Choosing displays isn't easy. While certain applications dictate specific displays, many others do not. Spec sheets don't solve all selection problems either. Unlike other devices, displays are often chosen for their looks and not their technical features. To learn how you can select them, and what's available, see page 52.
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- **Drift Current on CH (+125°C):** .5nA (TYP)
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  - 0°C to +75°C: $14.85
- **HA-2420**
  - -55°C to +125°C: $29.70
- **Hermetic 14 pin DIP package**
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Acurex Corp. sets the record straight

We have received a number of inquiries as a result of the article "Sensors in 5 Areas Are Getting Tinier, Cheaper and More Precise Than Ever" (ED No. 15, July 19, 1974, pp. 30-38). However, I was disappointed to find that Acurex was listed incorrectly with respect to the type of transducer we manufacture. We manufacture a line of torque transducers that are similar in concept to the S. Himmelstein & Co. unit shown on p. 38 of the article.

Our approach is slightly different, in that we take an existing coupling in a rotating power train and convert that coupling to a torque transducer. We also have the capability of measuring horsepower directly. This modification to an existing coupling permits the user to use existing design hardware without modifications to its power train. The equipment is hermetically sealed to permit indefinite operation in very hostile industrial environments.

We do not manufacture displacement transducers. Please correct this mistake. Our equipment can operate in severe industrial environments up to 150 C and up to 30,000 g of static acceleration load. For high-speed rotating equipment, we know of no other reliable method of removing data from the rotating parts.

Edward L. Rossiter
Marketing Manager
Acurex Corp.
485 Clyde Ave.
Mountain View, CA 94042

Atom-waste disposal: An 'ejection' idea

In regard to the letter of Ralph S. Gobel ("He'd Give Atom Waste a Place in the Sun," ED No. 16, Aug. 2, 1974, p. 7), we would like to point out some serious problems in solar disposal of atomic waste. A short calculation shows that it is energetically cheaper to achieve escape velocity from the solar system than it is to place a payload in an orbit that intersects the sun.

To hit the sun, essentially all the orbital velocity of the earth (30 km/sec) must be subtracted from the payload, whereas only 41% of the earth’s orbital velocity must be added to the payload to eject it from the solar system entirely. However, this is still not a very attractive solution, because even for relatively small payloads, achieving solar-escape velocity strains the limits of modern rocket technology.

One other technique requires slightly less energy than directly ejecting the waste from the solar system. This is to send the payload to Jupiter. Carefully guided close passages with Jupiter can be manipulated either to eject the payload from the solar system or to cancel its velocity entirely and send it falling into the sun. The latter technique requires enormous accuracy guidance.

Thomas A Sargent
Thomas N. Gautier
University of Arizona
Steward Observatory
Tucson, AZ 85721

Electronic Design welcomes the opinions of its readers on the issues raised in the magazine's editorial columns. Address letters to Managing Editor, Electronic Design, 50 Essex St. Rochelle Park, N.J. 07662. Try to keep letters under 200 words. Letters must be signed. Names will be withheld on request.
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Get all the facts. Spend a second and circle the reader service number. Or spend a minute and write Newport Laboratories at 630 East Young Street, Santa Ana, California 92705. For immediate information, call collect Dial (714) 540-4914. Ask for Lyell Kinney. Or TWX: 910-595-1787.

NEWPORT

In Europe: Newport Laboratories B.V., P.O. Box 7759, Schiphol—0, Holland, Tel: 020-45-20-52
INFORMATION RETRIEVAL NUMBER 8
Here are three little ways to solve the big problem of switch selection when space is at a premium.

Slide, snap-action and rotary switches in the new line of Centralab micro-miniatures offer more than just size benefits. They’re big in performance for a wide range of exacting applications.

The three new types of microminiature switches now available from Centralab, actually give you more than three ways to solve a switching problem. With the options available within each type, your selection is expanded to open a whole new world of design solutions for printed circuit board applications. If you’re designing equipment or instrumentation that requires switch control for encoding, calibration, troubleshooting or a wide range of other functions, you’ll find the perfect answer in this new Centralab line.

