Coax termination difficulties? Now you can mass-connect flat, multiple-conductor cables. Gang operations strip and terminate up to 26 precision-spaced coax lines. Compact and inexpensive, the cables come in 50, 75, 93 or 95-ohm impedance styles. To terminate your transmission problems, see story on page 95.
Don't cheat yourself on trimmer performance.

Compare element size and see why Dale gives you better value!

Low profile doesn't have to mean low performance. The larger cermet element in Dale Low Profile Trimmers gives you extra value for your money. Extra assurance of trouble-free performance. You get:

**More Power** 1 watt at 70°C lets you derate for assured long-term stability. **Better Adjustability** — ±0.10% output resistance, ±0.05% output voltage ratio. **Low Noise** 1% Contact Resistance Variation standard. **Low T.C.** ±100 PPM standard.

Immediate delivery from stock...

Cermet Models
(781, 783, 784)

Wirewound Models
(721, 723, 724)

Phone 402-564-3131 today for complete details.

DALE ELECTRONICS, INC., 1300 28th Ave., Columbus, Nebr. 68601
In Canada: Dale Electronics Canada Ltd.
In Europe: Dale Electronics GmbH
8 Munchen 60, Falkweg 51, West Germany
A subsidiary of The Lionel Corporation

INFORMATION RETRIEVAL NUMBER 252

Our complete product line can be found in Electronic Design's GOLD BOOK.
Meet the Unbelievable Datagraph

Introducing Bell & Howell's new Datagraph® Model 5-144. We call it the best four-channel, portable test instrument available. You'll call it unbelievable.

Datagraph is ideal for checking out and evaluating an unlimited variety of both analog and digital systems, components and circuits.

It'll handle four tests at once, and give you the answers now, in real time.

Datagraph is as easy to use as an oscilloscope, but it'll give you a hard-copy record up to 200 feet long for further study. Its four channels have a wider frequency response, higher accuracy and provide more flexibility than strip-chart recorders.

Like all Bell & Howell products, Datagraph comes backed by more than 35 years of experience in the development of quality, dependable precision instrumentation.

To see Datagraph, contact us for a demonstration.

We think we'll make a believer out of you.

Bell & Howell

For more information, write the CEC/Instruments Division at 360 Sierra Madre Villa, Pasadena, California 91109 or circle the reader service number below.

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INFORMATION RETRIEVAL NUMBER 2
Get on board with Teledyne I/O converter modules

Now Teledyne Relays offers its proven I/O converter modules in low profile packages for direct PC board mounting. The versatile Teledyne 675 series allows you to design programmable controllers, process and machine tool controls with flexible and economical I/O interface circuitry. The full line includes both ac and dc, input and output modules. All versions are optically isolated, with 1500 VRMS isolation, to protect logic lines from ac or dc power circuits. The AC output modules feature zero voltage turn-on to reduce switching noise and high dv/dt ratings to prevent false triggering in tough industrial environments.

Get on board with Teledyne Relays. We've got thousands of I/O modules at work in the field. Call your nearest Teledyne Relays office for location of your local representative or distributor.

TELEDYNE RELAYS
3155 West El Segundo Boulevard, Hawthorne, California 90250
Telephone (213) 973-4545

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45 Washington Report

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76 Know your a/d converter’s dynamic range. There are three basic definitions, but you had better consider your application before trying to interpret them.
80 Recognize hand-printed characters with a simple algorithm. Only a small amount of hardware is needed to identify a full set of numbers.
86 Ideas for Design: Current limiter added to power supply protects sensitive circuits . . . Programmable unijunction transistor protects op amp from overvoltages . . . Function generator produces sine, square and triangular waves.
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Cover: Photo by J. H. Troupe courtesy of AMP Incorporated, Harrisburg, PA
Choose any speed from Intel's new colle

We have expanded the 2102 series into a first-class family of versatile, easy to use, n-channel static RAMs. These new 1024-bit RAMs add very high speed and 256x4 modularity to the family. Our advanced 2102A series delivers a variety of very fast military and industrial RAMs. The 2101, 2111 and 2112 RAMs save packages in small, expandable memory systems.

The 256x4 organization is available in three package options: 22-pin 2101, 18-pin 2111 and 16-pin 2112. The 2101 has separate input and output lines while the other two have common I/O lines. Both the 2101 and 2111 have an output disable pin for controlling the state of the I/O bus. Both also have two chip enable inputs, whereas the 2112 has a single chip enable input. Like the 2102, these new RAMs dissipate only 150 mW typically.

The world's fastest static RAMs are in Intel's worst-case access time and minimum cycle times are guaranteed over full operating temperature range (-55 to +125°C for MC2102A-4 and MC2102A-6, 0 to 70°C for all other types). The 2102A-2's worst case access time is 250 ns. Like all the family's commercial RAMs, its speed is guaranteed from 0 to 70°C.

### INTEL'S 1K STATIC RAM FAMILY

<table>
<thead>
<tr>
<th>PART</th>
<th>WORST-CASE SPEED</th>
<th>SIZE</th>
<th>PINS</th>
</tr>
</thead>
<tbody>
<tr>
<td>2102A-2</td>
<td>250 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2102A</td>
<td>350 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2102A-4</td>
<td>450 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>MC2102A-4</td>
<td>450 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2101-1</td>
<td>500 ns</td>
<td>256x4</td>
<td>22</td>
</tr>
<tr>
<td>2102-1</td>
<td>500 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2111-1</td>
<td>500 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2101-2</td>
<td>650 ns</td>
<td>256x4</td>
<td>22</td>
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<tr>
<td>2102-2</td>
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<td>1024x1</td>
<td>16</td>
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<tr>
<td>2111-2</td>
<td>650 ns</td>
<td>256x4</td>
<td>18</td>
</tr>
<tr>
<td>2112-2</td>
<td>650 ns</td>
<td>256x4</td>
<td>16</td>
</tr>
<tr>
<td>MC2102A-6</td>
<td>650 ns</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2101</td>
<td>1 μs</td>
<td>256x4</td>
<td>22</td>
</tr>
<tr>
<td>2102</td>
<td>1 μs</td>
<td>1024x1</td>
<td>16</td>
</tr>
<tr>
<td>2111</td>
<td>1 μs</td>
<td>256x4</td>
<td>18</td>
</tr>
<tr>
<td>2112</td>
<td>1 μs</td>
<td>256x4</td>
<td>16</td>
</tr>
</tbody>
</table>

*Worst case access time and minimum cycle times are guaranteed over full operating temperature range (-55 to +125°C for MC2102A-4 and MC2102A-6, 0 to 70°C for all other types).*

ELECTRONIC DESIGN 3, February 1, 1975
and configuration of static RAMs.

For military temperature range operation, two worst case speed options are offered, 450 ns for the MC2102A-4 and 650 ns for the MC2102A-6.

Every member of the family is as easy to use as the 2102. They operate on a single +5V supply at TTL logic levels and have three-state outputs for easy OR-tying. They need absolutely no MOS/TTL interface circuitry. And all are fully static — no clocks or refresh.

The new series are as easy to get, from stock at your local distributor, as the 2102. See him now and choose these first-class RAMs in whatever variety you need to optimize system cost, performance, and modularity.

All of Intel's static RAMs are available now from Almac/Stroum, Cramer, Hamilton/Avnet, Sheridan Sales, Industrial Components, and L.A. Varah. Or write Intel for the n-channel static RAM information package.

Intel Corporation, 3065 Bowers Avenue, Santa Clara, California 95051 (408) 246-7501.
Start Getting Your Money'sworth Out of Power Modules

Now, you can really start getting your money'sworth out of power modules with Abbott's new LOW COST series. Designed to give you 100,000 hours of trouble-free operation (that's 11.8 years), these reliable units meet the needs of OEM engineers. Their purchase price is about $7 per year of service. The model LC series feature:

- 47-420 Hz Input Frequency
- ±0.1% Regulation
- +50°C Ambient Operation
- Single and Dual Outputs
- 1 Day Stock Delivery

These units provide more quality per dollar compared to similar items on the market. See table below for prices on some of our LC models. Many other LC models are listed in our catalog.

<table>
<thead>
<tr>
<th>Voltage (V)</th>
<th>Current (Amps)</th>
<th>Model</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>5V</td>
<td>6</td>
<td>LC5T6</td>
<td>$72</td>
</tr>
<tr>
<td></td>
<td>10</td>
<td>LCST10</td>
<td>$81</td>
</tr>
<tr>
<td>12V</td>
<td>10</td>
<td>LC12T10</td>
<td>$99</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>LC12T4</td>
<td>$81</td>
</tr>
<tr>
<td>28V</td>
<td>1</td>
<td>LC28T1</td>
<td>$72</td>
</tr>
<tr>
<td></td>
<td>2</td>
<td>LLC12T1.2</td>
<td>$99</td>
</tr>
<tr>
<td></td>
<td>4</td>
<td>LLC12T4</td>
<td>$135</td>
</tr>
</tbody>
</table>

If analyzing the many similar power supplies on the market is confusing; if you are concerned about the long-term reliability of those units, then decide on an Abbott power supply for your system. Your best buy in OEM power modules is ABBOTT.

Abbott also manufactures 3,000 other models of power supplies with output voltages from 5 to 740 volts and with output currents from 2 milliamps to 20 amps. They are all listed with prices in the new Abbott Catalog with various inputs:

6V @ 6 Amps 10V @ 10 Amps 15V @ 4 Amps 28V @ 1 Amp 60V @ 1.2 Amps ±12V @ 4 Amps

LC5T6 LCST10 LC12T10 LC12T4 LC28T1 LLC12T1.2 LLC12T4

$72 $81 $99 $81 $72 $99 $135

Please see pages 307-317 Volume 1 of your 1974-75 EEM (ELECTRONIC ENGINEERS MASTER Catalog) or pages 853-860 Volume 3 of your 1974-75 GOLD BOOK for complete information on Abbott Modules. Send for our new 60 page FREE catalog.

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Electronic Design 3, February 1, 1975
George A. Philbrick: Gentleman, innovator

George A. Philbrick is dead. A pioneer in electronic analog computing and a devotee of feedback, he is generally acknowledged to have been the originator of the modular operational amplifier, which is today so important to electronic circuit designers.

Scholar, gentleman, mathematician, writer, artist, teacher, poet, his fertile mind produced many innovations in automatic control and electronic circuit design. Moreover his every accomplishment evoked a feeling of style of unusually high order, that left an indelible impression on all who came in contact with him.

We who have had the experience of more extended acquaintance with him have known him to be a person of infinite complexity, yet of unexpected simplicity, too. An immensely private person, his thoughts were nevertheless global; no aspect of the world nor of humankind escaped his interest. Impressive in size and appearance, as well as in intellect, he was by no means perfect: He had friends and enemies, those he had befriended and those he had wronged. Yet all would agree that he was a special person.

Those in our field who did not know him (or even about him)—and there were many, in view of his retirement during the 1960s—should be aware of our generally unrecognized debt to him. Perhaps someone else would have proposed the operational amplifier as a circuit component if he hadn’t. But only he could have originated it (as an outgrowth of the modular unit operator, of which he was an early advocate), recognized its implications, communicated them to a technical world with verve and authority, built up a successful amplifier business (virtually unchallenged for 10 years) and nearly made “phil-brick” a synonym for modular operational amplifier (instead of “op amp”). Imagine what the world would be like today without the operational amplifier—

His presence has enriched all of technology, and his departure is a matter of regret for all of us, his beneficiaries.

Daniel H. Sheingold
Analog Devices Inc.
Route 1 Industrial Park
P.O. Box 280
Norwood, MA 02062

‘Nice’ engineer finds editorial is ‘sexist’

I read your editorial from the Dec. 6, 1974 issue (“Nice Young Girls and Consultants,” ED No. 25, p. 51), and I think that it is in very poor taste to make the analogy you made between prostitution and electronics. Isn’t it bad enough that your magazine uses the bustline to sell electronic equipment (same issue, p. 126). Do you also have to relate your experiences in the red-light districts of other countries to make your not-too-interesting points?

I suggest that before you write your next editorial you consider the fact that more and more women are entering the field of electronics and that your sexist attitudes are outdated and offensive to some of the “nice young girls” who are

(continued on page 8)
Open-loop measurement rates compliments

The method brought out by Dr. Pierce (see "Measure Open-Loop Servo Response," ED No. 24, Nov. 22, 1974, p. 170) is excellent. This approach has been in wide use in feedback control system work.

The two-channel sweep frequency-response analyzer (Model 913) manufactured by Bafco, Inc., is a much better instrument to use than the one mentioned, as it has built-in noise and harmonic rejection resulting from the internal mechanization of Fourier integral analysis. Open-loop results are obtained readily from closed-loop tests at signal-to-noise ratios up to 1 to 10. With some external equipment, measurements have been accomplished accurately at an s/n of 1/1000.

Abraham M. Fuchs
Vice President
Bafco, Inc.
717 Mearns Rd.
Warminister, PA 18974

Ed Note: The Hewlett-Packard gain-phase meter referred to in Dr. Pierce's article was mentioned as a representative instrument. It was not offered as the only or best possible choice. For more information on the Bafco instrument, Circle No. 316.

Let's get it right for CellMate

In the “Focus on DC/DC Converters” (ED No. 23, Nov. 8, 1974, pp. 70-78), we listed the old address and phone number for CellMate Div. of Seven Sciences Inc. The company is now located at 1405 Civic Center Dr., Santa Clara, CA 95050. (408) 249-8400.

Job hopping viewed as involuntary evil

In “'Meet' the Applicant Before Talking to Him” (ED No. 25, Dec. 6, 1974, p. 86), Alan J. Rider refers to a government manpower study, which states that two to seven years is ideal length of service for an engineer with any one employer. The study is referenced casually, then used as a basis for statements concerning the personal lives of the entire engineering community.

The engineer has throughout the 1960s been characterized as a nomad, following the jobs, living under feast or famine, depending on contracts that will either be canceled or simply fulfilled. Since when is the engineer voluntarily job-hopping for the purpose of becoming a better engineer? Excessive disruption of engineering families has been caused by the breadwinner trying to head off the layoff.

Sure, there's usually been an increase in pay accompanying moves, but that's only because there is a tradeoff between salary, security and convenience. In the engineering world, security is zilch; hence the community of technological nomads.

I hope Mr. Rider doesn't think poorly of me if I happen to have satisfied my employers for a great number of years.

D. J. Sweeney
Air Traffic Systems Div.
Mitre Corp.
Bedford, MA 01730

V/f converter supplier sets record straight

I have read with considerable interest the product descriptions of v/f converters that have appeared in recent issues of your magazine, in particular since North Hills Electronics, Inc., has been a pioneer in the development and application of these units. I feel that you are performing an important service in making the capabilities of these modules known to your audience, and I appreciate the inclusion of North Hills among the suppliers of such units. However, there is one error in the prices quoted for our units in ED 21, Oct. 11, 1974, p. 138.

Our unit, which is the equivalent of the one described, is the DF-20-310, not the DF-10-310, and it sells at $58 in unit pricing, which is competitive with the comparable units.

Sol Sherr
Executive Vice President
North Hills Electronics, Inc.
Glen Cove, NY 11542

ACROSS THE DESK

(continued from page 7)
reading your magazine.

Phyllis Kos
Production Engineer
University of Illinois Chicago
Circle Small Groups Laboratory
Box 4348
Chicago, IL 60680

The editor replies

I don't feel my attitudes are sexist. I feel instead that any field of human endeavor, including prostitution, is fair game for analogy. Incidentally, in walking down one of Hong Kong's main thoroughfares, I didn't know that it was a "red-light district." Nor did anyone else.

George Rostky

Hooker's technique called ad success

I would say that the charming Tokyoan (“Nice Girls and Consultants,” ED No. 25, Dec. 6, 1974, p. 51) followed your lessons to a T:

1. She knew her customer, on the basis of visual market research; Well-dressed Western businessman type.

2. Her interception of you “on the way to your hotel room” certainly testifies to her efficiency.

3. She projected her intended client's needs by admiring a receding hairline—a well-known testimony to an active social life.

4. She accomplished much more than a transitory transaction? You needed an editorial subject, which she furnished, in return for which you advertised her services to 334,585 prime and pass-along readers.

By the way, what was the name of your hotel?

Herbert H. Heller
Senior Staff Engineer
Information Services
Bird Electronic Corp.
30303 Aurora Rd.
Solon, OH 44139

Edward N. Pierce
Senior Staff Engineer
Information Services
North Hills Electronics, Inc.
Glen Cove, NY 11542

(continued from page 7)
New smart oscilloscope with built-in microprocessor gives you answers

HP has combined a high-performance 275 MHz scope, a microprocessor, and LED display to put an end to graticule counting, mental calculations, and most conventional scope errors. The new 1722A gives you a quantum leap in measurement accuracy and convenience. It's a working lab partner that speeds measurements of time intervals, frequency, instantaneous or dc voltage levels, and relative amplitude expressed in percentage. And, instead of conventional reading errors, the 1722A gives you a 3½-digit LED reading of your measurements...in seconds, Hz, volts, or percent.

The microprocessor takes over several tasks you used to perform. It keeps track of dial settings, automatically

(continued on page 3)
Measure wideband microwave networks—in one sweep

To characterize high-frequency networks—in a continuous sweep—over wide ranges, use the new HP 8410B network analyzer with the HP 8620A solid-state sweeper.

Two dramatic examples of continuous-sweep multi-octave measurements made with the new HP 8410B network analyzer:

Transmission characteristics (magnitude and phase) of 8-10 GHz bandpass filter, shown over 2 to 18 GHz range. Note that insertion Loss Trace (10 dB/div) is free from harmonic responses.

Frequency band switching is a thing of the past when multi-octave range networks are measured with the new HP 8410B network analyzer. The 8410B, successor to the popular HP 8410A* (which was limited to octave-wide sweeps), measures both the magnitude and phase of network parameters, vital data for microwave designers. Test configurations covering from 100 MHz to 40 GHz are offered.

Multi-octave measurements in one continuous sweep are possible when the 8410B is used with the HP 8620A sweep oscillator. For example, with the new HP 86290A sweeper plug-in, you can sweep test from 2 to 18 GHz. Or the HP 86320A RF plug-in and the 8410B cover from 100 MHz to 2 GHz, more than four octaves.

The 8410B network analyzer is a frequency-selective system that tracks the sweeper, resulting in a full 60 dB spurious-free dynamic range. Other multi-octave measurement schemes using broadband detection are typically limited to 20 or 30 dB range because of source harmonics.

*Existing 8410’s can be retrofitted for automatic tuning.

For more information, check F on the HP Reply Card.

Up to 24 Millicandels from new high-efficiency RED, YELLOW, and GREEN LEDs

A new series of high-intensity, solid-state LED 'illuminators' are now available from HP. The new high-efficiency Red LEDs have an intensity of 24 mcd at a forward current of 10 mA.

Packaged in the T-1 3/4 outline, the lamps come in both wide and narrow beam types; the wide beam lamps using a diffused lens and the narrow beam lamps with a clear lens. These lamps have long general purpose leads to facilitate all types of mounting.

Four lamps of each color are being introduced, two light output categories for each beam angle. High intensity is obtained using a new HP technology employing a transparent gallium phosphide substrate and adding a reflector in the package. Higher Intensity is possible under "pulsing" conditions (or up to 20 mA dc) as these LEDs do not saturate. These lamps are rugged and are ideal for use in high ambient light conditions. The narrow beam, high output models are used as pushbutton switch illuminators and "Dead Front" panel annunciators. The wide beam models are used for low power panel indicators or backlighting.

For your copy of the Data Sheet, check L on the HP Reply Card.

Red (5082-4650), Yellow (5082-4550) and Green (5082-4950) LED lamps.
NEW high-efficiency step recovery diodes

Special introductory price.

Our new high-efficiency step recovery diodes maximize cutoff frequency while maintaining a fast transition time. Thus, they provide excellent performance in low or high order multipliers and in comb generators.

The new 5082-0800 series diodes are passivated with a thermal oxide for maximum stability. You can buy them in chip form, in low-cost glass packaging, or in hermetically sealed metal-ceramic packages. Test data is supplied with each ceramic packaged device.

As an introductory offer, these devices are available in prototype quantity at the 100 piece price (offer good until April 30, 1975).

For more information, check E on the HP Reply Card.

New scope with microprocessor

computes time intervals and voltage levels, converts time measurements to frequency, and calculates percent. It even signals if you make an erroneous setting.

HP's dual delayed sweep gives you two adjustable intensified markers for displaying the start and stop points of a time interval. The microprocessor automatically computes and displays the time interval between the markers. This speeds digital timing measurements, reduces errors, and simplifies the adjustment of circuits to meet a timing spec.

The 1722A makes waveform measurements faster, more accurately, and more completely than conventional scopes costing up to twice as much.

For details on HP's microprocessor oscilloscope, check B on the HP Reply Card.

NEW HP-55 scientific pocket calculator offers 86 keyboard functions, programmability and built-in timer

HP introduces an extraordinary new programmable scientific pocket calculator. With all of the pre-programmed functions and operations of our popular HP-45, plus 38 new ones including statistical functions.

You can perform circular trigonometry in degrees, radians or grads and convert among any of them. Also, compute two-variable mean and standard deviation, linear regression, linear estimate, curve plotting and four simultaneous linear equations with four unknowns.

The HP-55 has 20 addressable storage registers—more than twice as many as any other scientific pocket calculator on the market.

And, the HP-55 is the only pocket calculator in the world with a built-in digital electronic timer with 100-hour capacity—a stopwatch that times and stores up to 10 events within the same experiment, accurate to 0.01%.

Whenever you wish to write a program to solve your particular calculations, just set the program switch, enter a program of up to 49 steps, then run it... as often as you wish. Meanwhile, you still have access to all 86 keyboard functions plus the 20 register memory.

And, with the HP four-register stack, enter the most complicated equations without having to keep track of the parentheses and brackets.

To learn more about the amazing new HP-55, check A on the HP Reply Card.
Faster graphs with new high-speed time-share plotter

New Hewlett-Packard Model 2640A CRT Terminal is microprocessor controlled. Model 9866A Line Printer (left) is optional.

NEW HP display terminal offers an intelligent addition to your computer

HP's new 2640A display terminal with built-in microprocessor is the intelligent, cost-effective answer to your data entry and information handling needs.

The 2640A operates either on-line or in stand-alone mode, with full editing capability. You can write 24 lines with 80 characters per line on the 5 by 10 in. (127 by 254 cm) rectangular display. High resolution ensures clear, precise character definition. You can also plug in three additional character sets, such as a line drawing set or a math set, and use them concurrently with the standard character set.

The 2640's dynamically allocated memory lets you store 8 to 50 lines or add optional memory modules and store over 400 lines depending upon line length. Memory protection is standard on all 2640A terminals.

