. The miniature vane sensors can function from zero speed to 100,000 operations per second. They are unaffected by dust, dirt or ambient light. Operate and rotate and release points are carefully controlled to tight tolerance. The vane sensor may be used as a limit switch by operating with a single large vane; as a tachometer sensor by using a toothed wheel, and as a machinery-synchronizing element by using a cam. The sensors may be interfaced directly with discrete transistors, $\mu$Ps, IC logic and SCRs. An 8- or 20-mA output eliminates the need for amplifiers in most applications. The 3AV needs a supply voltage of 4.5 to 5.5 V dc, and operates from 0 to 50 C. The 4AV series also uses 4.5 to 5.5 V dc, but three models of the series need 16 to 18 V dc, and the series operates from ±40 to 85 C.

CIRCLE NO. 386

Load cell is accurate and compensated

Celesco, 7800 Deering Ave., Canoga Park, CA 91304. Philip Ginders (213) 881-6860. $110 (1-qty).

Load cell is accurate and compensated. With an accuracy of 0.1% of full scale, the MB-101 series of load cells comes in seven models in ranges from 2.5 to 25 lb. The compensated temperature range for the device is from 30 to 130 °F. Temperature effect on zero balance and temperature effect on output are both spec’d at ±0.0008% of full scale per °F. The unit contains a four-arm Wheatstone bridge of etched-foil strain gages and can be supplied in either tension or compression. Deflection is approximately 0.002 in., with creep of less than 0.03% after 20 min., at full load. Overall operating temperature range is from -65 to +275 °F.

CIRCLE NO. 387

Relay series offered in power, low-level models

Oak Switch, Crystal Lake, IL 60014.

Dodi Almcrantz (815) 459-9000.

Two types of relays are offered in the type W series—a power contact type and a low-level model—with a combination of both contacts also available. Both styles are designed to operate at dc voltages of 6, 12, 24, 48 and 110, or ac voltages of 6, 12, 24, 115 and 220. Mounting options are plug in socket, or standard quick-connect terminals. The standard contact material is silver, with silver-cadmium-oxide or gold plate available as options. Power types have life expectancies of 10 million mechanical operations at 25 A resistive and inductive loads, ac and dc. Coil dissipation is 2.5-W dc and 7.5-VA ac, and operate and release time is nominally 25 ms.

CIRCLE NO. 388

Low-profile relays for dry-circuit systems

Omron, 238 S. Wacker Dr., Chicago, IL 60606. Frank Schwartz (312) 876-6800. $3.85-8.60 (100-qty).

Twenty-four models of low-profile relays designed to minimize contact resistance are offered in the LZN series. Though designed for dry-circuit applications in communications systems, the unit can switch up to 3 A at 24 V dc. Operating voltages of 6, 12, 24 or 48 V dc are available in two formats—dpdt or 4pdt. Typical power consumption in continuous operation is 300-mW for dpdt and 480-mW for 4pdt. Maximum operating time is 10 ms. All models measure 0.453 in. (H) by 1.201 in. (L) and fit PC boards mounted on 0.5-in. centers. The width varies with the contact configuration, being 0.87 in. for double-pole models, and 0.965 in. for four-pole units.

CIRCLE NO. 389
If you spend more than 20 minutes picking a P.C. connector

It's your guide to the broadest line of printed circuit connectors made by any single manufacturer. We have just about everything and in more combinations and more depth than anyone — more types of contact terminations, insulator materials, mounting styles, contact designs, types of plating.

Send for our catalog. Browse through it and you'll discover that picking out the right printed circuit connector for your job is as simple as it should be.

Quick delivery.

And you can get your hands on our connectors, too — in a hurry if need be. We keep a large inventory; so do our distributors.

Our "Whatever-you-need-we've-got" department.

As you can guess, we have a lot of tooling filed away. Our production engineers have a unique talent at taking an existing bit of tooling, fiddling with it, and turning out a "custom" connector that's exactly what you need. Your extra cost is only a modest set-up charge... a long way from a full retooling cost.

Use the coupon.

...you don't have this catalog.

Ok. Send me: □ Your latest printed circuit connector catalog.
□ ...and your nearest rep. I want to talk to him about a particular problem I have.

NAME: _______________________________ TELEPHONE: _______________________________

TITLE: _______________________________ COMPANY: _______________________________

ADDRESS: __________________________ ADDRESS: _______________________________

CITY: _______________________________ STATE: ___________ ZIP: ___________

Viking CONNECTORS
Viking Industries, Inc./21001 Nordinoff Street
Chatsworth, CA 91311 U.S.A./(213) 341-4330/ DATACON DIVISION

CIRCLE NUMBER 101
Complete microcomputer has printer and discs

INEX, 150 S. 600 E., Salt Lake City, UT 84102. Doug Hancey (801) 363-1177. $13,250; 90 days.

The “Total” microcomputer system, designed for use in stand alone applications, consists of a M6800 processor with up to 52 kbytes of RAM, an 80 x 25 character display monitor, a matrix line printer and a dual floppy-disc system. The system allows the user to program in Extended Disc Basic, and the disc operating system software includes a macro-assembler, editor, I/O handlers and variable length file handling.

CIRCLE NO. 390

No others quite measure up to MICROMATIC® Capacitors

CHECK THESE FEATURES
- Uniform self-encased construction
- Uniquely wound on their own leads
- Three versions available
  Polyester for broad applications
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Dual Dielectric with tight TC comparable to polycarbonate
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CIRCLE NUMBER 102

Frequency counter plugs into S-100 bus systems

International Data Systems, 400 N. Washington St., Suite 200, Falls Church, VA 22046. (703) 536-7373. $179 (kit); stock.

Precise frequency and period measurements controlled by a microprocessor are possible using the 88-UFC, a nine-decade universal frequency counter module. The counter includes provisions for four signal sources and the signal to be measured is selected under software control. Three of the inputs are general purpose and accept analog or digital signals. The fourth input accepts TTL level signals. One of the general purpose inputs includes a prescaler extending its range typically above 600 MHz. The other three inputs will typically count to 65 MHz, with 60 MHz guaranteed. An onboard crystal timebase is selectable under software control for count intervals from 100 ns to 1 s. For period measurement functions either half-cycle or full cycle measurement and the unit of measure may be selected under software control. Provisions are included for interrupts generated upon completion of a frequency count or period measurement. This option may be enabled or disabled under software control. Software is included to provide totalizing/accumulation, period measurement, time interval measurement, frequency measurement, and more, as well as storage for subsequent retrieval in ASCII, binary, or BCD.

CIRCLE NO. 391

Expanded SBC 80/20 board holds double the memory

Intel, 3065 Bowers Ave., Santa Clara, CA 95051. Rob Walker (408) 246-7501. $895 (80/20); $995 (80/20-4); 30 days.

