RFI and EMI are rapidly racing out of control. Major sources are new citizens-band sets, industrial fabricating equipment, switching power supplies and consumer devices. The FCC's response is to make stricter regulations. But these tougher limits will make EMI/RFI-proofing a major design task. For the story, see p. 24.
FEEL the pot . . .

CLICK the switch . . .

GANG the modules . . .

and add “quality-touch” appeal to your product.

FEEL THE POT . . . a smooth, quality feel, only from Bourns® 81/82 Model Potentiometers. Rotational torque range, only .3 to 2.0 oz. inch, is consistent for one, two, three or four cup assemblies.

Independent linearity of ±5% and low 1% CRV provide exceptional setability in both cermet and conductive plastic element types.

CLICK THE SWITCH* . . . one that really clicks, with positive action detent at either CW or CCW end. The Bourns Model 85/86 potentiometer/switch combination is rated at 2 amps in DPST style and 1 amp in DPDT. Contacts are constructed of fine silver with gold overlay. This provides exceptionally low contact resistance, for reliable operation at low level analog or logic signal levels — or any application requiring an “on-off” function.

GANG THE MODULES . . . potentiometers and switches. Up to 4 modules can be ganged on the same single or dual concentric shaft, without sacrifice to the satiny-smooth feel or the sure-fire click. Other options include a wide choice of bushing and shaft styles, P.C. pins or solder lugs. Think of the possibilities! Now you can specify custom pots and switches assembled from “off-the-shelf” modules — at standard cost and leadtime.

Add “quality-touch” appeal to your equipment with BOURNS Model 80 Family of Modular Potentiometer/Switches. Write or call today for complete technical information, direct or through your Bourns distributor.

FEEL, CLICK, GANG . . . BEAUTIFUL!

TRIMPOT PRODUCTS DIVISION, BOURNS, INC., 1200 Columbia Avenue, Riverside, California 92507, Telephone (714) 781-5122 — TWX 910 332-1252.

*Patent pending
The instruments on the left are our good old Models 152 and 159 programmable function generators—the ones that are ASCII coded and compatible with the GPIB.

And at right is our new Model 583 Autoprogrammer, designed to be used only with our programmables. By means of its plug-in memory, the Autoprogrammer can store commands for up to 100 separate tests. Test sequencing can be manual as well as automatic. Size of the memory is 1024 eight-bit words. You can program the memory supplied with the blank plug-in cartridge, or we can furnish you EROMs that are pre-programmed to your specs.

The Model 583 Autoprogrammer goes for just $995; the blank plug-in EROM cartridge is $150; a custom-programmed plug-in is $250. But none of these will do you any good unless you have one of our programmables. So get one. WAVETEK, P.O. Box 651, San Diego, CA 92112. Phone (714) 279-2200, TWX 910-335-2007.
Surprise! $2.95

Wideband Transformers

SURPRISE! Wide bandwidths, 0.015-600 MHz
SURPRISE! Low insertion loss, 0.5 dB
SURPRISE! Microminiature, 0.230" x 0.260" x 0.300"
SURPRISE! One week delivery

DESIGNERS KIT AVAILABLE:
2 TRANSFORMERS OF EACH TYPE
T1-1, T2-1, T4-1, T9-1, T16-1
KIT # TK-1...$32.00

NO "MAKE OR BUY" DECISION HERE...it costs less to buy
Mini-Circuits wideband transformers and there's no delivery delay.
Impedance levels from 12.5 to 800 ohms, with insertion loss typically less than 0.5 dB

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<td>$2.95</td>
<td>$3.45</td>
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For complete specs, performance curves and drawings, see pgs 192-193 of the 1976-77 MicroWaves Product Data Directory.

World's largest supplier of double balanced mixers

International Representatives:

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Cover: Cover designed by Art Director, Bill Kelly.
Thin-Trim capacitors

Tucked in the corner of this Pulsar Watch is a miniature capacitor which is used to trim the crystal. This Thin-Trim capacitor is one of our 9410 series, has an adjustable range of 7 to 45 pf, and is .200" x .200" x .050" thick.

The Thin-Trim concept provides a variable device to replace fixed tuning techniques and cut-and-try methods of adjustment. Thin-Trim capacitors are available in a variety of lead configurations making them easy to mount.

A smaller version of the 9410 is the 9402 series with a maximum capacitance value of 25 pf. These are perfect for applications in sub-miniature circuits such as ladies' electronic wrist watches and phased array MIC's.

Johanson

Johanson Manufacturing Corporation
Rockaway Valley Road
Boonton, New Jersey 07005
(201) 334-2676  TWX 710-987-8367
A better model for phonograph cartridges?

I liked the article, “Hold Noise Down With JFETs . . .” (ED No. 4, Feb. 16, 1976, p. 146), especially the design example for the phonograph preamplifier. It bears mention, however, that B. I. Hallgren of the Institute of Physics at the University of Stockholm has proposed a different circuit for a phono cartridge:

\[
\begin{align*}
\text{R}_L \quad & \quad \text{C}_L \\
\end{align*}
\]

In this version, \( C_L \) is mostly cable capacitance and \( R_{LT} = R_0 \), where \( \omega \) is the angular frequency, and \( R \) and \( k \) are constants determined by the specific pickup cartridge. Typical values for popular cartridges are as follows: for the ADC 27, \( R = 53.8 \, \Omega/\text{rad} \) and \( k = 0.67 \); for the Shure M75, \( R = 272 \, \Omega/\text{rad} \) and \( k = 0.51 \).

This model was published in the Journal of the Audio Engineering Society (Vol. 23, No. 7, September, 1975). Its accuracy appears to have been confirmed by Tomlinson Holman of Advent Corp., who commented on it at the convention of the AES (New York City, October, 1975).

Richard W. Bowser
Custom Electronics, Inc.
4448 S. 84 St.
Omaha, NE 68127

The author replies

I read Mr. Hallgren’s article with much interest when it was published. He used 83 third-octave bands (from 8.8 Hz to 114 kHz), a complex model and a computer for noise calculations. For the two phono cartridges (with specific loading) the RIAA equalized noise was 0.772 \( \mu \text{V} \) for an ADC 27 and 0.709 \( \mu \text{V} \) for a Shure M75.

I used the ADC 27 cartridge loaded with 250 pF and 47 \( \Omega \) (the same conditions as Mr. Hallgren) as an example. I used the following equation for the noise calculation:

\[
V_{EQ} = \left( |A_1|^2 V_{N1}^2 + |A_2|^2 V_{N2}^2 + \cdots \right)^{1/2}
\]

where \( V_{EQ} \) is the equalized noise, \( |A_n| \) is the magnitude of reflected gain at the center of each frequency band and \( V_{Nn}^2 \) is the noise of each frequency band.

With octaves starting at 20 Hz and ending at 20 kHz, the RIAA equalized noise worked out to 0.75 \( \mu \text{V} \). This is within 3% of the value of Mr. Hallgren’s example; if the same frequency range had been used, the difference would have been less. I don’t believe that the addition of \( R_{LT} \) to the model would significantly change the calculated noise value; there is no need to further complicate an already complex problem.

Complete details of this example will appear in National’s upcoming audio handbook.

On rereading my ELECTRONIC DESIGN article, I’ve discovered several small errors that I overlooked earlier. On p. 151, the equation should read:

\[
V_{\text{MAX}} = \left[ \text{min. signal}^2 - V_N^2 \right]^{1/2}
\]

\[
V_{GS,\text{LTP}} = V_{\text{P,LTP}} \left[ 1 - \left( \frac{I_D}{I_{DBS}} \right)^{1/2} \right] = 2.1 \text{ V}
\]

\[
R_S = \frac{15 \text{ V} + V_{GS,\text{LTP}}}{\frac{I_{D,\text{MAX}}}{11}} = 17 \, \text{k}\Omega
\]

(continued on page 6)
ACROSS THE DESK

(continued from page 5)

Also, on p. 152:

\[
V_{GS_{\text{max}}} = 2.8 \text{ V}
\]

and,

Final S/N =

\[
\frac{2 \text{ mV}}{1.73 \mu\text{V}} = 1.150 \text{ (61.2 dB)}
\]

John Maxwell
Senior Application Engineer
National Semiconductor Corp.
2900 Semiconductor Dr.
Santa Clara, CA 95051

Microprocessors—a topic of limited interest?

Microprocessors are indeed wonderful machines, but must 90% of each issue be devoted to them?

Quite frankly I am bored with reading three-page articles each time a microprocessor manufacturer changes a resistor value on his chip.

Would you consider articles on the other 90% of the electronics field that microprocessors have not revolutionized?

Larry W. Fort
Engineering Dept.
Progressive Electronics, Inc.
432 South Extension
Mesa, AZ 85202

Editorial on advisors continues to divert

I couldn’t help noticing the protests of your editorial, “The Czar’s Consultant” (ED No. 1, Jan. 5, 1976, p. 75). However, the worst taste of all was not shown by the editorial itself, but by the letter “Success Story” by Dan Sheingold of Analog Devices (ED No. 8, April 12, 1976, p. 14).

To describe as a “sales force” a political organization guilty of murdering 10 million human beings in the drive to collectivize agriculture alone is reprehensible and deserves no place in the discourse of decent men. The figure is Stalin’s own estimate. See, for example, p. 345 of The World Since 1939 by Carroll Quigley (Collier Books, New York, 1965).

There can be no excuse for call-
NEW HP microprocessor-controlled DVM makes 24 readings/sec in presence of noise

Hewlett-Packard's new Model 3455A DVM has high speed and good noise rejection for systems use and high resolution and computational capability for bench applications. DC measurements from 1 microvolt to 1 kilovolt can be made at 24 readings per second with 5½ digits; 6½ digits are used for greater than 1 ppm resolution measurements at six readings/second. Greater than 60 dB normal mode noise rejection and greater than 160 dB common-mode noise rejection is obtained on all DC ranges. Best DC accuracy is ±0.0023%.

True rms measurements are made up to 13 readings per second above 300 Hz. True rms is measured with best accuracy of 0.1% over a 30 Hz to 1 MHz bandwidth. Signal crest factors as high as 7:1 full scale can be measured.

Four or two-wire resistance measurements can be made from 1 milliohm to 15 megohms. Maximum current through the unknown is less than 1 milliampere.

Math functions built into the 3455A let the user offset, take ratios or scale readings so that readouts are in physical units. A % ERROR mode converts readings into percent change compared to a predetermined reference.

Use of a plug-in precision reference enables the instrument to check itself against the reference. Under control of a microprocessor, it makes its own error corrections. This reference unit can be easily removed from the 3455A for periodic calibration. A self-test feature verifies operation of DC circuits. If a problem is found, it is easily diagnosed using the front panel display.

Standard on the 3455A is an HP-IB (Hewlett-Packard's implementation of IEEE 488-75) I/O for systems operation. Front panel indicators on the 3455A display range, function and HP-IB status during remote operation.

For more information, check I on the HP Reply Card.
Automatic system speeds transceiver testing to 1000 MHz

Productivity is the watchword in receiver manufacturing. Radio maintenance shops are striving to improve throughput, test quality, and turnaround-time. R&D and incoming quality labs need to provide accurate, consistent, and comprehensive testing of today's sophisticated transceivers.

To help solve these requirements, Hewlett-Packard is introducing its 8950A Transceiver Test System. The combination of these mostly off-the-shelf instruments provide capability of testing AM and FM transceivers up to 1000 MHz and 100 watts. System control is via the HP 9825A calculator providing self-contained operation.

Amplitude modulation characteristics are measured from 1 to 95% depth and an accuracy of ±5%. FM deviation is measured to 20 kHz with an accuracy of ±3%. Audio measurements on the transmitter provide ±5% accuracy on sensitivity, with audio response indicated to 25 kHz for AM and 20 kHz for FM. Audio distortion is measured to <2% at 400, 1000 or 3000 Hz using the THD (total harmonic distortion) technique. Squelch tone frequency is indicated to ±0.1 Hz.

Receiver test capabilities include sensitivity tests at 12 dB SINAD for 1 kHz or with 20 dB quieting and can also be made at squelch threshold. Audio power output is measured to ±0.5% with a frequency response to 50 kHz; accuracy and audio distortion to ±1% at 1 kHz tone.

Model 8950A achieves maximum throughput and testing speed with a special interface and signal switch adapter panel mounted at the operator shelf. Automatic testing can improve test times by 10 to 1 over manual tests. Throughput of course depends on the particular test sequence, but a Citizen Band transceiver test can be run in 3 minutes including a printed test report.

Hewlett-Packard furnishes software test modules as sub-routines, segmented by type of test; for example, transmitter power, transmitter frequency, etc. The user then writes simple programs to access the tests as appropriate and compare test data against programmed limits or print out a test card.

For additional technical information, check Q on the HP Reply Card.

New, easy-to-use storage controls make your measurements faster, less complicated

For viewing low-rep-rate/fast rise-time signals, the variable persistence mode of the 1741A storage oscilloscope allows you to adjust the trace for an optimum display.

A newly-designed storage/variable-persistence CRT, used for the first time in Hewlett-Packard's new 1741A oscilloscope, produces exceptionally clean traces, and excellent trace-to-background contrast ratio.

New automatic storage controls make it easier than ever before to capture low-rep-rate, single-shot waveforms common in today's digital circuits.

As a dual-channel, 100 MHz general purpose scope, it has a writing speed of at least 100 cm/µs which allows single shot capture of glitches 1 division high and less than 20 ns wide.

The variable persistence mode allows you to adjust the trace for an optimum display. The third-channel trigger view lets you observe an external trigger signal simultaneously with channel A and B traces.

A x 5 magnifier permits two channel measurements as low as 1 mV/div to 30 MHz, without cascading.

The 1741A is suited not only to the laboratory and the computer room, but also to the more rugged situations common with communications and process control equipment.
Capture that unique digital event at the press of a button!

The handy HP 1230A Logic Trigger increases the usefulness of any scope in the data domain by providing a digitally-delayed jitter-free trigger just at that point in the data stream you require. When digital delay is added to word recognition, it is possible to select a unique word because the trigger pulse can be released on any preset number of clock cycles after recognition. The scope will display the data stream from any desired point after the trigger word without multi-triggering. Subsequently, this point may be shifted either direction simply by pressing the Up or Down button—continuously for fast shift, or successively for step-by-step.

In addition to the 1230's clock and eight-bit word recognition (HI/LO/OFF) inputs, a gate input allows further qualification. Delay (between 1 and 9998 clock pulses) is indicated on a 4-digit LED display.

The 1230A can be operated in a synchronous or asynchronous manner for maximum measurement flexibility.

For additional technical data, check O on the HP Reply Card.

NEW automatic phase noise system simplifies difficult measurements

The 5390A Frequency Stability Analyzer specializes in phase spectral density measurements made very close to the carrier. Offset frequencies from below 0.01 Hz out to 10 kHz can be analyzed with extremely narrow bandwidths.

With tightening bit error rate requirements in satellite communications, shrinking bandwidths in ground communications links and greater resolution requirements in many radar systems, the ability to characterize precision frequency sources has been meeting increasing demands. In many cases specifications for close-in phase noise have been limited by the capabilities of existing test equipment rather than by the need for the information.

Although the 5390A frequency stability analyzer is a complimentary device to today's high performance spectrum and wave analyzers, it excels in the difficult close-in measurements (e.g. 100 Hz and below) where such devices become inadequate. Frequency offsets well below 1 Hz can now be analyzed with sub-millihertz bandwidths and excellent sensitivity.

Data is automatically collected by a high performance counter in the time domain. Under calculator control, the system operates as a frequency selective digital filter and converts the data to the frequency domain. Since the system measures zero crossings, elaborate amplitude calibration schemes are unnecessary. Data is automatically reduced and the single sideband phase noise-to-carrier ratio, normalized to a 1 Hz bandwidth, is presented in terms of dB below the carrier (dBc) in both tabular and graphical form using the 9871A printer/plotter.

The system will take measurements on carrier frequencies from 500 kHz to 18 GHz. Observations of phase noise may be made at offset frequencies from below 0.01 Hz out to 10 kHz with typical sensitivities of greater than -150 dBc at 1 Hz away from the carrier.

Measurements are usually made by comparing two similar sources slightly offset in frequency from each other. Measurements can also be made on non-offsettable sources by using an additional mixer/amplifier module.

Besides the difficult phase noise measurements, the 5390A also makes long term drift measurements and can monitor short term stability in the time domain using an improved version of the Allan Variance technique.

The basic system includes the 5390A analyzer, a 9825A calculator and 9871A printer/plotter, software for frequency stability and phase noise measurements, diagnostics, and a technical handbook.

For a technical data sheet, check K on the HP Reply Card.
New HP-IB/21MX Minicomputer controls multiple instrument clusters, accesses data and develops new programs—all at the same time

HP-IB

In the past, interfacing instrumentation systems for measurement and test applications has been complex and costly. Not any more. With the HP-IB/21MX Minicomputer, automatic test systems for production, laboratory research, and automatic data acquisition systems can be implemented more easily and simply. HP offers for the first time a minicomputer with a multiprogramming operating system as a controller for instruments which conform to the IEEE-488 standard.

Take the simplicity of HP-IB* interfacing. Add HP's 21MX Minicomputer and Real-Time Executive (RTE) software for the power and control. Choose from over 100 HP and non-HP IEEE-488 compatible instruments, calculators and peripherals to handle test and measurement. Within hours, flexible and powerful measurement and test systems can be up and running. OEM's can focus resources on customer interfacing.

Controls multiple instrument clusters. Because the Real-Time HP-IB Minicomputer supports multiprogramming, it can simultaneously control several HP-IB clusters of up to 14 instruments each. Test/measurement equipment can be organized into multiple physical or functional groups—each connected to the HP-IB/21MX Minicomputer by its own HP-IB Interface Bus.

New instrument clusters can be added or reconfigured without downtime or effect on existing clusters. Systems can grow as needs grow. And, because of the new Real-Time HP-IB Minicomputer's speed as an HP-IB controller, throughput is increased in high volume or production testing.

Consolidates data. The Real-Time HP-IB Minicomputer's multi-priority program scheduling allows highest priority to run immediately and then later devote time to such operations as correlating and analyzing data, and producing timely management reports.

HP's new IMAGE/1000 data base management software adds a complete set of 'software tools' for consolidating files into a single data base. Once the data base is established, IMAGE/1000's English-like QUERy language allows users to interactively find any stored information by searching under multiple "key values" such as a part number, vendor code or failure type. IMAGE/1000 permits easy report generation with automatic sorting, summation, pagination and averaging.

Allows concurrent program development in multiple languages. While the Real-Time HP-IB/21MX Minicomputer is busy controlling instruments and consolidating data, it can also be used for program development. For the first time, engineers can readily access and develop software for the system via the IEEE-488 and with the popular scientific language FORTRAN IV. HP's Multi-User Real-Time BASIC, which can be learned in a few hours, and HP's assembly language are available. This multi-lingual approach brings the utilization of HP-IB to a wider cross section of users.

Supports multiple terminals. The Real-Time HP-IB Minicomputer also offers multi-terminal accessibility. Several people can use the system simultaneously—for program development, data entry or system control. As a result, testing and production data such as quality assurance information is available when needed for decisions.

Augments data networks. Finally, the Real-Time HP-IB/21MX Minicomputer extends the data gathering capabilities of today's computer networks. Off-the-shelf hardware/software data communications packages make it easy to connect the HP-IB/21MX Minicomputer to other HP 21MX computers or to link it upwards to a central computer.

For a video tape demonstration of the HP-IB/21MX, check the box on Item A of the HP Reply Card.

*HP-IB is Hewlett-Packard's implementation of IEEE Standard 488 and identical ANSI Standard MC1.1—Digital Interface for Programmable Instrumentation.

For more information on how these systems can help you gain management control over your automated testing, check A on the HP Reply Card.
Build your own automated test system easier and faster with the HP-IB

Multiple Instrument Clusters
Each independent cluster of up to 14 instruments is connected to the 21MX Minicomputer via a separate HP-IB interface cable.

Add New Clusters Easily
With on-line configuration capability, new independent instrument clusters can be added or changed without downtime or effect on existing clusters. Programming test procedures are simple BASIC "PRINT/READ" or FORTRAN "WRITE/READ" statements.

Component Test Clusters
A monolithic DAC is tested with an HP multiprogrammer and digital voltmeter.

Subassembly Test Cluster
At the same time, C-band microwave amplifiers can be tested with a sweep oscillator and an RF power meter.

Instrument Test Cluster
And, at the same time, a sweep oscillator can be tested with a frequency counter.

New Real-Time HP-IB/21MX Minicomputer
The HP-IB/21MX Minicomputer which automates test/measurement procedures, and permits concurrent program development and data retrieval consists of a 21MX Minicomputer and cartridge disc memory, managed by HP's RTE-II or RTE-III Real-Time Executive software. For more information on the Real-Time HP-IB/21MX Minicomputer, check A on the HP Reply Card.

Multiple Terminals for Concurrent Program Development or Data Base Access
The Real-Time HP-IB/21MX Minicomputer, with new IMAGE/1000, permits fast multi-lingual program development or data access by several users simultaneously.

Computer Network Connections
Incoming Inspection Satellite
A remote HP-IB/21MX Minicomputer in the nearby Inspection Department consolidates test data via the network connection system.

Central EDP
HP supported hardware and software connect the HP-IB/21MX Minicomputer to other 21MX Minicomputers or IBM 360/370 in a distributed management information network.
At the TRW Space Park facility in Redondo Beach, California, precise measurement and testing is a critical aspect of the company's activities. As a designer and manufacturer of scientific, military and commercial spacecraft systems, the Defense and Space Systems Group relies on 25 HP 2100/21MX computer-based Scientific and Measurement Systems for engineering and manufacturing testing.

Don Broutt, manager of TRW's automatic test systems department, adopted the Hewlett-Packard Interface Bus (HP-IB) to link numerous test instruments to his HP computers and HP calculators.

"Many of our programs involve extremely limited production runs . . . some products, for example, are one of a kind. Before adopting the interface bus, our efforts to reestablish test stations for each program was like reinventing the wheel. Now, when setting up a new test station with the HP-IB, we can easily add or reconfigure instruments in a computerized network with minimal set up time," explains Broutt.

With improved flexibility comes cost savings, according to Broutt. Prior to adopting the HP-IB, testing required specially engineered printed circuit board interfaces for each unique test device. If a device served as both a "listener" and "talker," it required two boards. Now, one board within a computer allows interfacing with up to 14 devices that meet the IEEE-488 standard. A single standard cable now replaces specially-engineered cables formerly required for each test instrument.

"In our pre-HP-IB testing, we wrote special driver software for each unique device. This consumed excessive amounts of computer memory. Now our engineers simply use a subroutine for each device to access an HP-IB standard driver. Gone is time-consuming reference to handbooks for device translation. Once a subroutine is written, the device interface is transparent to our engineers," relates Broutt.

With the growing availability of test devices using IEEE-488 and the expanding use of the HP Interface Bus, TRW has reduced the cost of interface design. Manpower and resources formerly allocated to this function can now be applied to other priority projects.

For more information on how HP computers in conjunction with the HP-IB can help you, check A on the HP Reply Card.
New HP display station: extensive stand-alone capability plus data communications flexibility

The HP 2645 display station is the latest and most powerful addition to Hewlett-Packard's growing family of general-purpose, interactive display terminals. Keyboard use is simplified by eight user-defined soft keys, each of which can be set up to issue a string of up to 80 characters or several control sequences stored in the terminal. You can simply press a key to trigger file searches, issue operator or computer instructions, dynamically configure the terminal, or perform other specialized tasks.

The 2645 is compatible with a wide variety of computer systems. It can operate at selectable speeds of up to 9600 baud, and has the optional capability of asynchronous or synchronous (BISYNC) multipoint polling with up to 32 terminals on the same line. This makes possible the sharing of modems, data lines, and computer I/O channels with significant savings in data transmission costs. Built-in self test ensures proper operation within a network.

Up to four 128-character sets can be viewed concurrently on the high-resolution display.

Optional, highly reliable cartridge tape transports provide 220,000 bytes of mass data storage, allowing the 2645 to batch information and to perform many operations on a stand-alone basis that normally require connection to a computer.

For more information on these products, check J on the HP Reply Card.

NEW Digital Test System enables production testing and test programming concurrently

Because of their increasing complexity and density, testing of logic circuit boards today is a major element in manufacturing costs. The use of manual or semi-manual fault location techniques on loaded logic boards costs precious troubleshooting hours.

The new Hewlett-Packard Digital Test System, DTS-70, offers printed circuit logic board manufacturers versatile capabilities that will result in improved test quality and high throughput.

A system consists of three elements, an HP 9571A Test Station, a 21MX minicomputer-based controller, and the HP 91075B TESTAID-III Test Generation Software. The HP 9571A test station handles logic assemblies to 200 MSI-type IC's (10,000 gate equivalents).

Go/no-go testing on the DTS-70 is fast—typically a few seconds for moderately large boards. Fault isolation using the computer-assisted FASTRACE guided probe is accurate and quick, typically locating the fault in less than a minute. When the fault is located, the fault data is automatically displayed on the CRT terminal and printed on hard copy by an optional repair ticket printer. The test operator attaches the repair ticket to the PC board so the fault data is available at the rework/service area.

An important feature of the DTS-70 is the ability to concurrently write and edit test programs at the test preparation station while production testing continues on the HP 9571A test station. Test programs are prepared using TESTAID-III, an advanced digital logic simulator. In addition to interactive program preparation on-line, TESTAID-III can have all controls preloaded into it for unattended or overnight operation, thus maximizing personnel and computer efficiency.

Designed to accurately test large numbers of complex logic assemblies, up to three HP 9571A test stations can be operated from one controller in the system. Add-on stations can usually be installed in less than two hours.

The system uses the Hewlett-Packard Interface Bus to provide control for analog functions: dc voltage measurements, frequency, time interval, power supply programming for units under test, and to control other system devices.

For more information, check D on the HP Reply Card.
New 200 Watt extended range DC power supply

The new HP 6002A power supply can provide a full 200 Watts output over the range from 20 Volts to 50 Volts. Output voltage is continuously adjustable from 0 to 50V while the maximum current available is automatically controlled to maintain a 200 watt maximum power boundary.

Lab grade performance is provided for general purpose research, design, and production applications.

An optional programming feature (Option 001) is available for controlling the output voltage (or current) via the Hewlett-Packard Interface Bus—either by calculator or computer. Switches on the rear panel of the 6002A allow either local front panel control, HP-IB controlled voltage, or HP-IB controlled current. A programmable range allows a $5 \times$ improvement in resolution when the 6002A is operated below 10 volts.

The power supply operating status is continuously shown by front panel indicator lights which reduce the need to interpret meter readings. Additional lights also identify overrange and overvoltage conditions. The overvoltage protector is a front-panel adjustable SCR type “crowbar”. Ten-turn controls permit accurate adjustment of output voltage and current when the supply is operating under local control.

For more information, check N on the HP Reply Card.

With HP-IB option, the new 6002A power supply can be digitally controlled using your calculator, computer or other controller.

Highest power yet for microwave sweepers

Two new RF plug-ins for the HP 8620C Sweep Oscillator capitalize on Gallium-Arsenide technology to deliver at least 50 mW of leveled power in the frequency ranges, 5.9 - 9.0 GHz and 8.0 - 12.4 GHz. These are highest power levels ever offered in solid-state sweepers—and higher than most backward wave oscillator (BWO) tube-type sweepers as well. Key to this achievement is a broadband power amplifier developed by Hewlett-Packard that typically delivers 100 mW output over a 5.9 - 12.4 GHz range with 10 dB nominal gain. The amplifier employs 1 \( \mu \)m Gallium-Arsenide Schottky-Gate Field Effect Transistors (GaAs MESFET).

The extra power is achieved without sacrificing other RF performance characteristics (such as frequency accuracy, linearity, stability, and residual FM). Harmonics are at least 30 dB below full rated output, non-harmonic spurious >60 dBc, and optional internal leveling to \( \pm0.5 \) dB is offered.

Using high power sweepers, it is often possible to eliminate additional amplification when performing saturation tests or high loss measurements. Higher power also permits padding to isolate test devices from source and detector for better matching leading to more accurate measurements. The new plug-ins accept direct modulation from the HP 8755 Frequency Response Test set which allows a full 60 dB measurement dynamic range even with padding for best match.

Model 86242C covers 5.9 - 9.0 GHz and HP 86250C covers 8.0 to 12.4 GHz.

For additional data, check P on the HP Reply Card.
The world’s first rectangular solid-state lamp

Rectangular solid-state lamps in three colors (high efficiency red, yellow and green) are now available from Hewlett-Packard. This is the first solid-state lamp in this configuration to be offered to the market place. The configuration of this lamp makes it ideal for lighted mechanical switches, flush-mounted panel indicators, backlighting, bar type scale indicators, or minus indicators in digital displays.

The 5082-4570, 4670, and 4970 are encapsulated in an axial lead rectangular epoxy package. They utilize a tinted epoxy with a thin, uniform segregated diffused layer at the emitting surface to provide a high on/off contrast plus a uniform light emitting area.

Dimensions of the flat light emitting surface are 2.54 mm (0.10") by 7.49 mm (0.295"). The axial luminous intensity for the red lamp is 1.0 mcd typical; for the yellow and green, it is 1.2 mcd typical. The typical operation forward current is 15 mA for the red and yellow; and 20 mA for the green.

For technical information, check L on the HP Reply Card.

Fastest microwave switch—guaranteed 5 ns rise time

HP offers the new 33140/33640 series SPST switches for operation from 0.1 to 18 GHz. Rise time is 5 ns; fall time is 7 ns. Isolation up to 80 dB is available. Designed especially to drive these 33140 series switches, the HP 33190A TTL compatible switch driver can be used to improve the switching time of any SPST diode switch.

For further information, check H on the HP Reply Card.

New rugged one micron GaAs FET chip

The HFET-1000 is a GaAs FET chip designed for low noise figure (3.6 dB typical); high gain (11.0 dB); and a high dynamic range of 14.5 dBm linear power output at 10 GHz.

The .065 x .028 mm chip is provided with a dielectric scratch protection layer over the active area. Gate width is 500 micrometers resulting in a typical linear output power greater than 25 mW.

New chip available for applications in telecommunications, radar and EW amplifiers in the 1-12 GHz frequency range.

Now available from Hewlett-Packard is a visible, near-IR, source using a GaAsP on GaP LED chip which has been optimized for maximum quantum efficiency at 670 nM. The emitter’s beam is sufficiently narrow to minimize flux problems, yet broad enough to simplify optical alignment.

The HEMT-3300 is designed for consumer and industrial applications such as optical transducers and encoders, smoke detectors, assembly line monitors, small parts counters, paper tape readers and fiber optic drivers.

This device comes in a standard T-1¼ configuration with an undiffused, untinted plastic lens. The axial radial intensity is typically 500 mW/sr at 10 mA.

For further specifications, check M on the HP Reply Card.

670 nM high intensity emitter simplifies optical alignment
Now, more memory—for less money

The HP-67 and HP-97 are the most powerful personal calculators Hewlett-Packard has ever built. The HP-67 (left) gives you shirt-pocket portability. The battery-powered HP-97 (right) gives you attaché case compactness plus a quiet built-in thermal printer.