Should the modular 2640A need repair, just lift up the top and replace the necessary printed circuit cards. And, thanks to a universal interface, the 2640A works with a wide variety of computers.

For more information or a demo, check C on the HP Reply Card.
21MX computer with new Dynamic Mapping System plug-in gives you million word addressing space

A new Dynamic Mapping System (DMS) devised by HP for its 21 MX series user-microprogrammable 4K RAM semiconductor memory minicomputer allows access to four independent memory spaces.

The 12976A DMS expands the memory address size to 20 bits, thereby providing a maximum main memory addressing space of 1,048,576 16-bit words. It does this without adding to the 650-nanosecond cycle time.

Accounting for the compactness and low prices of the new large-memory models, HP cites features common to the whole 21MX line. For example, all 38 of the new instructions are contained in a single 265 word module of microcode. Also included is read and or write protection on an individual 1K-page basis. All these instructions are on half of a single small circuit board. These new capabilities are plug-in installable.

The HP Dynamic Mapping System functions with main memory somewhat as “virtual memory” schemes function with disc memory.

The 38 new microcoded instructions in DMS firmware, including cross map moves and block transfers, give extensive control over memory allocation and protection. In addition to these 38 supplied by HP, the user can generate his own unique memory management and protection instructions using the standard microcode capability.

For more info on this new Dynamic Mapping System, check O on the HP Reply Card.

HP interface bus enhances signal generator

Joining the growing list of HP-IB compatible instruments is the HP 8660A/B synthesized signal generator. It’s a fully programmable signal generator with .01 to 1300 MHz frequency coverage, $3 \times 10^{-8}$/day frequency stability ($3 \times 10^{-9}$/day optional), +13 to -146 dBm output level, and AM, FM and pulse modulation capabilities.

When installed, the HP interface bus allows programming of:
- Frequency, in 1 Hz steps over the entire 1300 MHz range.
- Output level, in 1 dB steps over the entire 160 dB range.
- Modulation mode, either AM or FM.
- Modulation source, either internal 400 or 1000 Hz tone or external source.
- AM depth, in 1% steps from 0 to 99%.
- FM deviation, in 3 overlapping ranges, either 50 or 100 steps per range, from 0 to 1 MHz.

The HP-IB interface is available as option 005 on new instruments or as a field-installable kit 08660-60189 for instruments already equipped with the standard BCD interface.

To learn more, check M on the HP Reply Card.

Helpful techniques for using VHF signal generator

Three new application notes show you how to extend the usefulness and accuracy of HP’s 8640A/B VHF signal generator (450 kHz to 1100 MHz).

AN 170-1 explains how to improve the specified output level accuracy over narrower frequency limits—i.e., how to operate the generator for optimum accuracy. Also, special calibration can be used to minimize effects of frequency response, temperature, detector and meter linearity, and vernier error.

AN 171-1 describes a method for improving crystal filter measurements when using an HP vector voltmeter and the 8640A/B. This technique optimizes frequency tuning sensitivity by using a feedback signal from the phase meter to the generator external FM input.

AN 171-2 describes how to build a simple heterodyne circuit that extends the frequency down range to dc-450 kHz. The circuit mixes the rear-panel fixed 5 MHz crystal output with the tuned output signal and provides a stable frequency that can be read directly on the digital readout.

For your copies, check P on the HP Reply Card.

New application information available for 8640A/B.

For more info on this new Dynamic Mapping System, check O on the HP Reply Card.
New capabilities, more options for HP-5300 measuring system

Now there is a high resolution 8-digit display mainframe (Model 5300B) with temperature-compensated crystal option in the HP-5300 series of electronic counters and digital multimeters.

New snap-ons for the system include an 1100-MHz counter and a bus interface.

In the 5300 system, a complete instrument consists of two halves that snap together in about 15 seconds. The width of these units is a very compact 6¼ inch (160 mm). The upper half, or mainframe, contains the readout and associated circuitry. The instrument’s measurement functions are determined by the lower half, or “snap-on”, of which there are now 7 models for measuring frequency, time interval, ac and dc volts and ohms. The new 5312A ASCII “snap-between” module allows all of the 5300 functions to interface with data acquisition systems via the HP Interface Bus.

With the new 5305A 1100-MHz frequency counter snap-on, you get a sensitivity of 10 mV to 500 MHz and better than 25 mV to 1100 MHz, automatic gain control and manual attenuator to measure noisy or modulated signals, plus a front panel accessible input fuse to prevent costly front end damage.

With the new 5312A ASCII “snap-between” module you can mate other instruments and controllers to the 5300 series via the HP Interface Bus.

For more information, just check H on the HP Reply Card.

Now debug your control system design before you build it

With HP’s powerful 9830A programmable calculator and state-variables software, you now can know exactly how your control system will perform long before you’ve committed time, materials, and manpower to an expensive prototype.

The new state-variable software provides a complete transient response solution for control systems, whether for mechanical, electronic, hydraulic, optical, or hybrid systems. It’s a carefully developed set of programs that will assure you a stable system in a minimum amount of time. There’s no hassle with computer programming and interfacing. You just key in the values directly from your block diagram, and the 9830A does the rest automatically.

In 10 minutes or less, you get a high resolution plot of transient response and printed list of system parameters. If you want to adjust your design, you simply key in different values. Thus, you can explore alternatives—right at your desk—to find a better design or solution.

An extensive library of engineering and design programs are available from HP.

To learn more, check N on the HP Reply Card.

Low frequency spectrum analyzer offers unmatched resolution

Up until now, the biggest problem analyzing low frequency signals has been the display. Now, you can get a clear picture of mechanical vibrations, audio filters, or data communication channels with HP’s 3580A spectrum analyzer, covering 5 Hz to 50 kHz. The trace appears on a CRT with 1 Hz bandwidth—that’s the best resolution of any low-frequency spectrum analyzer on the market.

You can also store your trace in the CRT’s digital storage. In fact, store two traces, and compare them on the CRT. You can study and interpret spectral information easily and quickly.

Dynamic range is 80 dB. HP offers unique adaptive sweep that speeds up your measurements and reduces analysis time. The 3580A weighs just 35 lbs (16 kg) and operates on batteries, as well as line power.

For more information, check D on the HP Reply Card.
For versatility, ease of operation and wide applications, 50 MHz pulse generators

What every Logic laboratory needs: versatile, easy to operate 50 MHz generator.

The 8012B and 8013B pulse generators are ideally suited to the requirements of a general digital logic laboratory where ease of operation and wide range of applications are essential. Their 10V outputs and fast transition times (3.5 ns on the 8013B and 5 ns on the 8012B) enable you to dynamically test TTL, ECL and even the latest CMOS logic. You can simulate noise patterns and, in double pulse mode, test device recovery times and make noise immunity measurements. You can also use them as amplifiers when generating worst case data patterns.

These instruments not only enable you to set up pulses more easily, but also much more quickly. One big time-saving feature is the unique front panel layout; the slider controls provide a simple, straightforward design that enables you to set up your pulses very quickly and with a minimum risk of incompatible pulse settings. They also greatly improve the readability of the pulse parameters. Another time-saver is the square wave mode which enables you to set up pulses very rapidly without having to worry about pulse width or delay.

In addition, the variable transition times of the 8012B enable you to generate any triangular or trapezoidal waveforms, and the two independent outputs of the 8013B enable you to test circuits designed with bipolar supplies.

For more information on these extremely flexible pulse generators, check K on the HP Reply Card.

A 20 column low-cost printer that really is quiet

At last: a quiet printer that’s really quiet. The new 5150A thermal printer prints faster than 3 lines per second, without any noisy impact mechanisms. It accepts data from BCD or ASCII sources and can list 20 columns of alphanumeric information, yet the price is extremely reasonable.

The 5150A uses heat-sensitive paper and a thermal print head, so you don’t have to bother with ink spills or refills. Don’t let simple design or light weight fool you—the 5150A is a high technology peripheral that can interface with minicomputers, any Interface Bus (HP-IB) instrument system or other digital data sources having acceptable codes and voltage levels. Available options include clock, BCD or ASCII interface and scanner—whereupon it can serve as an HP-IB controller.

For more information, check G on the HP Reply Card.

The 5150A printer is available in several different configurations to fit your system; here, it logs data from a 5345A Electronic Counter.
New triple-output bench supply for IC test and development

Low cost, small size, and outstanding performance, make this new three-in-one lab supply a valuable aid to anyone designing or testing equipment using integrated circuits. Model 6236A delivers three outputs: 0 to 6V, up to 2.5A; and dual-tracking 0 to ±20V, 0 to 0.5A. The 0 to +20V and 0 to −20V outputs track one another within 1% to supply the symmetrical voltages needed by op amps and similar balanced-voltage-source applications. A single 0 to 40V @ 0.5A output can also be obtained by connecting across the −20 and +20V terminals.

All outputs are regulated to 0.01% +2mV, with ripple and noise of 0.35mV rms/1.5mV p-p. The dc outputs have smooth turn-on and turn-off characteristics so that no output voltage overshoot is produced when the ac line switch is operated. Both the 6V and ±20V outputs are protected from overloads by fixed current limiting circuits.

Model 6236A can be powered from a nominal 100V, 120V, 220V, or 240V, 47-63 Hz ac input. The supply weighs only 9½ lbs. (4.3 kg) and is 3½ in. high (8.9 cm), 8½ in. wide, (21.6 cm), and 12½ in. deep (31.8 cm). Single and dual-unit rack-mounting kits are available.

For more information on the three-in-one power supply, check 1 on the HP Reply Card.

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High-speed map making is the task of another CELCO customer using a CELCO precision display for topographical projects.

CELCO displays are helping a leading Oil Company in their oil explorations. While another CELCO display is being used in Eye Research.

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(average is so . . . ho-hum to us.)

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Analog signal processing moving to challenge digital

With recent developments in charge-coupled devices and MOS diode arrays, analog signal-processing techniques are being considered as replacements for some digital techniques now in use.

Engineers will learn of the latest advances in analog signal processing at the International Solid-State Circuits Conference in Philadelphia later this month.

Among the developments to be discussed will be these:
- An MOS diode array that does the same processing as CCD equivalents.
- A CCD that performs a 500-point Fourier transform.
- An analog CCD delay line that has parallel input taps.

While most of the progress in analog signal processing has been in CCDs, some work has been done with MOS diode arrays. Some of this work will be described by Gene Weckler, an engineer for the Reticon Corp. of Mountain View, CA, in a paper on "The Analog Signal Processor." Weckler notes that by using standard MOS technology, it is possible to signal correlators and delay lines. It is not necessary to go to CCDs, he says.

The device to be described by Weckler is a 128-bit serial-in, serial-out analog delay line. The circuitry, he notes, is actually a group of sample-and-hold circuits on a single chip. Each of the 128 stages of the device is made up of an input MOSFET, a diode whose capacitance is used to store charge and a MOSFET output buffer. In addition there are input and output shift registers that control the gating of the FETs.

Information is read in and out of the device by input and output scanners, and no transfer of charge is needed.

As with CCDs, signals can be read in and out at different rates.

The delay possible with the MOS array is limited to 40 ms, Weckler notes. But work is under way to use thin-film capacitors instead of diodes to store information. This could increase storage time by as much as two orders of magnitude.

A more sophisticated device that does use CCD technology will be discussed by Robert W. Brodersen of Texas Instruments. This is a 500-point Fourier transform chip that was originally developed for the Army's Electronics Command at Fort Monmouth, NJ, for remote target-surveillance pattern-recognition systems.

According to Dennis D. Buss, a co-author of the paper, the single chip device uses the chirp-Z transform algorithm to implement the discrete Fourier transform. The device, he notes, can be used in the audio and video frequency ranges, and it competes head-on with digital fast-Fourier-transform processors.

It's possible that some sort of Fourier-transform device will be among the first analog CCDs commercially available. Buss indicates that TI is working on a small modular device that can be used to make transformers of arbitrary length.

"We're thinking along the lines of a 64-point transform chip, but that's only a goal. We are not there yet," he cautions.

Another CCD device to be discussed at the conference will be a 64-bit analog delay line with multiple input taps. According to Roger Melen, a researcher at Stanford University, the device—known as a "razorback" CCD—can be used either to provide a selectable bit delay or to perform delay-sum and multiplexing operations. The device was developed for an acoustic imaging system so an electronic lens could be rapidly scanned while producing a three-dimensional image of an object.

The razorback CCD is not limited to this application, however. Melen notes that at least one semiconductor manufacturer—AMI—is interested in offering a device like this as a building block.

Describing some of the characteristics of the device, Melen reports that it has a bandwidth of 1.3 MHz, a delay that is adjustable from 3 to 8000 µs and has delay taps at 16, 32, 48 and 64 bits.

Standard CMOS ICs due for custom designs

With CMOS already a standard logic family and also a tool for custom designs, the next step in evolutionary development is about to take place: standard CMOS ICs to satisfy a variety of custom applications.

Motorola in Phoenix, AZ, plans to introduce the first dozen circuits over the next 12 months with the MC14400 series. According to Bob Berner, manager of CMOS product planning: "We will be introducing parts that will be directed at computer peripherals, appliances, watches, telephony and a variety of other specific markets."

The process used will be low-power metal gate and will be the same as the standard CMOS logic family. The parts will usually be available in both plastic and ceramic packages.

Typical of the products to be introduced this year are a pair of binary-to-phone pulse converters, a 2-of-8 keyboard to binary encoder, a liquid-crystal watch circuit, a quad precision timer/driver and a pair of oscillator/divider circuits. Other products in the series include modems, tone encoders, a/d logic subsystems and a hex contact bounce eliminator.

'Smart' cable links computer to peripherals

First the intelligent terminal, then the intelligent instrument, and now—the intelligent cable.

Announced by Computer Automation, Irvine, CA, the "smart" cable consists of a ribbon that goes from a minicomputer to a periph-
eral device, such as a printer, terminal or memory. Imbedded in the cable near the peripheral is a small processor that provides most of the electronics to interface the computer to the peripheral.

Most minicomputer systems require a separate peripheral interface card that costs several hundred dollars for each peripheral. In some cases the card might handle two peripherals.

In Computer Automation’s approach, a single half card—called an input-output distributor—and a set of intelligent cables, allow the computers to communicate with up to eight parallel or serial peripheral devices. The I/O distributor costs $380 in single quantity, and the cables are $145 each.

CIRCLE NO. 317

IBM desk computer designed for novices

Ease of use, low-cost comprehensive software and intersystem compatibility are keynotes of IBM’s new System/32 small computer. The over-all system is designed for users with no prior experience in data processing.

The basic desk-sized unit, which rents for as low at $770 a month, offers the following:

- Visual display.
- Simple operator commands and visual prompting.
- Two types of disc storage.
- Communications compatibility with many IBM terminals and systems, including other System/32s and the System/360 or 370.

Applications programs are supplied, at extra cost, for such industries as the construction, wholesale-food and paper and office-products and also for hospitals and membership organizations.

The basic computer is equipped with 5 Mbytes of fixed-disc storage, a six-line CRT display, 1024-bit shift registers shifted in parallel, so nine-bit bytes are stored or retrieved in a byte-serial mode. Each memory cell has 1.3 mil² area.

Input and output is via bidirectional three-state data lines, and a single two-phase external clock supplies timing. The operating frequency is 3 MHz, and power dissipation is 250 mW while reading or 30 mW during 50 kHz standby periods.

The unit is called the CCD 450, and the initial price is $90 in single quantities. The large-quantity production price is projected at $9 by late 1975.

According to Dr. Thomas A. Longo, vice president and general manager of the Fairchild Integrated Circuits Group:

“We will be introducing four other CCD memory products in the coming two-year period, particularly for mainframe computer applications. Each of the products will use our N-MOS process, making them practical to produce at high volume with a low cost per bit.

CIRCLE NO. 318

Serial printer shuns the costly electronics

A 30-character-per-second serial-impact printer with an integral microprocessor control and high-speed digital stepper motors eliminates costly front-end electronics and analog-to-digital conversion circuitry.

Announced by the Terminal Products Group of Interdata, Inc., Randolph, NJ, the combination of print-cup design, the microprocessor and the stepper motors gives high print quality, according to the company’s president, Daniel Sinnott.

Called the Carousel for its print cup, the printer has two paper paths—one around the platen for cut forms, the other for feeding continuous form sheeting up from the rear of the machines and over the platen.

The Carousel, which will cost $1500 in quantities of 50, is priced below the Diablo high-type printer, James Brennan, sales director for the Carousel, notes. A Carousel 300 terminal—which includes the printer, keyboard, communications interface, molded cover, power supply and forms-handling accessories—will sell for $2460 in quantities of 50.

Production deliveries of both the printer and terminal are scheduled to begin in May.

The Carousel print cup rotates during character selection at up to 2100 rpm. It has 94 fingers that contain the alphanumericics of the ASCII set. Six more fingers on the wheel are shortened to let the operator see the copy as it is printed.

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For complete U.S. Rep listing and product line see Microwaves' Product Data Directory
Circuits and substrates separated to make bigger, cheaper hybrids

Need a hybrid circuit larger than $2 \times 2$ in.? Till now you couldn't buy a standard alumina substrate that was much larger. It was also difficult to find a package to put it into. But a new multi-layer hybrid technology from Northrop Electronics, Hawthorne, CA, will let hybrids grow much larger.

According to Arthur Friedman, the company’s microelectronics engineering manager, “We have already prototyped hybrids that are $4 \times 6$ in., and we could go much larger if needed.”

Dr. Robert F. Vieth, chief of the Northrop microelectronics development group, adds: “Not only can we make the package larger, but we can do it at a reasonable cost. Even for standard-size hybrids, we are 10 to 20% cheaper. As the size goes up, the cost savings increases dramatically.”

The key to the technology is separation of the substrate from the interconnecting circuitry. Northrop calls this Thin-Pak construction. ICs are mounted on metal pads on a substrate. The circuitry is fabricated separately on an epoxy-glass material. Then the whole thing is laminated together.

The circuitry is thin film and is applied by photolithography. Density runs 20 to 40% higher than it does in silk-screened, thick-film hybrids. Friedman reports that ICs can be spaced approximately 30 chips/in². Lines can be deposited with 2-mil widths on 4-mil centers, maintained over a 6-in. span. Conventional thick film is not much better than 4-mil lines on 8-mil centers.

To construct a hybrid, Northrop starts with a 2.5-mil-thick epoxy-glass board coated on both sides with 0.7-mil copper. It then employs the following procedure:

- Chemically thins the copper to 0.3 mil.
- Coats both sides with DuPont Riston photoresist.
- Positions the pattern mask, exposes, develops and etches. This makes vias and cavities through the epoxy-glass.
- Coats with Riston again for the conductor pattern, and processes with a mask.
- Plates up conductors and vias.
- Prepares a substrate (ceramic or metal), with metal pads placed to fall under the cavities in the epoxy-glass.
- Places the epoxy-glass circuit of interconnections on top of the substrate, with the metal pads showing through the cavities.
- Laminates together.
- Places the IC chips in cavities and bonds them to the pads.
- Bonds the chips to the printed circuit either by wire bond or beam leads, if that type of chip is used.
- Coats with a conformal coating.
- Covers with an hermetically sealed top.

Friedman notes that an interface connector can be constructed on the edge of the board to make the hybrid into a plug-in module.

So far the technique has only been tried with two layers. However, Northrop sees no reason why more layers could not be constructed with the same technique.

The most significant application for the technology, says Friedman; is in dense, compact semiconductor memory systems. Other appropriate areas are in microprocessor systems, automotive electronics, aircraft systems, digital watches and military systems with low weight, small sizes and low cost.
Want high-volume component production?

Consider the capacity of 34 electronic plants in a company called TRW.

The fourteen Electronic Components Divisions of TRW, Inc. can supply virtually any component in almost endless quantities. One of our divisions, for instance, has the capacity to produce 375,000 resistors an hour. Another can produce 15 million connectors a month. If you need a source with high-volume capability, you've just found it in a company called TRW.
Launch control for space shuttle to lean heavily on minicomputers

The smooth launch-control system that got all the Apollo flights off the ground and to the moon is antiquated compared with the system being developed for the space shuttle, which is scheduled to make its first flight in 1979.

The Apollo system was partly computerized, but there were also a number of preflight ground operations that were monitored by personnel who watched meters.

For the shuttle, each function will be monitored by a minicomputer that has all the tolerances stored in its memory. It will warn the operator when something isn't right, and will refuse to proceed with an operation if it's given improper commands.

Preflight tests that took the Apollo crews two hours will be done by the shuttle system's computer in seconds.

For instance, the propellant console will contain everything to command and monitor discrete and analog functions associated with that operation. The console will contain subprograms to test and check out the propellants' transfer system during prelaunch activities and other subprograms to operate the system during tanking or detanking. If the operator's commands are out of proper sequence, the computer will immediately tell him so.

Why wasn't Apollo computerized?

"Computers were too slow then," says Frank Griffin, technical assistant to the associate director of the Launch Processing Development Center at the Kennedy Space Flight Center, Cape Canaveral, FL, where the system was conceived.

"There wasn't the sophisticated software we have now, and the older machines simply couldn't handle multiple tasks," Griffin says.

The shuttle is being designed for crews to fly satellites into low earth orbit, leave the satellites there and return to earth again. The shuttle will eventually take robot tugs into low earth orbit and release them to go on, on their own, up to satellites in higher, synchronous orbit (22,000 miles) and bring them back.

The Launch Process Control Room will contain 15 consoles, each of which will command and monitor test and checkout functions for a particular operation.

Overseeing the minicomputers that will run the consoles will be a large-scale data-processing machine as large as the IBM 360—in which all the programs will be stored. If it's desired to change a mini's program, the big machine will do it. A second identical machine, with shared, direct-access storage capability, will be on hand as a backup and for noncritical functions.

One big difference in the system being developed for the shuttle and the old Apollo complex is the use of a data bus. Two wideband cables will carry one complete data bus, which will take care of up to eight systems.

"This means two wires will replace 640 wires," Griffin says.

The contract awards for the system, which will be made by the Kennedy Space Flight Center, will probably be divided into three major categories: one contract for approximately 60 minicomputers, one for the two big computers and a third for the rest of the system. All requests for proposals to bid will go out this year.
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Nickel-cadmium batteries often take on a 'memory' if floated. Gates Energy Cells will never give you this kind of effect.

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INFORMATION RETRIEVAL NUMBER 248
Roll-your-own electronics can cut costs of high-quality equipment

Want to buy a $20,000 minicomputer system for $5000? Or a $750 dual-trace scope for $550? How about a $250 power supply for $90? These are only hints of the savings available when you purchase electronic equipment in kit form. And today, when money is tight, many companies are buying kits.

Kits provide an inexpensive way to test-market products and to help build the markets for assembly-line units.

Quality computer performance

One of the most impressive kits to appear in a long time is the minicomputer from MITS Inc., Albuquerque, NM. Known as the Altair 8800, the mini kit, when put together, becomes a full-blown, high-quality computer that rivals commercially available units in performance.