The SBC 80/20-4, an updated SBC 80/20, provides twice as much resident memory as the original model. It has 4 kwords of read/write memory and up to 8 k of nonvolatile program storage. Also, the program memory capacity of the original SBC 80/20 has been doubled. Users now have the option of storing up to 8 kbytes of program along with 2 k of data, at no increase in price.

CIRCLE NO. 392

ELECTRONIC DESIGN 19, September 13, 1977
1. In high-frequency power switching, heat is a prime factor in transistor failure.

2. Turn-off time is the dominant cause of destructive temperature rise.

3. The faster the turn-off, the cooler the transistor, the greater the reliability.

Take a look at competitive transistors in an actual 20 KHz bridge converter circuit:

<table>
<thead>
<tr>
<th>Case Temperature Rise Above Ambient</th>
<th>°C</th>
</tr>
</thead>
<tbody>
<tr>
<td>TRW 2N6583</td>
<td>20</td>
</tr>
<tr>
<td>DELCO DTS-519</td>
<td>25</td>
</tr>
<tr>
<td>MOTOROLA 2N6547</td>
<td>30</td>
</tr>
<tr>
<td>RCA 2N6251</td>
<td>35</td>
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</tbody>
</table>

TRW delivers the lowest operating temperatures and the greatest reliability in high-frequency off-line switching regulators.

And that's no small thing. When you need superior performance at high frequencies, the best combination of switchtime and energy capability add up to greater efficiency and longer life. And what circuit are you about to design that doesn't deserve the best?

Particularly when TRW discretes are not only competitively priced, but are also immediately available in any quantity.

But get all the facts on TRW's high-frequency discrete transistors. Use the coupon or telephone John Power at (213) 679-4561.

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14520 Aviation Boulevard, Lawndale, California 90260

☐ Please send me data sheets on TRW's switching power transistors.

☐ Please send me samples for ______ voltage and ______ current.

Name

Company Name

Position

Address

City State Zip

ED
µP-based terminal fits on single circuit board

Mostek, 1215 W. Crosby Rd., Carrollton, TX 75006. (214) 243-0444. $195; stock.

Built around the MK 3870 single-chip microcomputer, the Video Adaptor Board (VAB-2) forms the heart of a simple video terminal. When connected to an ASCII keyboard, video monitor and power transformer VAB-2 forms a complete video terminal. The board offers a screen format of 16 lines of 64 characters (5 x 8 dot matrix), and a ROM character generator for 96 characters, including lower case letters. Full cursor controls are provided, including screen-clear, erase to end of line/screen, and direct cursor addressing. Output is EIA composite video and data rates of both 110 and 300 baud are supported with either 20 mA current loop or RS-222 interface compatibility. The VAB-2 operates from a 5 V dc on-board power supply and measures 14 x 5 in.

Booth No. 1608-10 CIRCLE NO. 393

16 kbyte memory board mates with S-100 bus

Solid State Music, 2102A Walsh Ave., Santa Clarita, CA 91390. (408) 246-2707. $525 (kit); $625 (assembled); stock.

A 16 k static RAM board, Model MB-7, allows for system expansion beyond 64 k and is fully buffered. The board, compatible with the S-100 bus, uses 32 4-k RAMs with 200 ns access times. Automatic memory unprotect and protect features allow the user to protect memory in 4 k blocks with automatic unprotect at power-on. The SOL microcomputer compatible memory disable allows the ROM monitor of the SOL to initialize the system at power-up or reset.

CIRCLE NO. 394

Rackmount computer has 18 slot chassis

Vector Graphic, 790 Hampshire Rd. A-B, Westlake Village, CA 91361. (805) 497-0733. $225 (chassis); $90 (supply); stock.

A rack-mount version of the Vector 1 microcomputer includes card cage and 18-slot motherboard assembled and tested with 18 connectors, card guides and locking buttons for 18 cards. The motherboard is fully shielded to reduce noise on the bus. A heavy duty modular power supply is also available. The 18 A at 8 V, 2.5 A at ±16-V unit provides sufficient unregulated power for all 18 boards. Primary taps on the transformer permit line voltage of 110, 120, and 130 V.

CIRCLE NO. 395

Disc operating system aids PACE development

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. (408) 737-5000. $4,500; 30 days.

The IPC-16P/840, a disc-operating system (DOS) for the PACE microprocessor, simplifies the assembly, editing and execution of programs. Including a dual-floppy disc drive in a stand-alone enclosure, an interface circuit subsystem card, a ROM card containing firmware, the system comes with complete operating software on a diskette. The software includes a comprehensive file management capability, support for assembly programs, editors, linking loaders, utility programs and diagnostics. The system may be installed on any Z80-based microcomputer development system with 12 kwords of RAM and heavy-duty power supply.

CIRCLE NO. 396

EPROM programmer kit uses system software

Mini Micro Mart, 1618 James St., Syracuse, NY 13203. Maury Goldberg (315) 422-4467. From $24.95; stock.

The 3164-1, an EPROM programmer kit, is intended to program the 2708 series of EPROM. The newer (2 k X 8) Intel and TI devices can also be accommodated. Originally designed to function with the company's series of RM 8080 and Z-80 systems, the programmer is equally effective on any system that has available three latched parallel I/O ports. The programmer is software driven from the user's processor. Some software routines are included and are intended to run with a system monitor provided by the company. The user may need to tailor the software to his own operating system. A power supply kit is also available. The supply provides the regulated +12, +5, and -5 V, and a source of de for program pulses in excess of 25 V de.

CIRCLE NO. 397

Microcomputer board designed around Z80

Quay Corp., P.O. Box 386, Freehold, NJ 07728. R. Maly (201) 681-8700. $500 (100 qty); stock.

The 90 MPS, a single-board Z80-based microcomputer includes 6 kbytes of memory. Of the 6 k, 4 k is dynamic RAM, 1 k is static RAM, and the other 1 k is a monitor held in 2708 UV PROM. Two Z80 parallel I/O chips provide four parallel I/O ports. Also on board is a UART with RS-232C and 20-mA current-loop interfaces, a 2.5-MHz crystal clock, a Z80 counter/timer circuit, and a PROM programmer for 2708 type UV PROMS. The microcomputer measures 16.175 x 6.875 in. All I/O is via three 60-pin flat-ribbon connectors. The dynamic RAM can be expanded to 65 k and a total of 7 k of 2708 UV PROM can be installed on the board. Sockets are also provided to permit two more Z80 PIO chips. An option for 4 MHz operation is also available.

CIRCLE NO. 398
Meet our better half.
The New TI .156" x .200" H4 Series Edgeboard Connector.

Our better half from T.I. It's the edgeboard connector half of a PC board/edgeboard connector system. And definitely today’s best value.

Its minimum 75 microinches wrought-gold inlay provides greater reliability at contact mating surfaces to make our better half better.

Its bifurcated contacts provide greater connection reliability to make our better half better.

Its between-position polarizing key system allows more efficient use of the connector to make our better half better.

Its off-the-shelf availability through our extensive nationwide distribution network makes our better half better.