Two new HP calculators, the HP-67 and the HP-97, have more than three times the program capacity of the first HP magnetic card-reading calculator—the HP-65—and at a lower cost. But there's more to evaluating programming capacity of a calculator than just merely comparing the 100 steps of the HP-65 to the 224 steps in both the HP-67 and the HP-97.

The factor of three times the increase in capacity is specified because all functions, whether one, two, or three keystrokes long, use only one step of program memory.

Now, for the first time, you can transfer information from either side of the magnetic card into the data registers, or, record data from the registers to the magnetic card.

A significant operational improvement of the HP-67/97 is the “smart” card reader. In addition to data recording and reading, the card reader serves as a prompter for proper operation. It automatically checks and retains the display mode, angular mode setting and status of the four flags. It also detects whether information on the card consists of data for the storage registers or program steps. You will find it virtually impossible to improperly load programs or data from the cards.

There are many more powerful features including 10 user-definable functions, 10 conditional/decision functions and three types of addressing.

For more information on the HP-67 and HP-97, check B on the HP Reply Card.

Calculator that remembers, even when turned off

The HP-25C is the first HP scientific programmable pocket calculator that retains stored programs and data even when it is turned off. The HP-25C with continuous memory is otherwise identical in performance to the HP-25A.

With the keystroke programmability of the HP-25A or HP-25C, you can solve automatically the repetitive problems faced by scientists and engineers.

Both have 49 steps of program memory with merged keycodes and 72 built-in scientific, engineering and mathematical functions and operations, including full editing capability, register arithmetic and several conversions.

For further details on both calculators, check C on the HP Reply Card.

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CIRCLE NUMBER 6
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CIRCLE NUMBER 7
New standard clears up DMM/DVM accuracy specs

Users and vendors of digital multimeters and voltmeters might finally talk the same language when a new ANSI standard for their instruments appears some time next year.

The standard—an update of ANSI C39.6, the seven-year-old standard now in effect—defines terms and provides test methods for many of the important DMM performance characteristics.

The format includes both mandatory and optional procedures and ways to specify DMMs, says William Nichols, chairman of the ANSI Committee working on the standard and chief electronic engineer at Keithley Instruments, Cleveland, OH.

One source of confusion the standard attacks is the method of specifying accuracy. DMM vendors currently specify accuracy in terms of the readings, full range, full scale, overrange, or some combination of these. Since the terms mean different things to different people, and since each vendor uses his own method, there's no way to really compare competing instruments.

The C39.6 eliminates the doubts by limiting the accuracy statement to one method and by dropping the word "overrange" from the DMM lexicon. Accuracy is spelled out as a percentage of reading plus a number of digits.

Vendors who will use the standard are required to specify accuracy over a 10-degree span near room temperature. A ±1-degree range can be stated, if desired, or a wider range, say 0 to 50 °C, can be given.

Other DMM or DVM specifications covered by C39.6 include resolution, linearity, and tempco. But one difficult area that probably won't be covered is EMI specs. They will have to wait for future standards.

New, stronger battery powers electric car

A new battery that will enable an electric car to travel 150 miles at a speed of 55 miles per hour is being developed by Argonne National Laboratory in Illinois.

A prototype lithium-sulfur battery with a power density of 150 W/kg has already been fabricated, according to Bill Walsh, leader of the advanced engineering group. This density is two and a half times greater than the power density of current automotive lead-acid batteries. With a little more effort, notes Walsh, the power density of the lithium-sulfur battery can be raised to over 200 W/kg.

The components of the new battery, a lithium alloy and iron sulfide, make it more powerful than the conventional lead-acid battery because the components have a higher specific energy than the components of the lead-acid system.

To prove the feasibility of the battery in electric-car applications, Argonne engineers plan to contract with industry to build and test a prototype car that would be powered by the battery. The prototype is expected to be operational by late 1978 or early 1979. It will weigh about 2500 pounds, 880 of which will belong to the batteries.

Walsh notes that by 1985 the weight of the batteries will be reduced to only 550 pounds. To provide the same capability with lead-acid batteries, 2600 pounds worth of them would be needed, he adds.

In addition to its use in electric vehicles, the lithium-sulfur battery promises to become an important energy and money-saving tool for electric utility companies. The reason Walsh points out, is that during heavy consumer demand, many utilities must operate extra turbines. Power-generating efficiency could be increased if these extra generators, which are only used during peak loads, could be replaced by a large bank of lithium-sulfur batteries. They could store excess electricity generated during low-demand hours and release it during high load hours. In addition, Walsh says, energy-transmission costs could be cut by locating the batteries at substations that are closer to load centers.

Fortran compiler offered for µP design system

A resident Fortran compiler, just what microprocessor users have been waiting for, is finally available. Developed by Motorola, the compiler is designed to operate on the company's Exorciser development system.

Designated M6800FTNRO-10D the compiler uses a Fortran language that is a subset of the standard Fortran IV. Like the standard Fortran, the Motorola µP version accommodates variable names that consist of two to five alphanumeric characters. It also features implicit type designation, with variables starting with letters I to N denoted as integers, and all variables as real numbers.

The minimum hardware configuration needed to use the 6800 Fortran compiler is an Exorciser, 16-k of memory, a disc memory and a terminal. The compiler is available for delivery and sells for $500.

New mini features high density memory

The new Eclipse C/330 computer from Data General incorporates the
highest-density main memory in the company's computer line.

The C/330 has new 64-k bytes of semiconductor and 32-k bytes of core on single-board memory modules. Its memory allocation and protection unit (MAP) doubles main-memory capacity to 512-k bytes and provides hardware protection for user programs in dual programming applications.

The new Eclipse MAP and memory modules enable users to be more flexible when configuring main memory and peripherals into their systems. In addition, the dense memory results in fewer connections and interface components, so the reliability of the computer system is increased.

The C/330's interactive data-entry and access (Idea) system is the first produced in the minicomputer industry to permit users with limited programming knowledge to implement data-entry and data-management applications. The system uses Idea software that includes an easy to use, English-like language.

The MAP unit provides hardware protection for programs and data in multi-user systems and permits programs to operate concurrently. The unit also provides write protection so that several users can share memory blocks without altering data and procedures. The unit has four data-channel MAPs, so the number of peripherals that can operate concurrently on the data channel is increased. A new look-ahead algorithm in the MAP's memory-access logic markedly decreases system-mapping overhead.

The new Eclipse's 64-k-byte, semiconductor memory modules (NMOS) quadruple the 16-k bytes of NMOS memory previously available only on a single board. In addition, memory speed has been increased to 500 ns for read cycles compared to 700 ns read cycle time for the 16-k module.

Memory-error checking and correction is standard on the semiconductor modules.

The 32-k-byte, core-memory module doubles the density of already available 16-k core modules. The 32-k-byte memory has an 800-nsec cycle time. Data General uses a split-sense memory technique that increases the traditional 1-µs speed to 800 ns. Core and semiconductor modules can be interleaved up to eight different ways to reduce effective cycle time.

The new interactive data-entry-access software is supplemented by other software that includes a multitasking, real-time, disc-operating system; an ANSI-74 Cobol language system, an INFOS database-oriented file management system; RPGII sort/merge utilities and RJE/HASP communication emulators. The Eclipse commercial instruction set gives the computer data handling capability for commercial data processing applications. The instructions handle word-byte and word-bit addressing, code translation, and full editing for formatting functions and move and compare character strings. An Extended Arithmetic Processor provides fast operations on packed and unpacked numeric data. For large file handling, the C/330 supports over 700 M/byte on line disc storage.

Promising optical fibers developed by Corning

Electro-optical communications equipment that can offer not only a 50% improvement in source coupling but also a significant reduction in signal attenuation is now feasible, thanks to improved optical fibers from Corning Glass Works.

Called Corguide, the new fibers promise better transmission than was previously possible in the 800-to-1100-nm range. They also offer a higher numerical aperture (0.2) and decreased water-ion (OH-) absorption at 950 nm.

The four fibers now available combine 200 or 400-MHz bandwidths with 6 or 10-dB/km-attenuation levels. Such attenuation has been previously available only in the 820-nm range.

The standard length of the new fibers is 1 km, but longer runs are available on request. Multikilometer lengths of new fibers should withstand loads of 10,000 psi for 20 years, according to Corning, which conducted screen tests at 25,000 psi.

The fiber improvements stem from Corning's deposition process, which allows the introduction of controlled quantities of dopants.

High efficiency achieved with organic photocells

The highest efficiency to date of any organic photovoltaic material has been obtained at the IBM Watson Research Center. V. Y. Merritt, a researcher at the Yorktown Heights, NY laboratory, has converted hydroxy squarylium, a derivative of square acid, into thin films that have an energy-conversion efficiency of about 0.2%, roughly 10 times better than any previously obtained efficiency for a photovoltaic organic semiconductor.

Although inorganic photovoltaic semis have a better 4% efficiency, researchers at IBM indicate that it is possible to make the organic semis competitive with the inorganic by doping the organic film.

Minifloppy cuts cost of disc storage—maybe

A new floppy-disc memory that features a smaller disc and reportedly reduces the cost of disc memories by one-third has been introduced by Shugart Associates, Sunnyvale, CA. The Minifloppy sells for $390 in unit quantities, compared to $600 for the standard-size floppy.

Although the cost of owning a Minifloppy appears cheaper than owning a regular floppy, the Minifloppy is really much more expensive. In fact, on a per-byte basis, the Minifloppy is almost twice the price of a standard floppy.

The reason for the greater cost is the new unit uses a smaller 5-in. disc that holds between 80 and 90 k-bytes of data, depending on the coding format used. The standard floppy's 8-in. disc holds 250 k-bytes of formatted data. Thus, in unit quantities, the Minifloppy costs 0.43¢/byte for the drive, while the standard floppy costs only 0.24¢/byte.
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FCC swamped with complaints as sources of RFI/EMI increase

Radio-frequency and electromagnetic interference from a phenomenally growing number of sources, such as CB sets, consumer electronic devices, video games, computers, switching power supplies, ignition systems, and industrial, scientific and medical equipment has reached proportions beyond the effective control of the understaffed Federal Communications Commission.

Complaints of interference from the public—not including military and government agencies—have been pouring into the FCC at the rate of 100,000 per year. Currently, 87% of all complaints of interference to home electronic entertainment equipment—televisions, high-fidelity sets, FM receivers, electronic organs—involves Citizen's Band (CB) transceivers.

The CB units have interfered with nearly every mobile and fixed-communication service, including business, industrial, law enforcement, utilities, aircraft and other public safety devices.

While the problem of CB interference has received wide publicity and attention, it is, for the FCC only the tip of an interference iceberg, admittedly a big tip.

Aircraft navigation and communications equipment has been seriously interfered with from a wide variety of other RFI sources, including garage-door-opener transmitters, industrial rf heating, medical diathermy equipment, community-antenna television systems, super-power FM stations, and auto ignition systems.

In fact, electronic automotive systems for the control of braking and fuel injection have been disabled by transmissions from mobile equipment in passing vehicles.

Sensitive medical equipment in hospitals has been made inoperative by the radiation from nearby television or broadcast-station transmitters as well as by broadband EMI from surgical cauterizing equipment.

Further compounding the radio frequency interference (RFI) and electromagnetic interference (EMI) problems for the FCC is the appearance of literally millions of potential sources of interference in consumer devices. These devices include the familiar coin-operated electronic games with video monitors, consumer TV games with the outputs attached to the antenna terminals of the home receiver, switching power supplies, computers, and other devices incorporating clocks driving digital circuitry.

Confronting the problem of controlling RFI/EMI emissions, the FCC finds its task further encumbered by the continued development and proliferation of highly sensitive receivers in the consumer entertainment field, in mobile communications and in medical instrumentation.

‘David’ responds

Faced with the Goliath of RFI/EMI from licensed and regulated as well as unregulated sources, the public’s David—the FCC—has taken two approaches to the problem that unfortunately will add to the design requirements and costs of millions of future products incorporating any kind of electronic source of interference.

In the first place, the FCC has adopted stricter regulations for RFI emitters like CB equipment, even though the regulations are not completely satisfactory to anybody involved: the CB manufacturers; their principal adversary, the TV industry; even the FCC.
With a line of minis and micros like ours, we don't have to push any one of them.

With other companies, you might set out to buy a microprocessor chip and end up with the whole chassis. Or get a box when all you need is a board.

But Data General doesn't work that way. We don't have to push you into buying something you weren't really looking for. Because we can let you choose from microprocessor chip sets, microcomputer boards, completely packaged MOS minis and full-blown NOVA 3 systems. All four are compatible. And they give you a range of performance with a range of prices.

So, if you're a component user, there are both high-performance microNOVA chip sets and microcomputer boards that feature Data General's mN601 microprocessor. The mN601 is a full 16-bit NOVA-on-a-chip. And the microcomputer is a full 4K-word computer-on-a-board. You package them yourself, for greatest economy. (Speaking of economy, the board costs only $589 in OEM quantities of 100.)

And if you're not ready for components yet, there's our fully-packaged microNOVA MOS minicomputer. It's available with up to 32K words of MOS memory and peripherals like our diskette subsystem. And it's supported by our Real-Time Operating System and diskette-based Disc Operating System.

If you need bigger systems capabilities, take a look at our NOVA 3 computer. It's compatible with our microNOVA family. And it runs with high-performance peripherals, sophisticated software like Real-Time Disc Operating System, high-level languages like FORTRAN 5 and BASIC, and memory expansion to a full 128K words.

We've got it all. But we won't try to sell it all. Unless it's what you really need. If you don't believe that line, call us. Dial 800-225-9497 (in Massachusetts, 1-617-485-9100, extension 2509) and ask for information on microNOVA and on the free half-day microNOVA seminars that happen this fall all over the country.

Or write for our microNOVA and NOVA 3 brochures. And see for yourself.

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CIRCLE NUMBER 9
In addition, the FCC has proposed revisions which will strengthen two crucial sections of its regulations, Parts 18 and 15. The former regulates industrial, scientific and medical equipment. The latter covers devices with low-power intentional radiation, such as wireless intercoms, and devices with unintentional radiation, such as electronic games.

New regulations and standards are also being considered where none now exist, such as for gasoline-engine ignition systems.

A change in philosophy

A development with far-reaching implications is a change in the Commission's basic philosophy that will strongly influence future designs of all communications equipment susceptible to RFI/EMI. Historically, the FCC has considered the emitters of interfering radiation the villain. But with emitters growing by the millions, the FCC—apparently motivated by the philosophy, "If you can't beat 'em, join them"—is now considering imposition of regulations requiring the manufacturers of consumer-entertainment electronic equipment to make their products RFI/EMI-proof.

Currently, the FCC has no legal authority to do this. But this authority would be granted under bills filed in Congress by Senator Barry Goldwater and Congressman Charles Vanik to amend Section 302 of the Communications Act.

Key provisions of the Goldwater Amendment, introduced Feb. 25, 1976, include the following (proposed changes italicized): "SEC. 302. (a) The Commission may, consistent with the public interest, convenience and necessity, make reasonable regulations governing (1) the interference potential of devices which, in their operation, are capable of emitting radio-frequency energy by radiation, conduction, or other means in sufficient degree to cause harmful interference to radio communications, and (2) the use of protective components in audio and visual electronic equipment which are capable of reducing interference to such equipment from radio frequency energy.

(b) No person shall manufacture, import, sell, offer for sale, or dispose of devices and electronic equipment or use devices which fail to comply with the regulations . . ."

A survey of the electronics industry's consumer-entertainment-product manufacturers failed to turn up any proponents of mandated regulations on consumer equipment.

"We don't like to see any regulation on susceptibility," says Robert Grant, chief engineer for government compliance at Magnavox and chairman of the Electronic Industries Association (EIA) Interference task force. "The big problem we have now is the fact that there are no good test methods and..."
Greater RFI/EMI shielding in new, narrow-width contact strips from Instrument Specialties

Insufficient data to render a natural text representation.
The growth of EMI/RFI sources and receivers by the millions mandates a design emphasis on the use of components to minimize electrical noise and its effects. These components include: power-line filters (A) by Corcom, Chicago, IL; hermetically sealed, ceramic low-pass filters (B) by Erie Technological Products, Erie, PA; ferrite beads for reducing rf noise (C) by Fair-Rite Products, Wallkill, NY; knitted-wire mesh and conductive-elastomer gaskets for sealing enclosures against EMI (D) by Tech. Wire Products, Cranford, NJ; low and high-power transient-absorbing varistors (E) by General Electric, Syracuse, NY, (F) by Matsushita Electric, Secaucus, NJ, and (G) by Mepco, Morristown, NJ; and fast-acting clamps and crowbars (H) by General Semiconductor, Tempe, AZ, and (I) by MCG Electronics, Deer Park, NY.

equipment to measure susceptibility in order to comply with any regulations."

Grant did point out the considerable efforts of the National Bureau of Standards and various industry technical groups to develop susceptibility-measurement techniques.

No more design afterthoughts

As a result of the rule tightening and the forecast of even greater restrictions, interference control in emitters and suppression in susceptible receivers will no longer be an afterthought of design. Instead, they will substantially increase total development time.

Experts in the EMC field predict imminent shortages of EMC specialists for in-house development of new electronic devices and systems because for years interference control as an element of design has been neglected.

By adopting tougher require-

ments and rules to alleviate interference the FCC has found itself in the impossible position of trying to satisfy the technical requirements of opposing parties with conflicting economic interests. A classic case is the controversy between the CB and the TV manufacturers.

The effect of these conflicting considerations can be seen in a new FCC rule making (Docket 20120). The rule tightens CB-transmitter harmonic radiation specifications by increasing the harmonic-suppression requirement from -50 dB to -60 dB below the carrier. To achieve this new limit will require additional filtering in CB-transmitter antenna circuits, claims Hugh Barnes, vice president of E. F. Johnson Co., Waseca, MN.

Furthermore, this tougher spec must be satisfied with the connection of all permissible attachments, including external speakers, microphones, power cords and antennas.

Another new requirement: If insufficient harmonic suppression causes interference on TV channels 2, 5 and 6 of a neighbor's set, the guilty CB owner must insert a low-pass filter between the antenna rf-output jack and the antenna feedline.

Battle lines drawn

The new spec naturally has aroused strong differences of opinion between the CB and TV-set makers. As originally proposed by the FCC, the requirement was -70 dB, but the Commission softened its stand by -10 dB despite the TV-set manufacturers' united request for -112 dB, submitted by the EIA's Consumer Electronics Group.

CB makers are backed by the Citizens Radio Station of EIA's Communications Division. John Sadowsky, EIA staff vice president of communications, states the CB case:

"The Citizens Radio people contend that legally operated citizen's radio sets don't cause interference to TV sets. And when such interference does happen, it's the fault of the wide-open front end of the TV receiver."

Joseph DeMarinis, director of engineering for GTE Sylvania, Batavia, NY disagrees:
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Low cost R16 Series. Easily mounted p.c. board module. Delay on operate ranges: 0.2 to 2, 2.0 to 30, 5.0 to 100 sec. Potentiometer or resistor adjustable.

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Go with the Pros and you can't go wrong.
The feasibility of eliminating TV interference by RFI-proofing a CB set is demonstrated by GTE Sylvania at test site. With bare CB the RFI is objectionable (upper and lower left). When CB unit is shielded and filtered, the RFI on TV channel 2 is below the perceptible level (upper and lower right).

"The filtering and shielding of a TV set is an order of magnitude, or more, better than the state of the art of CB transmitters. Further improvements in the TV set will not be noticeable until the harmonic radiation levels of the transmitters are further reduced."

The principal obstacle facing the TV-set designers is that CB transmitter harmonics fall within the bandpass of TV channels. Hence, the recommended -112 dB level from the TV industry.

"Traps can't be used for in-band CB interference," explains DeMarinis. "And in order to even notice the fundamental of a nearby CB transmitter overload the TV receiver, the harmonics must first be lowered substantially.

"If the TV set is overloaded with a fundamental, harmonics are generated inside the tuner, and traps can be put in for that. We've taken a CB transmitter and added the filtering we think it should have. In tests on our 100-ft radiation site the TVs perform well."

For those CB makers pleased with the new -60 dB requirement, the FCC has added a warning to its ruling: "We believe that further tightening of the harmonic-suppression limit in the future will be necessary."

While CB transmitters have been widely recognized as sources of interference, less known is the fact that the radiation from oscillators of CB receivers has been creating interference problems for three public services: the Power Radio Service used by electric, gas, water and steam utilities in the 37-MHz band; the aircraft services band, 100 to 135 MHz; and the Forestry Conservation Service operating on 151.205 and 151.400 MHz.

Synthesizers cause interference

Interference to Power Radio Services stems from the heterodyne type of frequency synthesis used by many 23-channel CB receivers. To minimize the number of crystals the 23 oscillator frequencies are obtained by heterodyning the outputs of two oscillators. One uses crystal at 37.6, 37.65, 37.7, 37.75, 37.8 and 37.85 MHz. The other has crystals at 10.150, 10.170, 10.160, and 10.140 MHz. The combined total is 10 crystals for 23 channels.

The 37.6, 37.7 and 37.8 MHz frequencies happen to be those used by the Power Radio Service. To alleviate interference of all three services, the FCC amended Part 15C by adding a new Section 15.59 that requires the certification of CB receivers to new, low limits of oscillator radiation.

The limit of receiver oscillator radiation within a band of 25 to 500 MHz was reduced to 2.0 nW at the antenna terminals for receivers produced after Jan. 1, 1977. The lower level of 0.2 nW will be effective for receivers produced after Jan. 1, 1978.

With the CB receiver's antenna terminals connected to a shielded resistor equal to the rated input impedance, the emission at any frequency from 20 to 500 MHz is limited to a maximum of 5 \( \mu \)V/m, measured at a distance of 3 m, for those receivers produced after Jan. 1, 1977. The measurements must be made with the microphone and all other options attached to the set.

If the CB receiver can be connected to ac power lines, the conducted interference fed back into the lines must not exceed 100 \( \mu \)V at any frequency between 0.45 and 25 MHz. This requirement also applies to a battery-operated CB receiver that can be connected to the power line through a battery charger.

The manufacture of CB receivers not certified to meet these requirements must cease no later than Aug. 1, 1977, while the sale of noncertified units must end by Jan. 1, 1978.

Interestingly enough, the great majority of the new 40-channel CB equipment will employ a phase-locked-loop synthesizer using two IC chips and a single crystal. This
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innovation provides a better performance at lower cost than can be provided with the two-oscillator synthesizer. In addition, using the PLL system will eliminate the Power Radio Service’s interference problem.

FCC vs bootleggers

Illegal or bootleg rf amplifiers increase the CB-transmitter output many times its legal 4-W limit. The sale of these amplifiers—they are usually discovered in CB base stations—has been banned since August, 1975.

But a few irresponsible CB suppliers are making available to the CBer broadband linear amplifiers that can be sold legally for use in the amateur band. These amplifiers, the FCC points out, can be driven only by 3 or 4 W, so the subterfuge is obvious. Few amateurs have exciters with that low a power; most exciters are in the 100-W class.

To help combat bootleg operations and other sources of CB interference, the FCC’s Field Operations Bureau is investigating a random selection of TV-interference complaints. The bureau is engaged in the following activities:

- Monitoring a CB station unannounced to determine if a linear amplifier or other illegal accessories, such as a variable-frequency oscillator or a power microphone, are part of the CB setup.
- Inspecting CB-station equipment for spurious emissions through the use of spectrum analyzers. New test procedures for measuring such parameters as radiation from the CB cabinet are also being used.
- Inspecting a complainant’s TV receiver for received signal levels and antenna quality.
- Installing high-pass filters on the TV receiver and low-pass filters on the offending CB set.
- Making a neighborhood survey to determine the impact of interference on the local area around a CB set.

One result of the stepped-up monitoring activity was the seizure of over $10,000 worth of CB equipment used by eight unlicensed operators in Northern New Jersey. The culprits were engaged in illegal operations plus a year in jail, and a maximum $10,000 fine for unlicensed operation.

Most of the FCC regulations governing consumer electronics devices and equipment appear in Parts 15 and 18 of the Commission’s Rules. But Part 15 has not been amended since 1948, and the basic technical specs of Part 18 have remained the same since 1946.

Since then, however, vast technological advances have occurred. Semiconductors, integrated circuits and digital systems have appeared. Many new devices, operating at frequencies substantially higher than in the late 40s, present new interference problems.

Consequently, the FCC has proposed overdue changes to Part 15 (Docket 20780) and Part 18 (Dockets 20718).

(continued on page 34)
Down to earth economy from CTS

Overall cermet resistor network economy is what CTS has been putting into modern systems for well over a decade. For example, Series 760 DIP cermet networks, purchased in quantity, can cost less than 30¢ each.

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One proposed change in Part 15 is the certification of restricted-radiation devices with relatively high interference potential that are being widely distributed to the public. These include electronic (coin-operated) games that use rf energy, rf switching supplies operating above 10 kHz, wireless intercoms, and any other restricted radiation device that uses rf energy for the purpose of communications. Other devices will be added to the list as the need arises.

To certify these devices, the FCC proposes to discard its 1948 maximum-emission standard of 15 \( \mu \text{V/m} \), measured at a distance of \( \lambda/2\pi \). The Commission wants to substitute a table of radiated and power-line-conducted emission limits, with the latter measured between each power line and ground (see tables).

Switching-power-supply manufacturers claim that to conform to the new proposed emission limits would, in many cases, call for costly re-designing, a preview of the coming mandated emphasis on electromagnetic compatibility (EMC).

Wally Amos, chairman of the Computer and Business Equipment Manufacturers Association (CBEMA) subcommittee on EMI/RFI, differs with the FCC's proposed switching-supply standards:

"The FCC proposes to decrease the conducted limits of noise voltage measured with frequency while we would increase it. In the 10-MHz range, our limit is 70 dB above 1 \( \mu \text{V} \) (3 mV), while the FCC's is 40 dB (100 \( \mu \text{V} \)). This is a stringent and costly limit that is not necessary to protect communications services.

"Even more expensive is the FCC's extension of frequency limits down to 100 kHz, where filter components become large and costly. CBEMA advocates a lower limit of 450 kHz."

A real headache for the FCC is the TV game that can be connected to the antenna terminals of the owner's set. About 30 were announced at June's Consumer Electronics Show (ED, No. 15, July 19, 1976, p. 21).

"These games are potentially as popular as CB sets," says Milton Mobley, chief engineer in charge of the FCC's testing laboratory in Maryland. "We've had more applications for TV-game type approval in the second quarter of '76 than we had in the past four years.

"Toy firms with little or no expertise in EMI or RFI jumped onto the TV-game bandwagon. Rejection rate for new companies is more than 50% at the present time because the technical regulations are very strict for these Class I TV devices."

Even your hand drill

A number of interference sources producing random broadband electrical noise can be just as disruptive to communications as the narrowband emitters, such as CB sets.

These broadband sources, called incidental-radiation devices, include electric motors, hand drills, home appliances, light dimmers, electric-tool speed controls, and ignition systems.

As yet, these devices are unregulated by the Commission. However, complaints of interference from these products have increased.

For one of these broadband sources—ignition systems—the FCC has initiated a Notice of Inquiry (Docket 20654) to examine the advisability of establishing EMI-emission limits. The Commission has already conducted both in-house and outside studies on different facets of the problem. For example, the FCC measured the ignition-radiation levels of 10,000 vehicles at land-mobile communications frequencies. The Commission decided that objectionable degradation of communications had occurred, particularly in high-density urban traffic.

The Motor Vehicle Manufacturers' Association of the United States responded to the FCC's inquiry by questioning the validity of the FCC's test program of the 10,000 vehicles.

The U.S. automakers oppose mandatory FCC standards because, for one thing they abide by the voluntary Society of Automotive Engineering (SAE) Standard J551C. Nonetheless, the Detroit manufacturers have been working overtime for months to bring the ignition noise of their 1977 models within mandatory limits established by Canada's Dept. of Communications effective as of Sept. 1. These limits are required for cars manufactured or imported by Canada, parallel J551C.
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Basically, the purpose of the PIC is to generate a modified address to "ROM in response to prioritized inputs. Each interrupting device is assigned a unique ROM location with the starting address of the appropriate service routine. After the MPU responds to an interrupt, the PIC directs it to the proper memory location. The PIC also generates a Stretch signal, so the interrupt structure can be designed to accommodate the faster operations anticipated with improvements in processor speeds.

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<td>D40C</td>
<td>NPN Darlington</td>
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<td>D40D</td>
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<td>D40E</td>
<td>NPN/PNP 30-85 V</td>
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<td>D40K</td>
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<td>D40P</td>
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FCC to seek comsat regulation

The U.S. Position at the next World Administrative Radio Conference on 11.7-to-12.2-GHz broadcast satellites will be that orbits and frequencies should be subject to minimum regulation, the Federal Communications Commission announced.

The U.S. position is based on a 15-month study in which U.S. companies took part. If the position is adopted, participating countries will be permitted to move their communications satellites in orbit only one time each for a maximum distance of 10 degrees of longitude. The satellites would also have to be stable in orbit to within 0.1° of longitude. The study did not recommend a figure for antenna accuracy, but the FCC will propose 0.2°, which is a feature of the upcoming Intelsat V satellite and the current 6.4 GHz U.S. domestic communications satellites.

The conference will convene in Geneva, Switzerland, Jan. 10.

Navy testing new ship electronic defenses

The Naval Electronics Systems Command is due in October to complete operational evaluations of a new low-cost electronic-warfare suite for its patrol frigates and destroyer escorts, and possibly for a new anti-submarine warfare helicopter as well.

The system is known as the Design-to-Price Electronic-Warfare Suite (DPEWS), and the Navy is testing prototype hardware submitted by Hughes and Raytheon. Each firm has been asked to submit cost proposals for 285 production systems. The production contract will be awarded early next year.

Under the design-to-price restrictions, the unit cost of the basic DPEWS, which provides only threat warning, will be limited to $300,000 in production. The top-of-the-line system, which incorporates threat warning, surveillance and defensive electronic countermeasures, will be limited to $1.4 million in production.

Although initial production will cover only shipboard installations, the DPEWS has been specified for the Navy's planned Light Airborne Multi-Purpose System (LAMPS) ASW helicopter. Approval for at least 200 of those helicopters is expected next spring.

Soviets favor U.S. microwave landing system

The United States is picking up support from an unexpected quarter in its bid for worldwide adoption of the time-reference, scanning-beam
(TRSB) microwave landing system: the Soviet Union. Except for Australia, which has also proposed a TRSB system, all other countries favor the doppler system. The International Civil Aviation Organization (ICAO) will choose one as the global standard.

The Soviets are building TRSB hardware but have not put it into operation yet, according to Jeff Cochran, associate administrator for engineering and development at the Federal Aviation Administration, who recently returned from a tour of Soviet air-traffic-control facilities in Moscow and Leningrad.

Cochran said the Soviets were interested in increasing cooperation with the United States in such air-traffic-control areas as collision avoidance and discrete-address beacon systems (DABS). The Soviet Union has an automated terminal air-traffic-control system, which Cochran considered "roughly equivalent" to the U.S. ARTS III (air-terminal) system. The Soviet equivalent contains alphanumeric displays with altitude-encoding capability.

Drone aircraft contract protested

Teledyne Ryan, the losing bidder in the Air Force's competition for the Compass Cope multipurpose drone aircraft, has protested the selection of Boeing on the grounds that Teledyne, not Boeing, was the low bidder and the Air Force overestimated its cost proposal.