The heart of the Altair 8800, Intel's 8080 NMOS microprocessor, is the reason why this minicomputer is equal to, and in many cases superior to, commonly used minis today. According to Ed Roberts, president of MITS, the Altair is a parallel, 8-bit-data-word, 16-bit-address computer with a cycle time of 2 µs.

The performance characteristics of the mini are basically those of the 8080. It has a 78-instruction repertoire, including some instructions for double precision. This, says Roberts, is almost twice the number of instructions found in comparable processors. While the basic cycle time of the Altair is slightly slower than that of some competitive computers, the Altair may still outperform them.

Explaining how, Roberts notes that if a particular problem requires decimal arithmetic and much I/O capability, the Altair has the advantage. The 8080 contains a decimal converter that makes it easy to perform arithmetic on BCD numbers.

In addition, Roberts goes on, the 8080 has a very powerful I/O structure. It can connect to 256 input and 256 output devices. Most small computers available today can directly address 64 or fewer input/output channels.

Roberts admits, however, that the Altair may not look as good if it has to solve a CPU-related problem that requires considerable speed. In such cases, he says, a mini with a faster cycle time would look better.

"It's difficult to compare performance, because there isn't any software system—like Fortran—that's sophisticated enough to do benchmarks with," Roberts notes.

Another indication of mini per-
formance is the amount of memory it can directly address. The Altair, he says, can directly address 65,000 8-bit words. By contrast, most other minis directly address only about 500 words of data. For larger memories, it is usually necessary to address them indirectly through a base page.

**Instant market survey**

The Altair computer made its debut in a construction project featured on the cover of the January issue of *Popular Electronics*. Roberts notes that when the company offers a kit and features it in an article in a hobby magazine, it gets an instant market survey.

"Within two weeks after the project appeared, we had already sold 115 units," he says. An unusually high number of these orders were placed by industrial customers, many of whom are interested in buying between 10 and 20 machines. A few industrial buyers are even considering buying between 50 and 100.

In explaining why there is so much interest in this mini kit, Roberts notes that the cost of the kit is less than that of the components by themselves. MITS buys the components in large quantities at a saving.

Roger Melen, a researcher at Stanford University and one of the first customers for the Altair mini, says: "If I go to buy the Intel 8080 in unit quantities, it's going to cost $350. For $45 more, I can go to MITS and purchase a complete kit that includes the power supply, case and associated circuitry. I get a proven, tested design."

Melen notes that if he adds up just the cost of the critical ICs, he's far beyond the cost of a MITS kit.

**Cyclops: The solid-state camera**

Another kit that has just become available and is already finding use in industrial applications is a solid-state camera. It is called Cyclops and uses a $2 \times $2 element MOS photodiode array. The kit is being produced by Roger Melen and several other Stanford University researchers who have formed a company known as Cromenco, based in Palo Alto, CA.

The most startling thing about the camera kit is its price—$90. A $2 \times $2-element-array camera from Reticon, a leader in photodiode array cameras, costs $2250.

When asked to explain the tremendous difference in price, Melen cited several factors that help keep the cost low. First, he admits, the Cyclops is a lower-performance camera than the Reticon.

"Reticon's image sensors have no defects on them; ours have a few," Melen continues, adding: "The defects don't affect operation of the camera for the majority of the applications."

If you have an application that requires a lot of sensitivity or many levels of gray—between 64 and 128—the defects will cause problems, Melen says.

Most industrial applications, however, require only a low-resolution, inexpensive image sensor, he contends, and the Cyclops is designed to fill that need.

Another factor that makes the Cyclops cheaper than a Reticon is that much of the processing circuit is on the 'imaging chip. The output of the chip consists of a series of digital ONE or ZERO signals, while the Reticon device has a video output that uses extra circuitry to convert the signals to digital form.

In addition Cromenco offers very little customer support. The kit is provided so that a customer can build the camera and see that it works. If he wants to modify it, he has a working base to start from, Melen says.

Another kit offered by Cromenco is called the Altair Cyclops. This is a $155 camera designed to operate with the MITS minicomputer for motion-detection and servo-feedback applications.

Melen calls the kit approach valuable both from the user and manufacturer's point of view. As a user who has purchased several Altair computer kits, he notes that a kit is a learning experience. It shows how a set of components designed to work together can be reduced to circuit boards.

As a manufacturer, he notes that it is a way of getting sophisticated devices into the hands of many people at minimal cost. Citing an example, Melen says that a customer in the glass industry bought one of the camera kits because he was interested in monitoring a glass-pulling operation to see if the glass broke. That one kit has now generated interest by that customer for 300 wired units.

**Save $200 on a scope**

If you want to add equipment to your inventory and you happen to have a few technicians who periodically run out of work, the new IO-4510 dual-trace oscilloscope may be for you. It can be assembled by a technician in about 20 hours and can save you $200 over comparable instruments.

Of course, if you're going to have to hire a technician just to put it together, it probably won't pay. The IO-4510 is competitive with the 1220A from Hewlett-Packard, and if you buy it wired from Heath, it will cost you about the same as the 1220A—$750. But in kit form it's only $550.

According to Charles Gilmore, manager of Heath's instrument group, a lot of companies are
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Computer keyboards are also available in kit form. This 53-character unit from Southwest Technical includes an internal ASCII encoder.

switching to kit instruments. There is interest not only in the scope kits, he says, but in power supplies and ac VVTMs as well. In fact, about 50% of some of the Heath power-supply kits being sold go to industrial customers.

Gilmore notes that the Heath IT 27 power supply costs $90. The nearest competition for this 50-V, 1.5-A supply comes from wired units that cost between $200 and $250. But, as with the solid-state camera, the performance of the kit unit is slightly lower. However, not all applications require super regulation or super temperature stability, Gilmore notes.

"Many times a little bit less regulation and a little less stringent requirements on the nitty-gritty specs are completely acceptable," he says. "And we're doing a whopping business because of that."

It's not all good

Not all kit manufacturers agree that kits are the way to go for industrial applications. One kit manufacturer—Dan Meyer, president of Southwest Technical Products Co., San Antonio, TX—contends that it just doesn't pay an electronics company to buy a kit. He points out that he has advertised ASCII keyboard kits in the trade press and has received very poor results, even though the unit costs only $40 in kit form.

A lot of companies outside of the electronics industry have, however, purchased kits, Meyer reports. He attributes this to the need to acquire instruments in the cheapest way possible.

More to come

Plenty of kit developments are waiting in the wings. MITS has kits of peripherals for the Altair 8800. One is a disc-operating system for the computer. The controller for the disc will cost about $400, while the disc drive itself will be about $700.

Two other peripherals, both terminals for the Altair 8800, have left the drawing board at MITS. One is a CRT unit that will display 16 lines of information with 64 characters on each line. The terminal's memory will be able to hold four of these 16-line pages. The cost of the kit will be $600. This includes a built-in acoustic coupler, RS 232 modem interface and a Motorola or Miratel monitor.

A gas-discharge display terminal that uses a single 32-character Burroughs display has also been designed by MITS. Like the CRT unit, it has a built-in modem and acoustic coupler.

By building all of these units, the designer can put together a system that will consist of a processor, terminal and several disc drives for about $3000, MITS reports. That's comparable to a system that now costs between $15,000 and $20,000.
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The Democratic Congress: Changes, but not upheavals

Observers of the Washington scene are still hedging their estimates of how the new, heavily Democratic Congress will go about the nation's business. Undoubtedly it will be more liberal in political perspective and, because it's younger in average age, less prone to rubber-stamp defense proposals. But past experience has shown that initial zeal and pledges of reform have a tendency to mellow after Congressional sessions get under way.

Yet changes are already here, as witnessed in the House Ways and Means Committee, where one-man rule is apparently over. Other entrenched committee chiefs are threatened, and seniority alone isn't going to assure them of their lofty spots. In the House Committee on Armed Services, Rep. F. Edward Hebert (D-LA) is expected to retain the chairmanship but not be as all-powerful as he was in the last Congress.

In sum, expect changes, but no convulsions. The liberals and Southern conservatives may not even get it all together to ensure a cohesive Democratic majority.

AEC declassifies laser-fusion research

In hopes of developing usable fusion power more quickly, the Atomic Energy Commission has declassified additional aspects of its laser-fusion research. Now about 95% of the information in the field is available to the public.

The most recent declassification permits publication of theoretical and experimental studies of microscopic fuel pellets, which are filled with heavy hydrogen and used as targets in the laser-fusion process. This will allow studies of the design and performance of these targets and multiple-dimension calculations of them. The AEC, which becomes part of the new Energy Research and Development Administration, says the action was taken to allow free discussion of work in progress.

Environmental impact affecting electronic installations

The Federal Government is proposing some tough rules to implement the National Environmental Policy Act of 1969 that will affect the design of electronic systems. One major change would be in the definition of what constitutes a "major" facility. Before such facilities can be built, the builder must submit a statement detailing its potential impact on the environment.
Originally the thinking was to use a dollar figure—$100,000—as the threshold point for mandatory submission of the environmental-impact statements. But inflation and recognition of possible “visual pollution” from different construction prompted a new look. Now the Federal Communications Commission says it considers the following as “major”: All underground cable or waveguide routes and aerial transmission lines for long-distance telecommunications; private and common-carrier microwave relay antenna towers or supporting structures exceeding 100 ft; AM, FM, television and international broadcast antenna towers or supporting structures exceeding 300 ft, and all AM broadcast directional arrays whatever their height; other antenna towers or supporting structures, including pole-mounted microwave antennas that exceed 300 ft and are not in areas devoted to heavy industry or agriculture; satellite earth stations having an antenna of 30 ft or more in diameter; and communications facilities in areas designated as wilderness or wildlife preserves or in areas recognized either nationally or locally for special scenic or recreation value.

Even facilities that would affect districts, sites, buildings, structures or objects significant in American history, architecture, archeology or culture would be classified as “major.” And the birds are not forgotten. Antennas over 500 ft high “should be avoided if possible” along migration routes, the FCC specifies.

**Vhf replacing mf on the Great Lakes**

Medium frequency (mf) will give way to vhf on May 6 as the mandatory radiotelephone system on Great Lakes vessels. On that date, says the Federal Communications Commission, use of mf in the safety system will be discontinued under a 1973 agreement with Canada.

Vhf equipment will be required on every vessel over 65 ft long and on those engaged in towing, except where the total length of the units is less than 65 ft. Exempted are ships of war, troopships, ships in tow, sail-powered vessels and Government-owned ships.

The primary frequency will be 156.8 MHz. Also reserved are 156.7, 156.6 and 156.3 MHz. Transmitters will be limited to no more than 25 W and no less than 15.

**Capital Capsules:** The Air Force is seeking sources for development, fabrication and flight-testing of an imaging reconnaissance radar for remotely piloted vehicles. Modification of an existing, lightweight, low-cost radar is highly desirable. . . . Systems that will permit the development of a cannon-launched, beam-rider projectile are under investigation by the Army. . . .

The Office of Telecommunications Policy has extended for two years its two advisory councils—one on frequency management and one on electromagnetic radiation management. . . . The Army Electronics Command is looking for a developer of a multistage transistor amplifier that would operate at 12 to 15 GHz under small-signal conditions by utilizing microwave integrated-circuit techniques and GaAs or InP FETs. . . . The National Aeronautics and Space Administration’s compilation of research and technology activity for fiscal 1975 is now available as the NASA Research and Technology Operating Plan Summary (RTOP-75). Included are summary portions that spell out objectives and identify installations of primary interest. NASA officials predict the plan will be particularly helpful to small R&D companies. A copy costs $5 and can be obtained from the National Technical Information Service, Springfield, VA 22151.
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No chart recorder can reproduce exactly the waveform at its input. Since the ideal recorder doesn't exist, the relevant question is: How faithful a reproduction can you get? The question is simple. The answers may not be.

Each of the major components that make up a recorder can contribute an error. The pen-drive mechanism, input attenuators or amplifiers, paper drive—and even the paper itself—all have limitations. What you'd like to know is to what extent and under what conditions.

To find out, you'll have to pore over a slew of electrical and mechanical specs. In the electrical department, specs like accuracy, frequency response, linearity and stability must be pinned down; in the mechanical, you'll need to check into such items as chart-drive accuracy, line width and even paper stretch. And these aren't all.

Unfortunately you may have to stretch yourself before you finally get satisfactory answers. More than a few recorder brochures are long on photos of intricate, delicate curves to show off the recorder, but short on clear, practical performance data. The curves—while lovely to look at—are usually unrelated to real-life situations. Some specs that are needed are nowhere to be seen.

Adding to the problem is the lack of a universal standard to spell out definitions, specs and tests. Consequently when a vendor talks about linearity, for instance, which of the numerous definitions is he using? You really don't know. But you can be sure it's the one that puts his product in the best light.

To spotlight the one recorder that's best for you out of the thousands available, first shine some light on your exact needs. Look at your signal: What frequency range will it cover? What amplitudes and waveshapes? What temperatures and humidities will the recorder see? Is the application primarily one of low speeds and unattended operation or must you monitor fast changes? How accurate must the trace be?

**The movement toward standards**

Only after these and other questions are satisfied can the right stylus-drive mechanism, writing method, paper type, input conditioners, chart drive and necessary options be selected. The writing mechanism is a good place to start.

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Stan Runyon
Associate Editor
In general, accuracy and frequency response are limited by a recorder's writing mechanism, which also loosely defines the instrument's classification. Here, again, no standards exist and categories are vague. With vendors disagreeing about which recorder belongs in which category, and with the writing mechanism details often missing or stated vaguely, it's easy to compare apples and oranges unknowingly. To make matters worse, the terms accuracy, linearity, reproducibility, resolution and other forms are often interchanged.

Thus one major manufacturer splits recorders into three groups: strip-chart, direct-writing oscillographs and light-beam oscillographs. In this breakdown, X-Y recorders are listed as strip-chart units, with the time (T) axis replaced by a second (Y) variable.

The physical distinction between the three categories apparently rests with the pen (or stylus) mechanism. Strip-chart recorders, in this classification, use dc drive motors and pulleys, or cables, to position the stylus. A potentiometer or slide-wire element senses stylus position and feeds the information back to the input, where it is compared with the signal to be reproduced. Hence the strip-chart, in this definition, is a closed-loop servo system.

But another well-known vendor distinguishes between servo and oscillographic types, and lists servo, direct writing and other types as strip-chart recorders. Since many oscillographic units are also operated closed-loop, confusion results.

In general, strip-chart recorders are instruments intended to portray phenomena that vary with respect to time. The word "servo" refers to a servomotor-driven, null-balancing, closed-loop system characterized by the highest accuracy (at best, about ±0.1%), lowest frequency response (10 Hz, at most) and widest chart width (to about 11 in.) of the various recorder types. But you don't necessarily get the best of all three specs simultaneously. Strip-chart units are usually limited to two channels, but the traces can be overlapped.

Direct-writing oscillographs, by one definition, are moving-coil (D'Arsonval) or moving-iron galvanometers with the stylus attached directly to the movement (or penmotor) without intermediate gears or pulleys.

But a quick survey of recorder literature reveals that the meaning of the term "direct writing" depends on who's talking. One brochure states, "A direct-writing recorder writes the measured data 'directly' on a paper chart."

Another source of recorder information says that direct-galvanometer drive refers to the "direct" application of the signal to the coil, with no preamplification. The same source also talks about pens that are "directly" driven from the information being recorded—for example, temperature or pressure sensors that are mechanically linked to the pen motion.

Position, velocity or acceleration feedback can all be found in galvanometer recorders. For the galvanometric types, accuracy hovers, at best, around 0.5% full-scan; frequency response is limited to about 250 Hz and chart width to roughly 4 in. The number of channels can range to eight, and even more. In general, traces can't overlap in a galvanometer unit.

The light-beam oscillograph is the least accurate (about ±2%), but it can handle frequencies to 10 kHz and even higher, plotted on a chart up to 12 in. In the light-beam scheme a mirror attached to a galvanometer movement deflects a light spot across photosensitive paper, which is then developed to get the final trace.

Still another light-beam unit deflects a CRT beam to generate the moving spot. A fiber-optics bundle then transfers the light to photosensitive paper.
If it's an industrial recorder you need, check into Leeds & Northrup's wide line of 11 basic models with over 140 options. The company makes laboratory units, too.

paper. The result: a frequency response of greater than 5 kHz.

Other drive mechanisms with many variations can be found in commercial recorders. Some use stepping motors to position the stylus. Others don't write continuous lines at all but use print heads to bang out a series of sequential points on the chart paper. Still others are one-moving-part linear servos without gears, cables, pulleys, clutches or slide wires. And you can get analog recorders that scan dry electrosensitive paper, line by line, to give a facsimile-like presentation.

Whatever the type of recorder, it's the in-use accuracy that counts, not the inherent or theoretical capabilities of the mechanism. So many factors can combine to assault accuracy that it's probably the toughest to specify of all recorder parameters. And this is often reflected in the spec sheet.

Illusive accuracy specs

When a vendor states his instrument's accuracy as a percentage of full scale—and most do—how much trust can you place in the figure? A spec of 0.2% sounds pretty good. But does it account for the width of the line, which can easily approach the same percentage? You don't know.

Perhaps the figure represents the accuracy of the chart drive and not the indicating portion of the recorder. Or does it include both? Of course, when you plot a variable against time, you'll also want to know how steady the chart is. This depends not just on the chart motor, its drive frequency (if any) and gear train, but on the sprockets, guides or any other arrangement that can affect the position of the chart beneath the stylus.

What about the chart itself? Since no printing process is perfect, it's reasonable to expect some errors in the grid lines. For that matter, the chart paper itself can stretch or shrink with changes in temperature and humidity. Are these included in the accuracy spec? Since the paper dimensions can vary by ±1%, the answer is obvious.

Accuracy can also vary with the range setting of the input attenuator, and the figure may depend on how well you set the initial calibration adjustments—something the vendor can't control. Time, temperature and line-voltage variations are also out of the vendor's hands. But does he tell you how the changes affect the instrument? Probably not.

Whatever the stated accuracy does include, you can be almost certain that the spec in most cases is valid at just one temperature: 25 C. But temperature can and does affect recorder operation, as can humidity and line voltage. Thus gains can vary, zero settings can drift—and accuracy suffers.

Time is also unkind to recorder accuracy. Even
at constant temperature, recorders often drift over the short term (8 h or less). And since friction and mechanical wear build with time, accuracy over the long term will certainly degrade.

Where can you find this information on the spec sheet? In most cases, you'll have to ask for it. Even when listed, the drift figure may be referred to the input and specified at just one sensitivity. To get the actual drift—which can be 100 times higher—you'll have to determine the basic drift and then multiply it by the gain factor.

Particularly in servo-driven units, you may find an accuracy statement, but often tacked on alongside—or buried in the back—are numbers for such related items as deadband, hysteresis, repeatability and linearity. Sometimes deadband and hysteresis are lumped into the number for accuracy, repeatability or even linearity. How can you tell when this is done? You can't.

A loose servo is a dead servo

In a servo system, deadband is the amount the input signal must vary to get the motor going—that is, to overcome the friction of the stylus on the paper, and that of the drive train, and to accelerate the load. If a potentiometer serves as the feedback element, its resolution also affects the deadband.

A related effect—labeled hysteresis—can be traced to backlash or elasticity within the drive train, which limits the fidelity with which the stylus can follow the input signal.

Nonlinear frictional forces in galvanometers also represent a form of hysteresis and keep the galvanometer from moving until sufficient signal has been applied. The presence of nonlinear forces also means that removal of the signal doesn’t guarantee that the stylus will return exactly to its starting point.

Another effect that points to frictional nonlinearities: waveshapes that change when their amplitudes are gradually reduced.

Various repeatability tests can sum up such errors. One method applies a deflecting signal in alternate directions, with rest periods (zero signal) between reversals. A low-pass filter ensures that the signal is applied and removed gradually, with no overshoots. In the ideal recorder the rest periods all occupy the same level. Practical recorders exhibit some small offset.

Since galvanometers are basically rotating devices, curved grid paper must be used to match the radius of the stylus. Alternately—and this is usually more desirable—rectangular-coordinate paper can be used if the pointer arc is converted to rectilinear motion by a mechanical linkage. (In frequency response, however, curvilinear motion may have a slight edge over rectilinear.)
For the general-purpose laboratory user, Hewlett-Packard's 7015A X-Y recorder features electrical and mechanical flexibility to fit various applications.

Features normally found only in laboratory units—such as interchangeable plug-in signal conditioners—are offered in the TR-222, Gulton's portable recorder.

Unfortunately the sliding or rotating bearing contacts of the linkages increase the friction and inertia and contribute an additional area for wear.

Still another method of polar-to-rectangular conversion holds a long, hot element in contact with heat-sensitive paper. The paper is pressed between the element and a knife edge, over which the paper passes. With a sufficiently long tip, as the pointer rotates, one part of the element always maintains contact with the paper along the knife edge and thereby traces a straight line. This, of course, doesn't mean that the recorder performance is linear—just that the stylus writes a straight line as the coil rotates. The departure from linearity depends on the angle of rotation since the length of the visible paper mark is proportional to the tangent of the angle.

In galvanometers, as in most recorders, the quality of the trace improves as the contact pressure between stylus and paper increases. But increased pressure means increased friction—which is to be avoided.

To offset the effects of friction from contact pressure, linkages and other sources—and to improve linearity—some galvanometers are designed with position-feedback. In effect, the feedback increases the apparent torsional stiffness of the suspension for small deflections. In null-balancing servos most of the nonlinearity stems from that of the feedback element. But, though linearity may be improved by feedback, the method of specifying it isn't.

Walking the straight and narrow

A perfectly linear recorder would have an output (deflection) that is directly and linearly proportional to its input (voltage or current) across the entire chart span—that is, equal increments of input produce equal deflections, or amplitude changes, at any spot on the chart. (This, of course, is aside from linearity based on stylus-geometry considerations.)

Perfection doesn't exist in practical recorders. But the gap can be considerably narrowed—at least on paper—by auspicious selection of the method by which nonlinearity is specified.

Numerous methods exist, all based on variations of how a straight line can be drawn through an arbitrary series of points. The straight line, which represents the ideal input-output relationship, can be moved for a "best fit" to the curve connecting the actual input-output points.

The best fit obviously is the one that gives the smallest number for nonlinearity.

Actually any of the methods—of which the most popular are the least squares and end-point—is legitimate, at least mathematically. But 99 times out of 100 you're not told which method the manufacturer used. And even when you are, how do you relate the stated linearity to actual
individual errors—which can easily exceed the given value? You can't—at least not on paper.

Perhaps the best approach is to apply a small, constant-amplitude, sinusoid to the recorder and then move the resulting trace to various positions on the chart—especially the chart edges. Changes in the peak-to-peak amplitude of the trace will expose nonlinearities.