**INTERDIL SLIDE SWITCHES**

You’ll really appreciate the modular flexibility of these switches. They’re a DIP packaged, 2-pole switch that can be ganged to give you a pre-wired switch up to as many poles as required. There are three switching functions — SPST, DPST and DPST Reversing, with each configuration coded in a different body color. All have color-dot status display to tell you when contact is made. Lead centers are standard .1" x .3". Rated 0.5 amps @ 12 VDC, 0.3 amps @ 24 VDC, they’re a switch you can depend on for a guaranteed minimum life of 5000 operations.

**SNAP-ACTION SWITCHES**

Here’s a low-profile snap-action switch that has a power rating in both AC and DC. Depending on your particular application, you can select from ratings of 2.5 amps @ 110 VAC, 4.5 amps @ 12 VDC or 2.25 amps @ 24 VDC. You can specify either one or two pole versions with toggle or rotary actuation. You’ll look far and wide to match the power-handling capability of these new little switches. But equally important is their size — they require a minimum of space for circuit board mounting — .35" high, .39" wide and .854" deep for one pole versions; .35" high, .74" wide and 1.126" deep for two pole types. You get silver contacts on enclosed switches, gold contacts on those with low current construction. And contact resistance is less than 10 milliohms. These, and many other features make them the perfect ones to switch to for snap action.

**ROTARY SWITCHES**

With the wide range of features offered in these microminiature rotary switches, you can meet the switching demands of almost any design. And their construction makes them so easy to work with. They’re available as enclosed types with water sealed option, thus offering easy cleanup after flow soldering without risk of contamination.

To demonstrate their versatility, you can specify them in one, two or three pole versions, with 2 to 12 positions. They’re rated 0.5 amps @ 12 VDC, 0.3 amps @ 24 VDC. Four types of actuation are available to best meet your needs — knob, lever, thumb-wheel or screw-driver adjust. Knob types are bushing mounted but all others are designed for board-mounting. Their size — less than ½" diameter — makes them ideal for circuit board or panel mounting when space is limited.

Now you have a new world of options in specifying the micro-miniature switch that’s right for your design. The price and delivery are right too. Get all the details and specifications in Centralab’s Catalog 1614S. Just circle the reader service number or call your Centralab representative.
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The best distributor network in the country is ready to service your metal film resistor needs. Give them a call. For additional information, contact your nearest Corning Electronics sales office or Corning Glass Works, Electronic Products Division, HPA2, Corning, New York 14830, (607) 974-8652.
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For more information on these new computers, write Digital Equipment Corporation, Maynard, MA 01754.
Digital Equipment of Canada, Ltd., P.O. Box 11500, Ottawa, Ontario K2H 8K8. (613) 592-5111.

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I\textsuperscript{2}L turns up in wristwatch and a microprocessor chip

Commercially available integrated injection logic is about to make a big impact on the electronics industry.

The new circuit technique, which offers higher density than silicon-gate NMOS while promising lower cost and higher performance, has made its commercial debut in a new electronic watch produced jointly by Benrus and Texas Instruments.

A second shoe will drop on Jan. 23, when TI plans to unveil its long-rumored I\textsuperscript{2}L microprocessor. According to Charles M. Clough, vice president and marketing manager for TI's Semiconductor Div., the watch chip and the microprocessor are only a start.

TI is planning a whole new product line of grand-scale integrated devices (GSI). The components in this family will be constructed with the I\textsuperscript{2}L technology and contain a minimum of 1000 gates per chip. While early units, such as the watch chip, will be custom devices, Clough states that catalog items will be available by next year.

In describing the I\textsuperscript{2}L watch chip, the TI vice president notes that it contains more than 2000 bipolar transistors in a chip area that is 25\% smaller than the CMOS circuits with which it is now competing.

A big advantage of the I\textsuperscript{2}L approach is that it is possible to integrate the high-power digit and segment drivers, together with the time-keeping circuitry, on the same chip. With CMOS, additional driver chips are necessary. The new bipolar approach also reduces the component count from 23 for a typical CMOS watch module to five for I\textsuperscript{2}L.

TI's injection-logic microprocessor, known as the SBP0400, is reported to be a 4-bit slice processor with an execution time of between 800 and 900\,ns. The unit was developed for use in a new generation of high-speed computers, and the company is said to have given samples of the low-voltage micro to several of its customers. Versions that operate over the full MIL temperature range can be made, TI says.