The protest was filed with the General Accounting Office after the Air Force awarded Boeing a $77.2-million engineering-development contract to refine electronic subsystems and deliver three prototype vehicles. Only $2.75-million of that contract was actually obligated, however, pending Defense approval of a mission for the drone aircraft. Congress voted $6 million to the program for the coming fiscal year but directed the Air Force to spend not more than $3 million until the mission could be defined.

Compass Cope is envisioned as a replacement for manned aircraft used to pinpoint the location of enemy anti-aircraft missile radars behind battle lines. The Air Force plans to procure up to 100 of the drones, and might also use them to carry side-looking airborne radars, communications relay systems and ocean-surveillance sensors.

The principal aim of the subsystem program is to develop a more reliable dual-digital flight-control system. Honeywell, a Boeing subcontractor, will deliver a brass board system to replace the analog system used in the initial flight tests. Univac, another subcontractor, is developing a continuous-wave (CW), frequency-modulated command guidance system to replace the pulsed microwave system also used in those tests. Since the initial system used vacuum-tube technology and had to be multiplexed for the down link, it was susceptible to multipathing problems.

Capital Capsules: Dr. Richard C. Atkinson, on leave from Stanford University, has been named acting director of the National Science Foundation following the appointment of Dr. H. Guyford Stever as presidential science advisor (ED, Washington Report, Sept. 1). . . . The National Oceanic and Atmospheric Administration will use an airborne infrared doppler lidar (light radar) this September to measure the velocity of water particles in waterspouts off Key West, FL. By measuring the doppler shift of the particles, the researchers will be able to keep the aircraft (hearing the lidar), a T-28, a safe distance from the storm.
Sprague puts more passive component families into dual in-line packages than any other manufacturer.

Call Sprague First!

DIP MULTIPLE TANTALUM CAPACITORS

Solid-electrolyte tantalum capacitors with 2 or 4 sections per package. 8- or 16-pin configurations. Standard ratings are 6.8 µF @ 35V, 15 µF @ 20V, 22 µF @ 15V, 33 µF @ 10V. Capacitance tolerance, ±20%. Operating temperature range, -55°C to +85°C. Write for Bulletin 3542 or circle 151 on reader service card.

DIP MULTIPLE CERAMIC CAPACITORS

Monolythic® construction... alternate layers of ceramic dielectric material and metallic electrodes are fired into a solid homogenous block. 2, 4, 7, or 8 capacitor sections per package. Standard tantalum ratings, 16 pF to 0.1 µF @ 100V. Capacitance tolerance, ±20%. Write for Bulletin 6242 or circle 152 on reader service card.

DIP MULTIPLE METAL-FILM RESISTORS

Noble metal film resistors encased in protective glass. Choice of 7 or 8 resistors per 14- or 16-pin package. Resistance values, 50Ω to 100,000Ω. Power dissipation, 125mW. Standard resistance tolerance, ±5%. Operating temperature range, -55°C to +70°C. Write for Bulletin 7042 or circle 155 on reader service card.

DIP PRECISION RESISTOR NETWORKS

Noble metal film resistors in pull-up, pull-down, interfaci ng, and terminating configurations, for applications requiring repetitive resistance patterns. 14- or 16-pins. Up to 28 resistors per package. Individual resistors from 50 to 100,000Ω. Dissipation, 125 mW. Write for Bulletin 7042 or circle 156 on reader service card.

DIP MULTIPLE PULSE TRANSFORMERS

Four transformers in 16-pin package. All cores have exclusive protective coating. Inductance values from 10 to 1000µH. ET product values of 5 volt-µsec. Choice of four turns ratios... 1:1, 2:1, 3:1, 4:1. Operating temperature range, 0°C to +70°C. Write for Bulletin 40400 or circle 157 on reader service card.

DIP TAPPED DELAY LINES

Lumped constant delay lines... ideal for timing and pulse synchronization circuits. 14- or 16-pin packages with delays of 50, 100, or 150 nanoseconds at a characteristic impedance of 100Ω. Working voltage, 50 VDC. Operating temp. range, 0°C to +70°C. Write for Bulletin 45004 or circle 158 on reader service card.

Popular Types Now Available OFF-THE-SHELF From Your Sprague Industrial Distributor.


THE BROAD-LINE PRODUCER OF ELECTRONIC PARTS

Sprague®
THE MARK OF RELIABILITY

Electronic Design 20, September 27, 1976
What makes The faster and easier?

...Rapidograph, Rapidometric, Rapidograph SL

Finest precision, highest quality Technical Pens offer the most complete range of line widths. Points available in hard chromed stainless steel, sapphire jewel and tungsten carbide.

...Pelikan and Koh-I-Noor Drawing Inks

Specially formulated for the most exacting requirements.

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A virtually indestructible film with a fine-toothed surface for maximum precision and reproducibility in engineering drawings.
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Erasures can be made on the film with confidence and ease without marring the film surface, as often as required.

...System accessories
Designed to make drafting with ink on film even easier than you might suppose.

What makes us the authority?
Koh-I-Noor has developed Rapidraw, a System of totally integrated instruments and materials, providing a remarkable simplification of drafting techniques. This System makes direct ink drafting on film the most practical method to achieve precision engineering drawings, as confirmed by leading industries. We would like to give you a free manual completely describing our System.

YOU GET MORE FROM KOH-I-NOOR

Koh-I-Noor Rapidograph, Inc., 100 North Street, Bloomsbury, N.J. 08804
In Canada: Koh-I-Noor/Canada/Ltd., 4180 Ave. de Courtrai, Montreal, Quebec H3S 1C3.
Yes, we gotcha DECwriter II and we did it with such standard features as: matrix impact printing (no thermal paper!), 132 column print width, microprocessor electronics, portability (SuperTerm weighs less than 45 lbs), high speed (10, 15, 30, 45 and 60 characters per second are standard with 120 and 180 cps being optional), an IBM Selectric configured keyboard, a 33 key alphanumeric "gear shifted" key pad and a quick loading cartridge ribbon system.

In addition, SuperTerm's unique "anvil" printhead design is warranted for the life of the terminal! This means that should you ever encounter defects in printhead workmanship, Intertec will replace or repair the defective component(s).

OEM's will be pleased to learn that the Intertec SuperTerm provides all of this capability and more at an OEM price of only $1,400.

Low cost options available on every SuperTerm include: Super and subscripting, horizontal and vertical tabs, variable vertical pitch, forms control, pagination, direct X/Y addressing, adjustable left and right margins, reverse printing, double width characters, automatic CR on end of line, and a font programmable character set.

If your application calls for APL/ASCII, SuperTerm has that too. In fact, SuperTerm has got just about everything—except competition.

Want more? You've got it! A built-in micro-cassette (Supercette) is available to end users at only $700 in single quantities with OEM discounts available.

In addition to unparalleled price and performance, every SuperTerm is backed by Intertec's nationwide factory trained service network with over 160 service centers strategically located coast to coast.

For more information on the total performance and unparalleled low price that make the Intertec SuperTerm the very best buy for your terminal dollar, just call Intertec Data Systems, the only company with international sales, service and revolutionary SuperTerm.

INTERTEC DATA SYSTEMS
1851 Interstate 85 South • Charlotte, North Carolina 28208
Telephone (704) 377-0300 • TWX: 810-621-7831
Instrument analyzes µP systems in both data and time domains

The first µP analyzer geared for work in both the data and time domains in Davco's DM 230. Connect the unit's 40-pin squeeze clip across your µP, and you can look at the real-time waveforms of 32 input lines eight at a time on your own scope. Then flip some switches, and look at addresses and data on the 230's built-in hexadecimal readout.

With the analog capability, you can check rise and fall times, pulse timing, glitches and noise. The analog bandwidth of the 230 goes beyond 50 MHz, and its transition times are specified at less than 20 ns. Differential time delays stay below ±8 ns.

With the digital capability, you can record events that occur before or after an address that you set on thumbwheel switches. Up to 128, 32-bit words can be so captured. You can observe addresses and data side-by-side or hit a switch to see status registers along with a count of µP clock cycles.

Four LEDs on the Davco unit tell you that

(continued on page 51)

A low-cost EPROM programmer kit works under software control

Program and verify erasable, programmable, read only memories (EPROMs) under the control of your µP development system. Normally, transferring corrected programs that are in a RAM to a more permanent form of storage in EPROM may be done several ways. You can manually key in data on some programmers, or you can transfer RAM data to paper tape and then use that to drive a programmer, or you can output the RAM data, directly into another kind of programmer.

The first two methods are time-consuming and error-prone, requiring you take the intermediate step of reading out the RAM data into some other form to drive the programmer. The third method is most direct and least susceptible to error.

This method has been available on the Intel MDS system, at a system cost of several thousand dollars.

The Model 8700 kit, on the other hand, connects directly to a peripheral interface IC, the Intel 8255 PIA, for example, that is hooked into any development system. Under that system's control, you write contiguous bytes of RAM from the development-system memory into any manually selected starting address in an EPROM, then verify its contents. The EPROM must be a type 2708 or 2704, which are 1 k x 8 and 512 x 8 EPROMs, respectively. The supervisory program that does the housekeeping functions is not supplied. Flow charts are given, however, so you can write such a program.

Engineering Resources, 1903 Alameda Padre Serra, Santa Barbara, CA 93103. (805) 963-3801.
Ise introduces five new ways to make the competition turn green.

Your competition probably already thinks they're using the perfect display in whatever it is they make. Let them keep thinking it. While you prove them wrong with a new Itron display. They're designed to make the competition turn green. Which also happens to be the color of the segments.

All 17 of them on the 17-digit Itron. All 5 on the FG-512A1. Next comes an Alfa-Numerical Itron. A Linear-Analog Itron. And a Digital Clock Itron. Five ways to be heartless if you put a little heart into it.

Alfa - Numerical Display

Let them keep thinking it. While you prove them wrong with a new Itron display. They're designed to make the competition turn green. Which also happens to be the color of the segments.

Instruments & Large Calculator Display

FG6209M2

ef = 10V  ec = eb = 40Vp-p  ic = 10mAmp-p  ib = 8mAmp-p
Wd. 205mm  Lg. 40mm  Segment 9mm

FG179F2

ef = 7V  ec = eb = 35Vp-p  ic = 7mAmp-p  ib = 5.5mAmp-p
Wd. 170mm  Lg. 40mm  Segment 9.5mm

FG6512A1

ef = 3.5V  ec = eb = 24Vp-p  ic = 4mAmp-p  ib = 3mAmp-p
Wd. 100mm  Lg. 40mm  Segment 12mm

Digital Clock Display

FG425A1

ef = 5.5V  ec = eb = 35Vp-p  ic = 5mAmp-p  ib = 6.5mAmp-p
Wd. 140mm  Lg. 59mm  Segment 25mm

FG120S1

ef = 55V  ec = eb = 35Vp-p  ic = 4mAmp-p  ib = 0.2mAmp-p
Wd. 140mm  Lg. 40mm  Segment 8mm

Instruments & Terminal Units Display

Linear Analog Display

NORITAKE CO., LTD.
Electronics Office (U.S.A.)
22410 Hawthorne Blvd. Torrance California 90505
U.S.A.
Phone: (213) 373-6704.
Telex: 230674910

Electronics Division
1-1, Noritake-Shiramine, Nishi-ku, Nagoya City
Japan
Phone: NAGOYA (052) 561-7111.
Telex: J69738 NORITAKE

ISE ELECTRONICS CORP.
London Office
Norbit House 2, York Street W1H 1B, England
Phone: 01-639-7453 Cabled: LUCTUAL LONDON

NORITAKE WORLDWIDE
Phone: 01-561-7111
Telex: 230674910

CIRCLE NUMBER 25
Burndy's GTH connectors deliver good-as-gold reliability at a fraction of the cost.
FIELD PROOF

For high reliability and economy, GTH QKSTACK connectors are used in Honeywell’s new Series 60, Level 6 minicomputer.

For design flexibility and reliability, GTH FLEXLOK connectors are used by Aero Products Division of Litton Industries in the DIGIPROX™ ground proximity warning system.

For closer packaging density and high reliability, the GTH chassis Co-Planar connectors are used in Quasar’s remote control television.

With Burndy GTH connectors, you enjoy the performance characteristics of gold—without suffering its high cost. If that’s too hard to believe, just study the performance comparison chart.

The secret behind the amazing performance of GTH is the use of high pressure plastic deformation to achieve a gas-tight, corrosion-free contact, and a contact geometry that provides an ingenious mechanical interlock to insure good metal-to-metal contact despite vibration or thermal expansion.

Burndy GTH contacts not only eliminate the need for gold in the connector, they eliminate gold in the mating component as well. You save both ways—without sacrificing performance or reliability.

ADVANTAGES OF GTH CONNECTIONS

- **Low cost, high reliability:** Helps you cut interconnection costs up to 33% and more—without sacrificing reliability.
- **Interchangeability:** May be used with existing gold, tin or solder-plated components with no loss in reliability.
- **Design Flexibility:** Compact design for close packaging densities, simplified handling, installation and field serviceability.
- **Ease of Installation:** Requires no special tooling or operator training. Installs like any ordinary connector.

Unbelievable? Send for more proof. Simply check the convenient Quick Response Card and we’ll send you documented test data.
proof!
concept insures high-pressure, contact without the use of gold.

Spring force maintains contact pressure. Absorbs vibration, prevents fretting corrosion.

Unique contact geometry concentrates pressure at point of contact for gas-tightness.

Whisker-free tin-alloy plating.

Ordinary soft solder target rather than gold.

LABORATORY PROOF

TYPICAL CONTACT RESISTANCE VALUES (Milliohms)
After Environmental Test, at Dry Circuit Levels.
(Range of Values Within 99.9% Confidence Level)

<table>
<thead>
<tr>
<th>Environmental Test</th>
<th>GTH Contacts</th>
<th>Conventional Geometry Contacts</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Tin-Alloy Plate</td>
<td>15 Microinch Gold Flash</td>
</tr>
<tr>
<td>Initial</td>
<td>4.0 - 6.0</td>
<td>4.5 - 13.3</td>
</tr>
<tr>
<td>Thermal Shock</td>
<td>4.0 - 8.6</td>
<td>6.0 - 15.0</td>
</tr>
<tr>
<td>Humidity</td>
<td>4.5 - 7.0</td>
<td>10.1 - 31.8</td>
</tr>
<tr>
<td>Industrial Atmosphere</td>
<td>4.0 - 6.0</td>
<td>10.9 - 20.3</td>
</tr>
<tr>
<td>Gas Tightness</td>
<td>4.0 - 6.5</td>
<td>Not Applicable</td>
</tr>
<tr>
<td>Thermal Cycling</td>
<td>4.0 - 7.0</td>
<td>8.5 - 15.5</td>
</tr>
<tr>
<td>Durability</td>
<td>4.0 - 5.5</td>
<td>10.1 - 12.2 100 cycles</td>
</tr>
<tr>
<td>Vibration</td>
<td>4.0 - 5.5</td>
<td>5.0 - 5.0 5-500-5 Hz</td>
</tr>
</tbody>
</table>

IMMUNITY TO FRETTING CORROSION
Relative Lifetimes Under Accelerated Fretting Conditions
Without Lubrication

Cycles of Contact Fretting to Failure
Burndy GTH connectors: Your golden opportunity to cut connector costs up to 33%.

Burndy GTH connectors are available in all types of designs for all types of applications. All of them are currently being used to help control connector costs by some of the best known names in the electronics field. Names like Quasar Electronics, Litton Industries, Honeywell, National Semiconductor, Dictaphone, and Wang Laboratories to name just a few. Use the convenient Quick Response card for more information on how GTH can help you keep your competitive edge. We'll send you data that's worth its weight in gold.

QIKLATCH™ zero-entry Mother/Daughter PC connectors in sizes from 8 through 24 positions on .156" centers.

EDGE-TITE™ PC connectors in sizes from 10 through 50 positions on .100" centers.

QIKSTACK™ feed-thru connector. Board-to-board spacing from .250" to .625". Up to 30 contact positions.

EDGE-ON™ board-to-board receptacle. Up to 15 positions on .100" centers.

DIL IC SOCKETS for leaded packages, in sizes from 8 through 42 positions.

LED CONNECTOR board-mounted PC receptacle in a wide range of sizes and viewing angles on .100" centers.

FLEXLOK™ connectors for flexible circuitry and flat conductors in sizes from 6 through 21 positions on .100" centers.

CO-PLANAR solderless-wrap chassis connector in 15 positions on .156" centers.

HYPOINT™ leadless IC receptacles in sizes from 24 through 48 positions.
MICROPROCESSOR DESIGN

(continued from page 49)

selected address lines are active. To use this feature, turn the four hexadecimal address thumbwheels through all 15 positions, starting with the MSD, until all the LEDs light. When used with the 230's recorded information, the LEDs let you chart the system's program flow.

With another feature, a reset timer, you can weed out bad μP chips before the chips go into the system under development. To use the reset timer, set the thumbwheels to the address, or location, of the μP's reset vector (e.g., FFEE or FFFF for the 6800). Then throw a toggle switch, and the DM 230 will continuously cycle the μP, so that you can get a scope display of bus information.

Or you can single-pulse the μP to latch data into the 230's memory, then use the instrument's digital modes for analysis.

The Davco unit's $2900 price includes one probe buffer: electronics used to match the 230 in the μP under test. Buffers are now available for either the 8080 or 6800 μPs. Additional buffers cost $750. A printer option is also available. Delivery of the DM 230 takes 60 days. Davco Manufacturing Co., 169 Ridgedale Ave., Morristown, NJ 07960. (201) 267-4990.

CIRCLE NO. 505

PC board does floating point BCD functions for 8-bit systems

The Model A Floating Point Board performs add, subtract, multiply, and divide with up to 14 BCD digit accuracy, in record time. With a typical add/subtract time of 20 μs and multiply/divide time of 100 μs, your 8080 system operates at speeds, claimed by the manufacturer, to surpass most minis.

If floating point arithmetic were done by software routines in an 8080 system, it would take milliseconds to complete. Furthermore, such routines would take about 1-k bytes of memory. This card takes only about 30 bytes of your system's memory for the numbers. Extended Basic software accessing the board, in development systems, is available.

The Model A Floating Point Board costs $499 and is available on 30 days delivery. North Star Computers, Inc., P.O. Box 4672, Berkeley, CA 94704. (415) 527-6760.

CIRCLE NO. 506

Evaluator eases testing of 6800-based microprocessor systems

With the User System Evaluator just introduced by Motorola Semiconductor, manufacturers of products containing the 6800 microprocessor can now test them in a production environment.

Known as the M68USE, the evaluator consists of an M6800 processor module, an intercept module and a cable-and-buffer assembly. These modules make it possible to connect the Exorciser, Motorola's μP development system, to user-designed systems.

The interface between the Exorciser and the external system can be changed at will and modular options of the Exorciser—such as memory and I/O—can be incorporated into the external system during emulation. It is thus possible to compare simulated functions with actual functions performed by the external system.

In use, the processor module of the M68USE replaces the original MPU module in the Exorciser and is connected to the external system by the cable-and-buffer assembly. The intercept module connects a system analyzer to the processor module of the M68USE.

Motorola Semiconductor Products, P.O. Box 20294, Phoenix, AZ 85036. (602) 244-4556.

CIRCLE NO. 507

Two μP's are used to make development system 'crash proof'

The first “crash proof” prototyping and development unit has been developed for microprocessor applications.

Two μPs keep programs under development completely separate from the operating system in this new Signetics unit—dubbed TWIN from “testware instrument.” In other such devices, application-program malfunctions or operator errors can destroy or radically

(continued on page 52)
alter the resident operating system. But in TWIN, errors made in the development process cannot alter system integrity or software that has already been completed.

One microprocessor—a Signetics 2650—controls the whole system and is called the master; the second µP, a slave, is used for developing programs and for interfacing prototype devices. The slave CPU must match the one that will be used in the product being developed. This separation of central processors relieves the user of the housekeeping required to distinguish user programs from internal operations, and reportedly results in substantial savings in development time.

TWIN uses an assembler language with a syntax typical of minicomputer languages, and comes with a full range of supporting software... including a disc-based operating system, a text editor, a resident assembler and extensive debugging and diagnostic capabilities. Signetics, 811 E. Arques Ave., Sunnyvale, CA 94086. (408) 739-7700.

---

**A/d and d/a cards plug into popular development systems**

Analog interface cards plug directly into Motorola's Exorciser (6800) µP and Intel's MDS800 and SBC80 series of single-board computers. The cards, made by Burr-Brown, consist of separate a/d and d/a converters.

The a/d cards take either 8-differential or 16 single-ended channels, designated MP7208 and MP7216 for the Motorola system, and MP8408 or MP8416 for the Intel system. They output 12 bits into two words of the 8-bit wide data busses of the host systems.

The cards are resistor programmable, and have ±10 V to ±10 mV full scale ranges; with throughput accuracy of 0.1% on the most sensitive, down to 0.025% for the least sensitive (10 V) range. Conversion time ranges from 100 µs to 33 µs over the same full scales.

The d/a cards take 12-bit inputs and convert them to analog outputs, with strap-selectable unipolar or bipolar outputs, up to 10 V. Accuracy is 0.025% and output-settling time is 10 µs on all ranges. Model numbers are MP7104 for Motorola and MP8304 for Intel.

All boards in the series cost $695 (1-4). Burr-Brown, Airport Industrial Park, P. O. Box 11400, Tucson, AZ 85734. (602) 294-1431.

---

**A mobile-telephone-service control unit is given intelligence with a µP**

A mobile-telephone control head using a microprocessor has been introduced by Secode Electronics of Dallas. The control head is used in a system called IMTS—for improved mobile telephone service—and consists of a control head and transceiver. The control head generates and receives audio control frequencies that are used in these communications, and selects UHF or VHF-frequency pairs for full duplex (sending on one frequency, receiving on the other), service.

A Rockwell International PPS-4 4-bit µP was selected for the brains of the control head since only 4 bits are needed as input for dialing and as output for transceiver control. Previous control heads used only SSI and MSI logic. A µP was selected because the control head could be easily modified for use in non-IMTS systems, using different audio control frequencies and protocols, and reduced the unit's size and and chip count. The unit is also able to redial the last telephone number keyed in.

Secode Electronics, Div. of Communications Industries, Inc., Dallas, TX. (214) 742-7231.
extraordinary...
even for Data Precision.
Here's a miniature 3½ digit portable multimeter that delivers extraordinary performance and value for only $189.

Real miniature portability
Here is true miniature portability that delivers lab performance wherever you take it. And you can take it anywhere. The 175 operates from AC line, or rechargeable NiCad batteries for 6 hours of in-spec operation. Add this to the remarkably small size 1½"H x 5½"W x 3½"D, 34 cu. in., weight 22 oz. (4.45 x 13.97 x 8.89cm, 552cc,.63kg.) exceptional operating temperature characteristics, rugged construction...and you can see that this is real portability.

High performance
The Model 175 gives you 32 ranges of measurement capability, six functions, 0.1% DCV accuracy guaranteed for one year, and 100 microvolts resolution. You can measure DCV from ±100 microvolts to ±1000V, ACV from 100 microvolts to 500V with a frequency response of 30Hz to 50kHz, DC Current from ±100 nanoamps to ±2A, AC Current from 100 nanoamps to 2A with a frequency response of 30Hz to 50kHz, Resistance from 100 milliohms to 20 Megohms in two excitation voltages.

Right at home in the lab
Connect the 175 to an AC line and you have a great bench instrument. It's always recharging when line connected and ready to go into the field whenever you need it.

Data Precision proudly presents a 0.1% accuracy multimeter that brings the same high performance and value to 3½ digit portable instruments that our Model 245 brought to 4½ digit multimeters. The same levels of reliability, the same small size, the same great convenience and flexibility. The Model 175 has it all...and more for just $189.00.*

And the Model 175 gives you a lot more.
- Easy to Read, Big, Bright Display: 0.43" LED display for easy reading in dim light or bright light.
- Hi/Lo Resistance Measurement: Measure resistance in two modes. Hi excitation 2.5V (exceeds semiconductor forward threshold) and Lo excitation 300mV (below silicon junction threshold), for in-circuit resistance measurement without turning on semiconductor junction. No need to unsolder resistor.
- Automatic Zero: TriPhasic™ conversion eliminates need for any front panel zero control.
- Tells You When To Recharge: Blinking decimal point advises up to 10 minutes in-spec battery operation remaining.
- Overload Protected: It's forgiving. All DCV ranges can take ±1000V, all ACV ranges to 500V, all resistance ranges up to 250V...continuously—without loss of calibration or damage to the instrument. Current ranges are protected by 2A fuse easily accessible in a test lead.

Actual size, front view.

*Price U.S.A.
And Much More: Auto Polarity, 100% Overrange, Overload Indication, Internal DC and AC Current Shunts, LSI/CMOS Reliability, Exceptional Common and Normal Mode Rejection, Complete Documentation including NBS traceability and individually calibrated data sheet.

You get a complete package.

Everything you need to use the 175 is supplied with the instrument. Nothing else to buy. No extra costs. Standard accessories include the rechargeable NiCad battery module, line cord with recharger, a pair of fused test leads, alligator clips, carrying case and documentation.

Optional accessories that make the Model 175 even more versatile.

High voltage probe, AC current clamp, pedestal stand, rack mount, deluxe leather case and mini-to-standard banana adaptor.

The competition just isn't competitive.

The Model 175 is an extraordinary value offering the performance, size and price you want. Judge for yourself. The following is a comparison based upon manufacturers' data.

<table>
<thead>
<tr>
<th></th>
<th>Data Precision Model 175</th>
<th>HP 3435</th>
<th>HP 3176B</th>
<th>Fluke 8000 A</th>
</tr>
</thead>
<tbody>
<tr>
<td>Digits</td>
<td>3½</td>
<td>3½</td>
<td>3½</td>
<td>3½</td>
</tr>
<tr>
<td>Size</td>
<td>34 cu. in.</td>
<td>395 cu. in.</td>
<td>123 cu. in.</td>
<td>212.5 cu. in.</td>
</tr>
<tr>
<td>Display Size</td>
<td>0.43&quot; LED</td>
<td>0.30&quot; LED</td>
<td>0.25&quot; LED</td>
<td>0.25&quot; LED</td>
</tr>
<tr>
<td>Basic Accuracy</td>
<td>±1 Digit</td>
<td>0.1%</td>
<td>0.1%</td>
<td>0.3%</td>
</tr>
<tr>
<td>DCV Sensitivity</td>
<td>100µV</td>
<td>100µV</td>
<td>100µV</td>
<td>100µV</td>
</tr>
<tr>
<td>AC Frequency</td>
<td>30Hz-50kHz</td>
<td>30Hz-100kHz</td>
<td>45Hz-10kHz</td>
<td>45Hz-20kHz</td>
</tr>
<tr>
<td>Functions</td>
<td>6</td>
<td>5</td>
<td>5</td>
<td>5</td>
</tr>
<tr>
<td>Ranges</td>
<td>32</td>
<td>27</td>
<td>19</td>
<td>26</td>
</tr>
<tr>
<td>Hi/Lo Excitation</td>
<td>Yes</td>
<td>No</td>
<td>No</td>
<td>No</td>
</tr>
<tr>
<td>Calibration Accuracy Guaranteed</td>
<td>1 year</td>
<td>1 year</td>
<td>1 year</td>
<td>1 year</td>
</tr>
<tr>
<td>Overrange</td>
<td>100%</td>
<td>100%</td>
<td>10%</td>
<td>100%</td>
</tr>
<tr>
<td>Rechargeable Batteries</td>
<td>Yes</td>
<td>Yes</td>
<td>Yes</td>
<td>Optional ($50.00)</td>
</tr>
<tr>
<td>Recharges Batteries While Operating</td>
<td>Yes</td>
<td>Yes</td>
<td>No</td>
<td>Optional</td>
</tr>
<tr>
<td>Full Scale Voltage</td>
<td>100 millivolts (EIA STANDARD)</td>
<td>220-400 millivolts</td>
<td>100 millivolts</td>
<td>100 millivolts</td>
</tr>
<tr>
<td>Price With Batteries</td>
<td>$189.00</td>
<td>$400.00</td>
<td>$275.00</td>
<td>$349.00</td>
</tr>
</tbody>
</table>

All Model 175 specifications are covered by a one year warranty. Service is available from our worldwide service centers.

For complete information or a demonstration, contact your local Data Precision representative or Data Precision Corporation, Audubon Road, Wakefield, MA. 01880, (617) 246-1600. TELEX (0650) 949341.
The great anatomical anomaly

I think it was in some correspondence with Sigma Instruments many years ago that a long-forgotten sage put forth the observation that there are more horses' asses in the world than there are horses. Being an engineer, he expressed this in the form of an equation. It translates, roughly, to: the sum between the limits of zero and infinity of the horses' asses, greatly exceeds the sum of the horses.

As we read this expression, most of us chuckle and think of somebody we know. We think of Joe, who fell in love with the tunnel diode in 1960, and still wants to use it wherever possible. Or we think of Jack, who wants to run a Fourier analysis on every waveform he encounters. Or Frank, the frustrated football coach, who likes to give his engineers a pep talk every morning. Or Charlie, who's still trying to use up the supply of tantalum capacitors he was lucky enough to buy during the last parts shortage.

But we never think of ourselves. We never see that the anatomical anomaly may be a universal truth that applies to us, too. We don't see that, in the eyes of our colleagues, we may be Joe or Jack or Frank or Charlie. And that's good and bad.

It's good because that blindness protects some of us from seeing what's ugly or ludicrous in ourselves. It helps us overlook behavior that might be arbitrary, officious or arrogant; capricious or hypercritical; crochety, mean, rude, willful or stupid. It helps many of us avoid what we might be unable to bear.

But the blindness is bad, too. It conceals from many of us the personal flaws we might be able to correct.

All of us could be better with some flaw correction. We could become better engineers, better managers and better humans.
We’re introducing new products. Some are new developments we’re proud to take the credit for, and others we’re simply alternate sourcing. Some have broad areas of application and some are highly specialized, but they all have one thing in common. Somebody wants them.

That’s why our line of standards is so broad. That’s why we work so hard to offer you the best in reliability. That’s why we led the way with CMOS MSI and LSI. Motorola innovates . . . Motorola produces.

That’s the way it’s been at Motorola since we put our CMOS technology in gear, that’s the way it is now, and that’s the way we intend to keep it. By doing what you want, we get what we want.

**PRECISION MAKES IT THE SUPER ONE-SHOT**

Our new MC14538B is like our industry standard MC14528B Dual Monostable Multivibrator, with one great improvement. We added PRECISION, and made it the Super One-Shot. Pulsewidth variation from part-to-part and over the temperature range is a mere ±0.5%. Not RCA, nor National, nor anyone else can match it.

You’d naturally expect that kind of precision to cost a bundle, so maybe the best part of the Super One-Shot is actually the $1.76 price. Join the swelling ranks of Super One-Shot users today.

For information circle 241.

**ANALOG SWITCHES? PICK THE HOT ONES**

Our Austin, Texas "Silicon Ranch" is popping out great volumes of analog switches, and we’ve lined up some hot ones. The MC14066B quad analog switch/quad multiplexer is now generally preferred to the older MC14016 because it has significantly lower ON resistance at higher voltages. Try it at $.70. MC14051B, 14052B, and 14053B are, respectively, 8-channel, dual 4-channel, triple 2-channel analog multiplexer/demultiplexers. All three pin-for-pin replacements for the CD4051B, 4052B, 4053B can control analog signals over the full supply voltage range, and each is priced at $1.15.