Some manufacturers feel that all errors should be lumped into one over-all accuracy spec. Others say that in many cases absolute accuracy isn't the most important spec, since other portions of a measuring system—such as transducers—contribute far greater inaccuracies than the recorder. More important, this school of thought says, is repeatability, or reproducibility—the ability to get the same result over a period of time. Thus drift and nonfixed errors—such as deadband—should receive greater emphasis. But whatever the emphasis, one item everyone agrees is important is frequency response, or bandwidth.

All recorders are limited in frequency response. The trick is to find out how much. Unfortunately the best place to do this is not always the spec sheet.

A tricky spec

How a deflection system reacts with changes in the frequency of an input signal is what you'd like to know. But to really pin it down, you have to find out where you're operating on the chart, what your signal looks like and what input amplitudes to expect.

Each of these factors will affect the frequency response. And that's why many spec sheets tend to forget one or more factors. If no qualifiers are tacked on, forget the figure altogether and start asking questions.

Ask the vendor if the spec holds only at the chart center. In most cases, it does. Ask what amplitude the vendor used when he measured the response. What waveshape did he use: Sinusoid? Square wave? Triangle? Or what? And where were the damping and gain pots set at the time?

Remember that as frequencies go higher, a point is reached at which response begins to drop. This means that you won't necessarily get a full-scale swing at high input frequencies. More likely, you'll get a third or a fourth of the total chart width. This is a limitation you may be able to live with—as long as you know about it.

You can be pretty sure that most unqualified frequency-response specs are for small signals. What you can't always be certain of is exactly what the spec means when it's fragmented. For instance, when a statement says that frequency response is flat within ±1/2 dB, 0 to 50 Hz, and −3 dB to 100 Hz, does this mean that the response at 100 Hz is 3 dB below that at dc? It might.

But somewhere else on the document, you spot a fine-print clause that implies a signal other than dc was used as a reference. Now it looks as though the over-all deviation from flatness may not be 3 dB at all—it depends on where the reference point falls on the response curve with respect to the dc level.

In motor-driven servo units—where reaction is relatively slow—bandwidth and frequency-response specs are dropped for other terms: response time, slewing speed (or rate), acceleration and writing speed.

Because of its slow response, a servo recorder is usually used for static or slowly changing phenomena—temperature changes with long thermal time constants, for example. Most servos excel in these applications. But when it comes to dynamic performance, life isn't so easy.

Under dynamic conditions—important in X-Y units—a servo can slew just so fast and no more. When the velocity limit is reached, the servo will be unable to track the input signal, and errors will result. This limit is reached when a sinusoid's peak amplitude equals \( V_m/2\pi f \), where \( V_m \) is the servo's maximum velocity.

Peak acceleration limits also exist, beyond
which the servo can't follow the signal's rate of change. As in velocity limited operation, the servo saturates or becomes nonlinear, and errors result.

To specify servo response, many vendors list a response time—the time the stylus needs to cover the full chart distance after a full-scale step is applied. Others give slew rate instead, usually in inches per second. Whatever the method, make sure that settling time is included in the response spec. Make sure the response holds for both directions—some units are slower going one way than the other. And in ink-pen systems, note this: If the reservoir can't deliver ink fast enough, that impressive high-speed slew may be useless.

As in any moving system governed by the differential equation for balanced torques or forces, a recorder's response to a step or triangular input tells you how well it can reproduce an input waveshape.

Thus a step input will reveal oscillatory behavior or it will show that the instrument is underdamped, critically damped, or whatever. A triangle will establish the recorder's phase lag in addition to the amplitude distortion: Depending on the instrument's damping coefficient, square waves will exhibit rounded-off corners or overshoots; triangles will start to look like sinusoids with rounded, instead of sharp, peaks.

What damping level produces the best fidelity of response is a matter of opinion among vendors. Most recorders have 60 to 100% of critical damping. Some offer adjustable damping.

In galvanometer movements frequency response can be stretched, and damping controlled, by use of driving amplifiers and also by feedback loops with equalizing networks. To get the widest response, look for recorders that use both techniques.

Though galvanometers top motor-driven in-
In the Speed Servo II multipoint unit from Esterline Angus, a thermal matrix print head records up to 24 channels. Format is user programmable.

Instruments in frequency range, the motor drive is generally more sensitive. Sensitivity—a spec most recorder users are interested in—tells you how much voltage or current you'll need to move the stylus across the full chart span.

Some caution is needed to evaluate a unit's sensitivity. One recorder will list it as so many volts per millimeter, another as volts per inch, and still another as volts per division. You'll have to dig to find out how big a division is. Or you might see something that says "sensitivity: 0.1 mV." This can mean 0.1 mV will drive the stylus full span, or it can be the amount needed to move 1 mm. Find out.

For a unit to be very sensitive—that is, to move relatively large amounts with small inputs—the deadband must be negligibly small. So watch out when the recorder maker brags about microvolt sensitivities but lists millivolt deadbands: Like pickles and ice cream, the two don't go together. While you're at it, look for other "indigestible combinations"—noise rejection and response, for one.

Sensitivity can hurt

Like other instruments with sensitive front ends, recorders are susceptible to conducted or radiated noise. And since many recorders chop the dc input and use ac amplifiers to minimize drift, spurious ac signals are amplified along with the legitimate dc levels.

Unwanted signals that get by the front end can shift calibrations (zero level), produce deadbands, spikes and nonlinearities, and affect damping.

To avoid or reject noise, a number of techniques are available, including filtering, grounding, shielded and guarded construction, and physical isolation of circuits. Any or all of these may be used within one unit, and the resulting immunity is split into two specs: one for normal-mode rejection (NMR) and the other for common-mode (CMR).

But straight numbers for NMR and CMR—no matter how high—may not tell what rejection you'll get in your own setup. Both figures depend on such items as source impedance, frequency, waveshape, input-circuit imbalance and external grounding methods. Since the vendor can't measure the rejection for all possible combinations, he settles for one. If you're lucky, he'll at least tell you which.

Take CMR. In a perfectly balanced differential-input circuit—one in which the impedance from source to recorder to ground is equal in both the high and low legs—the CMR is infinite. Of course, some imbalance always exists, and the CMR spec will depend on the amount. Since no universal standard exists for the amount of imbalance, vendors can choose any value. Most have settled for a 1-kΩ imbalance. If no figure is given at all, be suspicious.

With NMR, other problems can arise. To boost NMR, vendors offer units with fixed input filters. Or you can get preamps with switchable filters. This is all well and good—until you remember that filters need time to settle. Thus that high-frequency response you expected may not be realizable unless you switch the filter out—at the expense of NMR.

Other recorder input characteristics may be important: The input impedance, for example, shouldn't be so low as to load your source. Remember that in some null-balanced units, the input impedance can plunge drastically as the servo moves off null; the faster the servo can follow the input signal, the closer it will remain...
toward balance—and high impedance. At any rate, you should be told the minimum impedance (at the point of maximum imbalance).

Protection—for both the machine and the user—may be a must. High common-mode voltages can burn the instrument, and ungrounded or nonisolated instruments, the user. If a high CMR attached to a weak common-mode voltage is thrown at you, duck. The high/low combination is a clue that something in the input circuit may not be so desirable.

In some cases the recorder's motor may need burnout protection—say, if the recorder will operate in a remote, unwatched site and at full-scale settings.

And as anyone who's ever used a sensitive recorder can attest, the stylus can also be damaged by off-scale slams or mishandling. Thermal styli have been known to open at the element, thereby breaking the heating circuit. Perhaps the best protection here is to look for the latest in stylus designs.

The old truss-work stylus that dominated the industry for many years has been replaced by more rugged designs: tubular, coaxial construction and folded-blade units made of titanium or

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**Who makes what in recorders**

<table>
<thead>
<tr>
<th>Company</th>
<th>Types offered</th>
<th>Formats</th>
<th>Drive types</th>
<th>Writing system</th>
<th>Paper system</th>
<th>Remarks</th>
</tr>
</thead>
<tbody>
<tr>
<td>Beckman (Dynograph series)</td>
<td>L = lab</td>
<td>Strip</td>
<td>C = continuous line</td>
<td>X-Y Nulling</td>
<td>C = Circular</td>
<td>Biomedical units. Change input units.</td>
</tr>
<tr>
<td>Data Technology</td>
<td>L, I</td>
<td>C</td>
<td>v</td>
<td>v</td>
<td>v</td>
<td>Flat bed or vertical. Charts: 4 to 10 in.</td>
</tr>
<tr>
<td>Esterline Angus</td>
<td>L, I</td>
<td>C, M</td>
<td>v</td>
<td>v</td>
<td>v</td>
<td>Broad line spans all types. Multipoint unit thermally brands up to 24 channels.</td>
</tr>
<tr>
<td>Fischer &amp; Porter</td>
<td>I</td>
<td>C</td>
<td>v</td>
<td>v</td>
<td>v</td>
<td>Dc torque motor with contactless feedback. Up to three pens.</td>
</tr>
<tr>
<td>General Scanning</td>
<td>L, I</td>
<td>C</td>
<td>v</td>
<td>v</td>
<td>v</td>
<td>Miniature units. Open or closed loop. Battery operation, low power.</td>
</tr>
</tbody>
</table>
stainless steel. Other designs prolong stylus life, improve performance or make maintenance easier—replaceable tips, ball tips, indirect heating elements, ceramic thermal tips are all available today. Before you buy, however, you'll first have to decide which writing method to opt for.

**Drawing the line on drawing the line**

Fluid flow . . . heat . . . pressure . . . light . . . electrons. Sounds like a course in basic physics, doesn't it? But each really is a way to draw a line on a piece of paper. And which to choose depends heavily on the application. Paper costs, trace permanence, reliability and convenience all play major roles in selection.

Of all the methods, capillary-ink writing is the simplest and most economical. Chart paper is the least expensive—no minor consideration where reams of data are to be taken. Lines are usually crisp and dark and can be easily copied, if desired.

The disadvantages of capillary flow are similar to those of the old fountain pen. To start the flow, some sort of priming system is usually needed. At higher writing speeds, ink may not
flow fast enough, and skipping results. At low speeds, too much ink may flow. If the pen stops momentarily, get out the ink remover. (But if the pen stops long enough, don’t worry about flooding. The quick-drying ink used to prevent smudges will probably clog the pen.)

To get around the problems of capillary flow, recorder designers have come up with the pressurized-ink approach—a completely enclosed hydraulic system that pumps ink to the pen at a rate determined by chart and pen speeds. Because of the optimized variable pressure, uniform lines over a wide speed range are produced. Ink blobs don’t occur because the pump stops when the pen does.

Pressurized systems are generally smudge-proof, since the ink is literally forced into the special coating of the chart paper. Contrast and paper gloss are usually high, and the resulting trace is probably the most permanent of all writing types. Because of the special coating, the paper for pressurized writing costs about 50% more than the plain paper used for capillary flow. And, of course, you’ve got to pay extra for the hydraulic system.

If you don’t want to fill reservoirs or periodically change pressurized cartridges (some can last a year or more), check out the host of dry writing schemes. You’ll avoid ink problems. But the tradeoffs are usually higher paper costs, less contrast and definition, and possibly reduced paper stability. And most dry-writing chart paper doesn’t take well to handling: unwanted smudges and marks are common.

Heat, electrosensitive and photosensitive papers cost roughly 4, 6 and 10 times more, respectively, than plain ink paper. For very high chart speeds, however, you may have no choice but to go to one of the more expensive recording methods.

Tradeoffs (other than economic) exist within Z-fold systems offer a number of advantages over roll paper, including no threading or spills.

Typifying the latest trend in paper systems are these Z-fold OEM units, manufactured by General Scanning.

Recently introduced, the Gould 110 is a thermal writer that uses a new type of paper to produce blue traces with a thermally fast-acting ceramic pen tip.
the many dry-writing schemes. Thermal styli don’t have to press as hard against the paper as pressure-sensitive ones, so thermal pens can usually write faster. Heat-sensitive paper is also less susceptible to accidental marking.

Older electro-sensitive schemes use a high-voltage stylus to break down a carbon-impregnated paper. The process leaves a carbon residue that must be removed. Newer, low-voltage units use a different form of paper to avoid this problem.

Not only the paper type, but how the paper is handled is an important consideration. Anyone who’s spent a frustrating half hour trying to load a difficult machine appreciates one in which paper changing is fast and easy. Ditto with pen servicing.

Equally appreciated are units that don’t spill streams of paper all over the floor during recording, and ones that let you write information alongside the trace without becoming a contortionist. Storing stacks of recordings can also be a problem. For these reasons, Z-fold (or fan-fold) recorders are becoming increasingly popular. Z-fold gives the user easy storage and handling, instant access to down-the-line data and doesn’t spill paper all over the floor, either.

But watch out. The Z-fold unit is harder to use than the standard roll-chart recorder, and performance may suffer for it. This is because some mechanisms used for standard rolls tend to remove the fold in Z-fold paper. Thus the paper may not stack as it leaves the machine. To avoid this, designers must come up with alternate mechanical arrangements. This isn’t easy, and friction, inertia, pen pressure and rigidity can all be adversely affected.

Other features besides Z-fold, can make life easier or are even necessary for a job. Let’s look at some.

**Options galore**

Perhaps in no other measuring instrument can you find the variety and quantity of options, features and type variations that you can in recorders.

Whatever recorder you need—industrial, OEM, military or laboratory—you’re sure to find one among the many offered by dozens of vendors. Some make them, some import them and a few offer “private-label” recorders bought from others.

Industrial units are generally large-quantity items that are built up with options and features for a single-purpose job. By contrast, lab recorders are usually general-purpose machines and, as such, come with interchangeable front ends and selectable speeds and sensitivities.

Features and options range from integral disposable pen-cartridges to stepping-motor chart drives to alphanumeric edge printing. Some units offer automatic ranging and automatic gain or damping. Retransmitting devices are available to provide output control signals, if needed.

If the thousands of features and options don’t do the job, many vendors will customize special units. Just ask.

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**Need more information?**

The products cited in this report don’t represent the manufacturers’ full lines. For additional details, circle the appropriate information retrieval numbers. For data sheets and more vendors, consult ELECTRONIC DESIGN’S GOLD BOOK.

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Esterline Angus Div., Esterline Corp., P.O. Box 24000, Indianapolis, IN 46224. (317) 244-7611. (Paul Lawall). Circle No. 424


Fitchburg Coated Products (Recorder Paper), Box 1106, Fitchburg, MA 01420. (508) 473-2035. Circle No. 448

Foxboro Co., 86 Neponset Ave., Foxboro, MA 02035. (617) 553-8750. Circle No. 427


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Incor Instrumentation Inc., 144 Lamar St., West Babylon, NY 11703. (516) 643-7070. (T. Swift). Circle No. 434


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Program multichannel audio gain
with FETs in the feedback paths of op amps. Quad chips allow up to 60 dB of control range with good tracking.

A field-effect transistor in the feedback path of a noninverting amplifier allows you to design gain-control circuits with a three-decade range. Besides the circuit's simplicity, it lends itself—with dual or quad op amps—to multiple-channel operation with tracking gain control. Since the FET is used as a voltage-controlled resistor, a single potentiometer or digital-to-analog converter can control any number of channels.

The gain-control range can be designed for values from below 2:1 to above 1000:1. Input voltage levels are limited by allowable distortion, and the bandwidth of the complete circuit depends on the maximum gain and the unity-gain bandwidth of the op amp.

Control FET channel resistance

The reciprocal relationship between FET channel resistance \( r_d \) and \( V_{GS} \) is used for the linear gain control. The ac resistance of the FET is given by

\[
r_d = r_o \frac{V_p}{V_p - V_{GS}} \tag{1}
\]

in which \( V_p \) is the pinch-off voltage. As \( V_{GS} \) approaches \( V_p \), the \( r_d \) approaches infinity.

In fact, the FET is often used this way as a simple voltage-controlled attenuator (Fig. 1a). But you can consider \( V_p - V_{GS} \) as a control voltage \( V_c \) and therefore

\[
r_d = r_o \frac{V_p}{V_c} \tag{2}
\]

The gain of an op-amp circuit and FET (Fig. 1b) is given by

\[
A_v = 1 + \frac{R_1}{r_d} \tag{3}
\]

Or, with \( r_d \) expressed as in Eq. 2,

\[
A_v = 1 + \frac{R_1}{r_o} \cdot \frac{V_c}{V_p} \tag{4}
\]

which proves that the gain is a linear function of \( V_c \).

When \( V_c = 0 \), the gain is unity; as \( V_c \) approaches \( V_p \), the gain increases to

\[
A_v = 1 + \frac{R_1}{r_o} \cdot \frac{V_c}{V_p}
\]

The actual circuits exhibit linear gain change with the control voltage; except near minimum gain (Fig. 2). Finite contact resistances at the source and drain cause the FET to act in a non-linear manner.

1. The FET as a voltage variable resistor easily controls the gain of an op amp. While the unit is often used as a simple attenuator (a), it provides linear control when used in conjunction with an op amp (b, c).

\[ A_v = 1 + \frac{R_1}{r_o} \cdot \frac{V_c}{V_p} \]

The gain values of such circuits can be as high as 1000.

The addition of resistor \( R_2 \) will limit the minimum gain to some value greater than unity (Fig. 1c). The gain equation becomes

\[ A_v = 1 + \frac{R_1}{R_2 + r_o (V_p/V_c)} \]

or more simply,

\[ A_v = 1 + \frac{R_1}{R_2} \cdot \frac{V_c}{V_p} \]

which remains linear with \( V_c \).

The actual circuits exhibit linear gain change with the control voltage; except near minimum gain (Fig. 2). Finite contact resistances at the source and drain cause the FET to act in a non-linear manner.

James Sherwin, Linear Applications Manager, National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, CA 95051.

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ELECTRONIC DESIGN 3, February 1, 1975
ideal way. However, for FETs with longer channels, the gain curve is more linear. For these units the controlled-channel resistance is a larger percentage of the total source-drain resistance. And where precise control is required, the long-channel device is desirable.

Signal distortion can be minimized

The value of $r_i$ is not constant with the ac signal across the FET. And this form of nonlinearity can introduce distortion. The effect is most pronounced as $V_{GS}$ approaches $V_P$. There are two simple ways to minimize this distortion: Limit $V_{DS}$ to small values when $r_i$ is large or use FETs that have large values of $V_P$.

The linearity of $r_i$ can be improved somewhat by feedback of a portion of $V_{DS}$ in series with $V_{GS}$. About half of $V_{DS}$ is applied to the gate (Fig. 3a). All that is required is the addition of two resistors and a capacitor. The capacitor blocks the control voltage from the drain and op-amp input. The addition of an emitter follower (Fig. 3b) prevents abrupt changes in $V_C$ from being coupled to the op amp.

The improvement in measured distortion with and without feedback is very significant (Fig. 4). Measured distortion at low signal levels is actually the result of noise, not circuit distortion. The plots are given for a maximum gain of 100 to avoid regions of low S/N. The total noise is that of the op-amp input stage plus the contribution from the FET—essentially the thermal noise of $r_i$.

The signal bandwidth of the circuit equals that of the op amp's closed-loop bandwidth. The control time constant depends on the FET input circuit (the value of $R$) and is limited by the slew rate of the op amp. The FET can react almost instantaneously to produce a step change in the feedback ratio.

There are numerous applications for these circuits; for example,
4. Large values of pinch-off voltage, $V_p$, as well as feedback (shown in Fig. 3), reduce signal distortion as shown by the curves on the lower right. Gain control range is from 1 to 100 for all four curves.

5. A maximum output of 8.5 V rms and a gain range of 1000:1 are readily achieved. Distortion is low, but the short-channel FET forces the gain curve to deviate from linearity with respect to $V_e$. 
Multiple-channel operation with excellent gain tracking is readily achieved by use of dual or quad monolithic FET chips. Monolithic FETs are recommended for a close match of $V_T$ on all channels.

- Remote or multichannel gain control.
- Volume expansion.
- Volume compression.
- Quad sound control.

At maximum gain, the circuit shown in Fig. 5 has a bandwidth of 20 kHz, a maximum output level of 8.5 V rms and a gain range of 1 to 1000. The FET has a large $V_T$ (8.2 V) to minimize distortion. The FET used is a short-channel type. Hence the circuit has a nonlinear gain-control characteristic.

The op amp used provides wide frequency range at maximum gain. The input voltage must be less than 8 mV rms at maximum gain to prevent output saturation. And the circuits provide an S/N of 60 dB measured with a 10-kHz bandwidth.

For a gain range of 1 to 100, an LM301A could furnish a 10 kHz bandpass, handle 80 mV signals and provide 80 dB of S/N.

**Monolithic FETs ensure gain match**

Any dual op amp used in conjunction with a monolithic dual FET (NSC 2N3958) can provide tracking gain functions. Alternatively, the LM324 quad op amp and AH5009 quad FET will provide four tracking channels (Fig. 6). The gain is variable over a range of 100:1 (40 dB), and you get a minimum S/N of 70 dB with 4.3 V rms output. And excellent gain tracking is possible, as shown by the curves. Monolithic dual (quad) FETs ensure a close match of $V_T$.

Noise is an important consideration for these gain-control circuits. For a 40-dB attenuator, you may have to add fixed attenuation at the amplifier input and perhaps at the output. Thus a low-noise amplifier is desirable. Low source resistance also helps. With an LM381 you can achieve about 100 dB of S/N with a 40-dB gain range or 80 dB S/N with a 60-dB attenuator.

To reduce sensitivity with temperature, use a silicon resistor for $R_1$. This will compensate for FET temperature sensitivity. If the FET were integrated on the op-amp chip, $R_1$ could also be included.

The linear characteristic of the FET gain control is ideal for use in volume expanders. The required control range is about 1:4, and the input signal level is low. Other requirements include these:

- Linear slope of log gain (dB) with respect
7. A volume expander built with FET gain control also has the necessary log-gain characteristic. Circuit gain is 0 dB at mid range (100 mV). Resistors R₃ and R₄ furnish the logarithmic characteristic.

8. The expander circuit is readily adaptable to stereo or quad sound systems.

to signal level (dB).

- 12-dB gain change for 30-dB input signal range.
- Linear peak detector with fast attack (1 ms or less) and discharge time of about 2 s.

A circuit built around a quad op amp achieves all these design goals (Fig. 7). Resistors R₃ and R₄ modify the linear gain curve to a logarithmic one. Half of the quad performs as a full-wave peak detector. The FET is biased off (minimum gain) for small signals and biased on progressively for large signals (maximum gain).

Resistors R₅ and R₆ attenuate the input signal before amplification. This reduces distortion (0.1% at all signal levels) and provides over-all gain of 0 dB at the mid-range of expansion. The S/N is a function of signal level, but the maximum is 80 dB.

The circuit technique is extended readily for use with stereo or quad applications (Fig. 8). You can choose to expand all channels together, derive individual control signals from each channel or obtain the signal from a summation of two to four channels.