The military version, the company says, can also be used under the hood of an automobile. Power dissipation is expected to be three to four times lower than that of an equivalent MOS unit.

Poof! And big reflector forms in ionosphere

The Defense Dept. has revealed that scientists have for several years been creating instantaneous giant reflectors in the ionosphere that bounce radio signals to far more distance points on the earth's surface than the normal ionosphere does. And the reflector will also handle much higher frequencies.

Normally signals in the 30-to-600 MHz band are transmitted and received in a line-of-sight mode and have a range of between 50 and 100 miles. With the artificial reflector, however, signals can be propagated several thousand miles.

The "communications relay satellite" is an aurora that the scientists create by beaming rf energy from a ground-based transmitter straight up to the ionosphere. They can dissolve the aurora instantly by turning the transmitter off. No trace of the phenomenon is left—no ecological pollution of any kind.

What happens is that the high-powered energy heats up the electrons in the ionosphere, creating scattering irregularities that are aligned with the geomagnetic field. The result is a reflector 100 miles in diameter and 10 miles thick. The enormous cloud can't be seen by the eye, but it can be photographed with an infrared camera.

The ground-based transmitter costs about $2-million. It puts out 2 million W, which, with a high-gain antenna, has an effective radiated power of from 20 million to 30 million W. The transmitter station can be manned by three people.

Research has taken place at three sites, one, near Platteville, CO, is operated by the Institute for Telecommunications Sciences. Another is the 1000-foot dish at Arecibo, Puerto Rico, managed by Cornell University. A third is at Gorkie in the Soviet Union, about 400 km east of Moscow.

Studies on the feasibility of the system as a communications technique are being carried out by Stanford Research Institute, Menlo Park, CA.

The work was originally funded by the Defense Dept.'s Advanced Research Project Agency. The agency was trying to find a way to lose up an enemy's ionospheric scatter communications and accidentally discovered that it was a good way to enhance one's own communications.

Automatic interrogator doesn't need a computer

An automatic medical-history interrogator and recorder uses multiple-track tapes and simple logic to eliminate the need for a computer.

The system, which can be used either in a doctor's office or remotely by telephone, is called DataQuest I and was developed by the Westinghouse Health Systems Dept., Pittsburgh.

Audio tapes ask the questions. The patient responds by pushing buttons on a console or on a Touchtone telephone. Language is no barrier, says the designer, John Waclo, since the system can be programmed to ask questions in one language and print the response in another.

Waclo explains that the history-taker contains three separate tapes.
The first contains all the questions. It has four tracks and can be read in the forward and reverse directions, which increases the storage capacity to eight tracks.

The multiple tracks make it easy for the system to branch in response to patient answers to questions. The tape also contains machine code for each question.

When a patient responds to a question, internal logic generates a code that controls a dictionary tape. This takes the patient's answer and converts it to an ASCII code, so it can be recorded further on a response tape or printed out directly on a printer. The response tape, which is a cassette, can hold information from 30 to 50 persons, each of whom gives about 300 responses. The response tape, Wacl says, makes it easy to batch-process the information and print out all the reports at once.

While the DataQuest I is not computerized, the project manager indicates that an interface is available to link the unit to any computer information system.

**Touchtone converted to pulsed dialing**

Increasing public demand for pushbutton telephone dialing has created a serious problem for many telephone companies: The tone signals for the Touchtone instrument will not directly operate the relays in central offices because they are designed for pulsed dialing. A recent solution permits push-button dialing with conventional central-office equipment.

The Sam/Bar Corp., Santa Ana, CA, a private telephone-equipment reconditioner, has introduced a printed circuit assembly that mounts under a conventional Touchtone pad and converts it to pulse dialing.

The converter, which contains about 95% of the circuitry, is made from an ion-implanted NMOS IC manufactured for Sam/Bar by the Nitron Div. of McDonnell Dougals Corp., Cupertino, CA. The chip uses a first-in/first-out shift-register memory to store numbers as they are punched. The chip simultaneously generates standard pulses. The remaining components on the PC board consist of a regualtator and switching transistors to open and close the telephone circuits.