Its construction, designed to meet or exceed demanding military performance specifications (MIL-C-21097), makes our better half better.

Its bifurcated contacts provide greater connection reliability to make our better half better.

Its between-position polarizing key system allows more efficient use of the connector to make our better half better.

Its bifurcated contacts provide greater connection reliability to make our better half better.

Its between-position polarizing key system allows more efficient use of the connector to make our better half better.

Its glass-filled thermoplastic polyester contact housing meets U.L. Flammability Classification 94V-0 to make our better half better.

Its practical design coupled with our low, low prices (as exemplified by our low cost IC’s) make our better half better.

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Its practical design coupled with our low, low prices (as exemplified by our low cost IC’s) make our better half better.

Its functional and dimensional interchangeability with common one-piece edgeboard connectors gives you price and delivery advantages and makes our better half better.

Its termination and mounting flexibility, including both solder tail and solder eye terminations, as well as flush or earless mounting, make our better half better.

Its glass-filled thermoplastic polyester contact housing meets U.L. Flammability Classification 94V-0 to make our better half better.

Its practical design coupled with our low, low prices (as exemplified by our low cost IC’s) make our better half better.

Its glass-filled thermoplastic polyester contact housing meets U.L. Flammability Classification 94V-0 to make our better half better.

Texas Instruments Incorporated
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□ For an immediate application.
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You've got our number! Dial it now, toll free, if you want to talk about special enclosures, (800) 321-1764; in Ohio, (800) 362-2265.

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**Interface board joins Pace to floppy drive**

Abler Data Service, 740 Garvenus Ave., Brookfield, WI 53005. Joseph Abler (414) 766-2448. $300 (board); $200 (PROM); stock.

Able to mate a Pace µP to an ICOM floppy disc system, a DOS-II interface card accepts the disc-controller cable on one end and the Pace system bus on the other. The card uses the 16-bit commands of the Pace and the 16-bit data words to speed the transfer. A typical IBM format diskette can be read or rewritten in 75 s. DOS-II monitor listings are included. The controller can support from one to four drives. An optional PROM-based bootstrap and the monitor on diskettes are also available.

CIRCLE NO. 399

**Video interface board mounts in S-100 bus**

Vectron, P.O. Box 20887, Dallas, TX 75282. John McCrady (214) 350-5291. $185 (assembled and tested), $155 (kit); stock.

Requiring just the unregulated 7 V dc from an S-100 bus system, the SCT-100 provides a video output for data display on a terminal. The board includes both ASCII and Baudot serial interfaces, and requires only the addition of a standard ASCII encoded keyboard and a TV monitor. Designed around the 3870 single-chip microcomputer, the board includes full X-Y cursor control (both absolute and relative), screen clear, clear to end of line, page mode and autoscroll, 96 displayable characters, 16 line by 64 character display, plus multiple baud rates up to 300 baud. For stand-alone applications an on-board rectifier and filter permits the operation of the board directly from an external 6.3 V ac, 1 A transformer.

CIRCLE NO. 403

---

**Communication processor handles up to 9 channels**

Micro Systems, 9551 Irondale Ave., Chatsworth, CA 91311. Roger Evans (213) 882-6890. From $880; 45 days.

The 20 Series communications processor is a completely self-contained communications-oriented microcomputer system. Built around the 286, the 20 Series consists of the CPU, up to a 19-k RAM buffer storage, up to 8-k PROM control firmware, up to nine communications interfaces, and integral operator's console. The 20 Series processor is normally supplied in turn-key communications controller systems complete with firmware to perform customer-specified communications network functions. It is also available to OEMs with a complete program development system to facilitate firmware development.

CIRCLE NO. 404

**Disc operating system supports multiple users**


The muPro-80D a multitask disc operating system can support multiple users. Combined with the firm's MUTE software, the system keeps costs low because a single microcomputer and floppy disc can be used with multiple terminals rather than having multiple microcomputers. The system consists of a dual disc drive and the company's µPro-80 computer. The full system with enough memory (48k) to handle two terminals costs $9750. Another 16 k of memory costs $800 and permits the system to be used with four terminals. Delivery is 30 days.

CIRCLE NO. 405

---

**An extra “special” offer! Win a trip to the next Super Bowl!**

Circle Bud's number on the reader service card and we'll mail you a brochure on our special fabrication service and an entry form for our Super Bowl Sweepstakes!
You're probably very happy with your Burroughs mainframe. But you'd undoubtedly like to have the versatility and dependability of Lear Siegler terminals. If only they were compatible with your present system.

Now they are. Complete with standard Burroughs polling and address line disciplines.

What's more, the ADM-2B's forms mode capability is compatible with the TD-820.

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Line diagnostic mode is switch selectable—which makes it extremely valuable for troubleshooting.

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That's the full price. Including serial printer port. Numeric keypad. 24x80 character screen. 16 function keys. 110-9600 baud. RS232 interface. Burroughs two-wire direct connect is available as an option.

The fact is, Lear Siegler's new ADM-2B terminal gives you the best of both terminals. So you can use it right alongside your present Burroughs terminals and mainframe.

So rest easy, Burroughs users. Because now Lear Siegler speaks your language.

For more information contact:
When it comes to the application of conductive plastic potentiometers or elements in servo feedback systems for recorders, controllers, and actuators, Waters wrote the book.

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plug-compatible reader

Reader with serial asynchronous RS-232C compatible interface. Designed to utilize ASCII defined control codes and operate with a terminal device on the same serial data lines or alone on a dedicated serial line. Reader will generate data at all standard baud rates up to 2400 baud.

Four modes of operation are possible:
- **Auto Mode I** — Simulates ASR-33 Teletype Reader using ASCII defined data codes DC 1 and DC 3 to activate/deactivate the reader;
- **Auto Mode II** — Utilizes RS-232C defined Clear-to-Send Signal to activate/deactivate the reader;
- **Auto Mode III** — Reader is activated/deactivated by DC code or the Clear-to-Send Signal;
- **Manual Mode** — Code transparent mode where panel alone activates/deactivates the reader.

High-speed, compact, with self-contained electronics and power supply. Complete in attractive noise dampening housing.


The Microemulator, an in-circuit emulator/EPROM programmer, can handle the 2704 and 2708 EPROMs. The unit extends the editing, assembling and debugging capabilities of the company's 8080/6800/Z-80 product development systems. A cable from the Microemulator plugs directly into a prototype's CPU socket and allows debugging of the prototype in its own environment. Programs residing in the microcomputer's RAM memory can execute and access the memory and I/O devices, emulating actual usage. In addition to basic monitor commands, provision is made for single step and trace execution, hardware breakpoints and 2708/2704 EPROM programming. The complete system package consisting of an M8-40 Microemulator and M8-41 debug and EPROM programmer costs $1250.

Microcomputer Systems, 140 Oakmead Parkway, Sunnyvale, CA 94086. (408) 733-4200. $195 (unit qty); stock.