If volume compression is needed, bias the FET on for low signals and let increasingly larger signals bias the FET off. The distortion is greatest at large signal levels (low gain) but still acceptably low, usually less than 0.1%. And the circuit is a logical mate to the expander. • •
Four new series of Schottky Barrier Rectifiers are now available from Varo Semiconductor, Inc. They are rated at 1A, 3A, 5A, and 15A (I(T)) with 20V and 30V (Vbr). Features are: Extremely fast recovery (ttr), very low forward voltages (Vf), high reliability and low cost.

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VSK 320 & 330, the 3A devices have 475 and 500mV (Vf); 250A peak 1/2 cycle surge and 75mA (Iir) at 100°C. Both the 3A and 5A series are in axial lead, epoxy packages.

The VSK 1520 & 1530 —15A series are in DO-4 metal stud cases and have 550mV (Vf); 300A peak 1/2 cycle surge and 75mA (Iir) at 100°C. All devices have a junction operating temperature range of -65°C to +125°C.

Typical pricing in 1000 qty ranges from $1.38 ea. (VSK 120) to $3.87 ea. (VSK 1530).
An Open Letter To Manufacturing Managers.

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Know your a/d converter's dynamic range.
There are three basic definitions, but you had better consider your application before trying to interpret them.

If you select an analog-to-digital converter based on the manufacturer's specification of dynamic range, be careful. Manufacturers use three different definitions to specify dynamic range. One highlights linearity, another sensitivity and the third distortion. Each is correct, but which will be useful to you depends entirely on your application.

The differences may be summarized as follows:

Linearity is important when precise arithmetic processes must be performed, such as in digital filtering. One actual instance is in the moving target indicator filter, or "clutter canceler," used in some radar systems. Insufficient dynamic range cuts into the subclutter visibility—the ability to detect a small signal that has doppler offset in the presence of large stationary signals.

Sensitivity is vital in ensemble arithmetic processes, such as correlation. One example of this is digital pulse compression or matched filtering. Each individual arithmetic calculation may be buried in noise, but the ensemble of all calculations provides the correlation gain.

Distortion is critical in frequency-sensitive arithmetic processes, such as transform algorithms. One of these is the inherently high-dynamic-range fast-Fourier transform. Spurious output products generated in the a/d conversion appear as artifacts (internally generated signals) aliased into the data.

Linear range: What is it?

What is linear dynamic range? It can be defined as the range of input values over which the digitized output value does not depart by more than 3 dB (Fig. 1). The input-voltage samples quantized by a/d converters are usually transformed into a binary output. A converter that delivers n bits can resolve an input voltage into 2^n discrete equally spaced values. Each bit output from the converter represents a doubling of the input voltage or a 6-dB change. The least-significant bit (LSB) is usually ambiguous—the accuracy of conversion is limited digitally to ±0.5 LSB.

The LSB error is only the quantization error and does not include analog errors due to a/d converter component tolerances or sampling errors due to aperture time (sampling gate uncertainty times the highest radian frequency present). Since the maximum signal error is ±0.5 LSB, the true signal value is equally likely to be found anywhere within the error band. Thus we can say that the average error will be ±0.25 LSB.

Sensitivity given in decibels

The sensitivity of an a/d converter is always 1 LSB, since an analog input voltage change equivalent to 1 LSB must occur to change the output state. The dynamic range of a converter is the span of signal amplitudes that the converter will quantize to within a predetermined accuracy.

As the input voltage decreases, the converter's binary count output decreases. It drops to the next lower number as the input passes the halfway point between the nominal voltage steps. For a 10-bit bipolar converter that is designed to digitize a voltage span from −5 to +5 V, the changes in output codes occur at 10-mV intervals. For the plot in Fig. 1, the ±3 dB departure occurs between the first and second bits, with an input voltage of −51 dB relative to full amplitude.

At the full-scale positive end, the digital output count should not exceed binary 511, since 512 would appear as the two's-complement form of the full-scale negative value. A well-designed a/d converter uses "saturation arithmetic" and will hold its plus sign (ZERO) and all ONEs for inputs that exceed full-scale positive. And likewise for the minus sign (ONE) and all ZEROs for inputs exceeding full-scale negative.

This overrange capability allows another 3 dB for excursions and justifies a 54-dB rating for the a/d converter's linear dynamic range. A handy method of computing the linear range of a converter that resolves to n bits is

\[
\text{Dynamic range} = 6(n - 1) \, \text{dB}.
\]

John D. Fogarty, P.E., 5130 Rondel Pl., Columbia, MD 21043.
The binary count output vs the input voltage amplitude is easily converted into a decibel scale.

Only unipolar converters with no sign bit can produce a true 6n-decibel linear dynamic range. The sensitivity dynamic range is expressed in decibels and is the ratio of the full-scale output to the minimum discernible signal. In a converter this signal is limited by the quantization noise or uncertainty in the LSB. If you use the conventional definition of tangential sensitivity, found in noise-figure analysis, the minimum signal equals the noise power. Thus the dynamic range equals the signal-to-noise ratio of the full-scale output to the quantization noise:

$$\text{Dynamic range (dB)} = 10 \log_{10} \left( \frac{1}{N_q} \right) = -10 \log_{10} N_q.$$  

To derive the quantization noise power, $N_q$, assume that the input signal has uniform distribution (equally probable) and the converter output can change only in steps of the least significant bit. Thus the analog excursion that causes an output change of 1 LSB is $q$ (Fig. 2). The
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3. A uniform distribution is rectangular and spans $-q/2$ to $+q/2$ when $p(x) = 1/q$.

noise power is the mean-squared value of the input voltage, $x$, required to produce the change.

$$N_q = \langle n^2 \rangle = \int_{-q/2}^{+q/2} (x - x_0)^2 p(x) \, dx.$$  

For uniform distribution (Fig. 3), $p(x) = 1/q$. This can now be simplified if you let $x_0 = 0$ to result in the expected value of $n^2$ of

$$\langle n^2 \rangle = \int x^2/q \, dx = \frac{1}{q} \left[ \frac{x^3}{3} \right]_{-q/2}^{+q/2} = \frac{q^2}{12}.$$  

If you put this value of quantization noise back into the dynamic-range definition, you get:

Dynamic range $= -10 \log_{10} (q^2/12)$

$= -20 \log_{10} q + 10.8.$

An n-bit a/d converter (including sign bit) has $2^n - 1$ possible output magnitude states. Therefore, for unity full-scale output, the smallest step, $q$, must be equal to $1/2^{n-1}$. If this value is again substituted into the dynamic-range definition, you get:

Dynamic range $= 20 \log_{10} 1/2^{n-1} + 10.8$

$= 6.02n + 4.78.$

This result can be rounded off to $6n + 5$ dB. With this new definition, for example, a 10-bit a/d converter has a range of 65 dB.

Distortion based on overload

When distortion is used as a measure of dynamic range, it is specified in decibels as the ratio of the minimum discernible signal to an input signal that produces spurious responses equal to the minimum discernible signal. Since this definition is based on experimental measurements of a system in overload, the results are not generally calculable.
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INFORMATION RETRIEVAL NUMBER 36

———

INFORMATION RETRIEVAL NUMBER 79
Recognize hand-printed characters with a simple algorithm. And only a small amount of hardware is needed to identify a full set of numbers.

It's easy for a logic circuit to "recognize" hand-printed characters. Surprised? The algorithm is extremely simple when the system is limited to numbers and a few other symbols.

The circuit need only record the regions where a hand-printed character begins and ends. These first and last regions, properly encoded, then address a PROM look-up table to provide the ASCII code for the hand-printed number. The characters are drawn on a standard data-tablet input system.

Consider a paper form preprinted with boxes, in which the characters are hand-printed. The dimensional aspect ratio of each box is 3 x 4, but each box is divided into nine areas, numbered as in Fig. 1a. Though the recognition task could include the direction, sequence and other characteristics of each stroke, not all of this information is needed for capturing only numbers from zero to nine plus four other symbols. Only the starting and ending points are needed (Figs. 1b and 2).

Conventional written symbols are used, unlike those in optical character-recognition systems (OCR), and little training in recognizing or writing the characters is needed. Surprisingly, the only instance where an ambiguous result is likely to occur—but is easily avoided—is in the case of the number 4.

Note that an "open" number 4 can be confused with the number 7, if the 4 is started in area 2 and ended in area 8 (Fig. 2). An open 4 must begin with the down stroke first—start in region 4 and end in 8 for the first stroke. Then a number 4 with an 8-6 or 4-6 code (for the complete character) is uniquely recognized by the circuit. This is the only special "training" needed to use this algorithm.

The preprinted paper form is placed on a standard data tablet, available from several manufacturers. The data-tablet system converts pen position to binary-coded coordinate outputs

Data tablet reads the writing

The data tablet divides each macro box into 128 x 64 position outputs, which the accompanying logic circuit partitions into the nine active micro regions surrounded by dead zones (Fig. 4). The over-all size of the macro box is arbitrary, and boxes can be placed throughout the page in any regular pattern.

Lines delineating the micro regions within each macro box need not be included on the preprinted form, though the lines are useful during the first minutes of training.

The system recognizes the completion of a character when it detects a transition from one preprinted box to another—a macro jump. A 1-s interval with no macro jump is also a signal for a character's completion.

The logic circuit for this character-recognition method uses a relatively small amount of TTL hardware. The operation of the circuit can be

Albert Whetstone, Technical Director, and Stephen Domyan, Design Engineer, Summographics Corp., 35 Brentwood Ave., Fairfield, CT 06430.
State flow chart for hand-printed number recognition

STATE 0 INITIALIZE ALL REGISTERS
SET TIF • 0

STATE 1 TRIGGER THE 1 sec TIMER

STATE 2
CHECK DATA AVAILABLE FLAG FROM DATAMARKER

STATE 3 LOAD X & Y COORDINATES INTO THE X & Y REGISTERS
DEAD ZONE IF X & Y COORDINATES ≠ DEAD ZONE

STATE 4 DATA READY

STATE 5 LOAD OLD & NEW MACROS

STATE 6 CHECK TIF FLAG
TIF • I
LOAD OUTPUT REG

STATE 7 LOAD LAST MICRO REGISTER

STATE 8
CHECK TIF & TIF FLAG
TIMEOUT AND / OR TIF • 0
LOAD LAST MICRO REG

STATE 9
LOAD FIRST MICRO REGISTER
LOAD MACRO REGISTER
SET TIF • 1

STATE 10
TIMEOUT AND TIF • 1
LOAD OUTPUT REG

PROM truth tables

<table>
<thead>
<tr>
<th>ADDRESS</th>
<th>OUTPUTS</th>
</tr>
</thead>
<tbody>
<tr>
<td>X Y</td>
<td>B B B B</td>
</tr>
<tr>
<td>A A A A</td>
<td>0 0 1 0</td>
</tr>
<tr>
<td>0 0 0 0</td>
<td>0 0 0 1</td>
</tr>
<tr>
<td>0 0 0 1</td>
<td>0 0 1 1</td>
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<tr>
<td>1 0 1 1</td>
<td>1 1 0 1</td>
</tr>
<tr>
<td>ALL OTHERS 0 0 0 0</td>
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Y-micro PROM

<table>
<thead>
<tr>
<th>ADDRESS</th>
<th>OUTPUT O, O,</th>
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</thead>
<tbody>
<tr>
<td>0—4</td>
<td>1 1</td>
</tr>
<tr>
<td>5—28</td>
<td>0 0</td>
</tr>
<tr>
<td>29—35</td>
<td>1 1</td>
</tr>
<tr>
<td>36—59</td>
<td>0 1</td>
</tr>
<tr>
<td>60—66</td>
<td>1 1</td>
</tr>
<tr>
<td>67—90</td>
<td>1 0</td>
</tr>
<tr>
<td>91—127</td>
<td>1 1</td>
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X-micro PROM

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<thead>
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<th>ADDRESS</th>
<th>OUTPUT O, O,</th>
</tr>
</thead>
<tbody>
<tr>
<td>0—4</td>
<td>1 1</td>
</tr>
<tr>
<td>5—17</td>
<td>0 0</td>
</tr>
<tr>
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<tr>
<td>39—45</td>
<td>1 1</td>
</tr>
<tr>
<td>46—58</td>
<td>1 0</td>
</tr>
<tr>
<td>59—63</td>
<td>1 1</td>
</tr>
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</table>

Micro-to-ASCII converter PROM

<table>
<thead>
<tr>
<th>ADDRESS</th>
<th>OUTPUT</th>
</tr>
</thead>
<tbody>
<tr>
<td>A A A A</td>
<td>O, O, O, O,</td>
</tr>
<tr>
<td>0 1 0 0</td>
<td>0 0 0 1</td>
</tr>
<tr>
<td>0 0 1 0</td>
<td>0 0 1 0</td>
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<td>0 0 0 1</td>
<td>0 0 1 0</td>
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<td>0 0 1 1</td>
</tr>
<tr>
<td>1 0 1 1</td>
<td>0 0 1 1</td>
</tr>
</tbody>
</table>

CHARACTER
ONE
TWO
THREE
FOUR
FIVE
SIX
SEVEN
EIGHT
NINE
ZERO

2. All the standard numerals plus four other symbols can be identified by a two-number begin/end code. Only the open number 4, if improperly drawn, can confuse the system. It will have the same code as number 7.

4. Each macro box on the preprinted form is scanned by the data tablet, and the pen's coordinates are identified by the codes shown in each micro box. The dead zone corresponds to the 1111 code.

3. A standard data-tablet system with a preprinted overlay sheet serves as the input to the character-recognition system.

followed easily with a flow chart (see chart) and block diagram (Fig. 5).

Following the logic

In the data-tablet system used, the pen position is sampled about 30 times a second, and 10-bit binary X and Y coordinates of the pen enter the recognition electronics for each sample. A translate-initiate flip-flop (TIF) in the character-recognition sequential circuit starts the cycle. A data-available flag from the data-tablet circuit loads the 10-bit X and Y coordinates into the X and Y registers. The six least-significant bits (LSBs) of the X coordinate form the X-micro word, and it addresses the X-micro PROM. Seven Y LSBs address the Y-micro PROM.

Output codes of the two micro PROMs provide the address for the S/C (stroke-code) PROM. Note that all ONE outputs of the two micro PROMs are ORed and designate a dead zone. And the S/C PROM converts its 4-bit sequentially numbered inputs into a special code (see PROM truth tables).

S/C codes of the first and last stroke positions are stored at the proper time in the sequence in corresponding registers. These two registers—the first and last micro registers—then form the 8-bit address for the micro-to-ASCII code converter PROM. This PROM needs to provide only four of the seven bits used in an ASCII character code, because in the numbers and the four other characters recognized by the system (Fig. 3) the remaining 3 bits are identical. Thus these bits can be hard-wired at the output connector to provide the full code.

The X and Y coordinates' most-significant bits (MSBs)—four X bits and three Y bits—form
5. Character-recognition block diagram shows how the coordinates of a character's start and end regions are combined to address character-recognition PROMs. The output words then address a micro-to-ASCII ROM.

6. All but seven of the ASCII alphanumerics begin with these five strokes. Only a 3-bit code—the LSBs of the S/C micro-region codes—is needed to identify the strokes (see Fig. 4).

common first strokes are shown in Fig. 6. These encompass all but seven characters of the ASCII alphanumeric set.

An expanded system could make use of the S/C PROM's special output code to identify the strokes. The code provides a form of data compression. Since each micro box is labeled with four bits, it seems at first that a three-box stroke would need 12 bits to label it. However, the five strokes of Fig. 6 can be identified by only a 3-bit code. The three LSBs of the S/C output for each micro box provide unique 3-bit combinations for each stroke.

Thus five 3-bit words can divide the total character set into five groups, or dictionaries. A sixth dictionary would contain those few characters that do not use the five common initial strokes. Thereafter, within each dictionary, other discriminants would identify the character uniquely.

The same discriminants need not be used in each dictionary; one may be more effective than others in a particular dictionary. ■

Expanding the system

Additional characters can be included in the recognition repertoire, but confusion soon sets in with this simple approach. More powerful discriminants must be used to handle the entire ASCII set. Since characters are created dynamically in real time with a data tablet, many character-formation features can be analyzed:

- The sequence in which the parts of the character are created.
- The speed of each character stroke.
- The number of direction reversals in the X or Y coordinates.
- Whether the Y velocity is high or low when X changes direction, and vice versa.

And many other discriminants can be added to this list.

The dynamic nature of a data-tablet input contrasts with OCR, where a static character is scanned and merely analyzed into black and white areas. No history of the way the character is created can enter the OCR analysis.

An extension of the character-recognition system to the full ASCII set is under study. Preliminary experimental results indicate that the location of the first stroke of a character is an additional excellent discriminator. The five most
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The limit circuit in the figure can be patched in series with almost any dual power supply to provide dual current (±V) limiting, selectable at value of 5 or 25 mA. Two LEDs each independently display an overload condition in a section of the supply. This feature is particularly valuable during breadboard and prototype testing. The limit circuit can be used on variable supplies from ±5 to ±22 V. The limiter requires no other power. The small voltage drop of about 0.3 V in each line caused by the limit circuit is negligible for most applications.

Since both halves of the circuit work in the same way, let's consider only the top half. Transistor Q₁ and R₁ form a bipolar current source, which is biased into operation by Q₂ and R₂, and the constant current delivered by the FET current source, Q₃ and R₃. The FET current is held constant to within 10% over the entire voltage range of the circuit. The output current is selected with R₄. The values of R₅ (R₂₀ or R₂₆) provide limits of approximately 5 or 25 mA. Other values can be used to provide different limits.

When Q₄ is not in a current-limit condition, its Vᵦₑ is low. When Q₄ goes into current limit, Vᵦₑ increases, which turns on the Darlington-connected Q₂, Q₃ combination and LED 1 to show the overload condition.

Transistor Q₄ is a large-geometry transistor that provides minimal saturation voltage and adequate worst-case power dissipation. Transistor Q₄ is identical to Q₃, so that accurate biasing of Q₄ can be achieved with minimal voltage drop across resistors R₃ and R₄.

For a fixed voltage supply, the constant-current source, Q₁ and R₁, can be replaced by a single resistor. For 5 mA, its value would be approximately

\[(2 \text{ V}_{\text{in}} - 1.9) / 0.005 = R.\]

Mark Stitt, Burr-Brown Research Corp., International Airport Industrial Park, Tucson, AZ 85706.

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INFORMATION RETRIEVAL NUMBER 32
Programmable unijunction transistor protects op amp from overvoltages

To protect an op-amp input from overvoltages, zener diode clamps often are used. But this solution doesn't work in high-impedance applications where the zener's reverse current may be too high. A programmable unijunction transistor (PUT) can solve this problem.

The leakage current of an MPU-131 PUT is only 5 nA in the unfired state. This makes the PUT suitable to protect even FET input circuits, without a substantial effect upon the input characteristics.

In the figure, the MPU-131 protects an LM-311 comparator against voltages higher than $V_p$. A 7400 gate drives an overvoltage-indicator LED. Adjustment of $R_2$ can vary $V_p$ from 1 V to $V_{cc}$. Removal of input overvoltage restores circuit.

H. Thomas, Zurich, Switzerland.

Function generator produces sine, square and triangular waves

A frequency range of six decades can be obtained with a single control in a sine-square-triangle function generator. It operates from below 10 Hz to 1 MHz with usable output to about 2 MHz.

The triangle wave is generated when switched current-source transistors $Q_1$, $Q_3$, $Q_4$, and $Q_5$ alternately charge and discharge timing capacitor $C_1$. This action generates a linear triangle wave follower without use of an op-amp integrator. A FET voltage follower, LH 0033C, buffers the triangle wave and drives the comparator, output amplifier and sine converter.

A precision dual comparator, LM319, sets the peak-to-peak amplitude of the tri-wave. It's essential to accurately control the tri-wave amplitude, since the sine converter requires close amplitude control to produce a low distortion output. The tri-wave is applied to the comparator inputs via divider network, $R_2$, $R_3$, and $C_5$. The comparators switch when the amplitude of the tri-wave is $\pm 2.5$ V. Capacitor $C_5$ compensates for delays in the comparator at high frequencies.

A square-wave output from the comparator appears at the emitter of $Q_6$, which drives the current switches and, when selected, the output amplifier. The current switches provide a 5-nA-to-5-mA current to timing capacitor $C_1$. The maximum output current is set by $R_{10}$ and $R_{11}$. It appears when the arm of the frequency control, $R_{11}$, ties all four emitters together. About 380 mV is developed across $R_{11}$, and this voltage corresponds to over a $10^6$ change in charging current.

Transistors $Q_6$ and $Q_7$ form a differential amplifier with emitter degeneration. The triangle wave is attenuated by $R_5$ and $R_6$ to about 450 mV and applied to $Q_6$. This drives the transistors nonlinearly to produce a sine-wave output current at the collector of $Q_6$, which then drives the output amplifier.

The output amplifier, an LM318, with feedforward compensation to maximize bandwidth and slew rate, scales all three waveforms to $\pm 10$ V. But even with the feedforward there is not enough bandwidth for good reproduction of the triangle or square wave at frequencies over 1 MHz. If the higher frequencies are of major importance, an external active filter can be used to improve performance.
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For further information on the Amperex line of high-performance, GHz-range transistors, write: Amperex Electronic Corp., Solid State and Active Devices Div., Slatersville, Rhode Island 02876, or phone (401) 762-9000.

<table>
<thead>
<tr>
<th>A GHz Transistor-Line Sampler</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>BFT24</strong></td>
</tr>
<tr>
<td>f_t (GHz) .......... 2.3 @ 1 mA</td>
</tr>
<tr>
<td>N.F. ............... 3.8 dB @ 500 MHz</td>
</tr>
<tr>
<td>M.A.G. ........... 17 dB @ 500 MHz</td>
</tr>
<tr>
<td>Price............. $2.10 each*</td>
</tr>
<tr>
<td>Package .......... Plastic Micro-T</td>
</tr>
</tbody>
</table>

| **A400**                     |
| f_t (GHz) .......... 5 @ 14 mA |
| N.F. ............... 2.3 dB & 200 MHz|
| M.A.G. ........... 18.5 dB @ 500 MHz|
| Price............. $2.38 each* |
| Package .......... TO-72 Metal |

| **A401**                     |
| f_t (GHz) .......... 5 @ 30 mA |
| N.F. ............... 1.8 dB @ 200 MHz|
| M.A.G. ........... 14.5 dB @ 500 MHz|
| Price............. $2.62 each* |
| Package .......... TO-72 Metal |

| **BFR91**                    |
| f_t (GHz) .......... 5 @ 30 mA |
| N.F. ............... 1.9 dB @ 500 MHz|
| M.A.G. ........... 16.5 dB @ 500 MHz|
| Price............. $2.95 each* |
| Package .......... Plastic Micro-T |

| **BFR94**                    |
| f_t (GHz) .......... 3.5 @ 90 mA|
| N.F. ............... 5 dB @ 500 MHz|
| M.A.G. ........... 13.5 dB @ 500 MHz|
| Price............. $7.25 each* |
| Package .......... Stripline Stud |

* In 1000 piece quantities

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INFORMATION RETRIEVAL NUMBER 33
IDEAS FOR DESIGN

interest, a faster output amplifier is necessary.