According to Gene Watkins, project engineer with Sam/Bar: “MOS was an absolute necessity in devising a converter to install in telephone instruments, because it was important to derive all operating power from the existing telephone loop current. The phone companies are intent that external power be kept away from their lines. We use about 4 mA at 5 V from the standard 24-to-25-mA loop current.”

Another feature of the converter is toll-call restriction. With a screwdriver adjustment, a phone can be prevented from dialing outside lines, outside operators or long-distance numbers.

Sam/Bar will either sell the boards or the complete touchpad converters for installation on any standard rotary dial phone. Or the company will modify phones as part of a reconditioning program.

**Laser unit to monitor driving visibility**

A gallium-arsenide semiconductor laser has been combined with an optical receiver to produce a new instrument for monitoring visibility along highways.

Known as the Model VS-1, by International Laser Systems Inc., Orlando, Fla, the unit will get its first tryout next month along a stretch of the New Jersey Turnpike.

The visibility sensor will detect fog, snow, smoke or blowing dust and transmit information on visibility by cable to the New Jersey Turnpike Authority headquarters. There someone monitoring the system can actual-local warning signs to alert motorists of conditions ahead.

The instrument works by measurement of the transmittance of a laser beam through the atmosphere. The distance between the transmitter and the optical receiver can vary between 250 and 2000 ft. The minimum resolvable visibility is 40 ft.

The transmitter contains a built-in sighting telescope that allows an installer to align the transmitter with the receiver. Alternately the receiver can be aligned with the transmitter via an integral signal-strength indicator.

Heaters in both the transmitter and receiver units keep the windows clear during fog or snow conditions.

**Digital-image system reconstructs in color**

A high-speed digital image reconstruction system that can produce full-color transparencies exposes over 28,000 picture elements per second—each 100 µm square—on a 10-by-10-inch film.

According to Glen Marcil, director of marketing for Optronics International, Chelmsford, MA, a principal factor in development of the Colorwrite C-3300 system was the use of a special white-light source—a glow crater tube. The tube can be modulated at high speed, yet it retains its white-light purity over an intensity-modulation range of 100:1.

The output of the glow tube is linear and is directly proportional to input current, Marcil points out. As a result, the current through the tube, which emits light in the 4000-to-7000-Å band, is pulse-modulated. The level of each pulse, which controls the exposure for each picture element, is defined, by an 8-bit data word that is stored in a buffer memory.

The system, which was developed to reconstruct color data for the Earth Resources Technology Satellite, can also be used in image enhancement and nondestructive testing, Marcil says. In the latter application, an X-ray is scanned and the various shades of gray in the X-ray are reproduced in color. With color it is easier to detect defects, Marcil says.

The system has a transparent rotating drum, and the film is clamped around it. The glow tube and its optical system move along the inside of the drum.

A wheel containing red, blue and green filters is used. One filter is inserted in front of the glow tube for each pass of the film. For full-color exposures, three separate passes are required, Marcil says. With a 100-µm picture element, about 30 min are required for three passes.
JUST HOW GOOD IS THE TELETYPE MODEL 40?
We think our data terminal system is so good nothing even comes close.

In fact, we believe the Teletype® model 40 system is so good it'll change the way business looks at data. We're that sure it's that good.

Here's why:

It's a complete, versatile, reliable terminal system delivering maximum efficiency in a wide range of applications. From message communications to computer input/output on switched network or private-line systems. Right now, the model 40 system is being used by airlines, news services, brokerage firms, manufacturers, law enforcement agencies and time-sharing services.

Significant features of the system are speed, ease of data preparation and editing, compactness and extremely low maintenance. And since the model 40 is completely modular, you can forget about obsolescence.

It's designed to grow as your needs grow.

Data is presented with extreme clarity on the big, 13-inch screen. Characters are 35 percent larger than standard print size and are formed on a 7 x 9 dot matrix. Screen capacity is 24 lines of 80 characters each for a total of 1,920.

Teletype's exclusive solid-state design makes the model 40's fast (up to 2400 wpm), heavy-duty impact printer the most cost-effective unit on the market. Its simplicity of design makes it one of the most reliable printers we've ever made. And after more than 60 years experience building printers that set the standards for reliability, that's saying something.