A terminal-resident, microprogrammed disc controller interfaces the HP 2646A, 41A, 49A intelligent terminals with up to four Ampex DM 440 series disc drives. These drives provide 40 Mbytes of on-line disc storage. The heart of the disc interface is the MSC-264X, a 13 x 4-in. microprogrammed controller. In addition to the I/O commands necessary for terminal-to-disc data transmissions, the controller is equipped with firmware diagnostic routines.

Disc controller connects
4 drives to HP terminals

ELECTRONIC DESIGN 19, September 13, 1977
Debug tool handles both hardware and software

RCA, Box 3200, Somerville, NJ 08876. (201) 685-6000. $1600; stock.

The Cosmac Micromonitor permits in-circuit debugging of any CDP1802 microprocessor system's hardware and software in real time. The CDP18S030 Micromonitor includes a built-in keyboard, display, and status indicator lights, as well as software debugging routines. A self-test card simulates a user system to allow verification and assurance of Micromonitor operation. A single cable connects between the CPU of a system under test and all the interfaces. Controlled by its own built-in microprocessor, the Micromonitor uses the CPU, power supply, clock, memory, etc. of the system under test to run a user program. It can be operated either from its own keyboard or from an external terminal if a hard-copy record is desired. Remote operation from a floppy disc file is possible when the Micromonitor is used with the Cosmac Development System II (CDP18S005). The Micromonitor provides 43 commands that permit the user to examine or modify memory and all CPU registers and flags. Break conditions can be programmed for: external flag lines, auxiliary break input, idle, interrupt response, or memory read/write. Three modes for running programs are available. One mode provides for real-time running, starting at a specified address or continuing from a break. Another mode provides for single or a specified number of instruction cycles. The third mode provides for a single or a specified number of machine cycles to be executed.

Booth No. 707-709

CIRCLE NO. 408

ROM-based Basic does floating point math

Electronic Arrays, 550 E. Middlefield Rd., Mountain View, CA 94043. John Lipinsky (415) 964-4321. $95 (1 to 24 qty); stock.

The EA3280 LLL 8080 Basic interpreter is solid-state software. It is a set of two (4 k x 8 ROMs) containing a 6 k Basic routine with floating point, TTY I/O, memory check and ODT-80 monitor routines. It is a high-level, easy-to-use language for use in an 8080 microprocessor system. The EA3280 chip set comes with an application note, assembly listing and user's guide.

CIRCLE NO. 409

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FEATURE MODEL 100A/10 HP-1607

Trigger Word 24 bits 16 bits

Data Displayed 3 bytes by 16 words deep (1 byte x 16 at any one time) 2 bytes by 16 words deep

Data Collection Pre- and post-trigger Pre- and post-trigger

Display Mode Single/Repeat Single/Repeat

Display Format HEX/OCTAL HEX/OCTAL

Qualifiers 2 (both trigger word & clock) 2 (trigger word or clock)

Digital Delay 999 clock pulses or 999 trigger words 9999 clock pulses only

Data Collection Rate 8 MHz 20MHz

External Scope Req'd Yes Yes

Auxiliary Memory No Yes

Map Mode No Yes

External Trigger Output Yes Yes

Logic Family Compatibility All but ECL All

Modularly Expandable Yes Yes

Intensified Trigger Word Yes Yes

Weight 7 pounds 14 pounds

Power 10 watts 120 watts

PRICE $599.95 complete $2900.00 plus probes

WHAT IF YOU DON'T NEED ALL THAT CAPABILITY RIGHT NOW? Fine. Start with the Model 100A Logic Analyzer and save over 50%. You'll find that the Model 100A is a powerful 8-bit logic analyzer in its own right. Then add the mating Model 10 expander unit for an additional 16 bits when you're ready. (An optional baseplate locks the two units together.) Incidentally, if you have a few spare hours, purchase the kit versions and save another 25% per unit.

WHAT ABOUT DOCUMENTATION? We've got it. The Model 100A and Model 10 each come with a comprehensive 100-page instruction and applications manual. In fact, if you want to see how well these units can satisfy your application, buy the manuals first for $4.95 each.

For additional information or a demonstration, contact your local PARATRONICS, Inc.

SALES OFFICES: AL, Huntsville (205) 533-5896; AZ, Phoenix (602) 253-6104; CA, Costa Mesa (714) 539-7160; Sunnyvale (408) 733-8600; CT, Canton Center (203) 693-0710; FL, Winter Haven (813) 294-5815; HI, Waikiki (808) 902-2152; IL, Elk Grove Villa (312) 695-7288; IN, Indianapolis (317) 293-9827; MD, Silver Spring (301) 623-4200; MA, Watertown (617) 245-9804; MI, Northville (313) 482-1229; MN, Minneapolis (612) 781-1611; NM, Albuquerque (505) 268-3941; NY, Syracuse (315) 446-1264; NC, Raleigh (919) 787-5818; OH, Centerville (513) 433-8171; Cleveland (216) 331-3900; OK, Tulsa (918) 299-2859; PA, Hatboro (215) 674-9600; TX, Houston (713) 461-4487; U.K., Bracknell Berks (0344) 53929.

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- OEM MODULES
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- PORTABLE DC

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Watertown, MA 02172
TEL: (617) 924-1010
CIRCLE NUMBER 119

Packaging & Materials

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Indium Corporation of America, P.O. Box 269, Utica, NY 13503. (315) 797-1630. $25 (unit qty).

An experimental indium plating kit tests indium plating on sample or prototype parts or surfaces. Each kit includes one liter of indium sulfamate bath, two anodes (1 x 12 x 0.030 in.) of 99.99% pure indium metal, and the new Indium Plating Guidebook. Indium is an excellent plating material for surface protection and hardening, decorative finishing, corrosion and wear-resistance of electrical contacts, and much more.

CIRCLE NO. 410

NiCd battery replaces rectangular 9 V dry cell

Sanyo Electric, 51 Joseph St., Moonachie, NJ 07074. H. Tamada (201) 841-2333. $9.95 (unit qty). See text.

A 9-V nickel-cadmium battery is offered in the popular rectangular case and a compact recharger accommodates it. The Model 6N-75P has a nominal capacity of 75 mAh. It can be recharged as many as a thousand times. The recharging unit ($5.50) holds a single battery, which recharges in 7 to 8 h.

CIRCLE NO. 411

D-shelled connectors mass terminate speedily


Mas/Ter-D pin-and-socket connectors for high-speed mass termination with 25 and 37-position contact arrangements are fully intermateable and intermountable with the Cannon D-subminiature series. This system terminates round-conductor flat cable or discrete wires. Connectors handle the wire ranges 22 through 24 AWG and 26 through 28 AWG, solid and stranded. Copper-alloy contacts are plated with gold over nickel; insulation is glass-reinforced thermoplastic, meeting the flammability requirements of UL 94 V-O. The steel shells are cadmium, chromate conversion plated. The connector has a dielectric-withstanding voltage of 1000 V ac, an insulation resistance of 1000 MΩ minimum and contact resistance of 15 mΩ after environmental testing. The operating temperature is −55 to 105 C.