The transistors that determine the timing current should be made to track with temperature changes. Small heat sinks should be used to thermally couple Q1 and Q2 to Q3 and Q4. Temperature differences between the pair will cause the wave symmetry to change.

To adjust the system, first set R11 for a 1-MHz output. Then adjust the output symmetry with R16. Now reset R11 to a 10-Hz output and adjust the symmetry again, but this time with R11.

Other adjustments may be necessary in the sine converter. Resistor R1 can be trimmed if the sine output from the LM318 has a dc offset. Also, it may be necessary to adjust R1, to minimize distortion. There can be considerable distortion if the tri-wave is not symmetrical and does not have equal slopes.

Robert C. Dobkin, National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, CA 95051.

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'Bucket' circuits used for weighted summing

Transversal filters using bucket-brigade circuits in a new weighted-summation technique have been developed at the Technical University of Budapest. The new technique is reported to be an improvement over the more usual methods for weighted summing, such as capacitance-splitting or gate-tapping with a FET source-follower network.

The Hungarian circuit uses a passive network and a node-tapping summation procedure. The simplest version is shown in Fig. 1. A simplified schematic is given in Fig. 2. Here the large rectangle is a capacitive m-pole passive network. The filter design satisfies the following general requirements:

1. The charge is retained by the capacitances.
2. There is no stray coupling between elements of the array to make the filter dispersive.
3. Multiple-outputs with different weightings are available.
4. The output level is independent of the driving-signal frequency.
5. Rectangular output pulses are produced.

Timing circuit uses step-recovery diodes

Step-recovery diodes have been used in a new circuit for short-delay timing in high-speed signal-processing, such as in a/d converters. Variable timing is an important advantage of the new circuit over the use of fixed delay lines. Timing pulses of 2 to 100 ns can be generated with very short rise and fall times and at pulse repetition rates between 1 and 140 MHz.

The practical monostable circuit was developed by Cambridge Consultants Ltd., Cambridge, England. A shortcoming of the step-recovery diode—recovery delay when the current though it is reversed—is eliminated by the back-to-back juxtaposition of recovery diodes, $D_2$ and $D_3$. The charge built up during the forward-current phase is passed back and forth between the diodes on current reversals. Thus the output-pulse rise and fall times can be kept very small.

The input applied to $Q_1$ has a minimum duration of 5 ns. The pulse turns off emitter-follower $Q_4$, and causes current to flow through $D_2$, $D_3$, and $Q_4$. The current also flows through $Q_4$, latching the input for the duration of the output pulse that appears at the collector of $Q_4$. The pulse duration is determined by the charge stored in $D_3$.

A no-energy approach to frequency modulation

Frequency modulation that requires no energy to shift the frequency has been achieved at Philips Research Laboratories in Eindhoven, the Netherlands. Normally the variation of capacitance in a harmonic oscillator requires energy to change the signal frequency. The Philips device avoids this by using a gyrator circuit that, in oscillation, has energy flowing back and forth between two capacitors.

As a result, no energy is stored or lost. Varying the gyration transconductance gives frequency variation without change of phase or amplitude—that is, ideal frequency modulation.

The Philips gyrator circuit is a conjunctor oscillator (described by S. Duinker in Philips Research Reports, 1962, pp. 1 to 19). Amplitude control is possible through instantaneous feedback in proportion to the signal, which is compared with a reference. The $Q$ factor of the resonant circuit is made to be almost infinite by a difference-signal feedback. In practice, the measured performance has shown that neither large frequency deviations nor high modulating frequencies result in distortion.
After all the noise, the quiet logic of HiNIL and 74C CMOS keeps you on the right track.

May 10, 1869. Promontory, Utah. The rumble of wheels, the hiss of escaping steam, the shouts of the celebrating crowd filled the skies with a deafening roar when they drove the golden spike that joined the Central Pacific and Union Pacific Railroads.

But today, when you link Teledyne's high noise immunity logic, HiNIL, and our 74C CMOS together in your digital or analog/digital control designs, you'll no longer have to worry about spikes or noise. Teledyne invented HiNIL to meet the need for high noise immunity found in practically all digital systems. The success of this large and still growing family has made Teledyne a leading supplier of logic for high noise applications.

Just put HiNIL on input-output lines to block heavy noise transients and drive high current peripheral devices. And use CMOS in the middle to minimize power dissipation and increase speed and circuit density. The combination of HiNIL's guaranteed 3.5V noise margin and 74C's low power dissipation lets them quiet almost any kind of system with high noise problems.

Our two logics interface directly, too. Standard 74C drives HiNIL directly and HiNIL drives more than 50 CMOS loads. Simply connect both to an inexpensive 12 or 15V ±1V power supply. You can even connect linear circuits to the same supply for extra savings.

HiNIL eliminates the need for drivers because it sources up to 15mA and sinks up to 65mA. That's ample capability for display tubes, LEDs, lamps and relays.

And with HiNIL you save on filter capacitors, get the extra flexibility and economies of diode-expandable inputs, and have a choice of active or passive pullup and open collector outputs. There's plenty of board-shrinking MSI in both families, too.

So write or call Teledyne today to find out about our HiNIL and 74C CMOS lines. We'll show you how easy it is to block out all the noise and stay on the right track.

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INFORMATION RETRIEVAL NUMBER 38

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INFORMATION RETRIEVAL NUMBER 39

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INFORMATION RETRIEVAL NUMBER 40
Electronic Design 3, February 1, 1975
Ribbon coax-cable design allows gang stripping and easy assembly

AMP Inc., Harrisburg, PA 17105. (717) 564-0100. See text.

Engineers need no longer accept degraded performance in high-speed and high-frequency systems because conventional coaxial cable is costly, bulky and difficult to terminate. AMP's new flat-ribbon, flexible, multiple-coaxial-cable assemblies meet most all of these objections.

The new coax cable is precision-made and designed for easy, mass termination. The bulk is reduced, since individual cables are spaced accurately—only 0.1 in. apart for presently available 50, 75 or 93-Ω assemblies, or 0.125 in. on a larger 95-Ω ribbon, available soon.

Coax cable, in both conventional single and flat multiple-conductor form, has been available for many years. But all of the previous multiple forms have been only ribbonized constructions of individual cables. And whether they were woven, laminated, chemically or heat bonded to make a flat package, the termination of the cables was still an individual, tedious operation.

In AMP's new cable assembly, each cable in a ribbon has its own center conductor, dielectric and shield. The center-conductor size, dielectric material and dielectric outside diameter are varied to provide the different characteristic impedances. But each center conductor is located on a predictable centerline-to-centerline spacing. The solid-wire center conductors are used for ease of wire stripping and termination.

The shield, a foil and drain-wire construction of aluminized Mylar totally covers the coax core. And the solid drain wire acts as a low-resistance path and way to terminate the shield.

The drain wires are also located on predictable spacings. Because both center conductors and drain wires are in known locations, mass stripping and terminating is possible.

The stripping action removes the foil shield together with the cable jacket to expose the drain wire and center conductor. The dielectric on the center conductor may be stripped or left in place.

Braid is not used because it is not easily gang-stripped or terminated. Also, braid uses an expensive form of copper and is bulky. And a single, solid wire at a known location can be controlled more readily. In addition the foil is removed easily with the jacket during stripping.

The cable design is an optimized compromise of factors such as size, mass-termination requirements, efficiency and economics. Losses in the dielectric and center conductor are major considerations. The larger the center conductor, the lower the resistive and skin-effect losses. Below 1 GHz, attenuation is mainly due to resistive loss. Skin-effect becomes increasingly important at higher frequencies. A good balance for the 0.1-in. center-to-center distances is a 28-AWG wire for 50-Ω cable and a smaller 30-AWG wire for the 75 and 93-Ω cables. The conductor material is tin-plated solid copper.

The dielectric for the higher impedance cables is a foamed polypropylene or polyethylene. The 50-Ω cable uses solid polypropylene. The use of a low dielectric-constant material for high-impedance designs (continued on page 96)
Intronics offers a high efficiency line of modular, compact DC to DC Power Converters, specifically designed for high input/output isolation. Each unit will convert a single unregulated DC voltage source to dual regulated output voltages and can be used to replace a separate AC input power supply many times its size. The compact design also ensures convenient circuit card mounting near the point of application, thus eliminating ground loop problems. Floating, tracking outputs with excellent regulation, low temperature coefficient, low output noise, current limiting to 150% of full load, current and maximum power source protection are additional advantages you can expect from these Intronics' models, all at a competitive price.

Features include:
- 5, 12, 28VDC Inputs
- ±12VDC, ±15VDC Outputs, at 25 or 100mA
- 10° ohms Input/Output Isolation
- 1% Preset Output Accuracy
- .02% Line/Load Regulation

Whether your design is for medical electronics, portable test equipment, ocean going or other mobile applications, specify Intronics' DC to DC Converters.

Engraving tool uses solid carbide tip

Mountain West Alarm Supply Co., 4215 N. 16th St., Phoenix, AZ 85016. (602) 263-8331, $15.75 (unit qty).

The D12 electric engraver permanently marks valuables to permit fast identification and quick recovery in case of theft. The engraver permanently marks steel, plastic, copper, brass, wood, or glass. A replaceable carbide tip is driven by a high-speed reciprocating motor at 7200 strokes per minute. The solid carbide tip is practically wearproof. A calibrated stroke-adjustment dial regulates length of stroke. The depth of engraving can be set from fine lines to deep marks. For continuous duty, a diamond point is available. The unit weighs just 2 lb and operates from 115 V ac at 60 Hz.

Set lead bender size with micrometer screw


Model N-300 lead bender is now equipped with a fine-pitch adjusting screw for smooth micrometer adjustment of bend spacing. The adjusting screw is permanently dry lubricated. Standard features include strain relief between component and bend, replaceable plastic guides and a rigid hard anodized aluminum frame. The unit eliminates measurement and trial-and-error bending of component leads. You match the pointers with eyelet holes in the circuit board and spin the knurled wheel with the thumb to automatically space the bends. All axial lead components to 1/2-in. x 1-1/2-in. long with maximum distance between inside of bends of 1.725 in. are accommodated.
Learn digital design with instruction kit

E&L Instruments, Inc., 61 First St., Derby, CT 06418. (203) 735-8774.

The LR Innovator series, for teaching digital electronics, includes modular hardware, called Outboards. The modules plug directly into an SK-10 solderless breadboarding socket. This allows the student to experiment with different digital-logic components. Over 750 pages of instructions and 90 experiments are supplied for self-programmed study. As new developments in digital electronics become available, the manufacturer will provide new modules and software to cover them.

CIRCLE NO. 304

Instrument knobs fasten without set screws

Interlock, 770 Airport Blvd., Burlingame, CA 94010. (415) 348-5625.

The Collet Knob has no set screw. This new knob is secured by means of a collet that tightens around the entire shaft to provide a tight-fitting, perfectly-aligned knob. The knobs are available in two styles, five sizes and hundreds of combinations of pointers, figure dials, stators and colored caps. The sizes available are 10, 14.5, 21, 28 and 36 mm. Different colored caps can be used to identify knobs. The basic knob can have different components added with ease.

CIRCLE NO. 305

Before you order switchlights, we challenge you to compare our low cost
"Persuader Line" feature for feature with other leading brands

We're the kind of firm that believes in more than one gun barrel and plenty of ammunition. So when you add our familiar S410* series to our new S190* series, you'll find we have a very convincing line of general purpose switchlights indeed. It's "The Persuader" —the line we invite you to compare for low cost, quality and versatility with that of any other manufacturer. Just check the list below, then get in touch with your local distributor for exact specifications. And we're easy to find... located in major cities world wide.

<table>
<thead>
<tr>
<th>Standard Features</th>
<th>Clare-Pendar &quot;Persuader&quot;</th>
<th>Micro</th>
<th>Dialight</th>
<th>Other</th>
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<tr>
<td>1. Low Cost</td>
<td>YES</td>
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<td>2. Distributor Stock</td>
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<td>3. U.L. Listed</td>
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<td>4. 2 Form C</td>
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<td>5. Wiping Contacts</td>
<td>YES</td>
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<td>6. Snap Action Contacts</td>
<td>YES</td>
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<td>7. 10 amp Rated</td>
<td>YES</td>
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<td>8. 2 amp Rated</td>
<td>YES</td>
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<td>9. 100,000 Cycle Life</td>
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<td>10. 6 Lens Shapes</td>
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<td>11. Split Lens Displays</td>
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<td>12. Solid/Proj. Displays</td>
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<td>15. Snap-In Mount</td>
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<td>17. Gang Frame Mount</td>
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<td>18. Quick Connect Trim.</td>
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<td>19. Engraved Legends</td>
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<td>20. Alt. Remain-In</td>
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<td>21. Mom./Alt./Indicator</td>
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*S190 $1.62 in quantities of 1000
*S410 $2.53 in quantities of 1000

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Add-on memory for mini uses 4-k RAM on a board


The Monostore VII/Planar is a single-board semiconductor memory system, with 12k x 16 organization, that fits a PDP-11 small-peripheral slot. Based on a 4096 x 1 NMOS RAM, the memory is hardware and software compatible with the PDP-11. It operates from the small-peripheral-slot power sources of 5 V and -15 V. Access time of 500 ns and cycle time of 700 ns allows maximum use of the bus speed. Existing programs can be used without modification. The small-peripheral-slot compatibility simplifies machine organization since the minicomputer can be ordered with minimum memory and all slots wired for small peripherals. The Monostore VII/Planar memory can then be added as required for a particular application. Two Monostore VII boards give more capacity than that given by four conventional boards. Power dissipation is 22 W at full speed, and 15 W in standby.

CIRCLE NO. 306

Pipelined array device does FFTs in 250 µs

Spectra Data Inc., 18758 Bryant St., Northridge, CA 91324. (213) 993-1622. $50k to $250k; 120 to 150 days.

Model 2000 array processor uses pipeline operation and can transform 1024 complex points in 250 µs. The unit also does forward or reverse FFT. To attain these high speeds circuits are dedicated to a stage of the FFT algorithm; each stage sends results to the next until the results pour out of the last stage. The unit accepts analog or digital data and handles arrays as large as 8192, 32-bit words.

CIRCLE NO. 307

Calculator-style unit is remote PDP-8 console

Douglas Electronics, 718 Marina Blvd., San Leandro, CA 94577. (415) 483-8770. $700; stock.

A small calculator-type keyboard with seven segment LED octal display performs remotely all of the standard functions of the PDP-8/e programmer's console. The Model RFP-80 operates with or without the standard front panel. Current memory address and selected register contents are continuously displayed. Choice of display, data entry and various instructions are rapidly accomplished with simple push-key operation. Debugging programs and temporary control of turnkey systems are therefore easier. Additional time is saved by not having to mentally convert from binary to octal and then back to binary when entering or reading data. The RFP-80 package includes a plug-in interface board, a thin 10-foot interconnecting cable and plexiglass front panel to replace the PDP-8/e front panel.

CIRCLE NO. 308

A/d converter sends results over phone line

Elographics, Data Systems Div., P. O. Box 388, Oak Ridge, TN 37830. (615) 482-4038. See text; 60 days.

The Datamat 11A analog-to-digital converter connects any analog output device to existing data transmission lines. The stand-alone unit accepts the analog voltage then formats, encodes and serializes it. Outputs are Serial ASCII with EIA RS-232C current loop, and parallel BCD; all provided simultaneously at rear panel connectors. Baud rate is selectable from 110 to 1200. The 11A can optionally accept data from several sources. In addition the unit can be inserted between existing communications components (e.g., between TTY and minicomputer or TTY and modem) without interfering with prior data transmissions. The standard Datamat 11A is equipped with its own 3-1/2-digit LED display or optionally with a four-digit display. The 11A with 3-1/2 digits costs $1395 or $1495 for four digits.

CIRCLE NO. 309

Acquisition system has amp on each channel

Tustin Electronics Co., 1431 E. St. Andrews Pl., Santa Ana, CA 92705. (714) 835-0677. $300 to $400 per channel; 60 to 90 days.

System 2400 for data acquisition features a digital gain-controlled amplifier for each channel. The unit provides 1 to 10,000 in decade ranges. CMRR is 160 dB and 140 dB at gains of 10,000 and 1000, respectively. Amplifier bandwidth is 100 kHz for all values of gain. Input offset voltage is 1 µV and offset current is 1 nA at 25 °C. Two to six-pole filters are optional. System throughputs are 650 kHz, 275 kHz and 100 kHz for 12-bit systems and 500 kHz, 200 kHz, and 75 kHz for 16-bit systems.

CIRCLE NO. 310

Buffer memory doubles PDP-11/45 speed

Fabri-Tek Inc., 5901 S. County Rd. 18, Minneapolis, MN 55438. (612) 935-8811. See text; 45 days.

The Model 4511 Memory Buffer is designed to increase the effective speed of PDP-11/45 main core memory. Processing time can be reduced by as much as one-half depending on the program used. The Model 4511 buffers the entire 124k words of main core memory of the 11/45, to achieve an effective speed of 450 ns. The unit uses bipolar technology and is contained on three PC cards which can be installed in minutes on the PDP 11/45 Fastbus. The memory buffer has 512 words by 16 bits of available storage and comes with a 5-V power supply. The Model 4511 with 8 k words of Fabri-Tek Model 11 Core Memory sells for approximately $11,810 (unit qty). Model 11 add-on core memory systems range in size from 8 k to 128 k words.

CIRCLE NO. 320
XENON corporation

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ER-3 ½ pound dry etchant—refill ................................... 1.25

ER-5 6 sheets photocopy film—refill ................................ 3.39

ER-6 Film process chemicals—refill ................................ 1.79

ER-7 Photo resist spray, 2.5 oz.—refill ................................. 2.95

ER-8 Resist developer, 16 oz. can —refill ............................. 2.95

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INFORMATION RETRIEVAL NUMBER 45

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- True RMS Current
- AC Watts

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The new 2504 digital AC instrument offers unexcelled accuracy and versatility for the measurement of sinusoidal and non-sinusoidal waveforms and for measurements at low power factors. Flexible design allows optional purchase of just the measuring functions required while push-button controls provide ease of operation.

The YEW 2504 is the AC DMM. Its 0.25% accuracy and 0.01% resolution, standard analog output, and low cost (Prices start at $1,590) make it the ideal instrument for quality control, lab, field maintenance, and instrument calibration applications. Write for details.
**DATA PROCESSING**

**Mag tape replaces paper with boost in speed**

*Dicom Industries, 715 N. Pastoria Ave., Sunnyvale, CA 94086. (408) 732-1060. From $1760 (qty).*

The Model 330 digital tape cassette can replace paper tape readers and punches. Speed increases of 33 times over synchronous units and 8333 times over asynchronous units are claimed. The Model 330 simultaneously emulates both paper tape punch and reader. Data storage capacity is 10 times that of a 1000 foot paper tape roll. A standard ANSI/ECMA cassette is used. Several standard versions of the Model 330 are available. These include: single or dual transport, FIFO buffer for 128 or 256 characters, and ANSI/ECMA formatter.

**CIRCLE NO. 321**

**Paper-tape reader loads microcomputer faster**

*Intel Corp., 3065 Bowers Ave., Santa Clara, CA 95051. (408) 246-7501. $975; 2 wks.*

The imm 8-90 is a high-speed paper tape reader for Intellec 8/MOD 8 and 8/MOD 80 microcomputer development systems. The reader transfers data 20 times faster than a standard TTY, tape reader. An asynchronous data transfer rate of 200 char/s allows an 8-kbyte program to be loaded in the Intellec memory in 1.5 min. Moreover, the new reader is completely software and hardware compatible with all Intellec 8 systems. Intellec 8 resident monitor software includes a general-purpose tape-reader driver that enables all system software to use the imm 8-90 features. The driver is also callable by user-written applications programs. In addition, the monitor provides dynamic I/O reconfiguration, for instantaneous reassignment of peripherals. Interface cables and documentation are supplied.

**CIRCLE NO. 322**

**Cassette reader mates with mini or terminal**

*Datel Systems, 1020 Turnpike St., Canton, MA 02021. (617) 828-8000. $2095 to $2795.*

The LPR-16 Cassette Reader accepts tapes written in Datel's complementary NRZI digital format and converts them to serial or parallel format. Two interface boards can be used with the LPR-16 Reader. The RS-232-C interface connects directly to many ASCII devices. The minicomputer interface transforms serial digital information recorded on the cassette (at 1700 bit/s) into parallel logic levels to be transferred on command to an external computer or processor.

**CIRCLE NO. 323**

**Distributed industrial network uses minis**


Three models of control satellites and a central computer unit are part of the industrial distributed network designated the 9600MX. Each control satellite contains a minicomputer interfaced to analog and digital I/O. The input-output segment can be separated up to 10,000 ft. from the control satellite mini (a 21MX). Model 9611A satellite offers a full line of industrial signals that include 50 V dc outputs, 117 V ac input and 250 V ac. Model 9603A offers the same capability but does not include terminal strips and signal conditioning. The Model 9602A provides an integrating DVM for data acquisition use only. The Model 9700 is a mini plus peripherals that acts as the central computer. The controllers become satellites to the 9700 and can communicate at rates to 1 Mbit/s over wire links up to 10,000 ft. The software executive RTE-II provides remote access to program and data files, task scheduling and peripheral sharing. Real-time programs can be written in Fortran or Basic. A spooling feature improves system throughput. Communications packages cost $6000 for the first link and $4000 for each additional link. Prices for the hardware units are 9700A: $37,300; 9611A: from $31,000; 9602A: $50,000; 9603A: $24,400; 9604A: $24,400.

**CIRCLE NO. 324**

**ELECTRONIC DESIGN 3, February 1, 1975**
INTEGRATED CIRCUITS

Eight CMOS ICs keep time


Eight standard CMOS circuits are offered for digital watches and clocks. The SCL5440 and SCL5445 are single-chip time base, LED decoder drivers for displaying hours, minutes, seconds and date. The SCL5440 has outputs compatible with common-anode LEDs, and the 5445 has outputs compatible with common-cathode LEDs. The SCL5441 is an upgraded design of the previous SCL5424 circuit for LCD displays showing hours and minutes. This decoder driver has switch anti-bounce inputs. Operating current is guaranteed to be less than 1 µA. The SCL5442 is a decoder driver for LCD displays showing hours, minutes, seconds and date, with AM-PM indication. It has an improved time setting technique, with seconds hold and advance capability. Operating current is less than 1 µA. A new single-chip low-voltage time base and LCD decoder driver, the SCL5443, reportedly has the lowest cost of any similar circuit. A second device is the SCL5447 time-base circuit, which would be teamed with the 5441 or 5442 decoder-driver. The SCL5419 digital-clock time base is an oscillator and 23-stage divider, with integrated oscillator and digital frequency trim. It is designed for use with a 4-MHz crystal. Digital frequency select permits factory adjustment of frequency without need for a trimming capacitor, over a range of 0 to 250 pulses per million.