It took a total corporate commitment to come up with something as good as the model 40. For example, we had to develop and manufacture our own MOS. It didn't come easy, but we think it's worth it. Because the solid-state components throughout the system deliver exceptionally high reliability. And the self-diagnostic circuitry and design modularity significantly reduce downtime and maintenance costs.

Operator comfort and efficiency are increased by human-engineering efforts like a brightness control and screen tilt, plus a glare-reducing display tube and an easy to operate keyboard.

The Teletype model 40 data terminal system. It's every bit as good as you've heard.

And probably even better.

The Teletype model 40 system.
The Teletype model 40 is so good it's worth looking into.

Listed below are some of the general specifications of the model 40 system.

**Display**
- 5½” x 11¼” viewing area on a 13” display tube.
- High resolution 7 x 9 dot matrix character presentation.
- 127 characters of ASCII code displayed (all except backspace).
- 1,920 character screen capacity composed of 24 lines of 80 characters per line.
- Anti-glare screen, brightness control plus tube tilt.
- Constant image cursor—when cursor is positioned over a character, character becomes a negative image.
- Refresh rate: 60 frames/second.

**Operator Console**
- Standard keyboard generates 127 ASCII characters.
- Six cursor positioning controls; Home, Return, Left, Right, Up and Down.
- Five data editing controls; Clear, Character Insert, Character Delete, Line Insert and Line Delete.
- Basic terminal controls; Send, Receive, Local.

**Optional Page Printer**
- Impact printer provides hard copy of data stored in the display memory, or of data received directly from the communication line.
- Printing speed is over 300 lines per minute (monocase), or 220 lines per minute (full upper and lower case).

**Optional Features**
- Expanded memory, scrolling, protected format, highlight, tabulation, form send. Plus more.

**Technical Information**
- Speed: serial interface; 105 or 120 cps. Code: 1968 USASCII.
- Method: transmission is serial by bit and character with low order bit transmitted first.
- Synchronization: asynchronous; 1 start bit, 7 information bits, 1 parity bit, 1 stop bit.
- Communication line: switched network at 105 or 120 cps.
- Bell System Data Sets 202C, 202R or equivalents. Other speeds optional.
- Error control: optional vertical parity detection on received data (substitute character printed for errored characters). Keyboard generates even vertical parity.
- Power requirements: 117V AC ± 10%; 50-60 Hz.
- Operating environment: + 40° to 110° F, 2% to 95% humidity.

For complete technical data, please contact our Sales Headquarters at 5555 Touhy Avenue, Skokie, Illinois 60076. Or call TERMINAL CENTRAL at (312) 982-2000.

Teletype is a trademark registered in the United States Patent Office.
While Japan's economy is reeling from massive inflation and staggering under the impact of quadrupled oil prices, her electronics industry is fighting back.

In virtually every segment, from consumer electronics to sophisticated test equipment, her industry is offering new and better products—some of them dramatic. Many of these products could be seen at this year's Japan Electronics Show in Tokyo. They may have contributed to the success of this year's show in comparison with last year's, which was held in Osaka. But the products weren't the only factor.

The Tokyo show, which has taken place in even years since 1958 (originally as the TV and Radio Parts Show) has always drawn more engineers, and thus has always been bigger, than the Osaka Show, which takes place in odd years.

From an attendance viewpoint, this year's show may also have been helped by the People's Republic of China Exposition, which was held across the mall at the Harumi Exhibition Pier.

George Rostky
Editor-in-Chief

Baumkuchen magnets from Fuji Electrochemical use the thin spiral construction of a famed German cake—with thin ferrite sheets rather than dough. The magnets, with radial rather than longitudinal lines of force, are more powerful than others of the same size and weight.

While the Tokyo show usually draws 30% more visitors than the Osaka show, the show management this year predicted that attendance would top 350,000 or 450,000, compared with 250,000 for Osaka last year. These figures should not be compared too quickly with attendance figures of about 30,000 for the IEEE or Wescon shows, as the traditions in Japan are different.

The seven-day shows in Japan are open to the public. So a housewife, wandering through the exhibits of silks, furniture and oil-field models at the China Exposition, could walk across the mall to the Japan Electronics Show and see the latest color TVs, stereo receivers, scopes, power supplies, ICs and computers. If she leaves one exhibit hall and visits another, she is counted again—as she is if she walks out of any of the three exhibit pavilions and returns.