For information circle 242.
Now it's practical to upgrade gate performance with Schmitt Triggers. The MC14584B Hex Schmitt Trigger and MC14093B Quad 2-Input "NAND" Schmitt Trigger eliminate race problems associated with gate and inverter functions like the MC14011 and MC14069 by squaring up slow changing waveforms. There's no need to change PC boards; they're direct plug-in replacements. Noise immunity also is superior. The kicker is price, and you never saw CMOS Schmitt Trigger prices like these. Each is $.54.

For information circle 243.

Can a CMOS MSI Phase Comparator with Programmable Counters find happiness in PLL applications? Judge for yourself. The MC14568B is barely introduced, yet more than a million units are already sold into PLL bliss. Programmable divide-by-N counters like the MC14522B and 14526B extend its counting range and coming soon is a dual BCD/binary counter (MC14569B), specially designed for operation with the 14568B. The plastic MC14568B is an MSI bargain at $2.61.

For information circle 245.

CMOS TRANSMITTER SENDS... TO REMOTE NMOS RECEIVERS

Start with a 22-channel CMOS LSI remote control transmitter, the MC14422, select the appropriate receiver from either the MC6525 or the MC6526, and you have the essentials of a versatile remote control transmitter-receiver system. Transmission is by time multiplexing five frequencies over widely spaced transmitter channels, precluding doppler effect interference. Use it for TV or radio, industrial controls, security systems, electronic games and toys, and anywhere low-power remote control is the object. The MC14422 carries a $6.10 price tag.

For information circle 246.

*McMOS is a trademark of Motorola Inc.

Note: All prices are based on plastic package and 100-999 quantity.
It pays to look into Metal Glaze™ from all angles.

We have designs on you. Especially if you're designing any type of low-power circuitry and need resistors with excellent load life stability and cost effectiveness.

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Another advantage, you can often double-rate our Metal Glaze resistors so you can use smaller resistors, saving board space.

The ability and toughness of Metal Glaze to withstand heat with minimum drift has been proven billions of times in all types of electronic equipment, worldwide. And they're available in ratings ≈ 3 watts, > 1% tolerance, with ranges as low as 1 ohm.

For complete resistor choice including Metal Glaze, carbon comp., thin-film, wirewound and networks, contact your local TRW authorized distributor or sales representative. Or TRW/IRC Resistors, an Electronic Components Division of TRW, Inc., 410 N. Broad St., Philadelphia, Pa. 19108, (215) 922-8900.
RG PULSE OR SURGE POWER RATING:
MAXIMUM APPLIED POWER/PULSE ON TIME

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1.5 150 Watts
2.5 15 Watts
30 Watts
10 Watts

Note: Average power dissipation not to exceed component rating.

Overload Protection
Rugged Metal Glaze construction provides excellent power surge capability. A 1/4w unit will conservatively operate within specifications when exposed to 16w, 10msec pulses, provided average power, and max voltage ratings are not exceeded. Ask us about your applications, including those requiring steady state conditions exceeding mil rated power.

TYPICAL TO-55 DESIGN TOLERANCE

Minimum Design Tolerance
(Design tolerance = a statistical summation of various parameters including load life, TCR, installation, and moisture resistance) All the features of Metal Glaze Resistors result in tight, predictable design tolerances which can be as low as -1.5%, depending upon your application.

TYPICAL DISTRIBUTION OF TEMPERATURE COEFFICIENT OF RESISTANCE

Absolute, Linear TCR
T.C.'s of 50, 100, or 200ppm are specified across the entire resistance range from 1Ω to 1MΩ. Our TC characteristic is essentially linear with temperature, and is a normal distribution centered near zero.

High Thermal Conductivity
A solid alumina substrate and other design features efficiently transfer heat from the resistor element. As an example, a 1/4w unit at full load has a hot spot temp rise of only 30°C, half the rise experienced in some other types. Cooler operation means stability and reliability are optimized.

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After a short while shopping for a digital multimeter, you may understand how a championship diver feels during competition: From the ground the board may be only 30 feet up, but from the board the water seems 300 feet down.

To keep the job of selecting a DMM within reasonable bounds, you must first brush aside the flotsam and jetsam of coined terms and short-changed specs. Then you must plunge deeply into the spec sheet to get the most for your money and the best box for the job; a casual approach can end up as a belly flop. Start with accuracy, one of the most fluid of all DMM specs.

Too good to be true

For any measuring equipment the first question you'll usually ask is: What's its accuracy? With DMMs, when the answer comes back as "0.1%" or "0.1% basic dc accuracy," the first thing to do is duck. Both numbers can be as deadly as a wild pitch.

Without saying a percentage of what, the 0.1% spec is meaningless. The "basic" spec might be OK. That is, if you lived in Utopia. In reality, no one-number spec can qualify a DMM's errors. Each range, each function, each set of environmental conditions carries its own inaccuracy handicap. Which does the DMM vendor highlight? Why the lowest, of course.

A DMM's inaccuracy should be spelled out for all conditions: as a function of time, temperature, line voltage, humidity, range, function, and more.

By the time you run down all the inaccuracy terms, that solid 0.1% basic accuracy has been chewed away to a shaky 1% or worse. How you combine the terms—straight sum or root-sum-square—can make a big difference, too.

Items like operating temperature range and accuracy tempco might be listed, all right. There's just one problem—the stated tempco doesn't hold or isn't linear over the full specified range. Or accuracy is specified over such a narrow range, you don't dare take the DMM out of the air-conditioned lab (which is kind of unfortunate if the DMM claims to be "portable").

The hedging over specs for temperature and

Stanley Runyon
Senior Associate Editor

That DMMs are becoming more versatile is signaled by the Digitec 2180, a unit that includes the measurement of decibels in its repertoire.
Pocket portables are getting smaller. Sencore's DVM 35 illustrates the trend toward lighter and more compact meters. The 3-digit 35 sells for only $124.

With internal µPs and memories, systems DMMs are growing in sophistication. This Hewlett-Packard unit is the first to offer a removable reference module.

It's a good bet that the same vendor writes his accuracy spec in disappearing ink. Or perhaps he'll give you accuracy as a percentage of full scale, alone or with other terms linked on. You can be sure he juggled the various terms so that no one term looks too poor.

For example, suppose a DMM's accuracy is given as ±0.5% of reading ±0.5% of range ±1 digit. What accuracy you'll get in practice now depends on where you are in what range scale and what ±1 digit means—in terms of the measured parameter, volts, amps or ohms.

On the low end of the range, errors can easily shoot past 5% of the reading. And that doesn't include the effects of temperature, humidity and other factors. Where is the DMM's advantage over the analog VOM now?

Don't forget that with a percentage-of-range spec, you must recalculate the possible error at every reading. And even though you can always switch ranges to get on to the more accurate portion of the next range, you might have to give up resolution to do so.

Another problem: when an autoranger switches its own ranges, will it do so for the best accuracy or resolution? Maybe not.

The percentage-of-range spec for fixed errors has long been a thorn in the sides of those who must specify meters. With the adoption some time next year of a new ANSI DMM standard (C39.6), accuracy will be stated uniformly as ± % reading ± a number of digits at a standard temperature or range. Perhaps C39.6 will finally remove the thorn.

Another deception the ANSI standard may squelch is the "overrange chop," a deft maneuver that neatly snaps errors in half—on paper, at least.

Don't count on your digits

To effect the chop, all a vendor need do in overranging DMMs is to define full scale with overrange included. Thus instead of dividing a fixed error by a full scale of, say, 1000 counts, the vendor divides by 2000 counts. Presto: half the error.

The word "overrange" would be well gotten rid of in any case for other reasons: 1. It's often confused with accidently going off scale, which is not what it means; 2. Overrange is usually specified in terms of a fractional digit, which tells you nothing about how many "extra" counts you get. (The new ANSI standard does drop the word, "overrange.")

Consequently, a 3-1/2-digit DMM may read to 1999 or perhaps even higher, but then again it may stop at 1100. There's no way of knowing since there's no agreed-upon convention. Best
Liquid-crystal displays are another trend in DMMs. The one used in the Danameter series of pocket portables draws so little power, the battery lasts for a year.

Still another source of confusion is the practice of mixing percentages and digits. Sure, you can easily convert from one to the other. But then the onus is on you—not the vendor—to come up with the right answer. You'll have to worry about what to count as full scale, and do so for all ranges on each function. Sound exciting?

Is there any easy solution to the problem of specifying accuracy? Perhaps not, though some have suggested an over-all, worst-case number for accuracy.

No matter how vendors specify accuracy, they must judge where to place both fixed and variable errors (offset, gain and linearity are the major errors), how to account for all the nibbling factors and what calibration cycle to specify. And this must be done for each function and for all ranges within the function. All in all, making the decisions is a tough job.

Representative of many of the advances in DMMs is Systron-Donner's 7003. With LSI circuitry, the unit offers true-rms measurements for less than $300.

For the ac functions, the job gets even trickier. Not only does ac accuracy suffer from the same ailments as the dc functions, it's got an additional problem—ac accuracy depends on the input frequency.

The rut-lined path to ac accuracy

If ac measurements are important to you, do more than casually glance at the DMM's ac specs. First, ac accuracy is almost always worse than the dc spec. Second, you can be certain that ac accuracy is given over a limited bandwidth to keep the number low.

Outside the stated bandwidth, accuracy plunges. You may have started out with 2% of reading at 1 kHz. By the time you get to 10 kHz, the 2% has dropped headlong to a poor 20%.

If there's no cliff in the spec to drop over, there may be local potholes, where accuracy dips at certain frequencies. You may find the holes on one range but not another. Where can you not find them? On the data sheet, naturally.

Beware when ac specs are given at spot frequencies, like 10 or 100 kHz. What happens in between is anybody's guess.

Remember, most DMMs use average detection and calibrate the readout for an rms reading. That calibration works for only one input—a perfect sinusoid. If your sine wave is distorted—and most are—reading accuracy degrades.

For a harmonically distorted sine wave, the error depends not just on the amplitude of the harmonic, but also on the phase and order. With a 3rd harmonic, for example—the one likely to give the worst reading—maximum error occurs...
Add a DMM to a portable scope and boost measuring power. The Tektronix DM44 reads not only resistance and voltage, but time intervals and temperature too.

at 0° or 180° phase, and can go as high as 14% at 30% distortion.

With more than one harmonic present, the situation becomes complex and pinning down errors isn't a trivial task. The answer here is to pay more money, and get a true-rms-responding DMM.

After you decide to do so, approach your favorite DMM supplier and ask: What do you mean by “true”?

To tell the truth

Like beauty, true rms is in the eye of the beholder. When it comes to DMMs, the truths being held aren't always self-evident.

There are those who believe that the only “true” true-rms converter is the one that responds to the equivalent heating value of the input signal. And there are those who stand with the mathematical approach, one that the heating group labels “quasi-rms.”

In the latter technique, active and passive circuit elements square the input components, take the average of the square and then find the square root of the average.

Which technique is best? Both have strong and weak points in terms of performance and cost. Generally, heating values are used in more expensive laboratory DMMs, while the mathematical calculation is common in lower-priced bench and portable models.

Which to choose depends on the bandwidths and waveshapes of the signals to be measured. Pin those down first, then see if the DMM in question can handle the inputs and still give the needed accuracies.

Check the range of the expected signal crest factors—the ratio of peak to rms value—then look up the DMM's crest-factor rating. Most signals found in practice don't carry crest factors greater than about 5. But gaussian noise and signals with long, narrow pulses can go much higher.

If the factor exceeds ten, you'll have to look for a unit with 1-MHz bandwidth or more.

After all is said and done, how important is accuracy anyway? How fully should it be specified? How much should you pay for it?

Too much of a good thing?

The answers to all three questions pivot on one key point: Know your job exactly, then match the DMM to the application.

By overstressing accuracy, you may overlook items of greater importance for the job at hand—items like protection or display brightness. Bear in mind that you'll probably pay dearly for high accuracy under wide temperature, time and frequency requirements.

Some observers see detailed, lengthy specs as cover-ups for inherent nonlinearities or inaccuracies. The argument goes that the vendor counts on the several noncorrelated effects to merge statistically—rather than to add up linearly—and so produce a better over-all spec. The counter argument: “Short, misleading specs border on the criminal.”

Whatever accuracy you decide on, be it 0.01% or 1%, realize that that number is ephemeral: Resistors drift with time. Trimmer pots and capacitors can shift with vibration. Insulation can deteriorate under attack by humidity, dust or air pollution. All of which means you must recalibrate a DMM periodically.

How often should you do so? As infrequently as possible, naturally. If you must recalibrate every 24 hours to keep 0.01% accuracy, forget it. The DMM literature should tell you what accuracy you'll get for various time intervals.

In fact, most DMMs are so specified. Unfortunately, not all units are specified alike. Thus you'll find numbers for 24 hours, 30 days, 60 days, 90 days, 6 months and 1 year. You may even get all six, or some other periods, on any one DMM. As a result of the nonstandardization, you can't always compare competing units.

If your Q.C. or cal lab dictates a recal period, then, of course, that's the interval to look for. However, you should also know both the short and long-term accuracies (whatever “short” and “long” mean to you). And you should know some other things, like:

Are all ranges calibratable? If not, how long does it take before those ranges drift out of spec? What must be done to get back into spec?
In your understandable concern for accuracy, burn one other thing into your mind: More digits buy more resolution, not more accuracy. And, sometimes, more digits don't even get you resolution.

Down for the count

On DMMs—or any digital-readout instrument for that matter—5 digits may not be more accurate than 4 digits, which may not be more accurate than 3 digits. That's because no matter how many digits a machine boasts, the reading can still be incorrect.

The last or last few digits may constantly roll around like so many wheels on a slot machine. (In this case, the payoff isn't three lemons, it's one—the DMM.) Or there's a dead zone around zero and the last digit stays glued in stubborn immobility.

Stability and accuracy must therefore be compatible with resolution. If the theoretical resolution outstrips the stated accuracy of the box, drop it. Thus a 3-digit DMM's over-all reading accuracy shouldn't be worse than 0.1%, a 4 digit's worse than 0.01% and a 5 digit's worse than 0.001%.

Now a 4-1/2-digit unit may not be more accurate than one with 3-1/2 digits. Does it at least guarantee more resolution? Nope.

Suppose both machines have 100% overrange. Suppose the “smaller” box reads 199.9 mV full scale on its most sensitive range, while the “bigger” unit goes to 1.9999 V on its most sensitive. Resolution of both DMMs: 100 µV.

Take another case. Suppose you mostly want to know the exact levels of some common power sources—12, 15 and 24 V dc, 115 or 230 V ac. Will two different 3-1/2-digit units give the same resolution on these measurements? Will 5-1/2 digits on one box give better resolution than 4-1/2 digits on another? Not necessarily.

If one 3-1/2-digit meter has only 10% overrange—1100 counts—you'll have to use the 100-V range to measure 12 V, the 1000-V range to measure 115 V. Resolution? Barely 1%.

If the 4-1/2 gives 200% overrange—30,000 counts—and the 5-1/2 counts to just 120,000 with 20% overrange, then the two are equivalent between 12,000 and 30,000 counts, the region that includes the common source levels.

Filtering your way through noise specs

Even when a DMM seems to check out as far as your required sensitivity, resolution and accuracy, you're not OK yet..... remember stability? On top of that, you've got to worry about the unit's noise-rejection characteristics.

It's rare to find a clean dc signal these days, so DMM designers take pains to counteract hum, ripple or noise riding on the signal or lurking in ground loops. How well the designers succeed is reflected in a DMM's normal-mode rejection (NMR) and common-mode rejection (CMR) specs.

The more common countermeasures include various forms of signal integration to cancel unwanted signals at line-related frequencies; active or passive filters in the front end to cope with broadband noise; and floating inputs or guarded construction—two techniques that boost CMR by increasing the impedance (isolation) between the low input and ground.

How much rejection is enough can be answered only in terms of your needs. To make sure that normal-mode errors from 50 or 60 Hz stay below 1 count in a 3-digit DMM, you'll need at least 1000:1 attenuation, or a 60-dB NMR.

Common-mode interference is a more insidious problem, since the source—or sources—of the trouble isn't easily spotted. In selecting a DMM for systems use, a high CMR is crucial and a guarded DMM is practically a must.

Remember three things when you look into NMR and CMR: 1. Filtering slows a unit down; 2. A CMR spec should be given for some imbalance—preferably 1 kΩ—between the high and low leads; and 3. Small “differences” in noise-rejection specs can mean the difference between a good reading and one in which the last digits are useless.

On the first item, find out if you can get both the impressive reading speed and the high NMR at the same time.

On the second item, every factor-of-10 reduction in the imbalance resistor “improves” the
CMR by 20 dB. Insist on a 1-kΩ spec. (While you're at it, see what the CMR is on the current ranges, too.)

If you are slowed down in trying to determine just how fast a DMM can operate, you're not alone. This is another DMM area that needs some standardization, and about the only way out of the quandary is to ask for definitions.

The shortness of it all

What does a vendor mean when he talks about "settling time," "response time," "reading rate," "digitizing time"? Settling time to what value—the rated accuracy or what? How does response time relate to the input waveform?

Speaking of relations, keep questioning and you may uncover a few black sheep—specs that should be attached to other specs but are kept closeted by the DMM vendor, probably to hide embarrassing behavior. Input impedance is a likely interrogative target.

High input impedance (Zin) is something to be desired. If Zin isn't high enough compared with the source impedance then rated DMM accuracy can be swamped. Even a 10-MΩ Zin isn't enough to prevent a loading error of 0.1% with a 10-kΩ source.

So vendors promote lofty 1000-MΩ and 10,000-MΩ input Zs in large, bold print. Completely missing—or buried inconspicuously—is another figure, without which any impedance spec is incomplete. The truant is bias current.

Almost all DMM input amplifiers need bias. When the current passes through the source impedance, you get a voltage drop—and a reading error. When the ambient temperature changes, so does the bias current. The hotter it gets, the bigger the error.

Although a 1-nA bias at 25 C sounds low, it really isn't when you realize that bias current roughly doubles every 7 C. In the field, when temperatures reach 35 C, accuracy melts away.

The input impedance you started with can also dissolve under certain other conditions—when you change a range or function; in the middle of the unit's analog-to-digital conversion; during or after an overload. Oh yes, input capacitance does its share in eating into Zin with ac inputs. Make sure you know what the Cin is.

Linger a bit longer at the DMM's input terminals, and you'll learn even more.

Is it a DMM or a power supply?

You may not realize it, but a DMM can be a two-way street. That is, the meter can pump energy out the input terminals. Few spec sheets tell you that such kickback signals exist, much less what the amplitudes are.

Even on the ohms function, where you expect output current, surprises may await. In some cases, the surprise is especially unpleasant—like 100 mA to 1 A coming out on the lower ranges, or 22 V of open-circuit voltage. Resistors may not wince at such levels, but what about fuses, diodes and base-emitter junctions?

You can try to extract vengeance on a troublesome DMM if you are so disposed. Just do deliberately what is often done quite inadvertently: apply a high voltage to the input while you're on ohms. If nothing burns out, you'll have at least learned something: how good the DMM's protection is.

A useful feature in digital meters is . . . an analog meter. Thus you can use units like Simpson's 460-3 for nulling, peaking and watching trends.

Often forgotten in selection—but sometimes more crucial than specs like accuracy—is a DMM's ability to withstand such abuse. All the accuracy in the world won't help you much if someone blows up the instrument unintentionally by applying 115 or 230 V to a sensitive scale.

That won't happen if the meter is adequately protected. What you'd like to know about protection is: how much, what kind, on which ranges? What you may not like are some of the answers.

Ohm is where the art is

Any DMM that can't handle at least the common line voltages on the ohms function is begging for a knockout. Those units that can measure 1000 V or higher had better be able to take that level, too—without damage, and on all ranges and functions.

Don't sigh with relief when a spec sheet does in fact say "protected to 1000 V." Remain cautious and ask, "for how long?" Any answer other than "continuously" spells trouble.

What form the protection takes is also significant. Three kinds prevail today—fuses, circuit
breakers and electronic circuits. A given DMM may use all three, one for each function (resistance, voltage, current).

When fuses form the line of defense, find out how easy they are to change. Must you open the box and get out your soldering iron? How many different types of fuses must you stock or carry around just in case? Even more annoying: Must the box go back to the cal lab because it's been opened?

Circuit breakers and electronic protective measures avoid these problems but can bring their own nuisances and limitations.

In a line-operated instrument, fuses don't care about brownouts, blackouts or low-line conditions. But circuits may. Circuitry doesn't get along with heat either. Consequently it's nice to know how overload protection is affected by temperature, line voltage or other conditions. The datasheet ought to tell you. It should also reveal whether an overload knocks the DMM out of calibration.

There are some other not-so-obvious considerations in protection. What happens to a DMM when you shuffle across a plush carpet and zap the function switch with a crackly spark? Or suppose you hit two buttons at once by mistake? What about an overload that catches an autoranger just between ranges?

**Low-power ohms measurement** is a feature that's appearing more frequently in low-cost DMMs. The 283, from B&K Precision, offers a switchable Hi/Lo ohms.

Most line-operated DMMs can't stand more than a few hundred volts of CMV. If you need more CMV protection than that, look into battery-operated meters, which can tolerate CMVs in the kilovolt region.

Suppose a meter's defenses do crumble somehow, or the overload exceeds the unit's rating. If, say, an input op amp blows, can you change it yourself? Do you have to change five other matched components as well? Are the parts commercial or custom? Study the unit's manual—it may be an eye opener.

Related to any discussion of protection is the two-lead vs. three-lead question. Those that offer one jack for both voltage and resistance measurements are quick to point out the convenience of the feature, and how it finally does away with irritating lead changing.

Those that keep the three inputs counter with a valid argument—what happens when voltages are applied to the ohms circuits? Can the unit suffer? How much can it take?

For that matter, while you're worrying about safety, perhaps you'd better ask yourself: how much can I take? Sometimes a DMM can also dish out what it receives.

**Danger: High voltage**

Danger lurks not just in the high voltages found within some units but in careless use of the DMM. Leads have been known to pull out rather easily from banana jacks. If the other end of a dangling lead happens to be attached to a kilovolt or so . . .

If you expect to work with dangerous levels, you can avoid this hazard by looking for binding posts rather than banana jacks. Some DMMs offer them. Other units offer recessed male terminals as the input.

After you've satisfied yourself as to a unit's basic performance and protective measures, you'll probably look for other things—for features that make life easier or that speed measurements. Even esthetic qualities can be important.

It's OK to want your field rep to carry a good-looking unit, but remember: while you're worrying about the color of the pushbuttons, you can get zonked somewhere else. Autoranging is a likely spot.

Recently the cost of autoranging has come down so sharply that you can get this feature even in $200 DMMs. But don't say yes to autoranging just because it's readily available. Say yes because you don't need what the vendor may have traded off for autoranging—things like accuracy, stability, ac bandwidth, and more.

Tight specs and autoranging aren't necessarily mutually exclusive, but to get both together you'll...
True rms, autoranging, autozero, compact size: The 8040A, latest from Fluke, gives all that in a compact package. The unit works from rechargeable or throw-away batteries, or from the line.

For $315, you can buy a DMM with autoranging, high or low ohms, lighted function indicators and more. The unit shown is the Keithley 168.

usually have to pay the price. And even in more expensive units, autoranging can have drawbacks. Continual ranging with noisy signals or with signals near a DMM's switching points are two annoying aspects of any autoranger. If you're looking for maximum resolution, you can't be sure you're getting it with autoranging, especially in the overrange regions. For these reasons, many autoranging DMMs have a manual mode.

Another point: several DMMs today offer a touch-and-hold feature, a switch or button that freezes a reading so you don't have to watch the display while poking around under a chassis. Nice feature, yes? Yes, until you think about it and realize how touch-and-hold affects autoranging.

If your application calls for autoranging, the feature can save many man-hours. And, as one vendor points out, relays can far outlast manual switches in lifetime.

Other features appearing in DMMs with increasing frequency include analog nulling or trend meters, low-power ohms, diagnostic indicators and even temperature or capacitance meters. If any of these are useful, fine. Just be sure the “extras” don't hide the performance of the DMM proper.

Buzzwords can also disguise performance. Lift the camouflage by asking, “Does ‘autozero’ really improve zero stability?” “What does ‘quadrislopematic integration’ really do to help a unit?”

Don't get caught up in the numbers game either. You may end up with 75 ranges—but only two functions. What good are a fistful of ranges and functions, anyway, when all you need are a few? In still another area—internal design—vendors may reverse and try to convince you that less is better.

In the highly competitive war to sell DMMs, the parts-count skirmish has become an all out firefight. The argument goes that the fewer the number of parts, the better the reliability. With major DMM functions being put today on one or just a few LSI chips, the parts count has plunged. Lift many of the newer DMMs, and you'll swear the box is empty.

Getting by on less

Does the reliability argument hold water? Maybe. But if a vendor really believes in his argument, or in his published MTBF, why does he warrant his unit for only 90 days?

Remember: It's not the parts that "count," it's the final performance.

The kind and size of display are often stretched out of proportion in a sales tug-of-war between rival vendors. Things like quality and brightness are subjective in a display, but current drain and life aren't.

Whether you prefer LEDs, LCDs, gas discharge or whatever, each type has merits and drawbacks—none can be all things to all men. What circuitry the designer has built around the display and how the display is packaged count too.

Because of LSI, the size, weight and price of portable and bench DMMs continue to drop. Alternately, you can get more in a DMM for the same price. In systems and laboratory units, the latest trends include built-in μPs and ROMs and capabilities like self-diagnosis and the IEEE-488 interface standard for programmability.

Thus DMMs today can do more than measure. They can calculate, linearize, watch for high/low limits, and more. Some units just about calibrate themselves; others watch for ailments and can almost, but not quite, repair themselves.

The new breed: thinking DMMs

DMMs with high IQs include Systron-Donner's 7115—the forerunner in μP meters—and the month-old Hewlett-Packard 3455A, the first unit with a removable reference.

One system DMM, from Dana, uses a μP to provide practically any desired interface. An-
other new systems unit, the Data Precision 7500, emphasizes speed, with 1000 conversions per second available to speed up one of the slowest links in a computer-controlled network.

There are even DMMs that count (or counters that measure, if you prefer) like Valhalla Scientific's 4440, a 4-1/2-digit DMM and 27-MHz counter (a $50 option). And if that's not enough, look into Vu Data's triple combination, the 975, which marries a DMM to a counter and an oscilloscope. Tektronix also offers several DMM options—the DM44 is the latest—for its portable scopes, as well as a bunch of DMMs for its TM500 line of modular test instruments. The 44 displays time intervals and temperature along with voltage and resistance.

Unusual units can turn up in unexpected places. Peek into your co-worker's shirt pocket and you may find a super-miniature, probe-like affair with digital readout, autoranging and more. Two such units exist—the HP 970A and the Logical Technical Services 12T, a DMM that also measures temperature.

Need long-term averaging of slowly fluctuating, random signals? Check out the Thermo Systems 1076, which measures rms, mean-square, or mean, at 10:1 crest factors.

Another group of meters specializing in rms measurements is offered by Yokogawa Corp. of America. The line includes models that measure power as well as voltage and current.

Specialized DMMs are the forte of California Instruments, makers of the Cimron product line. The company's broad line includes the DMM 42, a unit that spans the super wide resistance range of 100 \( \mu \Omega \) to 200 M \( \Omega \). Other Cimron models include a counter/DMM and an ATE unit that, among other things, takes ac/ac ratios.

In general-purpose DMMs, the action today is mostly in 3-1/2-digit portables and 3-1/2 and 4-1/2-digit benchtoppers. Packaging of the portables runs from tiny pocket models resembling hand-held calculators, to the tilt-bail configuration popularized by the Fluke 8000A. Prices of 3-1/2-digit units today have plummeted to the $100 mark.

**Those remarkable portables**

What should you look for in a portable? Ruggedness is a prime consideration. A portable is sure to suffer through whacks, drops, vibration, coffee spills, smoke and other miseries. Can your unit "tough it out"?

What about EMI susceptibility? Plastic cases aren't known for resistance to EMI. Does your vendor provide for this? Some do.

How easy is it to retrofit a battery-operated DMM to line operation or vice versa? Can the unit work off the ac line without a battery? Are batteries easily replaced? How long do they last? Are they rechargeable? How long to recharge? What's optional?

Will you use the unit in sunlight or other high ambient lighting? If so, look into display contrast. You might have to hide in a closet to read some units.

Don't overlook the physical features: shape, how it's carried or stored, where the controls and display are located. Lightweight units are fine—that is, until you push a button and send the DMM sliding across the bench. What's good for the field isn't necessarily good for the bench.

Remember, some DMMs sacrifice a lot to squeeze size or price. Accuracy of these units can fall far behind that of the analog multimeter.

Among the smaller portables, the standouts in-
clude units from Dana, IET Labs, Non-Linear Systems and Sencore. The Danamerter A features LCDs, one-year operation on a single 9-V battery, and once-a-year recalibration.

IET's pocket portable is the DM-50, a 3000-count unit with protection on all three functions, V, I and R. Non-Linear's midget line packs up to four digits, plus an active filter in the 3-1/2-digit unit, into a 1.9 x 2.55 x 4-in. case. And Sencore's two pocket units feature 30-MΩ input impedance when you hit an X 2 probe button.

Moving up to the more traditionally sized portables, you'll find units like Simpson's 360-2 and Weston's 6000. The dash 2 inherits the "look" of the familiar 360 VOM in a digital "update," with such features as low-power ohms and a built-in analog meter.

The 6000 is a sleek DMM using LCDs for 200 h of battery life. Other features: autoranging, autolamp, ability to hold readings, and more.

Compact benchtoppers have arrived with increasing frequency lately, no doubt sparked by the success of the Fluke 8000A, a unit that, with others, has catapulted Fluke to the leadership position in DMMs.

Frontrunners in these and other DMMs include Hewlett-Packard and Data Precision, with significant roles being played by Ballantine Laboratories, B & K Precision, Dana, Digitec, Keithley, Philips and others.

The 3-1/2-digit battle

Ballantine's 3028A, introduced at Electro '76, offers 3-1/2-digit rms response from a low 15 Hz to a top of 110 kHz. The B & K 3-1/2er, the 283, lights up with 0.41-in-high digits.

Data Precision's "miracle" of packaging, the 4-1/2-digit 245, has recently gained a younger brother, the 3-1/2-digit 175. Also boasting a very compact case, the 175 sells for $189.

Digitec's 2100 series of DMMs stand out with low bias current. One unit, the 2180, reads out directly in decibels.

The prize for the most prolific producer may well go to HP, which has turned out four new DMMs within the last year. The imaginatively packaged HP 3476A typifies much of the advanced technology going into today's crop of DMMs.

Another unit wearing the "new look" is Keithley's 168, a 3-1/2-digit box with autoranging, high or low ohms, two-terminal inputs and lighted function indicators.

Two units from Philips deserve attention: the portable PM 2514 autoranger and the PM 2523 tilt-bailer. Accuracy of the 23 is guaranteed for life—no recalibration is necessary.