CIRCLE NO. 412

Silicone-rubber contacts actuate CMOS circuits

Tecknit, 129 Dermody St., Cranford, NJ 07016. R. Ventimiglia (201) 272-5500.

Switch contacts, called ESCONs, made from high-temperature cured silicone rubber filled with conductive particles, provide a resistance of less than 300 Ω. The contacts can operate with high-impedance circuits (CMOS) to turn on 20-to-100-µA logic circuits. Silver-filled ESCONs are available for high-current (15-to-30-mA) applications. The typical silver contact has a nominal contact resistance of less than 0.3 Ω. ESCON was developed for the pushbutton switches used in digital electronic watches.

CIRCLE NO. 413

Electronic Design 19, September 13, 1977
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Strips for Faster and Easier solderless circuit building and testing. No special patch cords are required, and any solid wire up to No. 20 AWG can be used for connection. Strips accept all components with leads up to .032" diameter, and hardware and mounting templates are provided with every strip. Terminals are non-corrosive nickel/silver.

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CIRCLE NUMBER 120

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cable strain relief

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From $0.12 (1000 qty).

 Self-locking Blue Macs cable clamps
bundle flat flexible cables without special
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are adjustable, reusable and releasable
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with screw or adhesive-mounting bases
for bundling cable from 0.5-to-1-in high.

 CIRCLE NO. 414

E cores automatable
with round center legs

 Stackpole Carbon Co., St. Marys, PA
15857. (814) 781-1234. $210-to-
$450/1000; 4 to 5 wks.

 E cores for switch-mode power sup-
ply applications are now available with
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new cores may be specified in sizes
ranging from 35 to 70 mm. The materi-
al is popular for the energy-saving
power supplies because of its low core
loss and high-permeability character-
istics.

 CIRCLE NO. 415

Packaging systems

 A 60-page catalog covers micro-
electronic packaging systems and
hardware. Mupac, Brockton, MA
CIRCLE NO. 416

Synchro converters

 A 30-page catalog describes synchro
converters, displays and encoders.
Computer Conversions, East North-
port, NY
CIRCLE NO. 417

GGG substrates

 Material advances in gadolinium
gallium garnet (GGG) substrates for
magnetic bubble memory devices are
described in a four-page brochure. Un-
ion Carbide, San Diego, CA
CIRCLE NO. 418

Capacitor motors

 Capacitor motors and their per-
formance as a function of capacitance
are featured in the current issue of
Motorgram. Bodine Electric, Chicago,
IL
CIRCLE NO. 419

Test instruments

 Digital multimeters; communica-
tions and CB instruments; oscilloscope
and power supplies; transistor and
tube testers, and TV and radio service
equipment are described in a series of
five bulletins. Sencore, Sioux Falls, SD
CIRCLE NO. 420

Active filters

 Electrical specifications complete
with tabulated amplitude and phase
data and mechanical dimension draw-
ings of 10 active filter families are
given in a 36-page catalog. Frequency
Devices, Haverhill, MA
CIRCLE NO. 421

"Visit our booths 1132 and 1134 at the
WESCON Show"
CIRCLE NUMBER 123

Electronic Design 19, September 13, 1977
Microceram represents a major advance in the state-of-the-art of multilayer capacitors. Precise shape factor and technical performance data make Microceram units ideal for microwave circuitry applications. Their high Q performance persists even at high frequency, high power, high current and high ambient temperatures. Available as chips, pellets and leaded devices.

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**Miniature lamps**

A 40-page catalog has 70 new lamps listed, including 38 halogen-cycle lamps and 19 wedge-base lamps. Drawings, data, and specifications are arranged according to bulb size from 7/16 dia up to 2-1/16-in. dia. General Electric, Miniature Lamp Products, Cleveland, OH.

**Dc power supplies**

Performance capabilities of the company's high-reliability, low-voltage dc power supplies are outlined in a brochure. Elexon Power Systems, Santa Ana, CA.

**Volsensors**


**Coaxial relays**

Specifications, charts and drawings of coaxial relays are featured in a 28-page catalog. Magnecraft Electric, Chicago, IL.

**Data, memory products**

Data and memory products are covered in an eight-page brochure. Ampex International, Reading RG1 7XY, England.

**Rotary solenoids**

The Magton family of dc voltage rotary solenoids is described in a six-page brochure. Technical drawings are included. Oak Switch Div., Crystal Lake, IL.

**Card-edge connectors**


**Interface circuits**

A 576-page linear-IC catalog, "The Interface Circuits Data Book," provides information on line drivers, receivers and transceivers, memory drivers, MOS-interface drivers, sense amplifiers and peripheral drivers. The book costs $4.75. Postage and taxes will be added to invoice. Texas Instruments, P.O. Box 5012, MS 54, Dallas, TX 75222.

**Temperature controllers**

The full line of LFE temperature controllers, sensors and accessory equipment is described in a 32-page catalog. It also features an applications guide. LFE, Process Control Div., Waltham, MA.

**Recorder**

A six-page brochure describes the Brush 2800 high-performance, eight-channel, direct-writing recorder for industrial, scientific and biophysical use. Gould, Instrument Systems Div., Cleveland, OH.

**Terminals**

Hundreds of terminals, splices and disconnects are covered in a 60-page catalog. In addition to photographs, the catalog has dozens of drawings, charts and graphs. ITT Cannon Electric, Solon, OH.

**Optical waveguides**

Specifications and characteristics for four Corugide optical fibers are included in a six-page bulletin. Corning Glass Works, Corning, NY.

**Data-entry terminals**

The IC Switching Regulator that has everything!

The Ferranti Model ZN1066E Pulse Width Modulator for use in:
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Features:
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AIRPAX

CIRCLE NUMBER 135

Electronics Design 19, September 13, 1977

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CIRCLE NUMBER 136
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Mechanical linking of all switch positions prevents operation of more than one position at a time. A released button will return to the "up" position before the next button can be actuated. These switches can be illuminated either by an external circuit or directly from the switch. Lamps do not travel when positions are engaged, eliminating shock to the bulb.

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CAPITOL switches are rated at 3 Amps, 110 Volts AC, non-inductive.

CAPITOL manufactures a complete, high-quality line of push button and lever switches—illuminated if desired—standard and custom designs to fit your every need.