Further, while attendance figures at U.S. shows are normally drawn from registration data, the
Some of the world’s tiniest cores, from TDK Electronics, these are (clockwise from top left): sleeve pot, bobbin, another bobbin, rod, and bobbin slipping into a sleeve.

Zinc-oxide varistors from Matsushita now offer voltage ratings to 6.6 kV (center). They are used mainly as surge absorbers.

This four-pole coax switch for frequencies to 1 GHz is part of a new Fujitsu line.

Counts at the Japan Electronics Show are based on figures provided by men stationed at the entrances with hand-held clicker-counters. These figures are later modified by show personnel, who assume that the men at the entrances have missed thousands of visitors.

Tour of the Crown Prince

But there was one visitor they didn't miss—Crown Prince Akihito, son of Emperor Hirohito. While the prince did not see all 1315 booth units of 432 exhibitors, he did see some of the most impressive products at the show.

He spent most of his time at 10 exhibits, where he saw a wide variety of products, including consumer-electronic equipment (San- yo, Pioneer and Victor Co. of Japan), transformers for microwave ovens, (Tabuchi), closed-circuit color TV (Hitachi), a video facsimile storage system using slow-scan TV for transmission over telephone lines (Nippon Electric), liquid-crystal displays (Sharp), test equipment (Yokogawa), a microcomputer (Toshiba) and advanced semiconductors (Matsushita).

Broadly, these products reflected much of the advanced work in Japanese electronics. The major efforts appear in several areas.

Consumer electronics for the ear

An omnidirectional loudspeaker from Pioneer Electronics uses a piezoelectric polymer film as the vibrating element. Since the film has extremely low mass compared with that of the usual loudspeaker cone, and since its impedance is almost entirely capacitive, the speaker requires very little power and provides an unusually linear, distortion-free response in all directions (though it can be shaped to provide any directional pattern).

Its characteristics are similar to those of an electrostatic speaker, without requiring an additional high-voltage power supply.

The loudspeaker is now in development along with an extremely low-mass, high-compliance phonograph cartridge and a low-mass microphone. Stereo headphones using the film are already commercially available.

For the system between microphone and loudspeaker, the Victor Co. of Japan demonstrated quadraphonic stereo using the CD-4 system. There was more activity, though, in TV. Hitachi’s main feature was a closed circuit color-
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Forty years ago, ERIE foresaw a need and introduced the first ceramic capacitor to U.S. markets. Today, more than 7000 people—working in a million-plus square feet of plant space—in seven nations...are still dedicated to fulfilling customer needs. Our state-of-the-art ceramic technology continues to lead the way in the development of smaller, more efficient ceramic capacitors, both fixed and variable. And ERIE's line of high quality components is as broad as the markets we serve. So when knowledgeable people think ceramic capacitors, increasingly, they think ERIE. To remain number one in our competitive industry, we have to be responsive to your needs. We think we are. Try us.

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Erie, Pennsylvania 16512
TV system. And Sanyo showed a small video color cassette recorder using half-inch tape.

**A quick switch**

Perhaps less colorful than color TV, a new line of switches from Fujitsu can prove useful to engineers who must switch high-speed signals. The basic configuration is a Form A coax switch, suitable for signals from dc to 1 GHz. But units can be combined in a single package to provide other arrangements. A 5 Form A combination costs about 50,000 yen, which, at a recent exchange rate of 300 yen per dollar, works out to about $170 in small quantities.

Another manufacturer, Ise Electronics, a leader in fluorescent displays, is making a different kind of switch in expanding its traditional line of fluorescent displays for calculators and test equipment to include displays for digital clocks. The first versions are four-digit fluorescent displays, about 0.43-inch high. Later versions will be smaller and larger and will come with a colon and am/pm indicator.

Switching from its concentration on bare displays for the first time, Ise introduced a basic digital clock that uses its displays. The clock, the “Comet 12,” is available on an OEM basis and includes a 24-hour alarm and an eight-minute snooze feature.