Fluke isn't sleeping, of course. Hot off the assembly line at Fluke are the 8030A and the 8040A, with 3-1/2 and 4-1/2 digits, respectively. Virtues of the 30A: true rms for both voltage and current, plus a diode-test function. The 40A autoranges and reads true rms.

Newcomers and overseas vendors are also quite active in DMMs. De Forest Electronics, a new arrival, startled the industry recently with its $100 offering, the 3-1/2-digit MM 200. Takeda-Riken, a Japanese manufacturer, markets the TR-6355, a 3-1/2-digit unit with 10-μV resolution.

And Viz Test Instruments Group has acquired the old RCA line of equipment, and has added the WD750A—a 3-1/2-digit box with rf shielding, low-power ohms, an analog meter, and other features.

Need more information?

The products cited in this report don't represent the manufacturers' full lines. For additional details, circle the appropriate number on the Reader Service Card. For data sheets and more vendors, consult ELECTRONIC DESIGN'S GOLD BOOK.

Ballantine Labs, P.O. Box 97, Boonton, NJ 07005. (201) 335-0900. (M. Lichtenstein). Circle No. 450

B&K Precision, 6460 W. Cortland, Chicago, IL 60635. (312) 889-8870. (G. Rose). Circle No. 451

California Instruments Div. (Cimron), 5150 Convoy St., San Diego, CA 92111. (714) 279-8620. (P. Muller). Circle No. 452

Dana Labs Inc., 2401 Campus Dr., Irvine, CA. 92713. (714) 833-1234. (C. Everett). Circle No. 453

Data Precision Corp., Audubon Rd., Wakefield, MA 01880. (617) 246-1600. (R. Scheinfein). Circle No. 454


De Forest Electronics, 40 Fairfield Pl., West Caldwell, NJ 07006. (201) 575-8670. (P. Zagaris). Circle No. 456

Dynascorp B&K, 1801 W. Belle Plaine Ave., Chicago, IL 60613. (312) 327-7270. Circle No. 457

John Fluke Mfg. Co., Inc., P.O. Box 43210, Mountlake Terrace, WA 98043. (206) 774-2211. (C. Newcombe). Circle No. 458


IET Labs Inc., 335 Bear Hill Rd., Waltham, MA 02154. (617) 890-5105. (S. Aisenberg). Circle No. 460

Julie Research Labs Inc., 31 W. 61 St., New York, NY 10023. (212) 245-2727. (D. Komoroff). Circle No. 461


Logical Technical Services Corp., 71 West 23 St., New York, NY 10010. (212) 741-8340. (M. Norris). Circle No. 463

Non-linear Systems Inc., Box N. Del Mar, CA 92014. (714) 714-1134. (P. Akin). Circle No. 464

Philips Test & Measuring Instruments Inc., 400 Crossways Park Dr., Woodbury, NY 11797. (516) 921-8860 (S. Rachlin). Circle No. 465

Schneider Electronique 27-33 Rue D'Antony 94533 Rungis (M. Lichtenstein). Circle No. 466

Clix 165, France. Circle No. 467

Sencore Inc., 3200 Sencore Dr., Sioux Falls, SD 57107. (605) 339-0100. (B. Bowden). Circle No. 468


Systron-Donner Corp., Instruments Div., 10 Systron Drive, Concord, CA 94518. (415) 676-5000. (C. Bishop). Circle No. 470

Tektronix Inc., P.O. Box 500, Beaverton, OR 97007. (503) 644-0161. (K. Arthur). Circle No. 471

Takeda-Riken, 646-A Santa Cruz Ave., Menlo Park, CA 94025. (415) 325-3099. (H. White). Circle No. 472


United Systems Corp. (Digitec), P.O. Box 458, Dayton, OH 45401. (513) 245-6281. (M. Elowitz). Circle No. 474

Valtech Scientific, 935 Convoy Court, San Diego, CA 92110. (714) 272-2727. (H. Clark). Circle No. 475

Viz Test Instruments Group, 335 E. Price St., Philadelphia, PA 19144. (215) 844-2626. (M. Rusk). Circle No. 476

Western Instruments, 614 Frelinghuysen, Newark, NJ 07114. (201) 243-4700. (P. Rehnborg). Circle No. 477

Yokogawa Corp. of America, 5 Westchester Plaza, Elmsford, NY 10523. (914) 592-6767. (J. Stengenga). Circle No. 477

ELECTRONIC DESIGN 20, September 27, 1976
How can you guarantee your product for ninety days if the parts that go into it aren’t guaranteed for ninety seconds?

When you’re in the business of marketing information systems and modems that sell from $500 to $50,000 it doesn’t help to have your customers think of you as anything less than a really solid operation.

Of course, you’re only as solid as the products you sell.

The best way to get your customers believing in you and your product is to make that product better than anyone else—and to guarantee it.

But how can you be sure nothing will go wrong with the machines you make if you can’t be sure of the parts you put into them?

The answer is you can’t, unless you’re using guaranteed parts.

At MF Electronics, we make molded crystal oscillators the best way anyone knows how to make them. Since we feel they’re the best, we’re able to guarantee them for one full year.

The difference between oscillators.

What separates good oscillators from bad is space. Space is one thing there shouldn’t be any of inside an oscillator. But the way most oscillators are made, space is one thing you can count on.

The hollow truth about crystal oscillators.

Look at this oscillator. The fact that we can lift the cap to show you what’s wrong with it shows you what’s wrong with it.

After the crystal and other parts are attached to the base, the cap is glued on, creating a bond that’s tenuous at best. Air seeps through this bond, allowing dirt and moisture to collect. You’ve got a leaky oscillator, one that’s prone to loose parts and electrical shorting. That’s how deadly a breath of fresh air can be to the inside of an oscillator.

The un-holey oscillator: It’s molded. What a blessing.

A molded oscillator, on the other hand, has no holes, no open spaces, nothing to hide and nowhere to hide it. Its crystal is hermetically sealed and set in a monolithic block of solid black plastic. There are no spaces for air to penetrate, no room for dirt or moisture to accumulate. Wave soldering can’t even deteriorate the unit, so there’s no danger of loose pins or joints.

A test that rings true.

One of our customers, who is also one of the country’s largest users of crystal clock oscillators, tested the performance of various oscillators. He found that MF’s molded oscillator lasted 3000 hours in an 85°C/85% relative humidity test. If you’ve ever done any oscillator testing yourself you know how remarkable that is.

Two more solid reasons to use MF Crystal Oscillators.

3rd overtone crystals are used in MF’s molded oscillators to provide greater electrical and mechanical stability in frequencies exceeding and including 20 MHz.

And an MF molded oscillator is the only one made that meets the UL oxygen index guideline of 28%.

Because we’re solid, your product is more solid.

So when you use MF molded crystal oscillators, you’re giving your product a more efficient component, a heart that will beat longer. And your customers will be giving you fewer complaints and service calls.

MF Electronics is the only company that makes molded crystal oscillators. We invented them.

We make what we think are the best crystal oscillators you can buy. And we guarantee them, so your product can be “the best you can buy.”

Guaranteed!

THE MF GUARANTEE

MF Electronics warrants this molded crystal oscillator to be free from defects for one year from date of purchase.

Any oscillator found to be defective during this period may be returned to the factory, postage paid, for repair or, at our option, replacement without charge.

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CIRCLE NUMBER 33
Cancel 60 Hz and other noise with adaptive filters. Other benefits include less signal distortion than with conventional techniques.

How would you like to build filters that design their own parameters, provide excellent noise reduction, and give less signal distortion than conventional filters? The secret: adaptive cancelling of noise or interference.

Adaptive filtering and noise cancelling work best when:
- You can find a reference noise source in which the information-carrying signal is weak or undetectable (noise-cancelling case).
- The signal is nonstationary—that is, its statistical properties vary with time.
- Little or no beforehand statistical information is known about the input signals. In such cases, Wiener or Kalman-Bucy filters generally aren’t feasible and the adaptive method may be the only reasonable approach.
- In many cases, conventional, fixed filters efficiently attenuate noise but distort the signal. With adaptive noise cancelling, when applicable, you can reduce noise to levels that would be difficult or impossible with conventional filtering—with little risk of signal distortion.

What are adaptive filters?

Unlike conventional filters, an adaptive filter is fixed in structure, but its parameters are adjusted automatically by an optimal adaption algorithm—the key to the technique (Fig. 1).

The adaption algorithm requires a “criterion of goodness,” or performance index, to optimize the filter’s performance. The criterion is a function of an error signal, called the mean-square error (MSE):

\[ (\text{MSE}) = E \{ (\text{Error})^2 \} \]

where \( E \) means the expected or average value of the quantity in brackets.

To generate the error, many methods are possible, and a designer’s resourcefulness in producing the error is often a major factor in the successful application of the adaptive technique.

In general, the error can be considered as the difference between an actual and a desired response, or:

\[ \text{Error} = (\text{what you have} - \text{what you want}) \] (2)

However, the error signal isn’t always so simply visualized, that is, \( d \) cannot always be thought of as a desired output. Sometimes \( d \) is just a signal used to generate an appropriate error. The goal of the adaption algorithm is to adjust the filter parameters to minimize the MSE.

In adaptive noise cancelling, a variation of adaptive filtering, a reference input is derived from sensors located in a noisy environment in which the signal is very weak or undetectable (Fig. 1b). Thus, the reference noise, \( n_r(t) \), is uncorrelated with the signal, \( s(t) \), but is correlated in some way with the input noise, \( n_o(t) \).

1. An adaptive filter adjusts itself for optimum performance through an algorithm that incorporates a built-in performance criterion (a). One use of the filter is to cancel noise (b).

Gregory A. Clark, Electrical Engineer, Electronics Engineering Dept., Lawrence Livermore Laboratory, Livermore, CA 94550.
The adaptive filter conditions the reference noise, \( n(t) \), so that \( y(t) \) is as close a replica as possible of \( n_0(t) \). Then \( y(t) \) subtracts from \( s(t) + n_0(t) \), leaving approximately \( s(t) \):

\[
z(t) = s(t) + n_0(t) - y(t) \quad (3)
\]

Notice that the error in this case is identical to the output, and you really can't consider the error as the difference between a desired and an actual output.

**One tradeoff: Speed**

Note that when the signal plus the noise forms the input to an adaptive filter or noise canceller, the device does not deliver the correct result immediately. The system needs time to adapt to the incoming data, as illustrated by the MSE learning curve (Fig. 2). To quantify the adaption time, an analytical expression for \( \tau_{\text{MSE}} \), the MSE time constant, can be derived.\(^1\)\(^2\)\(^3\)\(^4\)

In typical feedback systems, the “plant,” so to speak, is fixed and the plant input is the error between the system input and a weighted value of the output. Thus feedback modifies the input signal to accommodate the plant.

In adaptive systems, the plant changes to accommodate the input signal—a profound difference.

Most practical adaptive-filter designs include the Widrow-Hoff adaptive linear combiner (ALC) shown in Fig. 3. The ALC simply forms a weighted sum of the inputs \( x_i \) to give the output \( y_j \), which is then compared with some desired response \( d_i \) to form the error signal \( \epsilon_i \). A linear mean-square algorithm (LMS) uses \( \epsilon_i \) and \( x_j \) to optimally adjust the weights and so minimize the error.

When the ALC first begins to work, or if a change in the input statistics occurs, \( \epsilon_i \) is usually large. The LMS algorithm then adjusts the weight values \( W_j \) (where \( W \) is a vector quantity) to minimize the mean-square error. In the algorithm, the constant \( \mu \) affects the rate of convergence to the minimum MSE.

To guarantee that the algorithm will converge and be stable, \( \mu \) must be greater than zero and...
5. For broadband signals, the adaptive technique takes the shape of a tapped delay line, or variable-weight transversal filter.

4. Various filters require different configurations. To filter a single frequency, use the configuration in "a." Another arrangement can handle several frequencies (b).

6. To cancel 60-Hz noise, the reference source comes right out of the wall socket. Other frequencies can also be cancelled by the technique, in which filtering is provided by an ALC.
A two-weight, analog, 60-Hz canceller is built up from standard commercial op amps and other building blocks. Scaling amplifiers adjust signal levels to prevent saturation.

Details of the canceller's phase shifter (a) and integrator (b) show typical component values, design equations and circuit performance.
NEW CAPABILITIES IN PLOTTERS

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The 4662 contains its own character generator, alpha rotation, and page scaling, thus minimizing support software. Proven graphic and plotter software is provided by Tektronix.

The 4662. Plug it in. It speaks for itself.
9. Scope photos show relative performance of a standard 60-Hz notch filter (a) and of the adaptive filter (b,c). Note the low signal distortion obtained with the adaptive filter compared with that of the notch type.

Hz noise causing the problem. Here, an ALC serves as the adaptive filter, with two weights.

Note that one ALC input comes directly from the wall plug and the other from a 90-degree phase shifter. With this arrangement, you can adjust the weights to give a 60-Hz sine wave of any magnitude and phase at point y. Note also that the ALC configuration is applicable to any single frequency.

The LMS adaption algorithm, using the error signal, adjusts the weights so that \( y = s + n_0 \) to leave approximately \( s \) at the output.

Today, with inexpensive, high-quality op amps and multipliers, analog, two-weight cancellers are economical to design (Figs. 7, 8). Op amps make it easy to produce the mathematical functions required by the LMS algorithm. These include 90-degree phase shifting, integration, weight multiplication and scaling. In analog form, the LMS algorithm is given by:

\[
W(t) = 2 \mu \int_0^t \epsilon(\alpha) X(\alpha) \, d\alpha
\]

Scalng amplifiers, with screwdriver-adjustable gains, carry a good deal of the “workload” because all of the canceller’s internal signals fall between \(-10\) and \(+10\) V—the dynamic range of the op amps and multipliers. Adjust the gains so that none of the op amps saturate with reasonable input magnitudes, roughly: \( 0 \leq |\text{signal}| \leq 5 \) V and \( 0 \leq |\text{noise}| \leq 1 \) V.

Additional input and output scaling amplifiers are usually necessary in practical circuits. A pot scales the amount of reference signal entering the adaptive filter.

In relative performance a typical 60-Hz notch filter effectively attenuates the 60-Hz, but distorts the signal (Fig. 9a). With the noise canceller, distortion is low (Fig. 9b,c).

A final note: Although adaptive filters are usually implemented with digital techniques, good analog delays are now possible with charge-coupled devices (see ELECTRONIC DESIGN, Vol. 24, No. 6, March 15, 1976, p. 70). This means that tapped-delay-line transversal filters can now be built economically in analog form. ■ ■

Acknowledgement
The author wishes to thank Charles Pomernacki for his helpful suggestions and John Elliott for constructing the noise canceller.

References
**NEW 3½ Digit Multimeter from B&K-PRECISION**

...you’ll want it for its features
...but it’s the price that will sell you!

- High intensity LED display is easily read from at least 6 feet in the brightest room
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An optional, internal battery pack (BP-83, $50.00) provides 8 hours of continuous use on one overnight charging and charges when the Model 283 is in use on 115/230VAC.

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Your B&K-PRECISION distributor has them in stock and will be glad to demonstrate its features to you. Call him, or write for additional information.

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Complete new circuitry makes the Model 283 the most dependable and versatile 3½ digit multimeter you can buy. The extra-bright display allows you to use it where other units would cause reading problems. The selectable “low ohms” function permits accurate measurement of semiconductor shunted resistors.
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WHO ELSE?
Reduce the noise output of linear rf amplifiers. High degeneration in the emitter of a grounded-base circuit reduces the noise figure to 2 dB, 10% from the carrier.

Because of the use of relatively high power in solid-state broadband transmitters, it's generally not recognized that keeping output noise low is a serious problem. Noise output can easily jam nearby sensitive receiver inputs in adjacent channels. The major source of such noise is the high noise level generated by the usual driver stage of a transmitter's final broadband Class B or C amplifier.

To improve the over-all noise figure it is first necessary to provide a cleaner drive, so noise-output reduction is a major objective in the 2-W linear, rf, driver amplifier shown in Fig. 1. It has an equivalent noise figure (NF) of only 2 dB at a frequency 10% removed from a 50-MHz carrier. This low NF is achieved by means of a series-tuned input that also serves as the emitter-degeneration element in a common-base configuration. The degeneration in the emitter circuit reduces the output noise (mainly transistor noise) by about 18 dB.

Series tuning has high off-resonance Z

In the amplifier's input circuit (Fig. 1a), capacitor C2 transforms the source impedance, Rsource, to match the load presented by the amplifier input; L1 and C1 form a series-tuned circuit to resonate at the carrier frequency. The emitter-base series-resonant circuit presents a comparatively high impedance (Z) to off-carrier noise frequencies; thus it provides the impedance needed for emitter degeneration.

Resistor R1, together with the bias supply, VEE, sets the collector bias current at 0.5 A. Inductor L2 serves as an rf choke between the supply, Vcc, and the collector, and the paralleling resistor, R2, suppresses any parametric oscillations.

Fig. 1b shows how the rf transistor's dual emitters are coupled to the circuit with a minimum of lead inductances. A semicircular 1/4-in.-wide copper stripline, on 1-mil paper for insulation, produces approximately a 1-Ω characteristic impedance, which matches the transistor's input impedance.

This driver amplifier stage, when used in a transmitter rf chain, provides a "clean" drive to the final broadband stage and 16-dB of gain. Because input power is only 50 mW, the input can be tuned with varactor diodes.

A linear noise model of the 2N5642—the rf power transistor used in the amplifier—provides a basis for calculating the amplifier's theoretical noise output. The measured values of the circuit are within 2 dB of the theoretical calculations.

Measuring the performance

To test the amplifier's noise performance, you may use a test set-up as shown in Fig. 2a. Measurements of amplifier noise-power output in dBm and carrier-to-noise ratio in dB made with
such a set-up are plotted in Fig. 3 for several frequencies, \( f_n \), on both sides of a 50-MHz carrier.

For each \( f_n \), you must first establish a noise reference. With no rf drive adjust the bias, \( V_{EE} \), to make the collector current, \( I_c \), equal to zero when \( V_{cc} \) is 10 V. Then set the output level, \( F \), of the calibrated noise source at zero; \( F \) is calibrated in terms of excess \( BkT_o \) above the thermal reference (\( k \) is Boltzman's constant, \( T_o \) is room temp in °K and \( B \) is bandwidth).

Finally, the cw-generator tuned to \( f_n \) must be

The plotted values of measured noise output \( P_n \) (Fig. 3) in dBm are calculated from the following relationship:

\[
P_n = -129 \text{ dBm} + 10 \log F + 12 \text{ dB.}
\]

The 12-dB value accounts for a 6-dB loss in the attenuator, a 3-dB loss in the bandpass filter and an additional 3-dB loss because the amplifier's output is split between two 50-Ω leads (Fig. 2a). The -129 dBm represents the log form of the reference level, \( BkT_o \), where \( B \) is the band-

2. The test set up (a) measures the noise performance of the amplifier. Replacement of the 6-dB attenuator and the bandpass filter with an adjustable attenuator allows the measurement of noise in the degeneration test circuit at an output level sufficient to “quiet” noise output from the AN/PRC-77 FM receiver by 10 dB. The AN/PRC-77 can be tuned over the range of 30 to 76 MHz.

With the receiver output at this -10-dB reference level, you may now apply rf drive to the amplifier, and then increase \( V_{cc} \) to the normal working voltage, which is 24 V. (This sequence — rf drive first, then the 24 V — is safest for the transistor.)

At this point the reduction in “quieting” provides a measure of the amplifier's noise output. To obtain a measurement, remove the rf drive and restore the reference conditions again. Now, increase the calibrated noise generator's output until you get the same reduction in “quieting” as obtained with the rf drive, and note the \( F \) reading on the noise generator's scale.

This procedure must be repeated for each value of \( f_n \) that you want to plot.

The noise components in the collector current can be attributed to three sources (Fig. 4). Assume the sources are uncorrelated so that their mean-square values can be added.

- First source is \( R_e + R_s \rightarrow i_n^1 \) (emitter and source resistances).
- Second source is \( e_n \rightarrow i_n^2 \) (base noise source).
- Third source is base-collector junction noise \( i_n^3 \).

Thus,

\[
\mathbf{\overline{1}}_n = \mathbf{\overline{1}}_n^1 + \mathbf{\overline{1}}_n^2 + \mathbf{\overline{1}}_n^3
\]  

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\[
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\]  

Measurements agree with theory

The noise components in the collector current can be attributed to three sources (Fig. 4). Assume the sources are uncorrelated so that their mean-square values can be added.

- First source is \( R_e + R_s \rightarrow \overline{1}_n^1 \) (emitter and source resistances).
- Second source is \( e_n \rightarrow \overline{1}_n^2 \) (base noise source).
- Third source is base-collector junction noise \( \overline{1}_n^3 \).

Thus, 

\[
\overline{1}_n = \overline{1}_n^1 + \overline{1}_n^2 + \overline{1}_n^3
\]  

Resistance \( R_e \) represents the Thevenin-equivalent source resistance that the emitter "sees," and
3. A plot of theoretical and measured noise characteristics of the amplifier shows close agreement.

R\textsubscript{e} represents the emitter’s series resistance. Since the transistor’s h\textsubscript{r} > > 1, the current in the emitter is approximately equal to the current flowing in the collector; therefore,

\[
i_{e1} = \frac{4 kT BR'}{\sqrt{(R' + \frac{1}{g_m})^2 + X^2_s}}
\]

where \( R' = R_e + R_c \).

The base noise source produces

\[
i_{e2} = e_B \frac{1}{\sqrt{\left(R' + \frac{1}{g_m}\right)^2 + X^2_s}}
\]

Resistance \( R_e \) is obtained by measuring the transistor’s emitter input resistance as a function of the dc collector current. The transconductance, \( g_m \), varies with this dc current; therefore, \( R_e \) is taken as the difference between the theoretical value of \( 1/g_m = 0.026/L_e \equiv 0.026/L_c \), which is also plotted, and the measured input resistance where the \( 1/g_m \) plots “flatten” out. At high \( I_c \) current, the \( 1/g_m \) term becomes small relative to the value of \( R_e \), allowing the emitter input resistance to approach approximately 0.3 \( \Omega \).

To find \( i_{e3} \) (the third noise component), the amplifier is modified by a large reactance placed in the emitter to minimize the noise from emitter and base sources (Fig. 2b). For this measurement, the 6-dB attenuator is replaced by a step attenuator, \( a_s \), and the bandpass filter is removed. Because of strong emitter degeneration \( f_{e1} \equiv f_{e3} \).

Then,

\[
p_a = \frac{\overline{i_{e3}} R_L}{4kTB} = \frac{R_{e2}}{R_{le}} a_e^2 kT B F,
\]

where \( R_e = 50 \Omega \), the standard reference impedance level.

The graph (Fig. 6) shows measured values of this collector noise of the third kind, as a function of the collector dc current. Clearly, this noise component is directly proportional to the collector current.

Empirically we find from the graph that

\[
\overline{i_{e3}} = 8.3 I_c.
\]

With \( R_L = 25 \Omega \), then

\[
\overline{i_{e3}} = 1.3 kT B I_c.
\]

Here, \( kT B \) is measured in watt-seconds (Ws) and currents in amperes (Fig. 2c).

**Noise is caused by shot effect**

The collector injection noise \( \overline{i_{e3}} \) is caused by shot effect in the dc collector current. The shot effect is usually expressed as

\[
\overline{i_{e3}} = 2eI_c S^2 B,
\]

where \( e \) is electron charge (coulombs) and \( S \) is a space-charge reduction (smoothing) factor.

The smoothing factor, \( S \), indicates how many electron charges hit the collector simultaneously: if one electron at a time hits the collector, \( S \) equals one. This is the case in noise diodes.

Eqs. 6 and 7, when combined, yield an \( S \) for the 2N5462 transistor of

\[
S^2 = 0.017,
\]

which is a characteristic of the transistor; it is determined by the transistor’s charge density.

**Evaluating base noise**

To evaluate the base noise, \( i_{eB} \), the emitter in Fig. 2b is bypassed. From Eqs. 1, 2, 3 and 6,

\[
p_{aB} = \frac{4kTBR'}{Z} + \frac{e_{B}^2}{Z} + 1.3 kT B I_c,
\]

where \( Z = \sqrt{(R' + \frac{1}{g_m})^2 + X^2_s} \).

If we now introduce an equivalent noise resistor, \( R_{e2} \), that creates equivalent noise as if it were in series with the base junction (Fig. 4), then

\[
e_B = \sqrt{\frac{4kTBR_{e2}}{Z}}
\]

\( R_{e2} \) is equal to zero for all signals other than noise. Substituting Eq. 9 into Eq. 8, we obtain the power ratio

\[
\overline{i_{e3}} R_L = R' R_L + \frac{R_{e2} R_L}{Z} + \frac{1.3 I_c R_L}{4}
\]

The power ratio is measured as before and the
logs of the ratios are plotted as a function of collector current, $I_c$, with the emitter both bypassed ($X_e = 0$) and unbypassed, to show the effect of degeneration.

With the left side of Eq. 10 known from measurements, $R_{an}$ can now be calculated by substituting measured value for the loss resistance of $L_1$, $-R_s = 0.1 \, \Omega$; the equivalent emitter resistance—$R_e = 0.3 \, \Omega$; and for $1/g_m$—an “average” value, 0.05 $\Omega$ taken at an $I_L = 0.5$ A from Fig. 5. When these values are taken together with the measured value of the power ratio at $I = 0.5$ A, we find that Eq. 10 yields $R_{an} = 1.7 \, \Omega$ (Fig. 2c).

Impedance $Z$ and the coil’s $Q$, when measured for frequencies between 40 and 60 MHz at 1-MHz intervals, provide the value of $R_e$, and also allow calculating the theoretical noise power as a function of frequency.

**Calculating the theoretical noise**

The total theoretical noise power in the load according to Eq. 10 can be calculated as a function of frequency because now all the noise-source parameters have been determined. Plotted values of these calculations in Fig. 3 show good agreement with the experimentally determined values, thus validating the accuracy of the noise model of Fig. 4.

If we define the noise figure of the amplifier as

$$NF = 10 \log_{10} \frac{P_n}{\text{Power Gain}} \left( kTB \right),$$

we find $NF = 2$ dB, at a point 10% away from the carrier.

Eq. 10 shows clearly the relative contribution of the three noise sources to the total noise output. For frequencies close to the carrier, where emitter degeneration is weak, the base noise source $R_{an}$, dominates the output noise. At frequencies away from the carrier, the base and emitter sources are strongly degenerated, and the collector shot-noise component dominates. Fig. 7 shows that as much as 18-dB improvement in noise output is achieved with full emitter degeneration.

**Reference**

1. Lohrmann, D. R., "Determine Transmitter Noise Figure," *Electronic Design* No. 13, June 21, 1975, pp. 86-89.
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### Ours and Theirs.

(The 9080A & 8080A)

<table>
<thead>
<tr>
<th>Specification</th>
<th>AMD</th>
<th>Intel</th>
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<tr>
<td>Minimum Instruction Cycle Time</td>
<td>1 microsecond</td>
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<td>Maximum Power Dissipation (at 1.3 microsec. 0-70°C)</td>
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<td>Output Drive</td>
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<td>MIL-STD-883 Standard</td>
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### Ours and Ours.

(AM9080A System Circuits)

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<th>Description</th>
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<td>Am9102A/B/C/D</td>
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<td>Am25LS377</td>
<td>4th Q. 1976</td>
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CPU: 9080A = 480 nsec. -2 = 380 nsec. -1 = 320 nsec. -4 = 250 nsec.
Model your ROM with NAND gates when you are using computer-aided design to prove out a digital system. This program models large ROMs, with minimal circuitry.

Digital circuitry is becoming so complex that it is quite difficult to design. For this reason, computer-aided-design (CAD) programs for verification and circuit simulation of digital circuits are becoming popular for pinpointing errors.

Digital simulators for logic circuitry use gates and flip-flops as the basic building blocks. From these building blocks, the MSI and LSI components are modeled for computer simulation of the circuit.

MSI components, such as ROMs, can be modeled using combinational circuitry. However, arriving at a minimal circuit representation for a large ROM by hand is a time-consuming job. A Fortran IV program described here generates that minimal circuitry for ROMs by using NAND gates.

This program is written for IBM 360 and 370-series machines that use the Fortran IV G-Level-20 compiler. The program requires 300-k words of core for a ten-input, eight-output ROM. Larger ROMs may be modeled on computers with larger memories.

A short review of switching theory

Three concepts from switching theory should be understood in order to describe the program flow. Let's take a quick look at them before going on.

Minterms. A minterm is an input pattern for which a function is true, and has all its input variables included. For example, in a function of four input variables—called A, B, C and D—the term ABCD is a minterm. AD is not, because B and C have not been defined. A minterm corresponds to a unique square in a Karnaugh map.

Prime implicants. Prime implicants correspond to groupings of ONEs (minterms) on a Karnaugh map.

Essential prime implicants. Essential prime implicants are prime implicants that contain a minterm contained in no other prime implicant.

James J. Hanratty, Electronics Engineer, Automatic Test Equipment Engineering Div., NARF Alameda, Alameda, CA 94501.
The truth table for the ROM used in our example is rather small, but ROMs of any size can be modeled providing your computer has enough memory.

Previous CAD programs have generated single-output combinatorial circuitry that could be used in the modeling of ROMs. This approach requires rerunning the program for each of the ROM outputs, a time-consuming process that results in circuitry that is not minimized.

Model ROMs with minimal circuitry

ROMGEN, the approach shown here, uses classical techniques and results in near-minimal circuitry. The program is an easy-to-read NAND-gate description of the ROM. As the flowchart shows (Fig. 1), the main program calls the eight subroutines serially. The first subroutine is called IOCON, which reads in the truth table containing the minterms for the ROM, and also converts the binary input to decimal.

The next subroutine called is MNSORT. It performs two sorts on the input data, first by the ascending decimal value of the minterm and then by the number of ONES in the minterm. This sorting speeds up execution time.

The following subroutine is DBCON, which converts the results of MNSORT back to binary. QMCMIN, the next subroutine, minimizes the Karnaugh maps generated from the input data. The minimization is done by a tabular technique known as the Quine-McCluskey method, and results in a table of prime implicants corresponding, as usual, to the grouping of adjacent ONES (minterms) on Karnaugh maps.

Following QMCMIN, the main program calls EPITGN. EPITGN takes the result of QMCMIN, the prime implicant table, and finds the essential prime implicants. After all the prime implicants that cover singular minterms have been found, any remaining minterms are covered by selecting an appropriate prime implicant.

Modeling a four-input, three-output ROM

Let's use the program to generate a model for a four-input, three-output ROM. The first step is to define the ROM truth table (Fig. 2). Next, enter the ROM data onto cards, formatted as shown in Fig. 3. The first data card contains the number of inputs, number of outputs and number of patterns. Following the first card, enter the input-output patterns, one pattern per card.

Fig. 4 shows the program output. The format is the same as that used in Digitest’s D-Laser, a digital circuit automatic stimulus generation and response simulation CAD program. As an example of how to interpret the output, take 19NA/990,3,991. Here, gate no. 19 has its inputs connected to output nodes 990,3, and 991. The // indicates that the output-node number of gate no. 19
4. The program output describes, in coded form, the outputs and connection points of all the NAND gates required in the model.

is also 19. Interconnecting these NAND gates forms the ROM model (Fig. 5). This ROM model requires only 14 gates.