CIRCLE NO. 325

1-k SOS RAM accesses in 120 ns

RCA, Route 202, Somerville, NJ 08876. (201) 722-3200.

A 1-k x 1-bit silicon-on-sapphire (SOS) RAM has an access time of about 120 ns at 10 V, with cycle times of 150 ns. Operating dissipation is about 20 mW at 1 MHz and 10 V. The chip employs a 16 row decoder, rather than the conventional 32, for increased speed.

CIRCLE NO. 326

YOU DON'T HAVE TO TAKE A SUBSTITUTE.

THE CAPACITOR:

Sprague's Type 192P Pacer ® …
The Dependable Low-Cost Miniature Polyester Film Capacitor.

THE DELIVERY CYCLE:

Large Production Quantities
4 - 8 Weeks ARO on All Popular Ratings. Off-the-Shelf Delivery from your Sprague Industrial Distributor.

THE CATCH:

None.
Sprague Delivers Film Capacitors.

Call your nearest Sprague district office or sales representative for complete information.
IT'S CLEARLY THE CHOICE OF
ELECTRONICS ENGINEERS — WORLDWIDE
WHEN YOU HAVE
Electronic Design's
GOLD BOOK
YOU DON'T NEED ANY OTHER INDUSTRY DIRECTORY

In just a few months, the first issue of *Electronic Design's* GOLD BOOK has become the leader among all directories used in this industry. Engineers have responded enthusiastically throughout the U.S. and from all over the world—especially in Europe where they've never seen anything like it before. The GOLD BOOK has become number one almost overnight.

HERE'S HOW YOUR FELLOW ENGINEERS RATE THE INDUSTRY ANNUALS

<table>
<thead>
<tr>
<th>Annuals Consulted Within Past Month</th>
<th>Annuals Preferred</th>
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<tbody>
<tr>
<td>Electronic Design's GOLD BOOK</td>
<td>85%</td>
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<tr>
<td>Electronic Engineer Master (EEM)</td>
<td>63%</td>
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<tr>
<td>Electronic Buyer's Guide (EBG)</td>
<td>32%</td>
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<tr>
<td>Thomas Register</td>
<td>16%</td>
</tr>
<tr>
<td>Conover-Mast Purchasing Directory</td>
<td>2%</td>
</tr>
</tbody>
</table>

**SOURCE:** Study by Dr. Eugene D. Jaffe, Associate Professor of Marketing, St. John's University, Nov. 1974. Base: respondents using directories. Totals exceed 100% due to multiple mentions.

The GOLD BOOK has revolutionized directory use patterns in this industry. Here's why: The GOLD BOOK is by far the largest, most complete one-step electronics purchasing and reference tool ever produced. And it's far easier to use. Look at these comparisons:

**COMPARISON OF ELECTRONICS INDUSTRY DIRECTORIES**

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<tr>
<th></th>
<th>EBG ELECTRONICS BUYERS' GUIDE</th>
<th>EEM ELECTRONIC ENGINEERS MASTER</th>
<th>ELECTRONIC DESIGN'S GOLD BOOK</th>
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<td>5,780</td>
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<tr>
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<td>Does manufacturers listing include facsimile equipment by make and call number?</td>
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</tbody>
</table>

²Paid listings only
²Includes Canada
²Standard Rate & Data; Oct. 24, 1974
²Includes fractionals

MOST THOROUGH, MOST COMPLETE, EASIEST-TO-USE ELECTRONICS INDUSTRY DIRECTORY IN THE WORLD
INTEGRATED CIRCUITS

Standard 74C CMOS extends temperatures

Harris Semiconductor, Melbourne, FL 32901. (305) 727-5107.

Having alternate sourced the basic 74C CMOS line introduced by National Semiconductor, the company is now also accompanying National in extending the temperature range of the 74C commercial line. The new range is -40 to 85 °C—up from a range of 0 to 70 °C.

CIRCLE NO. 327

1-k NMOS static RAM accesses in 60 ns

RCA, Somerville, NJ 08876. (201) 722-3200. $10.50 (1000); stock.

An NMOS memory, the MW-70011D1024 x 1-bit static RAM has pin compatibility with the AMS 7001L. The new RAM has a 60-ns maximum access time, 180-ns maximum cycle time and TTL-compatible inputs. Maximum dissipation is 0.5 µW/bit standby and 640 µW/bit operating. The RAM comes in a 22-lead ceramic DIP.

CIRCLE NO. 328

CMOS IC offers basic functions

Signetics, 811 E. Arques Ave., Sunnyvale, CA 94086. (408) 739-7700. 47¢ (1000).

A CMOS dual complementary pair plus inverter is offered in the Model N40007A. The IC, which is interchangeable with a like-numbered RCA version, accepts supply voltages in the range of 3 to 15 V. Input resistance is greater than 10^{12} Ω, and input current is less than 10 pA. All inputs have overvoltage protection.

CIRCLE NO. 329

Compact module improves watch designs


The company's latest digital watch module features decreased thickness, complexity and power requirements. Called the Compact Watch Module, or CWM, the new unit is only 0.25-in. thick. The CWM achieves a 49% reduction in the number of component elements and a 60% reduction in the number of electrical connections, when compared with the company's previous model, the HMM. In addition, a special liquid-crystal material in the display allows operation from supplies of only 3 V. As a result, a number of discrete components, including a voltage converter, are eliminated. Current consumed is 7 µA.

CIRCLE NO. 329

JAN & JANTX 2N4150 SWITCHING TRANSISTORS

are now available for your MILITARY SYSTEMS.

GENERAL SEMICONDUCTOR INDUSTRIES Manufactures Over 200 Types of HIGH SPEED, HIGH POWER NPN Switching Transistors Ranging From 1 To 60 AMPS.

GENERAL SEMICONDUCTOR INDUSTRIES, INC.
2001 West 10th Place, Tempe, Arizona 85281 • (602) 968-3101 • Mailing Address: Post Office Box 3078
8-bit micro set has 12 LSI I/O options

The PPS-8 family of 8-bit microcomputer circuits provides 12 LSI input/output controller options and a full complement of memories. The PPS-8 system architecture is based on a set of more than 90 expandable instructions, and the chips employ established p-channel MOS fabrication techniques. Memory circuits include 256 x 8 RAM, 1-k x 8 ROM, 2-k x 8 ROM, and, in development, an electrically erasable 256 x 8 ROM.

Main elements of the PPS-8 CPU are: 8-bit parallel adder accumulator for logic and arithmetic operations, five 8-bit registers for memory addressing and data manipulation, a pointer for a RAM data stack, processing logic for a priority interrupt structure, and logic for direct memory access.

The CPU can directly accept three levels of priority interrupts. More than 15 independent I/O circuits may be serviced for each priority level.

A load or store instruction can perform transfer, increment or decrement, and compare functions in 4 µs. Such multifunction instructions perform decimal arithmetic at the rate of 12 µs per digit. A table search takes 12 µs per byte and a block data transfer—moving bytes from one memory location to another—can also be done at a 12-µs byte rate.

For prototyping, available evaluation boards are priced at $600 to $700. A minimum PPS-8 microcomputer circuit set including CPU, a 2-k x 8 ROM, a 256 x 8 RAM, DMA controller and clock in 1000 quantities costs about $125 per set, including ROM encoding.

Rockwell International, P. O. Box 3669, Anaheim, CA 92803. (714) 632-3729. P: See text.

It's the PC card bus bar that saves space on a PCB. Saves money too. Makes board design and layout easier.

all these DIPs

How can you put 36 DIPs on a 30 sq. inch board without using costly multi-layer PCBs?

go on a 5" x 6" 2-sided PCB

Take Voltages and Grounds off the board with MINI/BUS. Use all the board geometry for interconnecting DIPs.

like this

With MINI/BUS, you'll save design and layout time. You'll save space on the board. And you'll save money — up to half the cost of a typical 4-layer PCB.

Rogers Corporation  Chandler, Arizona 85224  Phone: (602) 963-4584

Represented in Canada by LLOYD A. MEREDITH, 1560 Watersedge Road, Clarkson, Ontario L5J 1A4  Phone: (416) 533-2367

INFORMATION RETRIEVAL NUMBER 52

Electronic Design 3, February 1, 1975
hot stuff

or cold, CHR's family of TEMP-R-TAPE of Kapton provides outstanding endurance. They retain their excellent mechanical and electrical properties over a wide temperature range, —100 to +500°F.

Available in thicknesses from .001" to .0045" with a choice of several adhesive systems including adhesive two sides.

Find your CHR distributor in the Yellow Pages under "Tapes, Industrial" or in industrial directories. Or write for complete specification kit and sample. The Connecticut Hard Rubber Company, New Haven, Conn. 06509.

**COMPONENTS**

**Cross-patch module programs 100 points**

Aries Electronics, Inc., P.O. Box 231, Frenchtown, NJ 08825. (201) 996-4096. $40 to $80 board mounted; 2 to 6 weeks.

Aries cross-patch is a miniature XY programmable module with 100 interconnection points on a 10 x 10 grid configuration. The grid dimension is 0.100 in. Any x point may be connected to any y point by the use of bifurcated shorting plugs. Also, two sizes of diode interconnection plugs can switch functions. With shorting plugs installed, the height of the module is only 0.480-in. high. Both plugs and cross patch are available with color codes.

**Varistors available down to 20 V rms**

General Electric Co., Semiconductor Products Dept., Building 7, MD#19, Electronics Park, Syracuse, NY 13201. (315) 456-2021. $0.41 (1000 up); stock.

New GE-MOV varistors are capable of both dc and ac operation and voltage ratings for the new series are now as low as 26 V dc, or 20 volts rms. Higher voltage ratings are available to 81 V dc, or 60 V rms. Response time is less than 1 ns. Energy ratings range from one to 15 W-s with 1-A transient currents. Compared to zener diodes, these varistors are capable of handling 2 to 4 times as much current and up to 15 times the peak power.

**Tactile-tape keyboard switches with feeling**

Clare-Pendar Co., P. O. Box 785, Post Falls, ID 83854. (208) 773-4541. See text.

Softac, an 18-station keyboard, features soft-stroke, tactile-feel switching and low cost—less than $2 per assembly, less bezel, in low quantities and $1.60 in quantities of 50,000. The keyboard interfaces with conventional MOS, CMOS and TTL circuits. The tactile-tape technology allows the construction of arrays in single, double, triple and quadruple rows. A life of 10-million cycles is assured by sealing the contacts. Keys have an over-all travel of 0.050 in. and provide a positive switch-make feel. An integral ON/OFF slide switch is included.

**Custom assemble small motors to any need**

General Time, 135 S. Main St., Thomaston, CT 06787. (203) 283-5881.

The H4 motor system uses a modular design and assembly technique. This enables the company to manufacture and stock large quantities of motor components for assembly and delivery in a matter of days. The H4 motor system consists of four basic building blocks—the prime mover, the speed reduction unit, the output shaft and a pair of detachable leads. Combined, the components form an advanced 40 oz-in. torque timing work motor. The H4 system's prime movers and gear trains are completely interchangeable. They are stocked separately and easily mated to meet specific motor voltage, frequency and output speed requirements.

**INFORMATION RETRIEVAL NUMBER 53**

Electronic Design 3, February 1, 1975
Storage capacitors use single-anode foil

A broad line of low-cost Rubycon aluminum electrolytic discharge capacitors features low-leakage current and a single-anode foil design that replaces conventional double-anode foil constructions. Advantages claimed for the single foil include a small leakage current equal in microamps to the µF value, low dielectric loss and an improved pulse-rise characteristic to allow a short recharge time. Operating temperature is -10 to 40 °C and tolerance ±10 to ±30%. Type FO capacitors are rated for 330 and 360-V operation, with surge voltage ratings of 350 and 380 V, respectively. Type SF capacitors operate at 450 V with a 500-V surge. Capacitance values range from 200 to 2000 µF, in 100 µF increments.

CIRCLE NO. 335

Control motor designed with hollow rotor

Micro Switch, Div. of Honeywell, 11 W. Spring St., Freeport, IL 61032. (815) 232-1122. See text.

Miniature high-performance dc control motor, the 26EM, is smaller than a standard flashlight battery. Primarily designed for digital cassette recorders and cartridge drives, it will sell for about $10 in quantity orders. The motor features a hollow-rotor design, which makes possible an 18-ms response time and a rated torque of 1.65 oz-in. The rotor is epoxy coated. Standard models operate on 12 V dc, but options also include 6 and 24-V-dc models, ball bearings, two-hole mountings and lead wires.

CIRCLE NO. 336
Photometer offers any measurement units

Alphametrics, 532 Berry St., Winnipeg, Canada. (204) 786-1476. $1095.

Model 1020 lab/industrial photometer/radiometer is designed for applications where single parameter measurements are made on a repeated basis. Display is 3-1/2 digits plus any desired units of measurement. Controls include full-scale offset and seven decades of ranging. Analog output is standard. Sensitivity: 10^-12 W/cm², 10^-6 FC, 10^-4 FL. Spectral range: 200 nm to infrared. Options are BCD interface, automatic ranging and pulse mode.

CIRCLE NO. 337

Logic probe handles all CMOS voltages

Questronics, Inc., 3598 S. 300 West, Salt Lake City, UT 84115. (801) 262-9923. $25; stock.

This CMOS logic probe operates on all logic voltages (3 to 18 V dc) and indicates "1", "0" or pulse conditions with LEDs located near the probe tip. Logic "0" is a voltage less than 45% VDD while logic "1" is greater than 55% VDD. The pulse indicator flashes for 0.2 s each time a pulse of 500 ns duration or greater is present. Input impedance is 2 MΩ.

CIRCLE NO. 338

Rms/dc converter works to 0.25%

UFAD Corp., 700-36th St. S.E., Grand Rapids, MI 49508. (616) 241-6000. $795; 30 days.

Programmable true-rms-to-dc converter unit, Model 732, converts any waveform, including white noise, to a dc voltage proportional to the rms value of the input. Accurate to ±0.25%, the unit has a 1-MHz bandwidth, 6:1 crest factor, two remotely selectable response times and two time-delay outputs preset to user requirements. Input range is programmed by an external 3-bit BCD code and covers a 90-dB range in eight steps. The output is analog, 0 to +10 V dc. Three versions are available with input ranges of 100 mV to 300 V, 3 mV to 10 V, or 30 mV to 100 V, fs.

CIRCLE NO. 339

Quiet thermal printer accepts BCD or ASCII


Model 5150A quiet thermal printer accepts data from BCD or ASCII sources and prints up to 20 columns of alphanumeric information. Modular in construction, it is available in many different configurations and can function as an instrument system controller. The unit prints 5 × 7 dot-matrix characters at faster than three lines per second on heat-sensitive paper, available in rolls or fan-folds. The printer's mainframe contains a power supply, control logic and print mechanism. Input interfaces are provided by the use of plug-in circuit boards.

CIRCLE NO. 340

Time-interval meter resolves 100 fs


Model 8330 time-interval counter provides single-shot measurements with 100-ps resolution, time-interval averaging with 100-femtosecond resolution, along with period and period average measurements to the same high resolution. Arming is provided for selection of a particular signal to be measured from a sequence of signals. Full remote programmability and parallel BCD output are standard, as well as a variety of input/output control signals. Front-panel controls are single point programmed and trigger levels use BCD 8-4-2-1 code.

CIRCLE NO. 341

Compact DMM built around LSI

Philips, P. O. Box 523, Eindhoven, the Netherlands. $225.

The heart of the PM 2513 DMM is an LSI circuit that performs part of the analog circuit functions, the a/d conversion and the digital signal evaluation. The IC drives directly a 3-1/2-digit, seven-segment LED display with automatic decimal point. It also displays polarity, overload and low battery. Five ranges of ac and dc voltages cover 0.1 to 600 V and 0.1 to 1000 V, respectively. Basic accuracy is ±0.2%. Also handled are ac and dc current and resistance.
Sweep gen offered for 75-Ω applications


Series 1000 is a 75-Ω general-purpose, sweep/signal generator. Model 1001A covers a frequency range of 0.5 to 300 MHz and Model 1002 covers 1.0 to 500 MHz. Sweep linearity is 2%. Flatness of ±0.25 dB is accomplished with pin diode leveling. Output amplitude is +60 dBmV max, with total attenuation range of 90 dB. Attenuation accuracy is ±0.5 dB. These units also feature AM and FM capability and remote programming for center frequency, sweep width and attenuation over a 20-db range.

CIRCLE NO. 343

Electronic load handles up to 750 W

ACDC Electronics, Oceanside Industrial Center, Oceanside, CA 92054. (714) 757-1880. $850; 6-8 wks.

EL-750 programmable electronic load can simulate up to 750 W of dc power. The portable instrument operates in either a constant-resistance or constant-current mode. A dynamic switching mode is built into the units. A square-wave generator enables the load to switch between two adjustable current levels. Two frequency rates are selectable by a front panel switch: twice the input line frequency or 1 kHz, both 50% duty cycle. The unit provides a meter shunt output that can be used as a calibration check or for a digital meter readout.

CIRCLE NO. 344

A logical test for Digital Logic Test Systems.

1. Can response be measured 100 nanoseconds after simultaneous applications of stimulus? 
   Yes ☐ ☐ No

2. Are clocks programmable for frequency, pulse width and number of pulses? 
   Yes ☐ ☐ No

3. Is it economically expandable to three work stations with 1024 two-way interface lines in each station? 
   Yes ☐ ☐ No

4. Does the system software provide a debug feature which allows the operator to monitor and control the test? 
   Yes ☐ ☐ No

5. Does it provide File Management, guided-probe fault isolation and complete self-test to the card level? 
   Yes ☐ ☐ No

Hughes 1024 Digital Logic Test System answers yes to all the questions above. It also provides an optional simulation system, Digital Fault Analysis (DFA), which generates a logic model; simulates the unit under test; verifies using fault insertion techniques; and generates fault isolation data for the automatic guided probe. Time independent gate level simulation identifies "race" conditions and traces them to their origin.

LOOK FIRST IN

FOR
POWER
SEMICONDUCTORS

WHO MAKES THEM

You'll find 97 manufacturers of power semiconductors beginning on pages 353, 428 and 457 of Electronic Design's GOLD BOOK (Volume 1 - Product Directory). For your convenience, each manufacturer is listed with complete street address, city, state, zip and phone number.

SALES OFFICES—REPS DISTRIBUTORS

To find information about each power semiconductor manufacturer, turn to the Manufacturers Directory. Whenever possible it lists names of key officials, sales offices, export offices, foreign offices, U.S. and foreign reps followed by a list of U.S. distributors. In many cases there is additional data, when provided by the company: TWX, TELEX, cable address, facsimile equipment (make and call number), 800 (toll-free numbers) as well as number of engineers, number of employees and financial data.

CATALOG PAGES

Here's a rundown of the catalog pages you'll find on power transistors in Electronic Design's GOLD BOOK.

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<td>TRW</td>
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</tbody>
</table>

KEEP ELECTRONIC DESIGN'S GOLD BOOK HANDY WHEN YOU CALL

Refer to your copy of Electronic Design's GOLD BOOK before you dial your next vendor. Referral to specific product pages can shorten your long distance phone calls. LOOK FIRST in Electronic Design's GOLD BOOK.
Electronic Design’s
GOLD BOOK
FOR
COOLING
EQUIPMENT

WHO MAKES IT

You’ll find eleven categories of cooling equipment and related products listed in the Product Directory of Electronic Design’s GOLD BOOK. For blowers and fans 38 manufacturers are listed. For thermoelectric cooling/heating modules, 17; circulating liquid cooling units, 21; heat sinks and dissipators, 50; thermal conductive coatings, 23; insulators and insulating hardware, 52; transistor mounting pads, 23; epoxy potting compounds, 41; silicone greases, 17; and washers, 18. As with power semiconductors, data about each manufacturer, his reps and distributors can be found by referring to the Manufacturers Directory.

HERE’S A RUNDOWN OF THE CATALOG PAGES YOU’LL FIND ON HEAT SINKS AND DISSIPATORS ALONE

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<td>Hughes Aircraft Co.</td>
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</table>

TAKE WAKEFIELD ENGINEERING, FOR EXAMPLE

Wakefield Engineering’s 42 page catalog of semiconductor cooling products begins on page 1307 of Vol. 2. In addition to detailed specs and information about its heat sinks and thermal cooling products (most show curves of natural and forced convection characteristics) the pages include diagrams of 99 heat sink extrusion shapes with dimensions, surface area, and thermal characteristics. Wakefield’s unit also provides guides on HOW TO SELECT HEAT SINKS, ENGINEERING DATA, HEAT SINK MOUNTING SPECIFICATIONS, HOLE PATTERNS, U.S. DISTRIBUTORS, EUROPEAN SALES AGENTS, U.S. FIELD SALES ENGINEERS, and lists other available Wakefield catalogs.
**Tolerance**

**SCHAUER**

1-Watt ZENERS

**Immediate Shipment**

**Low Prices**

ANY voltage from 2.0 to 16.0

Quantity | Price each
--- | ---
1-99 | $1.07
100-499 | .97
500-999 | .91
1000-4999 | .86
5000 up | .82

All welded and brazed assembly
No fragile nail heads

Write for complete rating data and other tolerance prices.

**Buy the kit**

**Save a lot**

Kit contains a 51-piece assortment of SCHAUER 1% tolerance 1-watt zeners covering the voltage range of 2.7 to 16.0. Three diodes of each voltage packaged in reusable poly bags. Stored in a handy file box. Contact your distributor or order direct.

A **$54.57 value for**

ONLY **$24.50**

Semitcoa, 333 McCormick Ave., Costa Mesa, CA 92626. (714) 979-1900. $70.

An npn switching power transistor, Model SCA100-120, appears as only a 0.002-Ω resistance with a 100-A collector current. The device has a saturation voltage of 1.7 V at rated maximum collector current. The transistor is intended for high-speed switching operation at 120 V. Its Fτ is 50 MHz at an IC of 10 A and beta is typically 40 at a collector current of 50 A. The transistor characteristics show broad safe operating areas, with E_{R} of 200 millijoules, and I_{S} of 40 A. The unit can be operated continuously at 40 A, 100 V and 70°C. It is available in TO-3, TO-61, or TO-63 packages or a molybdenum-mounted chip.