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**Bulletin board**

**Microcomputer Rentals** has expanded its line of microcomputer-hardware-development equipment with the addition of the Intel Intellec MDS. CIRCLE NO. 435

The **Electronic Product Associates Micro-68b floppy-disk system** includes a disc-status-monitoring panel and write-product switches. The disc includes an interface to plug into the 6800 Exorisor or the 8080 S-100 bus. CIRCLE NO. 436

**Teledyne Relays’ JMJ640 solid-state-relay series** has received QPL approval to MIL-R-28750. CIRCLE NO. 437

**Optran** has been granted JAN TX approval for its JEDEC 4N22, 23 and 24 devices. CIRCLE NO. 438

**Wintek** has lowered the price on its 16-kbyte Wince RAM module to $399 from $889. CIRCLE NO. 439

**DEC's Computer Special Systems Group** has reduced prices from 13 to 22% for its TJU45 and TWU45 nine-track magnetic tape subsystems for PDP-11 computers. CIRCLE NO. 440

**Precision Monolithics** has reduced prices of its 8-bit d/a converters in 100-999 qty as follows: DAC-08A from $20 to $17; DAC-08Q from $7.95 to $6.75; DAC-08HQ from $9.95 to $8.20; DAC-08EQ from $5.50 to $3.95; and DAC-08CQ from $4.50 to $3.45. CIRCLE NO. 441

**Shugart Associates** has reduced prices 15% on its SA400 minifloppy disc drive. The price drops from $250 to $215 (500 OEM qty). CIRCLE NO. 442

**Hewlett-Packard low-noise microwave-transistor** prices have been reduced up to 37%. CIRCLE NO. 443

Prices have dropped about 12% on selected **Hewlett-Packard multiprogrammer-system components**. CIRCLE NO. 444

**Motorola** has a mil-temp version of its M6800. It is identical to previous M6800 products in electrical and software specifications. CIRCLE NO. 445

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**Annual and interim reports** can provide much more than financial position information. They often include the first public disclosure of new products, new techniques and new directions of our vendors and customers. Further, they often contain superb analyses of segments of industry that a company serves.

Selected companies with recent reports are listed here with their main electronic products or services. For a copy, circle the indicated number.

**San Fernando Electric Manufacturing Co.** Inductors and monolithic ceramic capacitors. CIRCLE NO. 446

**Scan-Data Corp.** Optical character recognition systems, key entry systems, data center services, field service engineering. CIRCLE NO. 447

**SRC Laboratories, Inc.** Photomultiplier tubes. CIRCLE NO. 448

**Western Union International.** International and domestic record communication services. CIRCLE NO. 449

**Engelhard.** Ores, minerals and metals. CIRCLE NO. 450

**SRI.** Research and development. CIRCLE NO. 451

**Medgeneral.** Medical electronics. CIRCLE NO. 452

**Data 100 Corp.** Multifunction terminal systems. CIRCLE NO. 453

**Pathcom.** CB radios. CIRCLE NO. 454

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(continued from page 16)

this chemical and its promoters shows it to be a fraud. The chemical plainly does not work. It has no objectively beneficial effects. The theory on which its use has been based is anti-scientific garbage. Many, many times the chemical has been shown to be absolutely, completely useless.

Every five years or so, a new fraud in the treatment of crippling or fatal diseases hits the world press. A standard tactic used by unethical promoters is to accuse the medical establishment of repression. Gradually real evidence comes in; the new wonder drug is firmly discredited; and the promoters retire with their millions, or find a new chemical.

The only defensible argument for allowing the use of laetrile is that it makes some people feel better. This is a more difficult question in philosophy than can be profitably argued in an electronics magazine, but I put it to you that the effects of laetrile can be duplicated by distilled water and so depend on psychological effects. Is it really in our best interest to allow the use of a chemical whose effectiveness depends on the ignorance of the patient? What are the consequences of having irrational behavior becoming more dominant in our societies?

A final word on the ethics of editorials. You seem obsessed with professionalism this last year. A professional engineer is supposedly trained in the scientific method. This means he should know something about the nature of science, the role of theory, and the importance of evidence. Except on the aforementioned utilitarian grounds, a scientist must remain skeptical. You have disgraced yourself as a spokesman of science. Remember your editorial five years from now.

Vaso Bovan

Engineering Science
University of Western Ontario
London, Canada

If we accept the premise that you are qualified to evaluate laetrile, then your editorial should have concluded with an invitation to the medical community to evaluate fiber optics, bubble memories and single-chip microprocessors!

And if you are saying that every new advance should be universally adopted upon announcement, then where would be the responsible, methodical testing that gave us proven semiconductors and other components that could safely carry living men to the moon and back?

The only cancer patient I know of who took laetrile was not helped in any way. She died a few months afterward.

"Why beholdest thou the mote that is in thy brother's eye, but considerest not the beam that is in thine own eye?" (Matt 7:3)

Jay C. Sinnett

Wakefield, RI 02879

Your editorial is an example of unprofessional journalism at its extreme. Your conclusions are without fact, and you, as an electronics-engineering journalist, are not competent to pass the judgments reflected there.

There is no scientific evidence that laetrile is a vitamin. By what authority do you call it vitamin B17? Second, are you aware that laetrile releases concentrations of cyanide, a highly toxic substance, into the bloodstream? Third, there are no controlled studies to show that laetrile has analgesic properties.

As for its acceptance in 26 countries, dictatorship is accepted in many more. Do you recommend dictatorship for the US?

Further, there are drugs that are partially effective in treating human cancers. No such drugs have failed to demonstrate tumor reduction in laboratory animals. Medical researchers consider it unethical (and properly so) to conduct clinical trials of drugs on humans without first having some success in using the curbs on laboratory animals and in demonstrating what risks, if any, are likely in using the drugs on humans.

I feel that you have become a victim of the so-called "Freedom of Choice" movement, which is being promulgated by laetrile profiteers. Do you know of the millionaires that have been made by laetrile promoters? I certainly hope that your technical articles, upon which I depend, are researched more carefully than this editorial.

Incidentally, a recent issue of Consumer Reports contains an excellent summary of a more rational view of laetrile and its quackery.

A. Brinton Cooper, III, Ph.D.
Bel Air, MD 21014

Three points: First, you're not qualified to judge the technical merits/demerits in the laetrile controversy.

While you're certainly entitled to take a personal position on emotional grounds, voicing your feelings as you have done before all but the most skimpv evidence has been brought in

(continued on page 190)
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CIRCLE NUMBER 143
and weighed is beneath someone in your position of editorial responsibility.

Second, you do an injustice to the medical profession by claiming that it has selfishly sought to prevent widespread acceptance of things beneficial to humanity ("...those who allowed thousands to suffer and die..."). There is no support for this nonsense, and to the contrary, it cannot be doubted that the medical profession can rightly claim its share of credit for many of the blessings of good health we enjoy today. The list is very long, but surely you have heard of Jenner, Pasteur, Reed, Fleming, Banting, Salk, etc. Once again, your attack demeanes your office and your publication. (And where were you when the FDA banned thalidomide?)

Third, and most important, the engineering profession should emulate the medical profession, not denigrate it! It's nice to have the great interests of all mankind at heart, but charity begins at home! I most respect the medical profession for looking out for #1, and despite occasional grumblings from the general populace (such as your editorial), most everyone else does, too. It's high time engineers snap out of it and stand up for their own interests. Before you lash out at the medical profession again, you tell me this:

How many engineers show up at work to find a waiting room full of clients? And how many engineers have an income even close to the median income for physicians? How many physicians were laid off their jobs this year? And how many physicians are still unemployed from the year before? Do physicians worry about wage-busting, as engineers do? How about physicians past their 30's...do they worry about becoming obsolete, of being replaced by interns fresh out of med school? How many engineers increase in value with age the way physicians do? WHERE'S OUR LOBBY IN CONGRESS?