References
(continued from page 91)

Continuing from the previous page, the text is difficult to read due to the nature of the code and the formatting. It appears to be a segment of a computer program, possibly in a high-level language like FORTRAN, given the use of variables and looping constructs. The code includes conditional statements, loops, and function calls, typical of programming logic used in scientific or engineering applications.

Without more context, it's challenging to provide a detailed explanation, but the general structure suggests a program that might be used for numerical computations or simulations, possibly involving iterative processes or decision-making logic based on certain conditions.
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Preselector/mixer alignment circuit uses receiver’s balanced mixer as a load

Sensitivity variations across the band are excessive when the bandpass of an rf preselector is adjusted in a test fixture with the use of a nominal 50-Ω load (Fig. 1a). The problem is that the 50-Ω load doesn’t sufficiently correspond to the load presented by the mixer usually fed from the preselector of a receiver system.

On the other hand, the direct use of a mixer (usually a double-balanced circuit) as a load would provide a distorted response to the test circuit’s rf-sweeper input and not allow proper adjustment, because of the mixer’s feedthrough-rejection characteristics. However, if a dc-bias current is introduced into the mixer’s i-f port, rf input would be properly detected by the mixer.

With an rf-sweeper input, the recovered bandshape is found to be essentially independent of this bias current. The mixer-diode impedance remains reasonably constant and the circuit of Fig. 2, by alternately biasing the diodes ±300 µA, can produce a meaningful scope display, be-

1. A preselector alignment system (a) provides the most accurate alignment (b) when the receiver’s actual mixer loads the preselector, not some nominal resistive load.

2. A dc bias current applied to the mixer’s i-f port allows a double-balanced mixer to function properly as a detector load for the alignment set-up and closely simulate true operating conditions.
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CIRCLE NUMBER 41
cause the preselector's load is now the load actually used in the receiver (Fig. 1b).

Capacitor C1 and resistor R1 differentiate the scope's sawtooth horizontal sweep to toggle the CMOS flip-flop. When the flip-flop's Q output is high, positive bias is applied to the mixer via R4. Amplifier A2 acts as an inverter with unity gain to provide a positive-going bandshape display on the scope. On alternate horizontal sweeps, the flip-flop Q output applies negative bias to the mixer, and the input to A2 is switched by G1 to produce noninverted unity gain to keep the bandshape positive-going.

Resistors R3 and R4 should be matched within ±1 percent to ensure that unity gain is maintained for both inverting and noninverting inputs to A2. Adjustment of R8 is required only if the mixer diodes must be selected within about 20 mV dc.

The alignment is performed with the local oscillator (LO) OFF. Also, it is possible to introduce the sweep into the LO system and align or check its bandshape.

Offset between the alternate sweep traces results from unbalance in the mixer, and the presence of defective transformers or diodes becomes obvious from observation of this offset and the relative shapes of the sweeps (Fig. 1b).

The diode bias current of approximately 300 µA determined by the series 18-kΩ resistor and the ±7-V output from the flip-flop is not critical, but is about the same as that flowing when the LO drives the mixer in normal receiver operation. Detector overload occurs at about 200-mV peak, so only 10 to 20 mV/cm, ac-coupled, vertical scope gain is recommended.

Resistors R5 and R6 serve to split the supply voltage into ±7 V. Absolute voltage is not critical, but symmetry is important, so the divider resistors should match within ±1 percent.

F. Patterson Smith, Research & Development, Narco Avionics, Commerce Dr., Fort Washington, PA 19034. CIRCLE No. 311

Temperature-measuring bridge uses constant-current FET circuits

Using a constant-current source instead of the conventional constant-voltage configuration avoids problems with unwanted voltage drops in measuring bridges.

In the temperature-measuring bridge of Fig. 1, a 1-kΩ thermistor (Corning) serves as the current-regulating element for a FET constant-current generator. This current generator is the active arm of the bridge. The thermistor controls the FET's gate-source resistance.

The passive arm of the bridge uses a trimming pot in a similar FET circuit to null the bridge. The gate-source resistances of both active and passive FET circuits should be equal at the desired nulling temperature.

Remotely mounting the thermistor causes no problems, because lead resistance can be easily kept small compared with the thermistor.

The current drawn by this constant-current bridge is only about 20% of that drawn by a corresponding constant-voltage bridge, resulting in considerable savings on battery-operated equipment.

Ivar A. Dybvik, Engineer, River & Harbour Lab., Klaebuven 153, N-7000 Trondheim, Norway. CIRCLE No. 312
The Raytheon 2900 family gains five new members

Whereas: Raytheon is the established alternate source for the Am2901 and Am2909, (franchised distributors stocked), and,

Whereas: Raytheon brought you RAYASM, the powerful micro-assembler available on the NCSS computer network,

Now Therefore: Raytheon announces five additional 2900 family components, giving us a total of seven, To Wit:

2901 A 4-bit Microprocessor Slice—the fastest, most powerful LSTTL microprocessor in the world. With its cycle-saving two-address architecture, the 2901's speed can't be touched.

2905 A 4-bit Bus Tranceiver—general purpose open collector bus interface device. Data to the 100 milliampere bus drivers is provided by a 4-bit register with a two-way multiplexer at its inputs. Data from the bus receiver may be held in the 4-bit receiver latch on its way to the three state receiver outputs.

2906 A 4-bit Bus Transceiver with parity—is equivalent to the 2905 but with the addition of an on-chip parity generator/checker.

2907 A 4-bit Bus Transceiver—similar to the 2906 with the two-way multiplexer at the input to the bus driver register eliminated to allow the device to be packaged in the space saving 20-pin DIP.

2909 A Microprogram Sequencer—that can branch anywhere in memory, perform sub-routines, then return with up to four levels of sub-routine nesting. The device is a cascadable 4-bit slice which allows addressing of up to 4K words of microprogram with three devices.

2918 A General Purpose 4-bit Register—with two sets of outputs: TTL and three state. This useful combination can reduce your package count for those status, command, and instruction registers which must drive both your control logic and a data bus.

93415 A 1024 x 1-bit Fully Decoded Random Access Memory—for your high-speed data and control stores.

Raytheon LSI is on the move. More 2900 family components soon to come include PROM's, sequencers, look-ahead carry generators, additional RAM's, and other goodies now in process.

For complete details, contact your local distributor or Raytheon Company, Semiconductor Division, Dept. 2900, 350 Ellis Street, Mountain View, CA 94042, (415) 968-9211.

Am 2900
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RAYTHEON
SEMICONDUCTOR DIVISION

CIRCLE NUMBER 42
IDEAS FOR DESIGN

Special-purpose pulse-width modulator produces an output of same polarity as input

In some applications—such as in hardware simulation, or in instrument-and-control applications that use pulse-width modulated hydraulic valves, pressure regulators or actuators—the pulse-width modulator's output must have special characteristics. The output must consist of a train of positive pulses if the input modulating signal is positive, and negative pulses, if the modulating signal is negative. No pulses should be present when the signal amplitude is zero.

Such a modulator can be designed with two op amps, two 555 (or one 556) timers and a few passive components (Fig. 1).

If a 555 timer, connected in the monostable mode, is triggered by continuous clock pulses (at pin 2), and the timer's threshold input (pin 3) is modulated by an applied signal, the circuit behaves as a pulse-width modulator. However, the modulator works only on positive input signals.

A second timer handles the negative part of the input-modulating signal. Its modulating signal is first inverted by an op amp. A second op amp then combines the outputs of both timers. This op amp inverts the output of the second modulator, and thus provides both negative and positive pulse-modulated waves, as required.

Diodes D1 and D2 automatically separate the positive and negative parts of the modulating signals to T1 or A1. The A1 op amp should be fast enough to handle the expected rise time of the output of the timers. Diodes D1 and D2 can be any general-purpose signal diodes.

M. P. Srinivasan, Design Engineer, Systems Group, Engineering Design Centre, Indian Institute of Technology, Madras 600 036, India.

CIRCLE NO. 313

MODULATING SIGNAL
DI
V
+0

MODULATED OUTPUT

1. A special pulse-width modulator generates both positive and negative pulse-width modulated outputs. The output polarities correspond to the input polarity; zero signal provides zero output.

SEND US YOUR IDEAS FOR DESIGN. You may win a grand total of $1050 (cash)! Here's how. Submit your IFD describing a new or important circuit or design technique, the clever use of a new component or test equipment, packaging tips, cost-saving ideas to our Ideas for Design editor. Ideas can only be considered for publication if they are submitted exclusively to ELECTRONIC DESIGN. You will receive $20 for each published idea, $30 more if it is voted best of issue by our readers. The best-of-issue winners become eligible for the Idea of the Year award of $1000.

ELECTRONIC DESIGN cannot assume responsibility for circuits shown nor represent freedom from patent infringement.

100 ELECTRONIC DESIGN 20, September 27, 1976
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The relays will be there
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matter of hours. But we frequently ship orders
in 24 hours. And, we can generally promise
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We're fast—but we're also something else—
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we run over 3 billion test cycles every day!
We make over 6000 variations of dry reed re-
lays so we undoubtedly have what you need.
And the cost? Well, you better call and get a
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GaAlAs laser used in fiber-optic system

A buried-channel GaAlAs laser for use in long-distance fiber-optic communication systems is ideally suited for the application because its emission is confined to a small area whose dimensions are of the order of the wavelength of the laser light.

According to Standard Telecommunications Laboratories in Harlow, England, who developed the new laser, the ideal injection-laser source for optical-fiber systems and integrated optics has carrier and optical confinement—not only in the plane perpendicular to the pn junction, but also in the plane parallel to the junction.

Standard Telecommunications has developed a method of fabricating such devices by using liquid-phase epitaxy. The buried active channel is sandwiched between continuous n and p-type passive layers, and has a parabolic profile, tapering gradually to zero at the edges.

The n-type GaAs substrate has a channel laser etched in the top surface; then an active layer is grown over the entire surface. The active layer naturally levels out the structure, providing an isolated active channel. The channel width in devices produced to date is about 10 µm. A 1 µm-wide device is being developed.

Analysis of the spectrum of the device's laser emission has shown that the modes of emission are limited by the width of the active channel. According to Standard Telecommunications Laboratories, a device with a 1 µm-wide channel would produce a single-mode laser.

Plastic thermal sensor has improved sensitivity

A low-cost plastic thermal sensor with substantially better sensitivity than similar metallic or semiconductor devices has been produced by a research team at the Marconi Research Laboratories in England.

The Marconi sensor is a thin film of polyvinylidene fluoride (PVF) that is sensitized by heating the film to 100°C and exposing it to an electric field of 1 mV/cm.

Metallic contacts are deposited and the film then acts as a perma-
nently charged capacitor. A change in the film thickness due to thermal expansion varies the effective capacitance of the device.

Laboratory prototypes have detected human body heat at 100 yards. A wide range of medical applications is seen, in addition to applications in security systems.

Because changes in air pressure also modify the sensor thickness, the transducer can function as a microphone. A prototype high-impedance condenser microphone built by the research team had a sensitivity of 10 mV at 1 kHz. It responded to frequencies ranging from below 30 Hz to above 4 kHz.

**New microwave devices boost flight safety**

Two new microwave developments by AEI Semiconductors Ltd., Lincoln, England, may advance flight safety by reducing the cost of navigation beacons and improving the reliability of radar equipment.

The first development is a pulsed Gunn oscillator that AEI says is the key element of a transponder that has a fundamental oscillator operating at 9.4 GHz. Output power is 250 mW minimum for a pulse length of 25 µs over a −20 C to +60 C range. The Gunn oscillator can be electronically tuned over a 200-MHz band. The pulse chirp is limited to 7 Hz and the temperature coefficient of frequency is 0.25 MHz/°C.

The second AEI development is a gallium-arsenide mixer diode that has increased tolerance to burnout. Use of this device improves the reliability of 8 to 11-GHz radar-microstrip mixer circuits. The spike-burnout limit is 100 nJ. The CW burnout occurs at 500 mW, while the peak-pulse rf burnout is at 1 W input.

The noise figure is 6 dB with a VSWR of 1.5:1 and an i-f impedance of 400 Ω.

**Researchers develop crystal for hot cathode**

An electron-gun hot cathode with 10 to 100 times the beam intensity of the best previous cathodes uses a single crystal of lanthanum borate for the electron source. The borate crystal, developed by the Japanese National Institute of Researchers in Inorganic Materials, is an artificially synthesized material with a hardness about one third that of diamond and a melting point between 2300 and 2400 C. The material is powdered and heated by rf induction to produce single crystals 7 to 8 mm in diameter and 5 cm long. An electric discharge tool reduces the single crystals to needle-like crystals 0.2 mm in diameter and 5 mm long. Electrolytic grinding further sharpens the tip to submicron size.

Hot cathodes are extensively used as electron beam sources in electron-beam machining tools, electron microscopes, cathode ray tubes and, more recently, in replacing optical beams used in semiconductor manufacturing where very high packing densities are required. Tungsten, barium and strontium oxide crystals have been used, as well as sintered lanthanum borate. The radius of curvature of the LaB₆ crystal is about 0.2 µm, compared to the 10-micron radius of sintered LaB₆, and causes a more stable beam.
MUNICH
GERMANY. NOV. 25 — DEC. 1, 1976
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This year's ELECTRONICA is going to be a stellar event. It's the "show of shows," largest in the world.

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CIRCLE NUMBER 48
Analyzer excites, then measures response

EMI Technology, 20 Old Ridgebury Rd., Danbury, CT 06810. (203) 744-3500. Start at $6700; stock to 30 days.

Series SM2001A digital transfer-function analyzer provides sinusoidal excitation and measures response in coordinate values. Range is 0.00001 to 999 Hz, extendable to 1 MHz. The unit analyzes the dynamic transfer function of any system or component, from an electronic filter to a battleship gun turret. Display is cartesian, polar or log/polar. Measurement accuracy is ±0.5% of reading ±1 count, and results are displayed on 4-digit panel readouts.

CIRCLE NO. 301

Two monitors offer small spot, storage

Tektronix, P.O. Box 500, Beaverton, OR 97007. (503) 644-0161. 607, $1800; 4-6 wks.

Two display monitors are targeted for OEMs. The 606 produces a very small dot size—6.0 mil at normal intensity and 5.0 mil at low intensity—which is uniform across and 8 x 10-cm CRT. Electronic correction provides optimum focus over a 7 x 9-cm area. The 607 features variable-persistence storage and spot size of 20 mils stored, 12 mils nonstored. Image persists up to 50 minutes.

CIRCLE NO. 302

Small counter measures 60-MHz frequencies

Non-Linear Systems, P.O. Box N, Del Mar, CA 92014. (714) 755-1134. $195; stock.

A frequency counter joins the company’s line of miniature, battery-powered test instruments. The FM-7 measures only 1.9 x 2.7 x 4 in. It monitors frequencies from 10 Hz to 60 MHz and displays the results to seven digits using 0.25-in. LEDs. Input sensitivity is 30 mV rms from 50 Hz to 50 MHz, 100 mV rms from 10 Hz to 60 MHz.

CIRCLE NO. 304

Preamp boosts instrument sensitivity


Designed to enhance measurements of low-level signals, Model 10855A preamplifier increases sensitivity of scopes, counters and analyzers by more than 10 times. Minimum gain is 22 dB (24 dB typical) 2 to 1300 MHz ±1 dB. It operates from a power supply of +15 V at 40 mA or with those HP instruments with a probe power output. Other features: 50-Ω input and output impedances, fuse protection, and reverse isolation of greater than 45 dB.

CIRCLE NO. 305

PROM programmer is fully interactive

International Microsystems, 122 Hutton St., Gaithersburg, MD 20760. (301) 840-1078. $1295; 4 wks.

Series 1000 µP controlled PROM programmer offers fully interactive operation in any of three programming modes—keyboard entry, terminal control or remote computer control. A 32 k bit buffer RAM memory allows the user to edit the data in RAM from the keyboard of the programmer prior to the actual programming operation. A 14-digit hex display gives 4 digits each of address, copy PROM data, and master PROM data, plus a 2-digit entry and error code.

CIRCLE NO. 306
INSTRUMENTATION

Transnet recorder
features 20-MHz ADC

Data Laboratories Ltd., 28 Wates

A transient waveform recorder
made in Britain features a 20-MHz
a/d converter which takes a measure-
ment every 0.05 µs. Two versions
are available: the single-
channel DL920 and the twin-chan-
nel DL922. The latter samples
simultaneously on both channels
at a rate up to 10 MHz per chan-
nel, but can also be used as a
single-channel instrument. Elusive
signals, such as one-shots, are re-
corded in a 2048-word memory (a
4096-word option available) and
may be reproduced on an oscillo-
scope or as hard copy on a pen
recorder.

CIRCLE NO. 309

Current calibrator
works to 1 A

Zi-Tech Div., 223 Forest Ave., Box
26, Palo Alto, CA 94302. (415)
326-2151. $340; stock.

TE505 compact de current
source offers 0.1% accuracy. The
unit has three ranges: 1 mA, 10
mA and 100 mA full scale. An op-
tional 1-A range-extender unit is
available. Four decades of thumb-
switches are provided for the cur-
rent setting. The internal refer-
ence is a precision zener, aged and
selected for performance. The in-
strument is overload protected and
a front-panel indicator shows if
drive voltages greater than 10 V
are called for.

CIRCLE NO. 310

INSTRUMENTATION

Chart receiver gives
24-h field operation

Kay Elemetric, 12 Maple Ave.,
Pine Brook, NJ 07058. (201) 227-
2000. $1895.

Model 9021 digital chart re-
ceiver and recorder provides a
built-in timer (0.25, 0.5, 1 and 2-
hour intervals) for portable, unat-
tended CATV measurements. You
can get 24-hour unattended opera-
tion from one fully charged auto-
motive battery. The unit can also
be operated from an external
source or from ac. Specs include a
frequency range of 5 to 400 MHz;
minimum signal input for 1/2-
scale deflection of 0 dBmV; verti-
cal and horizontal resolution of 8
bits; and a memory size of 2000-
bits.

CIRCLE NO. 307

‘Nude’ DPM mounts
behind panels

International Microtronics Corp.,
4016 E. Tennessee St., Tucson, AZ
85714, (602) 748-7900. $47; stock-
4 wks.

Model 325, called the “Naked
DPM,” is built on a single PC
board measuring 2.9 × 1.4 × 0.35
in. Display is orange LEDs, 0.4-
in. high. Features include auto-
matic-polarity indication, external
decimal-point selection, 1000-MΩ
input impedance, ±0.1% accuracy
and linearity, 7-pA typical in-
put bias current, tempco of
±0.006%/°C and power consump-
tion of 550 mW. Ranges available
are 1, 10, 100 and 1000 V dc with
up to 1200-V overvoltage protec-
tion.

CIRCLE NO. 308

Digi’tal meter reads
capacitance in 250 ms

GenRad, 300 Baker Ave., Concord,
MA 01742. (617) 369-4400. $2785;
2 wks.

Measurement of capacitance and
dissipation can be made automati-
cally with the GR 1686-A digital cap-
citance meter. Capacitance can be
measured from 0.01 pF to
200,000 pF at test frequencies of
120 Hz and 1 kHz with 250-ms
measurement time. Basic accuracy
is 0.1% for 1-kHz measurements
and 0.5% for 120-Hz measure-
ments. A measurement-mode switch
allows either single or repetitive
measurements at rates ranging
from four per second to one every
10 s.

CIRCLE NO. 310

ELECTRONIC DESIGN 20, September 27, 1976
Compare our SOA and $E_{S/b}$ to theirs and you’ll understand why our high current/voltage transistors work.

High voltage and high current specs aren’t enough. If you’ve ever specified transistors above 50 amps, only to find they fail on the job, you know how high-current specs may actually be misleading.

The truth is, unless you see the SOA and $E_{S/b}$ specs, there’s no way of knowing whether a high-current device has the guts to withstand a surge, and not blow out.

That’s why we publish both our Safe Operating Area and $E_{S/b}$ specs.

We want you to see precisely the kind of super-ruggedness you can expect from PowerTech—and only PowerTech—high-current transistors. Compare our $E_{S/b}$ ratings, from 1.5 to 6 joules, against the millijoules or unpublished ratings of other high-voltage/current devices.

Copper makes the difference. We use extra-heavy copper-metallizing on our bigger, beefier chip—thereby assuring maximum thermal and electrical conductivity and yielding the highest resistance to second breakdown with the lowest $V_{CE(sat)}$. Their smaller chips use thin aluminum-metallizing with fragile, current-limiting wires (ours have solid copper posts).

Which would you rather have your circuit depend on? And we don’t stop there. To guarantee rapid delivery, we pre-mount our chip on an integral moly-copper heat sink so we can categorize and pre-test the module at high currents to insure maximum reliability prior to mounting in the package of your choice (again 100% tested to the most stringent MIL/AERO specs).

They, on the other hand, must first mount their chip on the packaging, then test to determine if it’s shippable.

**Delivery and prices.** Our catalogs come complete with prices...we don’t believe in secrets.

While our initial device cost may be slightly higher, in the long run we believe you’ll find that it’s less expensive to use transistors that keep on working.

We rely on direct factory-to-customer contact to ensure 100% responsiveness, backed up by the flexibility of chips already built, pre-tested and ready for whatever electrical/packaging requirements you may have.

But see for yourself: call for further information and applications assistance: Sales Engineering, PowerTech, Inc., 9 Baker Court, Clifton, N.J. 07011; (201) 478-6205.

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**PowerTech, Inc.**

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**Typical Products**

<table>
<thead>
<tr>
<th>$I_C$</th>
<th>$V_{CE}$</th>
<th>$E_{S/b}$</th>
<th>Part No.</th>
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<td>6.0J</td>
<td>MT-5007</td>
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<td>120V</td>
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<td>800V</td>
<td>2.5J</td>
<td>PT-3856</td>
</tr>
</tbody>
</table>

JAN-TX Types Also Available

Guaranteed SOA
If we told you it has a premium quality switch and precision pins (not bent switch leads) would that help? Or that it's magnetically shielded, U/L listed and meets NARM/EIA proposed standards?

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Hard to believe, but true. All the prices are right. They're the under 25, 100 or MORE and 25,000 prices respectively.

To believe, but true. And we have many other types available, handsomely priced, to fit your needs and budget. So if you'd like to know more, write us (on your letterhead) for a free sample, or call us for a high volume price quote and let us show you how, at Wabash, the price is always right.

**Components**

$5 solid-state relays retain all features

Wabash Controls, Div. International Rectifier, 1521 Grand Ave., El Segundo, CA 90245. (213) 322-4987. 1000-up prices: $5.45 (Series 2), $4.95 (Series 3); stock.

Solid-state relay competition with traditional electromechanical relays gets hotter with the Challenger series, offered in production quantity for as low as $5. Power is rated to 8 A and all features associated with solid-state relays are available. Among features in the Challenger series that other low-cost units lack, according to Crydom, are zero-voltage turn-on, internal snubbers for the triac, half-cycle response and a firm bi-stable turn-on action. In addition, competitive units require higher control current, says Crydom and they don't accept spade-type quick-connect terminals as the Challenger units do. The Challenger series comes in two styles: a miniature unit for PC mounting and a unit with an integral heat-sink mounting surface and push-on connectors for direct-panel or external-finned heat-sink mounting.

Series 2 units can handle 8 A rms, when mounted on a heat sink and a one-cycle surge current to 80 A. Isolation, output-to-base and output-to-input is 1500 V ac or 2100 V dc. Blocking voltage is 500 V and rate of rise (dv/dt) is 100 V/μs minimum. Series 3, a PC mount version has a very flat profile and is rated for 2 A rms, 90 to 280 V ac with a surge current rating of 40 A rms. Blocking voltage is also 500 V and dv/dt is 100 V/μs. The units are SPST NO switches.

**Circuit Breakers clear in 9 ms**

AMF Inc., 200 Richland Creek Dr., Princeton, IN 47671. (812) 868-1000. From $3: single pole (OEM qty), stock.

The Mini-Mag Series W67 single-pole, W68 double-pole and W69 triple-pole breakers feature circuit-clearing time as fast as 9 ms on moderate to heavy overloads. In addition, the slight inductance of the breaker coil helps limit I-T on steeply rising fault currents. Available in triip-current ratings from a fraction of an amp to 30 A, these compact breakers will interrupt fault currents to 2000 A. All standard models are UL recognized as appliance components, and CSA recognized as appliance component protectors. The breakers feature wipe-on-make contacts and a trip-free mechanism, which allows the contacts to open an overload even if the toggle is held in the ON position. On double and triple pole models, an overload in any circuit opens all circuits. Maximum operating voltages are 250 V ac, 60 or 400 Hz, and 50 V dc. All models are temperature stable between -40 and 85 C.

**Illuminated PB switch meets MIL specs**

Control Switch, A Cutler Hammer Co., 1420 Delmar Dr., Folcroft, PA 19032. (215) 586-7500. $11.92 (unit qty).

An illuminated momentary-action pushbutton DPDT switch (part number A20267) meets all requirements of MIL-S-22885/18-01. It's environmentally sealed and shock and vibration resistant. Temperature range is -55 to 85 C. The switch maintains stable contact resistance, especially at minimum current as specified in the MIL spec. It's rated at 28 V dc or 115 V ac, 2-A resistive, 1.5-A inductive and 0.5-A lamp load. Its operating force is 2 ±1 lb.
Keyboard designed to clean easily

DataNetics Corp., 18065 Euclid St., Fountain Valley, CA 92708. (714) 549-1191. $2.90 (10,000 up); stock to 45 days.

Low-cost touch keyboards can be used in both home appliances and industrial systems. The Series 700 is thin (0.15-in. thick), waterproof and completely sealed. Units are available in an unlimited choice of sizes, styles and colors, with or without both bezel and tactile feedback. The standard keyboard interconnects through connectors, or it can be hard wired. Because the keyboard has no cracks or pockets, it is easy to clean.

CIRCLE NO. 325

Rotary switches provide 60 positions

Oak Industries Inc., Crystal Lake, IL 60014. (815) 459-5000. $2.30: single section, $3.60: double section (1000 up); limited production.

A rotary switch with a capacity of up to 60 positions, designated the Communication-Series switch, has three rotary-switch design innovations: contacts never touch the laminate, thus eliminating scraped-off particles and intermittent opens; dead and live metal areas on the rotor are separated by grooves that clean each contact as it passes over them; a PC rotor has an integral cam that functions as a precision detent, eliminating functional backlash from loose rotors and stack-up tolerance problems. Oak guarantees switching accuracy for the life of the switch on all applications received by Oak to date. A single section can accommodate two 7-bar readouts or two 8-bit binary codes with separate commons. Plastic materials used have 94 VO UL flammability listing, and terminals are designed for PCB insertion.

CIRCLE NO. 326

A NEW GENERATION OF IMAGE SENSORS

SIMPLICITY OF USE -
Requiring less than a dollars worth of circuitry to drive—and barely more than that for video processing—is just one of the key features of our new “G” series image sensors. Compare the non-critical single TTL clock needed for the “G” device to the complex multi-phase clocks prescribed by others.

You need only this for Reticon

You need all these for others

HALF THE PRICE -
Or even less will bring you 256, 512, 768, or 1024 sensor elements on 25µ centers or up to 1728 elements on 15µ centers in our “H” series.

SUPERIOR PERFORMANCE -
Low dark current allowing low light level operation, on-chip noise cancellation, and smooth spectral response from visible through infrared makes this new generation the unquestionable choice.

APPLICATIONS -
Page readers, facsimile, OCR, point of sale readers, non-contact measurements and inspection and many others.

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PHONE: (408) 738-4266 TWX: 910-339-9343

CIRCLE NUMBER 51
Whatever your linear actuation needs, check with Ledex for the answer. Over 100 design variations are waiting on the shelf to insure 48 hour delivery of your prototypes.

Models range from a space saving 1/2" x 1/2" tubular solenoid to a hefty 33/8" pancake solenoid that will develop up to 350 pounds of force. You'll probably want something in between and we've got it with our full line of Tubular, D-Frame and Pancake Solenoids.

If your application calls for something special, we'll put over thirty years of solenoid experience to work for you to find the optimum solution.

The optimum solution could be something other than a linear solenoid. That's why we make a full line of Rotary Solenoids, Stepping Motors and Electro Proportional Solenoids. And that's an option no other manufacturer can give you!

Write or call today for our 36 page Linear Actuation Line catalog and price sheet.

Ledex Inc.
123 Webster Street, Dayton, Ohio 45401 (513) 224-9891
Ironless-rotor motors
cog less, make less noise

North American Philips Controls Corp., Cheshire Industrial Park, Cheshire, CT 06410. (203) 272-0301. $6.52 (500 up); prototypes from stock, production 12 to 14 wks.

Low noise levels, rapid acceleration, low cogging and compact size are advantages claimed for the Series 4322-010-77000 dc ironless-rotor motors. Designed for 9-V-dc operation, the motor has a 0.76-g-cm² moment of inertia, 8.5-g-cm starting torque and a motor constant of 50 ms, typical. A gold-plated five-segment commutator and silver-plated brushes are used for optimal commutation. This permits the use of accurate electronic control for servo motor or tachometer service.

CIRCLE NO. 329

Low-profile relay
fits 0.6-in. spacing

AMF, Potter & Brumfield Div., 200 Richland Creek Dr., Princeton, IN 47671. (317) 388-1000. $4 (100 up).

A lightweight 6-form-C relay, series T10, permits PC-board spacing on 0.6-in. centers and accepts drive directly from ICs. Coil voltages of 6, 12, 24 and 48 V dc are available, and permissive-make contacts are rated 0.1 to 3 A at 28-V-dc or 120-V-ac resistive. Bifurcated contacts are rated low-level to 1 A at 60 V dc or 12 V ac resistive. The permissive-make arrangement gives all T10s long operating life because of minimal contact bounce. Life expectancy is a minimum of 50-million operations mechanical to 50,000 operations at full load. Initial contact resistance is 50 MΩ or less.

CIRCLE NO. 330

Join the hundreds who have already discovered the versatility of Repco's modular RF links.

How versatile? The overwhelming response to our Undiscovered Genius contest proves the true versatility of Repco's modular RF links. Prizes were awarded for these winning ideas:

- Hospital data system
- Bank teller alarm
- Remote drone fire fighter
- Cardiac rate alarm
- Mine roof failure alert
- Portable ticket vending system
- Silo inventory control
- Boat security system
- Remote timer/counter
- Porpoise communicator
- Radio controlled shark
- Remote corrosion monitoring

What can you do with RF links? While building a remote-control shark may be a little too zany for you, consider some of the innovative and commercially proven applications now utilizing Repco modular RF links:

- Air to ground communication
- Alarm systems
- Electric power line monitoring
- Fire nozzle pump operator
- Mine pollution monitoring
- Ocean monitoring buoy system
- Remote crane control
- Repeater link
- Seismic monitoring
- Small craft emergency beacon
- Traffic emergency assistance
- Water flow monitoring

Repco's modular RF links are designed for voice, low-speed digital, or tone operation. Frequencies available are 25-50 Mhz, 72-76 Mhz, 132-174 Mhz, and 450-470 Mhz ranges (66-88 Mhz for overseas usage). All units are built to stringent FCC & EIA specifications.

Be a Genius . . . design Repco's RF links into your system. Write or call for free specs brochure.