CIRCLE NO. 345

**DISCRETE SEMICONDUCTORS**

**Power transistor made for switching circuits**

Semicr0, 333 McCormick Ave., Costa Mesa, CA 92626. (714) 979-1900. $70.

An npn switching power transistor, Model SCA100-120, appears as only a 0.002-Ω resistance with a 100-A collector current. The device has a saturation voltage of 1.7 V at rated maximum collector current. The transistor is intended for high-speed switching operation at 120 V. Its Fτ is 50 MHz at an IC of 10 A and beta is typically 40 at a collector current of 50 A. The transistor characteristics show broad safe operating areas, with E_{R} of 200 millijoules, and I_{S} of 40 A. The unit can be operated continuously at 40 A, 100 V and 70°C. It is available in TO-3, TO-61, or TO-63 packages or a molybdenum-mounted chip.

CIRCLE NO. 345

Rf power transistors operate from 16 V

Communications Transistor Corp., 301 Industrial Way, San Carlos, CA 94070. (415) 591-8921. $39 (BM70-12); $21.50 (BM40-12); stock.

The BM70-12 and BM40-12 rf power transistors can simplify amplifier design. The units make it possible to design a 100-W amplifier with only three transistors instead of the customary seven. The transistors are guaranteed to withstand infinite VSWR at all phase angles when operated at rated power with a 16-V supply (dc). Both units have internal matching and are designed for operation in the 138-to-174-MHz frequency range.

CIRCLE NO. 346

**Darlington photodetector has two sensitivities**

**Asea-Hafo AB, Siktgatan 5, S-162 26 Vällingby, Sweden.**

The 6B82, a silicon photodetector with a very high sensitivity, consists of a photodiode and a three-transistor Darlington amplifier. It is hermetically encapsulated in a TO-18 case with a lens cap. When using only two transistors, the detector works like a conventional photodarlington and its sensitivity is typically 150 mA/(mw/cm²) at a wavelength of 940 nm. The main advantage of 6B82 is, however, its third transistor, with which the sensitivity can be further increased more than 100 times. As an example, an irradiance of only 5 µW/cm² is sufficient to give an output current of approximately 100 mA. Typical values of 6B82 when using two and three transistors are as follows: saturation voltages 0.8 and 1.4 V, rise times 30 and 500 µs and fall times 25 and 350 µs, respectively.

CIRCLE NO. 347

**Switching diode has 135-V breakdown voltage**

**Cerberus Ltd., CH-8708 Mannen­dorf, Switzerland.**

The GD 135 switching diode is designed for dc and trigger circuits. The uniform breakdown voltage of 135 V and the current input of 0.1 to 2 mA make this diode useful for such applications as measuring circuits, automatic control systems and trigger circuits.

CIRCLE NO. 348
Metal oxide varistors come in many models

General Electric, Electronics Park, Bldg. 7, Mail Drop 49, Syracuse, NY 13201. (315) 456-2021. $0.25 (10,000 pcs); stock.

The "MA" series of MOV varistors is designed for automatic insertion. These units are capable of both dc and ac operation. Voltage ratings range from 121 to 365 V dc, 88 to 264 V ac rms. The metal oxide varistors are voltage dependent, symmetrical resistors which perform in a manner similar to back-to-back zener diodes. There are seven models available in each of two selections. Selection A is classified at RETMA voltages $\pm 15\%$ at 1 mA dc. Selection B is classified at RETMA voltages $\pm 10$ mA dc. Energy ratings range from 100 to 700 milli-Joules, operating temperatures from $-40$ to $+125$ C. The molded axial-lead package has a diameter of 3.68 mm (0.145 in.) and is 8.5 mm (0.335 in.) long, excluding leads.

CIRCLE NO. 349

Rectifier stacks come in two versions

Semtech Corp., 652 Mitchell Rd., Newbury Park, CA 91320. (213) 628-5392. From $1 (100-up); stock.

A rectifier stack, claimed by the company to be the smallest in the industry, can meet or exceed the environmental requirements of current military and space programs. It measures $0.215 \times 0.07$ in. The stack is available in two different types, with specifications as follows: General purpose, $t_{tr}$ of 2 \mu s, PIV of 2 to 4 kV, average current of 125 mA at 55 C, maximum reverse current of 100 nA at 25 C, and one cycle surge current of 7 A. The fast recovery stack has a $t_{tr}$ of 250 ns (300 ns for 4000 to 6000 kV units), a PIV of 1500 to 3000 V, an average current of 100 mA at 55 C, a max reverse current of 100 nA at 25 C and a one cycle surge current of 5 A.

CIRCLE NO. 350
Temperature controller setpoint is 1%

Thermo Electric, 109 5th St., Saddle Brook, NJ 07662. (201) 843-5800. $137; 3 to 5 day.

The Model 32126 temperature controller is specifically designed for use with resistance temperature detector inputs. The controller provides on-off proportional control. The proportional band is centered about the setpoint and fixed at 3% of full scale. Self-adjusting on-off cycle time compensates for rapid temperature variations due to process load changes. Potentiometric setpoint accuracy is 1% of full scale span. A tamper-proof setpoint knob is used to prevent accidental changes of temperature settings. Direct temperature indication is provided by a built-in meter with an effective width of up to 30% of full scale span. Indication and setpoint are on the same scale to eliminate dual meter confusion, yet provide indication independent of control action.

Sample/hold amp has aperture jitter of 1 ns

Analogic, Audubon Rd., Wakefield, MA 01880. (617) 246-0300. $39 (100-up); stock to 2 wk.

The MP240 sample-and-hold module has an aperture uncertainty (jitter) of ±1 ns. Its transfer accuracy is within ±0.01% of specified gain of 1, and the linearity is ±0.005% of FSR. The signal feedthrough in the hold mode is -90 dB and the unit has an acquisition time of 5 µs to acquire a 10-V step to within 0.01%. The s/h amplifier contains a high-impedance input buffer for minimum loading of analog signal sources, TTL/DTL/CMOS compatible switching control, propriety signal-guarded and signal-compensated acquisition and disconnect switching circuits.

S/d converter provides ±5° offset null

Transmagnetics, 210 Adams Blvd., Farmingdale, NY 11735. (516) 293-3100. $595 (1 to 9); stock to 4 wk.

The Model 1623F is a miniature, 14-bit s/d converter that has an internal ±5° null offset capability. This model can be supplied to convert either the standard frequencies of 60 or 400 Hz, or special frequencies as low as 30 Hz or as high as 10 kHz. Output is either 14-bit binary parallel, four decade BCD or both. The Model 1623F is supplied in an encapsulated package that measures 2.625 × 3.125 × 0.82 in.

Retro-reflective control has max range of 30 ft

Mektron, 2728 N. Jessup St., Portland, OR 97217. (503) 285-3681. $155 (1 to 9).

The Model 220-20 retro-reflective infrared limit switch is a completely self-contained unit. It measures 2 × 6 × 6.5 in. and is housed in a NEMA 4/12 extruded aluminum enclosure with an internal ambient light shield. Operating range of the standard 220-20 unit is 30 ft when a 3 in. dia. reflective disc is used and 5 ft with low cost reflective tape. Multiple units can be mounted on 2 in. centers for conveyor and log measuring applications. Each switch contains a pulsed, solid-state, infrared transmitter; tuned receiver; power supply; input transformer; heavy-duty, 10-A relay; sensitivity adjustment; time delay (adjustable 0 to 9 s); alignment indicator; and a programmable mode select to ease compatibility of the standard unit to a variety of applications.
Photoelectric controls use modulated LEDs

Warner Electric Brake and Clutch, 449 Gardner St., Beloit, WI 53511. (815) 389-3771. MCS143: $105, MSCP144: $112; stock.

Two self-contained LED modulated photoelectric sensors are designed for controlling a wide range of packaging applications and industrial functions. The MCS-143 LED scanner comes complete with infrared light source, sensor, power supply, amplifier and plug-in output relay contained in one housing. A modular version, MCS-144, offers a choice of four-time-delay modules and three output switching devices: relay, hybrid switch or logic output, in addition to the standard MCS-143 features. The light is modulated at a high-frequency in order to operate effectively over long distances —up to 30 ft. The light receiver circuitry is also modulated synchronously with the LED, thus making the unit immune to all other light and environmental conditions. The enclosures for both controls are of high impact strength plastic, completely gasketed and designed to meet NEMA 1, 3, 4, 12 and 13 standards. Total weight is 25 oz. maximum.

Microphone preamp has low distortion

Custom Sound Productions, P.O. Box 54, Village Station, New York, NY 10014. (212) 691-8754. $160 (8-up).

A microphone preamplifier is designed for ultra-low noise and low distortion operation. The amplifier uses all tantalum capacitors and carbon film resistors mounted on a G-10 glass-epoxy circuit board. It features adjustable gain operation from a single 40-V power supply or battery and a single-ended output up to 24 VU. Specifications include a balanced input; a 3-pin XLR-type locking connector; an unbalanced output; up to 13 V into 8 kΩ (or greater); a power supply ripple voltage rejection of 120 dB; a noise of 0.5 µV typical and a total harmonic distortion of 0.1%.

Minelco's new Dual In-Line Potentiometer is a low cost trimmer specifically designed for PCB automatic insertion equipment.

The DW-5 wire-wound model offers low TC to ±50 PPM and resistance values up to 25K.

The DC-5 model with CERMET element and multiple point wiper contact for stability and reliability will retain accurate settings within 0.5% of desired voltage, TC of ±100 PPM, resistance range up to 2 megs, infinite resolution.
Switch switches fast

On those rare occasions when a switch malfunction shuts down equipment, STACO's Model 49 Illuminated Push-button Switch, with its plug-in switch module, can have things running again in less than 60 seconds. Simply flip a lever to remove the display pushbutton, and pull out the toilworn switch module. Slip in the plug-in replacement unit and reinsert the display pushbutton. It's that simple... and that fast!

No need to touch the behind-the-panel wiring. Once terminations are wired into the system, plug-in modules can be removed and replaced from front of panel. Choice of economical, dependable solder or wrap type terminations.

If your operation cannot tolerate downtime, then STACO's Model 49 can help keep the wheels turning. Its proven switch mechanism assures long service life and when at long last it needs replacing, a new module quickly plugs in. There's a choice of switch action and circuitry to meet your requirement.

When you think switch... think STACOSWITCH.

STACOSWITCH

Other STACO Company products: Fixed Ratio Transformers, STACO, INCORPORATED, Richmond, Indiana; Variable Transformers, STACO, INCORPORATED, Dayton, Ohio.

INFORMATION RETRIEVAL NUMBER 65

Battery charger ends charge at any voltage

Alpha Components Corp., 115 Eucalyptus Dr., P. O. Box 947, El Segundo, CA 90245. (213) 322-7780. $48.50 (10); stock.

Model 20BC12, OEM open-frame battery charger, will deliver 20 A to a 12-V discharged battery and senses voltage to automatically reduce charging current. Designed for 115 V de, the charger is voltage regulated for 100-to-125-V input. Output is protected from continuous overloads by a dc circuit breaker, and the charger design is inherently protected from short circuits and accidental battery reversals. A control provides full adjustment to end charge at any desired voltage.

CIRCLE NO. 359

Constant-current source offers hefty output

Keithley, 28775 Aurora Rd., Cleveland, OH 44139. (216) 248-0400. $925; 30 days.

Model 227 constant-current source offers outputs to 1.1 A at a compliance voltage of 50 V, and even higher compliance voltage (300 V) at lower currents. The unit features an output range of 1 µA to 1.1 A in four decade ranges. The current level is selected digitally through the use of three in-line dials on the front panel. The compliance voltage limit is selected via front-panel control from 3 V to the maximum. Output resolution is 50 ppm.

CIRCLE NO. 360

Voltage reference lists low 1-ppm/°C tempco

Codi Semiconductor, Pollitt Dr., Fair Lawn, NJ 07410. (201) 797-3300. $46 to $275 (10 pc. qty); 4 to 8 wks, some stock.

This series of precision voltage references offers tempco's as low as 1 ppm/°C. Standard "Certavolt" models feature a short-circuit-protected output of 10,000 V, with tempco specified from 15 to 55 C and long-term stability as low as 10 ppm/year. The units are said to be ideal voltage references for precise (12 to 16-bit or better) a/d and d/a converters, inertial guidance platforms and precision analog computation.

CIRCLE NO. 358

Compact UPS is self-contained

Deltec Corp., 3849 Gaines St., San Diego, CA 92110. (714) 297-4466. $1425.

The DSU 710 uninterruptible power system (UPS) maintains conditioned ac power to critical computer systems and other electrical and electronic equipment. The unit is self-contained and includes battery charger, battery reservoir and output inverter regulator. Output from the DSU 710 is an isolated 117-V-ac ±5% sine wave. Standard accessories are alarm indicators and remote signals for loss of utility ac and battery low, ac current and voltage output meters and reverse transfer switch which automatically switches the critical load to utility power should an unexpected failure occur in the system.

CIRCLE NO. 357

POWER SOURCES

Compact UPS is self-contained

Deltec Corp., 3849 Gaines St., San Diego, CA 92110. (714) 297-4466. $1425.

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CIRCLE NO. 360

Electronic Design 3, February 1, 1975
MICROWAVES & LASERS

Adjust bandwidth of L-band klystron

Varian, 611 Hansen Way, Palo Alto, CA 94303. (415) 495-4000.

The Model VA-963A L-band klystron provides either broadband or narrowband operation from the same tunable tube. Individual cavity tuning knobs can be quickly set in the field to factory determined positions using digital counters. Curves of tuner setting versus frequency are supplied with each tube, and the basic frequency range is 1250 to 1350 MHz.

CIRCLE NO. 361

Compact module simplifies radars

Amperex Electronic Corp., 230 Duffy Ave., Hicksville, NY 11802. (516) 931-6200. $47.50; stock.

The DX-489 compact radar module includes an integral antenna, gunn-oscillator transmitter and Schottky-barrier diode detector. According to the company, the module conforms to FCC regulations for 10.525-GHz Field-Dispersion Sensors. The gunn-oscillator transmitter section typically consumes less than 1 W from a 7-Vdc supply, and it radiates about 8 mW of 10.525-GHz power.

CIRCLE NO. 363

You know our reputation in DC to DC

Wait till you see Tecnetics' new 400 Hz AC power supply

We earned a reputation with our line of DC to DC power supplies. Now, we add to it with a new 400 Hz AC power supply. Like our 28VDC power supplies, the AC model features extremely high packaging density, high efficiency and reliability. Most important, it's small, measuring in at only 4x4x2 inches and weighing 36 ounces fully encapsulated. These power supplies are designed to meet the rugged vibration, shock, humidity and altitude specs of the aerospace industry (M.E. 5400). They also have separate, remote error-sensing terminals to compensate for voltage loss, assuring that the voltage level remains constant at the load.

Write for our 26-page catalog that gives full specs and prices on these and over three hundred other power supplies.

SPECIFICATIONS

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<th>3000 SERIES - DC TO DC</th>
<th>4000 SERIES - 400 Hz AC TO DC</th>
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Tecnetics® The Power Conversion Specialists
P.O. Box 910, 1625 Range Street, Boulder, Colorado 80302 (303) 442-3837 TWX 910-940-3246

INFORMATION RETRIEVAL NUMBER 66

117
Electronic Design's GOLD BOOK IS READY

VOLUME 1 DIRECTORIES

• PRODUCT DIRECTORY
Want to know who makes a given product? Electronic Design's GOLD BOOK is the first place to look. Manufacturers are listed under almost 5,000 product headings or cross references. You'll find everything an electronics manufacturer would require — components, computers, hardware, test equipment, instrumentation, systems and services — they're all there, from "Abrasives" through "Zone Boxes."

Knowing only a name or state isn't much help if you or your secretary want to contact several manufacturers at once for information or a quote. That's why Electronic Design's GOLD BOOK repeats each manufacturer's full name, street address, city, state, zip and phone number every time the manufacturer is listed.

• MANUFACTURERS DIRECTORY
You'll find 7,528 manufacturers listed in Electronic Design's GOLD BOOK — more than twice the number contained in "the other industry directory." In addition to complete address and phone number, whenever provided by the company you'll also find:

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• DIRECTORIES OF DISTRIBUTORS
Want to find a distributor near your town? Use the geographic Directory of Distributors. Access is by State, then City. 5,700 distributors are listed. The same distributors are also listed alphabetically for your convenience, often with additional information about their business volume, key personnel, etc.

• TRADE NAME DIRECTORY
If you've heard the trade name, but can't remember who makes it, here's the place to look. Over 4,600 industry trade names are included. Listing includes brief description of item and company name.

TOTAL DISTRIBUTION: 91,000 — 13,200 COPIES OVERSEAS, INCLUDING 11,000 COPIES IN EUROPE
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- 520 CATALOG PAGES ON ICs AND SEMICONDUCTORS
- 300 CATALOG PAGES ON INSTRUMENTS
- 290 CATALOG PAGES ON POWER SUPPLIES
- 210 CATALOG PAGES ON WIRE AND CONNECTOR PRODUCTS
- 150 CATALOG PAGES ON SWITCHES

Volumes 2 and 3 of Electronic Design’s GOLD BOOK are filled with manufacturers’ technical data and product catalogs — a gold mine of information for the engineers, engineering and purchasing managers of this industry. Products are classified by related families and are organized in 52 product categories, over 2,800 catalog pages in all.

Volume 2 contains Components and Materials; Volume 3 contains Equipment, Hardware, Panel Components, Power Supplies, Tools and Production Equipment, Engineering Aids, and “Company Profiles and Capabilities.”

Electronic Design’s GOLD BOOK is READY WHEN YOU ARE. Keep it on hand for product search, sourcing, or for instant technical and specifying data. It puts the entire electronics industry at your fingertips.

Electronic Design’s GOLD BOOK is the largest, most complete, most comprehensive one-step purchasing and reference tool ever produced in this industry. Its PRODUCT DIRECTORY contains more than twice the number of editorial pages than the other industry directory; almost 50% more pages of TRADE NAMES; half again the number of pages in its MANUFACTURERS DIRECTORY; almost twice the number of pages in its DISTRIBUTORS DIRECTORIES. It’s far and away the biggest and best electronics directory in the world.

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<th>The Other Industry Directory</th>
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BETTER BY EVERY MEASURE
Send today for your FREE brochure, price list and dealer list.

**OmniScribe™ 75**

**TOP SELLING STRIP CHART RECORDER**

$395

Here’s America’s number one strip chart recorder for 1975! And for a $395 rock bottom price in an age of inflation. Yet look at these features:

- Multi-speed chart drive — field adjustable for English/Metric scaling.
- Self-aligning sprocketless paper drive
- New patented transducer eliminates troublesome slide wire.
- Two-pen models available at $595 up

Pick a winner for 1975! Write for details today.

---

**Model 5112-1**
Single Pen Recorder with 1, 2, 5, 10 in/min. chart speeds and 10 mv fixed input spans

$395

**Model 5212-2**
Dual channel recorder with 1, 2, 5, 10 in/min chart speeds and 5 input spans of 10 mv up.

$690

**Model 5215-14**
1 mv dual channel recorder with electronic integrator, 2.5, 5, 10, 20 cm/in chart speeds.

$940

---

**TOP SELLING STRIP CHART RECORDER**

Here's America's number one strip chart recorder for 1975! And for a $395 rock bottom price in an age of inflation. Yet look at these features:

- Multi-speed chart drive — field adjustable for English/Metric scaling.
- Self-aligning sprocketless paper drive
- New patented transducer eliminates troublesome slide wire.
- Two-pen models available at $595 up

Make the big change-over to the new DMM from T.R.I.

High performance, low cost ($279) and compact size, 10V Resolution.

10µV resolution, $279
Model 6355 is a portable DMM having a 10µV (DC voltage) resolution. It is comparable to DMM’s for laboratory use, priced at an economical $279, and sets a new standard of performance for portable DMM’s.

Fully automatic
Operation is as simple as selecting the function and signal connection. The measured value is displayed through the automatic selection of 5 functional modes: range selection, unit display, polarity, overrange indication and overload protection.

True portability
It measures 4-3/8" (W) x 2.7-9/16" (H) x 6" (D) and is a light weight 1.8 lbs for complete portability. The shock-resistant design even protects the unit against accidental drop damage.

Rechargeable battery (Option)
Besides the AC power supply, the standard composition includes an alkaline battery. Optionally available is a rechargeable battery. Standard accessories include a battery charger.

---

**Model 6355 Mini-multimeter $279**

---

**new literature**

**Retaining rings**

A 44-page edition of a retaining rings catalog and manual features sections on metric retaining rings, retaining and snap rings for bearing retention and wire rings. Accessories, including pliers, dispensers and applicators, are covered. Anderton Darby, Clifton, NJ

CIRCLE NO. 364

**SCR power supplies**

Over 50 models of single-phase and three-phase SCR power supplies are detailed in a six-page data booklet. Covered are specifications for the units as well as price information. Electronic Measurements, Neptune, NJ

CIRCLE NO. 366

**3-digit universal DPM**

A universal three-digit digital panel meter and its supporting accessories are detailed in a brochure. Analogic, Wakefield, MA

CIRCLE NO. 367

**Pot and trimmer standards**

A revised version of this Variable Resistor Components Institute’s standards for wirewound and non-wirewound precision potentiometers and trimming potentiometers may be purchased at $5 a copy. Complimentary copies may be obtained by companies that are members of VRCI. Variable Resistor Components Institute, 1717 Howard St., Evanston, IL 60202

INQUIRE DIRECT

ELECTRONIC DESIGN 3, February 1, 1975
Data logger

A 52-page brochure describes the Digitrend 220 "smart" data-acquisition system. A system description is presented, with photographs, as well as options, specifications and prices. Doric Scientific, San Diego, CA

CIRCLE NO. 371

Microwave switches

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Radiotron handbook

F. Langford-Smith's "Radiotron Designer's Handbook" contains 1500 pages of comprehensive vacuum tube theory and practical application information and is written in an easy-to-understand style with many illustrations. It is available in limited supply at $15 a copy. RCA Commercial Engineering, Harrison, NJ 07029

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Servo systems
Engineering characteristics for over 30 different amplifiers for driving dc and ac motors, dc torquers, clutches and resolvers are given in a four-page catalog. Parameters shown are output power, output voltage, input impedance, gain and power required. On the last page is a compilation of frequently used conversion factors helpful when designing servo systems. Control Technology, Long Island City, NY
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Rotary switches
Rotary, lever, ganged and PC board switches for low-current applications are covered in a 32-page catalog. The catalog contains illustrations, a cross-reference guide to comparable military switches and is fully indexed. Standard Grigsby, Aurora, IL
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Voltage standard
Accuracy, resolution, range and stability of the Model AN3100 secondary dc voltage standard are given in a six-page catalog. Another brochure provides 31 useful applications for the instrument. Analogic, Wakefield, MA
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Tools and safety equipment
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CIRCLE NO. 376

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