"Professionalism"? It's just a fancy word for plain old Respect! The medical Profession? Hell! Plumbers are more professional than engineers! Respect is the issue. Respect comes down to dollars and cents. I'd rather be a rotten S.O.B. with a good, steady income and some solid security than that really hard-working Nice Guy who's out of a job, broke, and standing in the unemployment line. You bet I want that kind of professionalism! Would it be so bad if engineers had at least some say about what happens to them? About how fast the job market is being flooded with new engineers? And especially about how fast the semiconductor manufacturers can make them obsolete?

I don't think so at all.

Mitchell D. Brody, Ph.D.
Brookline, MA 02146

Editorial was great

I appreciate your remarkable editorial on professionalism and laetrile. Never before have I seen you write so clearly on so heated an issue. I applaud wholeheartedly.

There isn't much I can add to the penetrating assessment, except to call attention to the underlying (and false) philosophical premise without which elitism would receive little intellectual support. That premise is: the anti-conceptual view of man.

We are told by doctors who want to ban laetrile that people won't follow their medical advice voluntarily. That is an open admission of professional failure. I wonder if it has occurred to those doctors that their medical judgment might receive far greater respect from the public if those doctors were not so reckless in their advocacy of physical force and so eager to avoid having to reason with people. It is as if laymen are viewed in the same category as laboratory animals—not just physically, but mentally too.

Originally a substance could be banned only if it was extremely dangerous—too dangerous to be used, even in small quantities. Laetrile certainly doesn't fall into that category. Even if laetrile consumption were as harmful as staying in the sun too long or eating uncooked meat, still it would be nowhere near as dangerous as implied by attempts to ban it.

Today, of course, substances can be banned if there is a statistically measurable probability, no matter how small, that laboratory animals will get cancer when forced to ingest massive doses. In other words, big doses carry a small risk of cancer, as big doses carry a small risk of death. No probability is too small if it is statistically significant. In other words, medical professionals are deceiving the public by projecting the cancer risk of massive doses of laetrile into the death risk of moderate doses. It is as if we were to project the death risk of a small bullet wound into the death risk from a small cut. A mere statistical risk is all that is required, and the medical profession must be charged with deceiving the public about the dangers of massive doses.

(Circle number 145)

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CIRCLE NUMBER 152

(continued from page 190)

ual has the mental capacity to resolve such questions, not even with advice sought from a doctor.

At first glance, the "big dose, small risk" rule doesn't seem to apply to laetrile, since laetrile isn't a cancer cause and may even be beneficial in cancer treatment. If our premise is to do everything possible to fight cancer, then we ought to legalize laetrile immediately. Yet, incredibly, opponents of laetrile are using that same premise to urge a ban. They are trying to extend the premise to include psychological as well as physiological factors, as if man's mental condition (including one's opinions of doctors and laetrile) were as unconsciously determined as his physical condition. The unreality of that view of man is matched only by the destruction it brings when people try to make it real.

D. W. Johnson
Huntington Beach, CA

It's a brave stand you've taken. I predict you'll get a lot of heat.

Whether one agrees or disagrees with the proponents of laetrile, the crux of the matter is, as you've said, that it is "resisted with a passion." The medical profession and its cohorts would be a lot more credible if they maintained their cool.

Wasn't it less than a decade ago that Chinese doctors in this country were being arrested for quackery when they used acupuncture on their patients?

And I'll bet that for centuries before Fleming, witch doctors were feeding their patients molds (uggh!) to help them shake off infections.

Speaking of acupuncture, if a practitioner could combine it with voodoo, he wouldn't have to make house calls.

Dan Sheingold
Waban, MA 02168

Probability .25!! That's the likelihood that we engineers (and every other American) will develop cancer. A statistic so given as this must deflate us—but we are justifiably elated to read your gutsy editorial which joins the thunderous grassroots roar calling for the legalization of laetrile therapy, the proven-effective alternative.

Damn the cancer Establishment—its orthodox "cures" defy rational critique. Surgery, radiation and chemical poisoning (chemotherapy) serve only to disfigure the hapless patient while influencing the spread and/or development of cancer elsewhere in the
body. Correction—this witchcraft also serves to fatten the Establishment's pocketbooks and destroy the patient financially if not physically. Who's kidding whom?

It's high time we expose the phonies in the American Cancer Society, FDA and AMA and demand of our legislators that freedom in medical therapy be a reality, now! With one thousand cancer deaths per day, we haven't a moment to lose.

Henry E. Zeuli
Medford, MA 02155

Your laetrile editorial is the best piece of writing I've ever seen in Electronic Design.

One of the foremost experts on laetrile is Dean Burk, Ph.D., a founder of the National Cancer Institute who served as its chief chemist and head of the Cytochemistry Section. In addition to his observation that laetrile kills cancer cells "like flies" under the microscope, Dr. Burk states that positive, statistically highly significant, anticancer activity by laetrile in animal-tumor systems has been observed with a wide variety of animal cancers by at least five independent institutions. These include (1) Southern Research Institute, Birmingham, AL; (2) Scind Laboratories, Univ. of San Francisco; (3) Pasteur Institute, Paris; (4) Institute von Ardene, Dresden, Germany; (5) Sloan-Kettering Institute for Cancer Research, New York.

Although Sloan-Kettering has been testing laetrile since 1972, it has refused officially to release the experimental data. However, Dr. Kane-matsu Sugiura, who conducted this research at Sloan-Kettering, stated the following in a letter to us:

"I have tested the effect of laetrile isolated from apricot pits on the growth of spontaneous mammary cancers in mice many times and on the development of lung metastases. I found that prolonged intraperitoneal injections of 2000 mg/kg/day of laetrile inhibited the growth of small tumors (less than 1.5 cm. in diameter), in many cases temporary. Laetrile had a strong inhibitory action on the development of lung metastases—approximately 80% against approximately 20% in control mice. The general health and appearance of laetrile-treated animals with large tumors were better than those of the control animals with large tumors."

Laetrile Case Histories, a book by John Richardson, M.D., contains im-
(continued from page 193)

pressive case histories, verified by meticulous medical documentation. Over 800 American doctors are using laetrile and 50,000 Americans are taking it. Laetrile (amygdalin) has been recognized as nontoxic by the medical pharmacopoeias since 1834 and is on the FDA’s GRAS list, being less toxic than white sugar. It is an essential vitamin (B₁₇) with a strong ability to prevent sickness-cell anemia, as well as cancer. In the country of Hunza, where the people eat large quantities of apricot seeds, cancer is totally unknown.

Dr. Linus Pauling has called the FDA “derelict” in its ban on Vitamin B₁₇ since “nothing is wrong with it as a treatment or dietary supplement.”