CIRCLE NUMBER 53
Low-cost inverters deliver 30 to 320 VA
Abbott Transistor Labs, 5200 W. Jefferson Blvd., Los Angeles, CA 90016. (213) 936-8185. $262 to $361; stock to 8 wk.

Series KN, PN and LN are said to be the lowest cost dc to sine-wave inverters, in the 30-to-320-VA range, you can buy. They operate from a dc input of 11 to 15, 22 to 30, or 29 to 38 V, producing ac at either 115 V at 60 Hz or 220 V at 50 Hz. Their maximum distortion is 5% and regulation for line or load is 3%. Additional features are: a surge-current capability of three times the rated output and the ability to withstand input transients of 45 V dc for 0.1 s. A magnetic circuit-breaker provides overload protection.

HV supply is stable and analog-controlled

Spelman High-Voltage Electronics Corp., 1930 Adee Ave., Bronx, N.Y. 10459. (212) 671-0300. $580 up, 8-12 wks.

The SEM25N6000X stable high-voltage dc power supply has a continuously-variable output of 0 to 25 kV at 0.25 mA. It is a completely solid-state unit with an encapsulated high-voltage section. The supply features line and load regulation of 0.001% from 10% to its maximum rated voltage, max ripple of 10 ppm from 2.5 to 25 kV and 50 ppm from 1 kV to 2.5 kV, max drift of 10 ppm in four minutes or 50 ppm per hour and a tempco of 0.005% per °C. Either an external resistance or voltage can control the supply's output. For safety, the control circuits are referenced to ground and, the HV return is floated above ground and clamped not to exceed 15 V. This feature lets you use independent grounding of the load-return circuit to eliminate a possible ground loop. The floating HV return is also an aid in the measurement of load current. The unit is protected against arc-over and overloads and has automatic recovery.

De/dc converters deliver 140 W

Wilmore Electronics, P.O. Box 2973, Durham, NC 27705. (919) 459-3318. $320 (10); stock-30 days.

Designed to power equipment such as mobile-radio base stations, data processing and process-control equipment, the Model 1295 dc/dc converter feature efficiencies of greater than 80%. Standard input voltages are 24 and 48 V dc; standard output voltages are 12, 24, 26, 48 and 125 V dc. Each unit can provide 140 W continuously. Model 1295 comes in a 5-1/4 × 12 ×19-in. rack-mount or smaller enclosure. All versions weigh less than 12 lb.
Rugged inverters run off 10 to 400 V dc

Advance Conversion Devices, 109 Eighth St., Passaic, NJ 07055. (201) 778-0707. From $285; stock to 90 days.

These ruggedized inverters feature 50,000 hours guaranteed MTBF. They operate from 10-to-400-V-dc inputs with efficiencies in excess of 80%. Outputs of 36 VA to 15 kVA are available at 50 (series D), 60 (series A), or 400 Hz (series C). All units withstand high-voltage spikes and ripple on the input and provide a true sine-wave output with distortion limited to 5% rms.

CIRCLE NO. 334

375 W packed into small dual-output switcher

LH Research, Inc., 1821 Langley Ave., Irvine, CA 92214. (714) 546-5279. $525; stock to 90 days.

The MMX-720 is a two-output switching-regulated power supply in the Mighty Mite series. Its package is 3 x 9.5 x 13 in. The main output delivers 5 V at up to 75 A, while the other output can be any one of the following: 2 V at 24 A, 6 V at 24 A, 12 V at 20 A, 15 V at 20 A, 18 V at 16 A, or 24 V at 10 A. Note that the maximum combined power of both outputs is 375 W. Other operating characteristics include: efficiency of up to 80%, ripple of 1% or 50 mV pk-pk, noise output of 1% pk-pk, or 50 mV, line regulation of 0.4% over the entire input range, load regulation of 0.4% from no-load to full-load and response time of 200 μs to 1% after a 25% load change. Its operating range spans 0 to 70 C. Full rating is maintained to 40 C but must be derated to 60% at 70 C.

CIRCLE NO. 335

48-V input operates 5-V dc switching regulator

ACDC Electronics, 401 Jones Rd., Oceanside, CA 92054. (714) 757-1880. $672, stock to 4 wks.

The model JD5N100 dc-to-dc supply accepts inputs from 42 to 60 V, and delivers 5 V at up to 100 A. It has an efficiency of 70%, measures approximately 5 x 7 x 15 in. and weighs 19 lb. Overvoltage, thermal and reverse-voltage protection is standard. Provisions are made for remote-sensing, remote-shutdown and remote-control. These supplies also can be paralleled.

CIRCLE NO. 336

OEM DESIGNERS

Get this FREE Design File on CDC's new modular switching power supplies

These compact, modular power supply switchers simplify design in 300-600 watt applications and keep costs down too. (They're priced at less than 90¢ per watt!) Benefits to the end user include low EMI noise levels (we are designed to meet VDE STD 0875) and highly reliable operation plus convenient maintenance and easy add-on capability up to 1200 watts in a single, 19 in. rack. Get specs, prices and feature details today from:

Magnetic Components Group

CIRCLE NUMBER 56

ELECTRONIC DESIGN 20, September 27, 1976

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OUR EASIEST-TO-USE 2650: NOW MULTI-SOURCED.

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CIRCLE NUMBER 57

a subsidiary of U.S. Philips Corporation
**POWER SOURCES**

**High-current supply drives ECL circuits**

ACDC Electronics, 401 Jones Rd., Oceanside, CA 92054. (714) 757-1880. $720; stock to 5 wk.

You get the two voltages needed to power ECL logic—5.2 V at 16 to 80 A and 2.2 V at 0 to 50 A—from the Model JF102. These voltages can be remotely programmed ±5% for system margin-checking. The unit operates from 115/230 V ac ±15%, 47-to-63-Hz single-phase. Either can be selected by using the appropriately marked input terminal. Measuring 5 x 8 x 10.5 in. and weighing less than 20 lb, the unit contains a replaceable fan that permits full output at 50 C, derating linearly to 70% at 70 C. Overload, thermal and overvoltage protection is standard.

**CIRCLE NO. 337**

**Four-output dc supplies are not custom-priced**

Deltron, Wissahickon Ave., North Wales, PA 19454. (215) 699-9261. $86-$109, 1 wk.

The “Quad” series of four-output power supplies consists of standard modules mounted in a single chassis. You can thus bypass the usual engineering charge when you need a custom supply. The Model 888 consists of a QT-2 triple-output power supply (rated: 5 V at 6 A, ±12 to ±15 V at 1 A) assembled in a common chassis with any of the three QPS series single-output supplies. The Model 8899 consists of an MPS-2 triple-output power supply (rated: 5 V at 7 A, 12 V at 1 A, and 9 V at 1.2 A or 5 V at 0.75 A) assembled in a common chassis with any of the three QPS series single output supplies. Specifications for the “Quad” series are the same as those of the MPS, QT and QPS models they are derived from.

**CIRCLE NO. 338**

**25-W regulator meets MIL-E-5400 P class 2**

Abbott Transistor Labs, 5200 W. Jefferson Blvd., Los Angeles, CA 90016. (213) 936-8185. $355 (1-4); 10 wks.

The UN25 series of switching regulators is fully encapsulated and hermetically sealed to meet the environmental requirements of MIL-E-5272C and MIL-E-5400P class 2 and the EMI requirements of MIL-STD-461. The units operate from 115 V, 400 Hz. They output from 5 to 50 V dc at 25 W. Output current is full rated from —55 to +85 C derated 80% at 100 C. Regulation is 0.3%/°C. Other standard features include short circuit protection, input transient protection, remote error sensing, input to output or case isolation is 250 V de and output to case is 50 V de. MIL connectors and overvoltage protection are available as options. Case size is 3.5 x 5.5 x 2.5 in. They weigh 2.8 lb.

**CIRCLE NO. 339**

**Cabinet mounted UPS series spans 3 to 15 kVA**

Topaz Electronics, 3855 Ruffin Rd., San Diego, CA 92123. (714) 279-0111. $5000 and up, 1-4 wks.

Standard models of the 81000 series of uninterruptible power supplies (UPS) are single-phase output units with 3, 5, 10 and 15 kVA ratings. They are mounted in NEMA type-2 front-access cabinets. On all standard models, continuous display of the system's operational status is provided by a status-monitor and control panel. Options available include: static-transfer switch, audible-alarm and acknowledgement switch, output-frequency meter, battery-float equalize capability with timer, and battery ammeter.

**CIRCLE NO. 340**
MICROWAVES & LASERS

Delay line is switched in discrete steps


The Nanno Switch is a switch-variable delay line designed for the nanosecond range. The units consist of individual delay lines each with its own switch. Time delay is changed by switching one or more individual delay lines in series with the input and output connections. Units are available in 50 and 75-Ω impedances with eight switches, including 1, 2, 4, 8, 16, 32, 64 and 128-ns delays.

CIRCLE NO. 341

Need a compact, remote multiposition switch?

Miconetics, Inc., 36 Oak St., Natick, MA 01760. (201) 767-1320. Start at $195; stock-4 wks.

Model RS series of remote miniature multiposition coaxial switches covers a frequency range of dc to 18 GHz and has an rf power rating of 50 W average. Isolation is 60 dB min., insertion loss is 0.5 max., VSWR is 1.6 max. Impedance is 50 Ω.

CIRCLE NO. 342

Power divider splits input five ways

Sage Laboratories, 3 Huron Dr., Natick, MA 01760. (617) 653-0844. $250; 45 days.

Model FP1835-24 is the forerunner of a new series of five-way power dividers. The unit has an operating frequency range of 2 to 4 GHz, over which it features maximum VSWR of 1.5:1 at all ports, 15-dB min. isolation, 0.6-dB max. insertion loss (0.3 dB typical), and 0.5-dB max. imbalance. Size is 3.25 x 3.00 x 0.50 in.

CIRCLE NO. 343

tiny trimmers... tiny price!

MuRata's new line of subminiature trimmers has established a standard of performance in the economical trimmer field second to none... Alumina-base, non-combustible design, extreme resistance to solvents, and a wide 100 ohm to 2 megohm range of resistances. What's more, they are backed by MuRata's world-wide reputation for quality you can count on. Find out how these new pots can be put to work for you. Send for complete technical information today.

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Rockmart Industrial Park, Rockmart, Georgia 30153
Phone: 404-684-7821/Telex: 54-2999/TWX: 810-766-1340

CIRCLE NUMBER 59
Electonic Design 20, September 27, 1976
Laser claims mini title

Only 8-5/8 in. long and 1-3/8 in. in diameter, this new 0.8-mW cylindrical laser, the ME-620, may be the world’s smallest mass produced helium-neon laser. Front and rear rings are locked in place with an Allen wrench. The beam can be positioned concentric with these rings or can be aimed off-center according to the user’s requirements. The output power is near the maximum permitted for Class II lasers.

CIRCLE NO. 344

Metrologic Instruments, 143 Harding Ave., Bellmawr, NJ 08030.

Need answers on rechargeable power sources?

Call the guys who’ve been there

800-433-2684

in Texas 800-792-8767

Call our Hot Idea-Hotline toll-free and we’ll help you design a nickel-cadmium sealed cell power package to fit your specific needs. In addition, we’ll give you hard facts on sizes, ampere hours, configurations, prices, delivery. Chances are, all the applications we’ve done on hand tools, appliances, calculators, toys, and communication equipment will provide some short cuts for you. Call us. We’ll deliver. Marathon Battery Company, P.O. Box 8233, Waco, Texas 76710. A division of Marathon Manufacturing Company.

Gunn oscillators claim low AM noise

A new series of mechanically tuned Gunn-effect oscillators covers the 18-to-60-GHz frequency range and features inherently low AM noise characteristics. Each unit is factory adjusted to one of eight specific center-frequency ranges. Minimum power outputs range from 10 to 250 mW, although not all outputs are available in all frequency ranges. Mechanical tuning range is from ±250 MHz in the lower frequency models to ±150 MHz in the higher frequency units.

CIRCLE NO. 345

Blue laser lives for 4000 hours

This helium-cadmium laser, Model 4100, offers a tube life expectancy of more than 4000 h. Previous tube life in blue lasers is said to have rarely exceeded 2000 h. Range of operation has also been increased from 0 to 50 C, and the laser package eliminates complicated mirror-adjusting plates, springs and straps. In addition, the resonator structure has environmental shielding for maintenance-free operation.

CIRCLE NO. 346
TWT amplifier offers protection features

Logimetrics, 121-03 Dupont St., Plainview, NY 11803. (516) 681-4700. $16,000; 120 days.

The A 700 series of traveling-wave-tube amplifiers offers a minimum rf output of 1 kW over the frequency range 1.0 to 16.0 GHz. All models use solid-state power supplies protected by a front-panel circuit breaker. All controls are front-panel mounted. The tubes are protected by helix current and voltage sensors, filament surge limiting and thermal overload sensors. Minimum gain is 35 dB.

Couplers feature stripline construction

Omni Spectra, 21 Continental Blvd., Merrimack, NH 03054. (603) 424-4111. $35 to $175; 3-8 wks.

All fourteen models in new coupler series 20190 feature stripline construction. Standard available frequency ranges are 1.0 to 2.0, 2.0 to 4.0, 4.0 to 8.0 and 7.0 to 12.4 GHz. Mean coupling values of 6, 10 and 20 dB are offered in each frequency range. Temperature range is -54 to 125 C. The 20190 incorporates three OSM jack connectors. Isolated port is terminated with 1/2-W, 50-Ω load.

GaAsFET amplifier shows noise figure of 2.6 dB

Trak Microwave Corp., 4726 Eisenhower Blvd., Tampa, FL 33614. (813) 884-1411. $2150; 30-40 days.

Model 8040-1030 is the first in a family of GaAsFET solid-state amplifiers. Designed to operate in the 3.7-to-4.2-GHz region, the low-noise amplifier has a gain of 50 dB min and a noise figure of 2.6 dB max. Gain variation is ±0.25 dB max, with a gain slope of 0.1 dB per 20 MHz max. Intermodulation intercept is +23 dBm min and VSWR (input/output) is 1.25:1 max. The 8040-1030 operates from -40 to 60 C, weighs only 14 ounces and measures 3.6 x 3.9 x 1.25 in.

Guess the number of caps in the jar and win one. Free.

Right—we'd like to give you a free sample. Just to show you how easy it is to get the right film capacitor for your high energy pulse discharge, communications and instrumentation circuits.

Our line includes metallized film and film-and-foil capacitors with polyester, polycarbonate, polystyrene, polysulfone and polypropylene dielectrics. Values from 0.001-25 µF, voltages to 900 V and higher, with tolerances as tight as ±0.5%. And they're available off-the-shelf from our distributors or in 4 to 5 weeks ARO for production quantities.

Ask for details and your free sample today. You can't lose.

In film caps, it's no contest.

ELPAC COMPONENTS

CIRCLE NUMBER 62

CIRCLE NUMBER 347

CIRCLE NUMBER 348

CIRCLE NUMBER 349

CIRCLE NUMBER 63

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(A) PLµS Compiler for 16- & 32-bit computers and on Time-share.
(B) 16- & 32-bit Assemblers and Simulators.

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CIRCLE NUMBER 63

CIRCLE NUMBER 62
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**12-bit D/A!**

**MDS-1240**
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**12-Bits, 40NS**

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**PACKAGING & MATERIALS**

**Solder cream comes in homogenized formula**

Assembly Systems, Inc., P.O. Box 9084, Dept. S, Providence, RI 02940. (401) 331-9154. $1.50/oz. (20 oz.-up).

A solder cream, called Tech Solder 6000, comes in a homogenized formula. It combines a fine-mesh powdered-solder metal with a noncorrosive flux and vehicle system. The formula flows at 374°F for use in all standard soldering applications. It contains no cadmium or fluorides. Tech Solder 6000 can be used with either automatic dispensing equipment or a manual syringe.

**CIRCLE NO. 350**

**Plastic boxes come with divider slots**

W. D. Adam Co., Inc., 630 W. 27th St., Costa Mesa, CA 92627. (714) 646-4488.

These units, called Modular Tote Boxes are available in 42 sizes. Plastic dividers allow each box to have compartment widths of multiples of 1.125 in. They have dust proof snap-on lids and identification ticket holders. A special circuit board holder is also available.

**CIRCLE NO. 351**

**Filler**

Thanks to advances in medical electronics, researchers have discovered that insanity is inherited. You get it from your children.

**Dummy DIPs stand in for the real ones**

Micro Electronic Systems, 8 Kevin Dr., Danbury, CT 06810. (203) 746-2525. 14-pin: $3.00; 16-pin: $3.65 (small qty); stock.

Skip-A-Dip is inserted into the holes of a PC board when a DIP is missing due to parts shortages or missing components. Skip-A-Dip keeps the holes free of solder for insertion of the DIP at a later time. The PC board is then wave soldered. The unit is simply removed at the end of the wave solder machine and reused over and over again. It comes in two sizes, 14 and 16 pin. Teflon coated units also are available for water-soluble fluxes.

**CIRCLE NO. 352**

**Three breadboards come in Eurocard size**

 vero Electronics Inc., 171 Bridge Rd., Hauppauge, NY 11787. (516) 234-0400. $50 each; stock.

Three different boards—a CPU, a memory and an interface board—are suitable for the evaluation and production of microprocessor-based systems conform to the single-width Eurocard size. The 100 x 160-mm cards can be put together into a full system using the manufacturer’s card-frame system and case-frame parts. The boards are produced on a high-grade, fiber-glass laminate and are totally wire-wrappable. They are preassembled with mini-wrap DIP sockets of the correct size and number for the specific function of the particular board, together with additional test point and component mounting pins. They are also fully decoupled by means of solid tantalum capacitors (0.1 μF, 35 V) and fitted with a 64-pin connector with mini-wrap terminations. The CPU board is fitted with a range of sockets to accommodate the microprocessor chip and the minimum memory, clock and interfacing chips. Space is also available for the addition of discrete components and potentiometers. The memory board has eight 28-pin sockets fitted to accommodate 8-k words of additional memory. The interface board contains, in addition to the IC sockets, space for adding discrete components and a crystal.

**CIRCLE NO. 353**

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Electronic Design 20, September 27, 1976
Solder alloy melts at 293 F

Polyethylene bags prevent static buildup

Cable clips adhere to any smooth surface

Solder alloy melts at 293 F

Polyethylene bags prevent static buildup

Cable clips adhere to any smooth surface

A solder alloy has a much lower melting point than standard alloys. The melting point of this alloy is 294 F, compared to standard 60/40 solder, which melts at 380 F. The alloy, called TLC, is a composition of tin, lead and cadmium and is completely non-toxic in use. The alloy is furnished as a wire core solder with 5-cores of rosin flux, or in solid wire form.

Richmond, Div. of Pak-Well, Box 1129, Redlands, CA 92373. (714) 794-2111. 5.4¢ (1000-up).

Electrostatic damage to CMOS and other sensitive circuits can be prevented by using transparent pink bags made of antistatic polyethylene film. Containing no free-carbon particles, the 6 mil thick RC AS-1200 film is qualified for military use. The bags allow static-safe assembly and handling of static-sensitive circuitry, without the need for conductive floors, seat covers, or air ionizers.

Richco Plastic Co., 5825 N. Tripp Ave., Chicago, IL 60646. (312) 539-4061. SK-3: 9.5¢; SK-6: 12.9¢ (100-999).

Two cable clips, called Sticky-Klips, require no installation tools to mount on a smooth surface. They have a polyethylene adhesive backing and are made of aluminum. The cable is inserted and the clip snaps shut over the wire. Sticky-Klips are available in two models: SK-3 holds cable with diameters up to 5/32 in., while SK-6 accommodates cable sizes to 3/8 in.

CIRCLE NO. 354
MulticoreSolders, Inc., South Service Rd., Westbury, N.Y. 11590. (516) 334-7450. $5-7/lb.

CIRCLE NO. 355
Cable clips adhere to any smooth surface

CIRCLE NO. 356
Richco Plastic Co., 5825 N. Tripp Ave., Chicago, IL 60646. (312) 539-4061. SK-3: 9.5¢; SK-6: 12.9¢ (100-999).

Two cable clips, called Sticky-Klips, require no installation tools to mount on a smooth surface. They have a polyethylene adhesive backing and are made of aluminum. The cable is inserted and the clip snaps shut over the wire. Sticky-Klips are available in two models: SK-3 holds cable with diameters up to 5/32 in., while SK-6 accommodates cable sizes to 3/8 in.

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CIRCLE NO. 356
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Two cable clips, called Sticky-Klips, require no installation tools to mount on a smooth surface. They have a polyethylene adhesive backing and are made of aluminum. The cable is inserted and the clip snaps shut over the wire. Sticky-Klips are available in two models: SK-3 holds cable with diameters up to 5/32 in., while SK-6 accommodates cable sizes to 3/8 in.

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Two cable clips, called Sticky-Klips, require no installation tools to mount on a smooth surface. They have a polyethylene adhesive backing and are made of aluminum. The cable is inserted and the clip snaps shut over the wire. Sticky-Klips are available in two models: SK-3 holds cable with diameters up to 5/32 in., while SK-6 accommodates cable sizes to 3/8 in.

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Cable clips adhere to any smooth surface

CIRCLE NO. 356
Richco Plastic Co., 5825 N. Tripp Ave., Chicago, IL 60646. (312) 539-4061. SK-3: 9.5¢; SK-6: 12.9¢ (100-999).

Two cable clips, called Sticky-Klips, require no installation tools to mount on a smooth surface. They have a polyethylene adhesive backing and are made of aluminum. The cable is inserted and the clip snaps shut over the wire. Sticky-Klips are available in two models: SK-3 holds cable with diameters up to 5/32 in., while SK-6 accommodates cable sizes to 3/8 in.

CIRCLE NO. 354
Multicore Solders, Inc., South Service Rd., Westbury, N.Y. 11590. (516) 334-7450. $5-7/lb.

CIRCLE NO. 355
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PACKAGING & MATERIALS

Flat cables come with molded-on connectors

AP Products, Box 110-P, Painesville, OH 44077. (216) 354-2101. $4.01, 50 wires, 1-ft long, socket each end (500 up).

A line of flat ribbon cables with connectors, called Great Jumpers, comes assembled and pre-tested. They are available in cables having 20, 26, 34, 40 and 50 conductors. They come with the three connector types; card edge, PC board, and socket. The connectors are molded directly onto the vinyl ribbon cable with integral molded strain reliefs. The cable has either solid or stranded #28 AWG conductors. Great Jumpers are front and rear coded to identify both the wire number (in repeating decimal sequence) and the wire group (in groups of 10).

Busses for socket pins act like 18-AWG wire

Rogers Corp., Electro Components Div., Rogers, CT 06263. (203) 774-9605. $1.31/ft (100 ft up).

To connect selected pins on PC boards, Strip/Bus has a current carrying capacity in excess of 18 AWG copper wire. The strips work with staked-in wire-wrappable pins or with DIP sockets having wire-wrappable tails. They can be used with solder preforms. A low profile keeps Strip/Bus from interfering with subsequent wire-wrapping or with the lay of wires. Models are available for 0.025 and 0.045 in. square pins, and for 0.031 x 0.062 in. rectangular pins, with center-to-center spacings of 0.100, 0.187, 0.200 and 0.250 in.

Flux-cored wire solder comes as fine as 34 AWG

Multicore Solder, Inc., S. Service Rd., Westbury, NY 11590. (516) 334-7450. $2.50-$6.50 (1/2-lb spools); stock.

Flux-cored solder comes in standard gauges as fine as 34 (0.009 in. dia.). It also comes in No. 22 (0.028 in. dia.), 24 (0.022), 28 (0.014) and 32 (0.010 in.) gauges; either in 60/40 or 63/37 tin/lead alloys. The cores are noncorrosive, nonconductive RA and RMA rosin flux. Multicore fine-gauge solders are on the QPL list and meet Federal Specification QQ-S-571e. They come in 1/2-lb spools.

Desoldering tools don't clog up

Hunter Associates, 729 Partridge Dr., Bridgewater, N.J. 08807. (201) 526-8440. $29.95 (unit qty).

Two desoldering tools, models ESS or GSS, use a suction principle that prevents tip clogging. A source of continuous air pressure is applied through a tube and creates pressure in the tool through a venturi principle. The tools require only infrequent emptying of a stainless-steel solder catcher. The Model ESS is fitted with a 4-mm dia tip for standard radio and television applications. The Model GSS is fitted with a 2.4 mm dia. tip.
Coil winding machine sells for $269

Innes Instruments, Box 3216, Pasadena, CA 91107. (213) 796-3288. See text.

The Coil Winder costs $269 and comes with a built-in dereeler, SCR motor drive, mechanical counter, and a detachable universal mandrel. The mandrel will hold bobbins with inside diameters of from 3/16 to 1 in. and lengths up to 3 in. Special mandrels and chucks are also available. In use, semi-skilled personnel make setups and feed wire by hand. The machine is built on a cast aluminum frame and weighs 8 lb.

CIRCLE NO. 361

System does interactive PC board design

Redac Interactive Graphics, Inc., 225 Great Rd., Littleton, MA 01460. (617) 486-8751. $90,000; 90 days.

A computer system that helps you design PC boards is claimed to cost less than most others. Called the Mini-PCB-Designer, the system has interactive capabilities. The Mini system uses the DEC PDP-11/34 computer system with a 17-in. refresh-graphics terminal. It has automatic component placement, auto-routing, design rules-checking and multilayer wiring ability.

CIRCLE NO. 362

Screw-terminal strips can be cut to length

Electrovert Inc., 86 Hartford Ave., Mt. Vernon, NY 10553. (914) 664-6090. 6.8¢ (100-up).

A series of terminal strips, called the EDS series, are flexible and can be easily cut to size. Twelve poles come on one strip. The insulating body is molded of nylon, and can be shaped to the mounting surface. The strips can be cut with a knife or saw blade. The EDS series is made in three sizes for use with 16, 12 and 8 AWG wire. The screw connectors are made of nickel plated brass. All metal parts are either deeply recessed or completely enclosed.

CIRCLE NO. 363

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CIRCLE NUMBER 69

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THINK

CIRCLE NUMBER 69

123
Conductive adhesives don't settle on curing


A series of three copper-filled adhesives is claimed to be nonsettling and electrically conductive. The adhesives are Conduct-X 5031, 5032 and 5033. Number 5031 is a general-purpose, heat curable type; 5032 is suited for screen printing and 5033 is a two-part room-temperature curing type. All of the materials exhibit volume resistivities of 0.001 Ω-cm or less and may be applied by syringe dispensing, screen-printing or drawdown. They may be diluted for brush or spray application with common solvents. An evaluation kit containing 0.5 lb of each of the three types is available for $25.

CIRCLE NO. 364

DANA INTRODUCES THE SMART COUNTER.

Series 9000: World's First Microprocessing Timer/Counter.

The Dana Series 9000 is smart enough to make your work a lot easier. Microprocessing controls provide all the features of a premium timer/counter, a reciprocating counter and a calculator. Plus interfacing options and operating capabilities never before available in one instrument.

The Dana Series 9000 Microprocessing Timer/Counter goes so far beyond all other counters it takes a whole brochure just to explain its capabilities. Ask for it. It's the smart thing to do.

Dana Laboratories, Inc., 2401 Campus Drive, Irvine, California 92664, 714/833-1234.

Push mounts hold cable ties to a flat panel

Panduit Corp., 17301 Ridgeland Ave., Tinley Pk., IL 60477. (312) 532-1800. PM2H25-M, 3.4¢; PBMS-H25-M, 3.8¢; (1000-up).

Two types of push mounts hold cable ties, which secure wire bundles to panels, cabinets or equipment frames. One push mount, the PBMS-H25, is used wherever access to both sides of the mounting surface is available. The mount is pushed through the mounting hole from the side opposite the wire run, and an appropriate cable tie is inserted to secure the bundle. The PBMS-H25 comes in either natural-nylon or telephone-gray colors. The other push mount, PM2H25, is used where access is available only on the side of the mounting surface to which the wires are being attached. The cable ties can be inserted through the mount and fastened around the wire bundle either before or after the mount is pushed through the panel hole.

CIRCLE NO. 365

Hot-air tool solders and shrinks tubing


A dual-purpose tool solders connections and shrinks plastic sleeves. The Thermopencil, as it is called, features a plug-in power pack that provides 24 V to the tool and to the low-pressure air supply. An alternative power pack, omitting the air pump, is available for customers who already have a suitable air-supply system. Air flow is directed on the connection or sleeve by a slim pencil-type nozzle. A 6-ft cable and air tube is supplied as standard. The MK 1 power/air pack measures 14.5 × 8.75 × 10 in. and is bench mounted. It incorporates an integral air-supply pump with an air flow controller that can be set to supply air at a pressure from 2 to 8 psi. A fail-safe power cutoff is included.

CIRCLE NO. 366
Modules & Subassemblies

Delay-on-operate timer now MIL qualified
Hi-G Co., 550 Spring St., Windsor Locks, CT 06096. (203) 823-4811. 1-to-9 prices: $21 (6100); $45 (6150); $50 (6001); stock.
Qualified to MIL-R-83726/13, the Model 6001 thick-film timing modules provide a delay-on-operate function. The modules weigh less than 12 grams, but provide delays of 50 ms to 60 s. There are 30 preset qualified models from which to choose. They are hermetically sealed, operate from -55 to +125 °C and are housed in 14-pin metal DIPs. Model 6150 is the commercial version of Model 6001 and can be ordered for any delay period from 50 ms to 60 s. An industrial version, the 6100, is a less expensive but similar device, housed in a plastic, epoxy filled enclosure. It is temperature rated for -55 to +85 °C.

Fast s/h amp acquires signals in under 350 ns
Datel Systems, 1020 Turnpike St., Canton, MA 02021. (617) 828-8000. $189 (1 to 9); 4 wks.
The SHM-5 modular sample-and-hold amplifier can acquire a signal in only 200 ns to 0.1% or 350 ns to 0.01%. When used with a 12-bit, 2 µs a/d converter, sampling and conversion at up to a 400-kHz rate is possible. The s/h amp has a 5-MHz tracking bandwidth, a 25-V/µs slew rate and an input impedance of 106 Ω. Hold-mode droop is 20 µV/µs, maximum, and hold mode feedthrough is 0.005% of input signal, max. The SHM-5 operates in the inverting mode with a gain of -1 and has a 15 ppm/°C temperature coefficient of gain. Its output offset voltage drift is ±30 µV/°C and the sample to hold offset step is ±5 mV. A 2 x 2 x 0.375-in. epoxy package holds the SHM-5, which has ±15 V dc at 75-mA power requirements. The operating range spans 0 to 70 °C.

LVDT signal conditioner delivers 4 to 20 mA
Schaevitz Engineering, US Rte. 120 and Union Ave., Pennsauken, NJ 08110. (609) 662-8000. $281.10 (unit qty.); stock.
The CTM-401, a fully encapsulated two-wire LVDT signal conditioning module, delivers a 4 to 20 mA dc signal. The signal is directly proportional to a change in LVDT core position. The CTM module does not require any additional external power since it operates from the dc current of existing process controller, recorders, or readout devices. It delivers a nominal 1 V rms excitation to an LVDT. The CTM has an intrinsically-safe design because the current can be limited to 50 mA even with accidental over-voltage of internal short circuiting. Performance features include a frequency response of dc to 100 Hz (within ±1 dB), nonlinearity and hysteresis of less than 0.1% full scale and stability (after 15 minutes) of 0.25% full scale.
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CIRCLE NUMBER 74

Electronic Design 20, September 27, 1976
**A/d converter delivers 16 bits in only 8 µs**

Intech/FMI, 282 Brookaw Rd., Santa Clara, CA 95050. (408) 344-0500. $1300 (unit qty.); stock.