Numerous cancer patients attribute their recoveries to laetrile (generally coupled with an anti-cancer diet).

Arlin J. Brown
Director
Arlin J. Brown Information Center, Inc.
P.O. Box 251
Fort Belvoir, VA 22060

The editor’s turn

As I indicated, I don’t know if laetrile works. My point, though, is that if we are to be professionals it should not be at the expense of the public. But many readers saw a different message.

It’s apparent that the facts obtained by some readers are not the facts I obtained. First, as to laetrile’s effectiveness. I have read many reports of humans who feel they have been helped by it.

In a case this April, Judge Mark Brody of the U.S. District Court in Brooklyn, N.Y., gave permission to Dr. Baldassare Cumella to import 375 grams of laetrile for his patient Joseph Rizzo. Dr. Cumella said that, after 30 days of laetrile treatment, 69-year-old Rizzo no longer suffered pain from his incurable cancer of the pancreas and had regained enough strength to take short walks. Further, his jaundice and itching had diminished, the swelling of his ankles had disappeared and his hemoglobin count had doubled. Dr. Cumella reported that he had not seen so noticeable or rapid an improvement in his 30 years of experience.

What about the vitamin-deficiency diseases cited by Mr. James and Dr. Risk? That’s precisely the point. Most of the pioneers in vitamins were denounced in their day. A suggestion that there could be another cause—a nutritional deficiency—was clearly absurd since science had already proven that germs and poor hygiene were the cause of disease.

According to The Vitamin Pioneers by Herbert Bailey (Pyramid Books), almost all these pioneers were ridiculed for years by the medical establishment. In many cases, their findings were suppressed. Even today, the ample documented findings of Drs. Wilfrid and Evan Shute about the astonishing value of Vitamin E in treating burns and cardiovascular diseases are routinely ignored and even suppressed by the medical establishment.

As to the medical pioneers cited by Dr. Brody, I never suggested that no medical researcher had ever made an important contribution to mankind. But Dr. Brody’s examples can prove instructive.

Edward Jenner’s discovery of vaccination against smallpox was at first attacked by the medical profession of the late 18th century, especially by the celebrated surgeon, J. Ingenhousz.

Louis Pasteur’s early work, the work that established his reputation, was aimed at conquering diseases of wine, silkworms and chicken. His work was treasured, as it was a treasure for three important industries. Only later did Pasteur develop an inoculation to stop rabies.

Sir Alexander Fleming’s penicillin, Sir Frederick Grant Banting’s insulin and Jonas Salk’s vaccine against infantile paralysis all furnished new products and new markets for the pharmaceutical industry. Of course, their contributions weren’t opposed. They made money.

I believe that the essential controversy lies between the views I tried to express and the views in the final paragraph of Dr. Brody’s letter.

He argues that the medical profession is to be admired because it takes care of its own financial interests first and, if necessary, the public be damned. I feel we ought to be better than doctors and, as professionals, place humanity’s interests first. I know that engineers often get a raw economic deal, and I feel we should fight for a better deal. But I don’t feel we should block technical or human progress to protect our economic interests.

George Rostky
Editor-in-Chief
Electronic Design

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ENCLOSURES

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GAS SENSOR 196

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OMRON MINI-SLIM THUMBWHEELS 198
New and current products for the electronic designer presented by their manufacturers.

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<tr>
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<th>DIMENSIONS</th>
<th>COST</th>
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<tr>
<td>One column inch</td>
<td>1-3/4&quot; x 1&quot;</td>
<td>$45.</td>
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<tr>
<td>2 col. in.</td>
<td>1-3/4&quot; x 2&quot;</td>
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<tr>
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<td>5-1/4&quot; x 10&quot;</td>
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<td>1 page</td>
<td>7&quot; x 10&quot;</td>
<td>$1800.</td>
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**Electronic Design** is mailed every two weeks. Because of its timeliness, personnel recruitment advertising closes only two weeks before each issue’s mailing date.

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<th>1977</th>
<th>Mailing Date</th>
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<td>Nov. 18</td>
<td>Dec. 20</td>
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HARDWARE DESIGN ENGINEER

Primary responsibilities will cover the specification and design of the Common Control hardware system and development of control processors, memories, peripheral controllers, network, network controllers, and trunks. Prefer a minimum of 3 years' experience in diagnostic software and hardware development in large real-time systems, system architectural planning, digital logic design, and TSO and SCL and structural programming techniques. Requires a BS or MS in Electrical Engineering or Computer Science and specialized study in logic design, assembly or computer language programming and fundamentals of sequential design.

THICK FILM ENGINEER

Responsibilities will focus on the review and analysis of circuit design for possible application to thick film packaging; hybrid design, providing liaison with circuit designers and submitting documentation to engineering departments. Prefer 3 or more years' experience in thick film hybrid microelectronics design and processing. Requires a BS or MS in Electrical Engineering and specialized study in circuit design, hybrid design, costing, functional trimming and materials in hybrid processing parameters.

TELETRAFFIC ENGINEER

Responsible for the analysis of teletraffic probability and queuing problems on digital and analog switching systems and the development of computer programs for switching systems. Prefer a minimum of 3 years' experience in real-time control systems teletraffic problems, systems equipment quantity specifications, and exposure to switching system specifications. Requires a BS or MS in Electrical Engineering, Computer Science or Math, a strong statistical background and experience in PL/1 or Fortran programming and model simulation.

ELECTRONIC PACKAGING ENGINEER

Will be engaged in the development and evaluation of electronic system packaging for effectiveness and cost reduction purposes, includes development of packaging standards and maximizing effectiveness of hardware systems with respect to packaging density, thermal efficiency and I/O constraints at the PCB and chassis levels. Prefer 3 or more years' experience in electronic system packaging design and development and the functions of PWC generation. Requires a BS in Electrical Engineering, Mechanical Engineering or Applied Sciences and specialized study in packaging mechanics, materials and production processes.

COMPUTER AIDED DESIGN ENGINEER

Responsible for specification, design and implementation of integrated Computer Aided Design-Computer Aided Manufacturing (CAD/CAM) systems. Includes planning and design of information system architecture, data base systems, simulation systems, and the development of interactive user access and PCB Physical Design system. Prefer a minimum of 3 years' experience in software development for CAD or CAM systems, data base systems, data base administration, and interactive graphic systems or computer systems. Requires a BS, MS or PhD in Electrical Engineering, Computer Science, or Math and specialized study in high level programming languages and techniques.

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Will analyze, evaluate and test integrated circuit assemblies, discrete devices and prototype systems; generate parameter measurements and operational life testing; design test circuits and perform failure analysis on semiconductors. Prefer a minimum of 3 years' experience in integrated circuitry, design of logic systems (digital T/TIC families), failure analysis and assembly processes. Requires a BS or MS in Electrical Engineering or Physics and specialized study in semiconductors, integrated circuits, digital circuits, electrical measurement and programming.

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