The A-856 16-bit a/d converter can deliver a data word every 8 µs. The unit has a gain tempco of 7 ppm/°C max. and a nonlinearity tempco of ±2 ppm/°C. The built-in sample-and-hold amplifier that's mounted on the converter's 4.5 × 5.5 × 1.75 in. circuit board increases the conversion time by only 2 µs when switched into the hold modes. Input impedance of the s/h amp is 109 Ω. The over-all converter requires ±15 V at 150 mA and +5 V at 300 mA and operates over 0 to 50 C.

**Pressure converter made for critical locations**

Amtek, 860 Pennsylvania Blvd., Feasterville, PA 19047. (215) 355-6900. From $190; 6 to 8 wks.

The Model 58 pressure-to-electric converter has its own power supply and can operate from a 115 V, 60 Hz line. It is available in a four-wire version with a Factory Mutual approved explosion-proof for Class II, Div. 1, Groups E, F and G. The converter comes in a cast-aluminum housing that also meets requirements of NEMA Type 4 Watertight specifications. The two-wire version, Model 56, is certified by Factory Mutual as Intrinsically Safe for Class I, Division 1, Groups B, C and D when used with approved barriers. The Model 56 operates from 16 to 80 V dc lines and is available with either 4 to 20 or 10 to 50 mA dc outputs. The Model 56 has a nickelplated steel housing suitable for control room type environments. The Models 56 and 58 both have 0.25% FS accuracy.

**Current output d/a's settle in under 85 ns**

Teledyne Philbrick, Allied Dr. at Rte. 128, Dedham, MA 02028. (617) 329-1600. From $119 (unit qty.); stock.

The Models 4060 (8-bit) and 4061 (10-bit) high-speed d/a converters are monotonic from 0 to +70 C. They have both unipolar and bipolar outputs of 0 to +10 mA and ±5 mA. Both models have a maximum settling time to within ±1/2 LSB of 85 ns, with 40 ns typical for the 4060 and 60 ns typical for the 4061. The converters only need ±15-V supplies but are directly TTL compatible.
The single-chip 2650 is easiest-to-buy, too. Now only $21.50 (100-up).

Full support of customer and product is the key to ease of development with the 2650. Applications engineers in the U.S. and abroad are at your beck and call at every stage. Software for almost anyone’s requirements and machines. Development hardware is versatile and inexpensive. All circuits are multi-sourced.

Flow Chart: How to travel safely and quickly from spec sheet to your µC.

1. Applications Engineers — in the field now, more coming. Specific assistance to you is available around the USA, and in Belgium, Holland, Germany, France, Sweden, Britain, Italy, etc.

2. Multi-sourced 2650 — available in any quantity from Signetics, at the unprecedented low price of $21.50. Also available from AMS and Philips, and from Signetics’ authorized distributors.

3. Development Software — includes the PL µS, an extremely efficient High Level Language (compiler) that reduces programming effort and cuts development time. ANSI standard Fortran IV executes on most machines without alteration. 2650AS1000/1100 Assembler and 2650SM1000/1100 Simulator are available in both 32- and 16-bit, on GE and NCSS time-sharing.

4. Multi-sourced Support Circuits — You’ll need MOS and/or Bipolar Memories, Interface and Logic. Signetics has everything for a complete system. Back up any item from other sources. Coming soon from Signetics are: Programmable Peripheral Interface and Communications Interface, A-D Converters, Synchronous Data Link Controller, 16k NMOS & Bipolar ROMs, 4k & 8k NMOS EROMs, and 8k Bipolar PROMs.
Development Hardware — Design/develop prototype with a variety of cost/capability levels of hardware support. Including prototyping cards and kits, smart typewriter demo card, 4k-byte RAM card, and more. Applications help if you need it.

TWIN With Floppy Disks — "crashproofs" your system checkout. With DOS, Resident Assembler, and Text Editor. You develop programs and circuits together in an actual system environment with TWICE (TestWare In Circuit Emulator). PROM programming, too.

Over 30% Faster 2650 — By the time you've proven out your µC, you'll have available a faster 2650 if you want it. Uses the same software. For still higher speeds, call Signetics Bipolar Microprocessor Marketing about our 2650 emulator using 3000 series µP.

You go from gleam-in-your-eye to proven prototype in less time for less cost, and the µC you develop is easier and cheaper to produce in quantity, when you start with the 2650. Start now by mailing the coupon.

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CIRCLE NUMBER 77
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730 SERIES A new 0.600" LED character in super bright red, seven-segmented readout... low power... draws 10mA/segment or less... operates with standard IC power supply levels. Very high contrast ratio... visible from 40'. Available with or without on-board decoder/driver, plus or minus bar, and with bezel mounting. In 1000-lot quantities each LED 730-6007 .... $6.05. 730-6001 .... $2.55.

745 SERIES A new 0.300" LED character in a very bright red, seven-segmented readout... low power requirements. Standard 14-pin DIP... available with left and right decimal with ± 1, and with and without on-board decoder/driver. Compatible with most TTL and DTL circuits. In 1000-lot quantities each LED 745-0014 .... $2.10.

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Opportunities involving sequential, high-speed and I/O interface logic and microprocessor applications in digital, signal processing, communication and aerospace systems. Familiarity with MSI/LSI desirable. Requires several years experience in progressively more challenging logic design. BS/MSEE.

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Needs extensive background in core memory organization, circuits and magnetics, and familiarity with logic design. Experience in the design of precise high current, high frequency digital circuits essential. BS/MSEE.

COMPUTER ENGINEER

Requires BS/MSEE and 10 years diversified experience in design & application of digital computers to airborne applications; customer liaison experience; ability to formulate responses to customer requirements as well as satisfactory execution of contractor requirements in a computer development program.

SIGNAL PROCESSING ENGINEERS

Involves analysis and design of Signal Processing-Digital Communications Equipment for avionics plus TEMA and IGNI applications. Requires BSEE degree, Master's preferred, plus 2-5 years experience in communications theory, digital filters, coding theory, signal processing techniques, A/D analysis, error correction, phase locked loops, and related digital and RF hardware design.

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Requires BS/MSEE and 2-5 years experience with the development of FORTRAN programs to simulate electronic systems for signal processing of RF, Baseband, noise, etc.

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- COMPUTER SYSTEMS DESIGN
- AIRBORNE ELECTRONIC PACKAGING
- NAVIGATION SYSTEMS DESIGN & ANALYSIS

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CIRCLE NUMBER 78

CIRCLE NUMBER 250
Speech compressor has 56 dB dynamic range

Lexicon, Inc., 60 Turner Street, Waltham, MA 02154. (617) 891-6790. $100 (lge. qty.); stock.

The Varispeech Model 20 is a real-time pitch shifter and speech compressor/expander. All circuitry, including a 4-K RAM, 8-bit d/a converter and pitch computer chip are mounted on a 3.5 x 5 in. PC card. All units shift pitch in real time from two times higher than normal to 0.4 times lower than normal. The device corrects the pitch of rate-altered speech, thus permitting the listener to listen at his own rate of comprehension between one-half and two and one-half times original speed. The Model 20's have a dynamic range of greater than 56 dB, a distortion and noise (total) of 0.6%, and a frequency response of 100 to 5000 Hz (+0/-3 dB). The circuit requires +12 V at 150 mA and -12 V at 50 mA.

CIRCLE NO. 379

Multiplying DACs accept 15-bit digital inputs


The DAC-M is a high-performance multiplying d/a converter. It handles 15 bits and works in all four quadrants. The converter is housed in an encapsulated module, 2.625 x 3.125 x 0.42 in. and weighs only 5 oz. Accuracy grades between ±0.024% and ±0.0031% are available. Power and analog signal grounds are isolated to minimize the effects of intersystem ground noise and common-mode interference. The DAC-M has a short-circuit-protected output of ±10 V at 10 mA and dissipates less than 2 W. Its output slew rate is 5 V/µs, minimum, and it has a CMRR of 70 dB. Digital setting time is 5 µs, maximum.

CIRCLE NO. 380

If you've got a complicated problem with EMI, we've got a simple solution

Electromagnetic Interference. It shows up as static on radio and snow on TV. It can make computer terminals register input error. Make a pacemaker or an EKG malfunction. And interfere with sensitive navigation equipment.

Obviously, you've got to shield your equipment against EMI. You can use sheet metal. Or foil. Or a plating process. These are fine for small enclosures with flat surfaces. But when it comes to large cases and complex shapes, you need a better solution.

And here it is. Electrodag® coatings. We've engineered a whole range of them. To give you from 10-70 dB attenuation, from 1 MHz to 10 GHz. With varied physical properties that let you apply them to almost any material.

This means that you can build your enclosures out of light plastic, coat them with Electrodag, and still get perfect skintight shielding. Even on honeycomb structures and flexible parts made from foamed resins.

And you can forget about expensive techniques like plating, metallizing and vacuum deposition. With Electrodag, all you need is a spray gun, a simple dipping technique, or a paintbrush.

You can use these new coatings for everything from CB radios and EKG units to data terminals and microphones.

This is a new field, but we're the oldest company in it. With the greatest experience, the biggest R&D staff and the most EMI coatings. For technical advice on specific applications, write: Acheson Colloids Company, Electrical Products, Port Huron, Michigan 48060. Or call (313) 984-5581

Acheson
high technology coatings

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CIRCLE NUMBER 79
INTEGRATED CIRCUITS

Dual, low noise preamp has s/n ratio of 76 dB

Esar Integrated Systems, 750 Palomar Ave., Sunnyvale, CA 94086. (408) 733-7700.

The XR-4739 is a pin-for-pin replacement for Raytheon's 4739 dual low-noise op amp. It is available in a molded-plastic 14-pin DIP, and operates over a 0 to +75 C range. The dual amp has a signal-to-noise ratio of 76 dB (RIAA, 10 mV ref.), a channel separation of 125 dB, a unity-gain bandwidth of 3 MHz, output short-circuit protection, and only 0.1% distortion at an 8.5-Vrms output into a 2-kΩ load.

CIRCLE NO. 381

BCD to phone pulse converter stores number

Motorola Semiconductor, 3501 Ed Bluestein Blvd., Austin, TX 78721. (512) 928-2600. From $6.98 (100-up); stock.

The MC14408 CMOS circuit accepts BCD or binary inputs from control logic, memory, or the MC14419 keypad-to-binary converter and delivers a string of dial phone pulses. An internal memory holds a 16-digit number that will remain stored until replaced by another entry. A re-dial input eliminates the need to re-enter a number if a call cannot be completed. Four other control inputs: Hold, Call Request, Interdigit Time, and Make-Break Ratio add to the flexibility of this part. On-chip circuitry combined with an external capacitor and inductor provide the clock frequency. The phone system normally uses a 16-kHz clock frequency but the part will operate over a frequency range of 4 to 80 kHz. A variation of the MC14408 is the MC14409—identical in function with the exception of the signal output at the dial rotating output. In the MC14408, DRO remains high during continuous outpulsing of all digits and in the MC14409, DRO is low between each digit pulse burst. Both circuits operate over a range of 3 to 6 V and are available in either ceramic or plastic 16-pin DIPs.

CIRCLE NO. 382

CMOS clock circuit operates from 1.5 V

Intersil, 10900 N. Tantau Ave., Cupertino, CA 95014. $3.15 (100-up); stock.

The ICM7038B CMOS clock circuit operates from a 1.5-V battery. The circuit performs the function of oscillator, frequency divider and output driver for miniature synchronous motors. Inside the circuit are an oscillator and 16 binary dividers. The ICM7038D version has the final output from a 17th binary divider. The ICM7038E and ICM7038G have 18 and 19-stage binary divider options. The total output driver impedance is typically 350 Ω. An alarm output also has a low resistance, making it suitable for driving a transducer buffer. The circuit, housed in an 8-pin DIP, typically consumes 105 μW at 1.5 V and operates over a -20 to +70 C range. Current drive is 1 mA, minimum.

CIRCLE NO. 383

8-channel multiplexers have overload protection

Hybrid Systems, Crosby Dr., Bedford, MA 01730. (617) 275-1570. From $19 (1 to 9); stock to 4 wks.

The MUX 202-M and MUX 203 multiplexers are eight-channel, single-ended units. They are housed in 16-pin hermetic DIPs and have overvoltage protection on both the analog and digital inputs. The multiplexers are also protected against channel interaction when the power is removed. The MUX 202-M is fully processed to MIL-STD-883. Key specifications of both units are: accuracy to 0.01%, cross talk of 0.01% at 10 kHz and an address time of 0.5 μs. The units are TTL/CMOS compatible and will operate from ±15-V supplies.

CIRCLE NO. 384

CB synthesizer IC provides all 40 channels

Nitron, 10420 Bubb Rd., Cupertino, CA 95014. (408) 255-7550. $2.50 (10,000-up); stock.

A low-cost 40-channel frequency synthesizer can be built based on the NC6402 digital phase-locked-loop circuit. The circuit synthesizes all 40 CB channels while positively locking out all other frequencies. A logic-level input selects the transmit or receive mode of operation and seven-segment-coded switch closures to ground select the channel and simultaneously operate a two-digit display. In addition to the 16-pin DIP NC6402, all that is required to complete a minimum cost synthesizer is a crystal reference oscillator, a VCO, a one-wafer rotary switch, a mixer, a dual-D flip-flop and an optional two-digit display.

CIRCLE NO. 385

Design your own logic with 158 gate array

TRW, One Space Park, Redondo Beach, CA 90278. (213) 536-1500.

Configurable gate arrays offer logic designers many custom LSI options without the expense and time required for a complete custom circuit design. A logic designer can configure a wide variety of circuit elements using the 158 gates (3-input TTL NAND gates) available on a single array. Turnaround time from a completed logic interconnection program to fully tested arrays is typically six weeks. Standard and driver 3-input, TTL NAND gates with open collectors or active pull up can be configured on the array, along with 3-input gate expanders. The designer can choose from 5 to 25 kΩ pull-up resistors and isolation diodes. Logic designers can also select a three-diode excursion clamp. There are 38 pads available for signal I/O and two are required for the +5 V supply and ground. Typically, the arrays require about 100 mW and have a propagation-time delay of 40 ns per gate, average. Due to the custom nature of the circuit, costs depend on interconnect complexity and quantity, so contact the company for a quote.

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CIRCLE NUMBER 81
Electronic Design 20, September 27, 1976
Programmable dividers toggle at up to 500 MHz

Plessey Semiconductors, 1674 McGaw Ave., Irvine, CA 92714. (714) 540-9945. From $11.50; stock.

Five uhf programmable dividers provide toggle frequencies as high as 500 MHz. The dividers can be logically programmed to divide by 5 or 6 (for the SP8740 and 8745), 6 or 7 (for the SP8741 and 8746), or 8 or 9 (for the SP8743). They are available with ac-coupled inputs or, for broadband applications, with dc-coupled inputs. All dividers have ECL-compatible inputs and outputs. Operating temperature ranges are: suffix A, -55 to +125 °C; suffix B, 0 to +70 °C; and suffix M, -40 to +85 °C. Devices in the series include the SP8740, 8741, 8745 and 8746 A, B and M and the SP8743 B and M. All but the SP8743 have 300 MHz toggle rates. The SP8743 has a 500 MHz toggle rate.

Peripheral drivers deliver up to 1.2 A

Sprague Electric, 115 Northeast Cutoff, Worcester, MA 01606. (413) 664-4411. 100-up prices: $1.75 (3600), $1.87 (5700); stock.

Twelve monolithic peripheral power drivers have been added to the company's line of digital interface products. The new devices, Series UDN-3600 and UDN-5700, are packaged in 8 and 16-pin plastic DIPs. They are rated for continuous operation over 0 to 85 °C. The UDN-3600 units are dual two-input drivers, designed for loads such as incandescent lamps, LEDs, memories, heaters and other noninductive loads of up to 600 mA at 80 V. The UDN-5700 dual and quad drivers have transient protected outputs and are designed for use with inductive loads such as relays, solenoids or stepping motors at up to 1.2 A (four drivers) or 600 mA (one driver) at 80 V.

Pin replacement for 6820 offers benefits

Mostek, 1215 W. Crosby Rd., Carrolton, TX 75006. (214) 242-0444. From $5.50 (100-up); stock.

The MK 6820 peripheral interface adapter is an improved performance, pin-for-pin replacement for Motorola and AMI 6820. The circuit can also function as a generalized input/output for any microprocessor bus. Advantages of the MK 6820 include: availability in two, low-power versions, a 300 and a 400 mW max model; operation at a 2 or 1 MHz max rate rather than 1 MHz only; fully TTL compatible inputs including Enable; and it can handle two TTL loads on each output instead of one. In addition, the MK 6820 is completely static and thus there are no dynamic limitations on the Enable input. Operation is specified for the 0-to-70-C range.
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Electronic Design 20, September 27, 1976 135
CRT terminal features programmable baud rate

Omron Corp. of America, Information Products Div., 432 Toyama Dr., Sunnyvale, CA 94086. (408) 754-8400. $2750; 60 days.

A programmed CRT terminal, the 8030, allows user programming of communications functions from its keyboard. The operator can set up transmission baud rate, parity, bits per word and stop/start bits. The end-of-block terminating character is also user programmable. The terminal contains a two-page refresh memory with a total of 3840 characters, permitting the operator to edit the data before transmitting it to the host computer. The 8030 terminal has a 15-in., diagonally measured, 1920-character display.

CIRCLE NO. 393

150-line/min printer available for $900


The model 2610 prints 150 lines/min with a 64-character set, or 84 line/min with a 128-character set, both in an 80-column format. The $900 price of the 2610 includes ASCII control logic and column buffering in addition to electronic and mechanical chassis. A belt-impact printing method is employed. The standard, 256-character belt contains four sets of 64 characters. An optional belt provides the same character count in two sets of 128 characters. Paper widths of up to 10-in. with up to three carbons may be accommodated. The 2610 line printer measures 6.2 x 17 x 15.5 in. and weighs 33 lb.

CIRCLE NO. 394

PC-board video digitizer sends data to a computer

Echolab, Inc., 213 Middlex Turnpike, Burlington, MA 01803. (617) 273-1512. $975 (PC board).

A video digitizer converts 60-k picture elements/s, allowing connection to the programmed I/O ports of most computers. The digitizing technique uses a semi-random access method. The computer specifies an x-axis address via a 9-bit binary number. The video picture is digitized beginning at this address, and continues for four picture elements. The digitizer converts the analog voltage of each picture element into 4-bit words. Four 4-bit words are then packed into a 16-bit word and transmitted to the host computer's parallel I/O port. This process repeats for each video line. The analog video signal is quantized at a 12-MHz rate. The digital word is converted to an analog voltage so that a TV monitor can be used to view the reconstructed picture. The PC board measures 7.5 x 8 in.

CIRCLE NO. 395

Tape drive is compact, uses 3M cartridge

Instrumentation Technology Corp., 18333 Eddy St., Northridge, CA 91325. (213) 886-2034. $470 (100 up); 30 days.

The Micro-Drive tape transport, model 101, takes the 3M DC100A data cartridge. The unit's dimensions are 4-1/2 x 4 x 3 in. Read/write tape speed is 25 in./s, and the rewind/search speed is 75 in./s. Recording density is 1600 bit/in. The unit requires only one supply voltage of 15 V dc at 700 mA for running current and standby current is 15 mA. The cartridge can store up to 1.3 Mbit and the Micro-Drive can transfer data at the rate of 20-k bit/s.

CIRCLE NO. 396

Graphic plotter talks via RS232

Tektronix, Information Display Group, P.O. Box 500, Beaverton, OR 97077. (503) 644-0161. $3995.

An interactive digital plotter, called the model 4662, can communicate with alphanumeric terminals through a modem using RS232C compatible lines. Additionally, the plotter can couple with other systems over its built-in General Purpose Interface Bus. Up to a 10 x 15 in. image size can be produced. The 4662 has a hardware character generator, digitizing capability, 22 in./s pen speed, 0.005 in. accuracy and ±0.0025 in. repeatability as standard features. It also has a 1600-byte input buffer. Data can be transferred at 110, 150, 300, 600 or 1200 baud. Digitizing is made easy through the use of the joystick control. By moving the pen to the desired position and pressing the call key, the X-Y data points can be sent out to the host. Character-size change is possible through program control, as is character rotation in 1-deg increments.

CIRCLE NO. 397

Cache memory speeds up DEC PDP-11/45

Mintronics Co., 2975 Furness St., St. Paul, MN 55109. (612) 770-5247. $9240; stock to 30 days.

The Model-45 cache memory plugs into the DEC PDP-11/45 and 11/50, speeding up program execution by 50 to 100%. The Model 45 consists of three PC boards and an optional power supply. The cards are installed in about 20 min by plugging them into DEC Fastbus slots. No hardware or software modifications to the host computer are required. An on-off switch for the cache memory eases benchmarking and troubleshooting.

CIRCLE NO. 398

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DATA PROCESSING

Two calculators store 224 steps on mag cards


Two programmable calculators can store 224 steps on magnetic cards; three times more than the company’s first magnetic-card calculator, the HP-65. The 11-oz HP-67 is the same size as the 65. Both calculators perform identical computing functions, and have identical program and data storage register capacity. Both models run on rechargeable batteries or line current. The 2.5 lb HP-97 additionally has a built-in thermal printer and a buffered keyboard. The models feature more programming power than the HP-65. Each has 26 data storage registers, 20 user-definable functions, three levels of subroutines, and label, indirect and relative addressing.

CIRCLE NO. 399

Terminal printers come in four models

Data General, Southboro, MA 01772. (617) 485-9100. $2650 (single qty).

The 6040 series of terminal printers comes in four models: a 30 and a 60 char/s printer are each available in keyboard or receive only versions. Keyboard models can also be used as typewriters. All models print full 132-column lines on paper widths of from 4 to 15 in. They interface with all Eclipse and Nova minicomputers. The printers can interface to 20-mA current loop and EIA RS232-C devices, using asynchronous controllers or multiplexers.

CIRCLE NO. 400

Acoustic phone coupler works at 450 baud

OmniTech Corp., 2405 S. 20th St., Phoenix, AZ 85034. (602) 258-8244. $300 (single qty).

The Model 401C acoustic coupler operates in both full and half duplex, switch selectable, at a data rate of 450 baud. It offers EIA (RS232) interface. The unit has a receive sensitivity of -50 dBm, and a transmit level of -10 dBm. The “sound-seal” cushions of the coupler have a non-linear response to various energy levels to provide maximum acoustic shielding. The 401 also is made of an impact resistant material in 27 different colors.

CIRCLE NO. 401

Paper-tape reader sends at 16 baud rates

Teleterminal Corp., 12 Cambridge St., Burlington, MA 01803. (617) 272-8504. $695; stock, 30 days.

The Fly Reader 232 reads paper tape at a rate of 300 char/s. The reader has a bank of programming switches located on the back panel. The switches allow the user to easily select any one of 16 different baud rates. The character length, parity, number of stop bits and the inhibiting or enabling of the RS232 control signals can also be switch-controlled. In addition to RS232, the Fly Reader transmits using current loop or serial TTL interface. It will read any standard one-in.-wide tape that has a transmissivity of less than 60%. The 232 allows remote start/stop of the reader either in a continuous reading mode or in a character at a time (step) reading mode. In addition, the current-loop (TTY) interface can be jumpered as either passive or 20-mA active.

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ORDERING INFORMATION

CIRCLE NO. 403

CIRCLE NO. 404

Varactor diodes cover 10:1 cap range

MSI Electronics Inc., 34-32 57th St., Woodside, NY 11377. (212) 672-6500. $5 (100 to 999); 2 wks.

The 10:1 capacitance tuning ratio provided in the MSI type MV1405 varactor diode assures at least 3:1 coverage in frequency. This tuning diode has a nominal capacitance at 2 V bias of 250 pF, which goes to less than 25 pF at 10-V bias. The breakdown rating of 12 V provides a sufficient safety margin for rf signals of up to 2 V pk-pk. The Q of 200, minimum, at 2-V’ bias measured at 1 MHz makes the diode particularly suitable at the lower rf frequencies. Furnished in a JEDEC DO-7 glass package, which is hermetically sealed, the diode meets or exceeds MIL-S-19500 environmental specifications.

CIRCLE NO. 405

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Microsemiconductor Corp., 2830 S. Fairview St., Santa Ana, CA 92704. (714) 979-8220. $5.45 (100 to 999); stock to 30 days.

A new line of high-speed, switching, 2 and 3-A silicon rectifiers combine miniature size, high surge capability, low thermal resistance and rugged mechanical design. The rectifiers feature a hermetic-seal hard-glass case, solderable silver leads and an opaque painted body that is insensitive to ambient light. Solvent-resistant cathode bands in contrasting color are provided and type number is printed. The rectifiers are designed and manufactured to meet or exceed the requirements of MIL-S-19500.

CIRCLE NO. 406
Microwave freq counter

Written to help the microwave engineer understand the capabilities and use of frequency counters, a 10-page ap note covers three common down-conversion techniques: prescale, heterodyne and transfer oscillator. Hewlett-Packard, Palo Alto, CA

CIRCLE NO. 407

Tape transports

A 55-page OEM Users Manual contains data for the design, preparation, and installation of an interface for Pertec's T5000, T6000, T7000, T8000A and T9000 digital magnetic tape transports. Pertec, Chatsworth, CA

CIRCLE NO. 408

Modal analysis processor

A six-page brochure on a modal analysis processor shows why and how modal analysis makes vibration easier to understand. Nicolet Instruments, Northvale, NJ

CIRCLE NO. 409

BiMOS op amp

The CA3140 op amp, which features a high-voltage PMOS input stage and a high-voltage bipolar output stage with a wide output range, is described in a 12-page application note. The brochure contains a business reply card that the reader can use to order a free sample of the CA3140 op amp. RCA Solid State Div., Somerville, NJ

CIRCLE NO. 410

Coil winders

"The Coil Winders' Idea Book" is a sketchpad of production and testing systems that can help boost productivity for manufacturers of coils, solenoids, relays, and so on. The sketches show how to apply readily available components for limited automation in production and testing operations. Nationwide Electronic Systems, Streamwood, IL

CIRCLE NO. 411
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CIRCLE NUMBER 95

Power amplifiers

Specifications and data for solid-state rf power amplifiers, wideband power multicouplers and transformers are provided in a 24-page catalog. Electronic Navigation Industries, Rochester, NY

Test accessories

A 25th-anniversary catalog of electronic test accessories includes charts, photos and a new-products section. The 76-page catalog also has a cross reference of UG number, and an alphanumerical index. ITT Pomona Electronics, Pomona, CA

Regenerative blowers

Performance and application data on regenerative blowers are given in a six-page brochure. Rotron, Woodstock, NY

Solid-state databooks

The SSD-200D two-volume, 1232-page set of solid-state databooks for RCA Solid State Div's complete line is now available. The volumes contain complete technical data on all standard types plus abstracts of all application notes relating to those devices. $6 each or both for $10. Box 3200, Somerville, NJ 08876

Screened-image displays

Screened-image displays that incorporate gas-discharge technology with design flexibility are described in a new bulletin from Beckman Instruments, Fullerton, CA

Fuller's earth

Uses for Fuller's earth and its high adsorptive capabilities in filtering, reclaiming and purifying industrial oils, are described in a 16-page brochure from Carborundum Co., Lebanon, IN

Power-supply catalog

A 34-page catalog on 28 families of line-operated power supplies and dc/dc converters is available. It includes application notes. Semiconductor Circuits, Haverhill, MA

Laser products

The latest news on laser products and applications from one company is available in a quarterly newspaper that also covers sophisticated optics and accessories. Coherent Radiation, Palo Alto, CA

Rf, microwave filters

Rf and microwave filters, components and subassemblies are described in a 40-page catalog. Teltronics Altair, Laguna Beach, CA

Plasma etching

An 8-page bulletin describes the use of low-temperature plasma to etch metals, semiconductor materials and dielectrics in the production of microelectronic devices. International Plasma Corp., Hayward, CA

Servo recorder

A four-page catalog features the Rustrak 400, 4-in. servo recorder line. Photos of each recorder style, electrical and mechanical specifications, complete list of accessories and plug-in range cards and ordering information are included. Gulton Industries, East Greenwich, RI
Beat Cost Problems With Continental’s Standard Connectors! 
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Electronic Design 20, September 27, 1976
There is no more accurate 12-bit A/D converter on the market... and it’s monolithic.

Differential and overall linearity within $\frac{1}{2}$ LSB. Inherently monotonic operation (and no missing codes). Immunity to noise transients. They all add up to unusually high accuracy for our 8702, a single chip, 12-bit CMOS A/D converter.

The 8702 has some other important advantages, too. CMOS technology means very low power dissipation — typically less than 20 mW. It is easy to use; no active auxiliary components are needed. And its latched parallel outputs are ideal for inputting to microprocessors.

Compared to modules, the 8702 offers immediate significant cost savings plus the prospect of even greater future economies due to its monolithic construction. And the savings in PCB real estate go without saying.

The 8702 comes in a 24-pin ceramic DIP. Other versions include 8 and 10 bit devices in ceramic, and an 8 bit unit in plastic for commercial environments. Call or write for full details.
What's new in solid state...

Gold CHIP LICs pile up 18 million hours with near-zero failure rate.

Test results from 18.2 million unit-hours and 1.5 million unit-cycles are in—and the verdict is unanimous. RCA Gold CHIP LICs are significantly more reliable than their counterparts with aluminum metalization. Here is a summarized report based on testing by three different kinds of users, plus—perhaps our severest critic—ourselves.

U.S. Army jungle/salt air tests
In Panama, the Electronics Technology and Devices Laboratory of the U.S. Army Electronics Command tested 63 Gold CHIP LICs to 1,479,000 unit-hours. The tests were done under conditions designed to reveal potential electromigrative shorts and metal corrosion: 27°C, 90-98% R.H., 4.5 V reverse bias. Result: zero failures. Or a failure rate of 0.062%/1000 hrs. at 60% confidence level.

OEM reliability tests
A major OEM systems manufacturer has completed extensive testing of Gold CHIP bipolar ICs. These were operated at high power and high junction temperature. After 15,000,000 unit-hours: 2 degradational rejects not related to metalization. That's a 0.02% failure rate.

U.S. Navy plastic IC program
The Naval Electronic Systems Command has awarded RCA Solid State Division a $1.44 million contract to apply Gold CHIP technology to plastic packaged ICs for military use. MIL-M-38510 specifications will be used.

RCA reliability tests
In a continuing program, RCA has run the following tests under industry accepted testing conditions.

- Operating Life: 332 units, 376,500 unit-hours.
- Temperature/Humidity Bias: 314 units, 1,244,000 unit-hours.
- Thermal Fatigue: 30 units, 750,000 unit-cycles.
- Pressure Cooker: 510 units, 92,460 unit-hours.
- Thermal Shock: 673 units, 214,760 unit-cycles.
- Temperature Cycle: 1,630 units, 510,000 unit-cycles.

Results: 1 failure in the pressure cooker test. It was caused by a bond wire break at the frame and was not chip related.


RCA. Full house in Linear ICs.