**Semis—simple to complex**

While most of the effort of semiconductor manufacturers is aimed at LSI developments, there’s occasional but significant progress in discrete, small-signal devices. An important example is the “lambda” diode, so-called by Matsushita because of the shape of an important segment of its EI characteristic curve. This diode is intended mainly for use as an oscillator in the 2-to-3-MHz range. But it’s also useful in low-voltage warning circuits, overvoltage protection circuits and a host of other applications. In sample quantities, it’s now available for 500 yen (about $1.70).

Matsushita Electronics has moved another step ahead in discretes by boosting the surge-

![A low-mass piezoelectric film is the vibrating element in Pioneer Electronic's developmental omnidirectional loudspeaker.](image)

voltage ratings available in its zinc-oxide varistors—used mainly as surge absorbers—from 3.3 kV to 6.6 kV.

But the company hasn’t restricted its efforts to discrete devices. One of its more dramatic developments is a new $2 	imes 512$-bit bucket-brigade device that is just going into production. A silicon-gate PMOS device, it uses a tetrode configuration to improve charge transfer.

The BBD works with clock rates from 10 to 800 kHz and consumes no more than 4 mW, including the dissipation in a source-follower resistor. The initial price in sample quantities is 5000 yen (about $17). In production quantities, the price should dip to about 3000 yen.

Equally impressive are memory developments from Fujitsu. The company is now working on a prototype 8-k, n-channel RAM with 120-ns access time. In production are 1-k p-channel RAMs as well as 1-k, 2-k and 4-k n-channel RAMs.

LSI developments, of course, are not restricted to memories. Toshiba, for example, demonstrated its TLCS-12 microcomputer, which uses 12 microprocessor chips. The computer uses a 1.2-MHz timing-generator chip and a controlled microprogram offering one microstep in 800 ns and one full instruction in 10 microsteps, or 8 µs. The machine includes 18 basic instructions.

**Mag memories alive and well**

While there are some who feel that semiconductor memories will take over the world, others believe that magnetic memories will have a place for many years to come. Toko, for one, is offering a line of small-capacity, woven, plated-wire memories. As one might expect, Toko emphasizes nonvolatility. But the company also stresses flexibility: its Mini-ROMs, with minor modification (in one case by the flick of a switch), can be used as ROMs, electrically alterable ROMs, RAMs, or partial ROMs, in which the basic 1024-word × 8-bit or 9-bit system is divided into four 256-word units, each of which can serve as RAM or ROM.

Mini-ROMs are currently available in four versions. The slowest unit, Mini-ROM-A, has 1024 8-bit words (or 2048 4-bit words) on a board of about 8 × 10 × 1 in. It has only one sense amplifier, so readout is serial and access and cycle times are somewhat leisurely at 2.4 and 3 µs. RAM and EAROM capability are provided by an add-on 3-3/8 × 3-3/4-in. piggyback board. Including the board, Mini-ROM-A sells for $260 in quantities of 1 to 10.

Mini-ROM-B, a 1024 × 9-bit memory, fits on a smaller board, 8 × 8 × 3/4 in. and offers parallel readout, 0.5-µs access and 1-µs cycle time. It has switch-selectable RAM or EAROM operation and costs $380 in 1 to 10.

Toko’s Mini-ROM-C is quicker, with 300-ns access and 600-ns cycle...
The Schottky sandwich.

The Augat Schottky board is something you can really sink your teeth into.

On the outside there are two ground planes, top and bottom, instead of just one.

On the inside there's a special voltage plane that's made of a generous slice of copper.

Laminated together, it makes a very neat sandwich that goes perfectly with Schottky TTL design.

For example, it increases distributed capacitance by as much as 400 percent. And at the same time, it greatly reduces high frequency noise.

It has ground embraced socket and I.O. connections that enhance isolation of signal interconnections.

Individual DIP decoupling capacitor zones and electrolytic-type decouplers at every power entry point.

And voltage and ground socket pins that are soldered directly to their planes to drastically lower impedance.

All in all, the Augat Schottky board can save you up to 90 percent in breadboarding and prototyping time. Tens of thousands of dollars in start-up costs. And many expensive hours in field maintenance.

The Augat Schottky boards are standard catalog items available right now in any quantity and in any multiple of patterns, from 30 up to 180.

If you'd like a taste of what it's all about, contact any of our worldwide distributors or Augat, Inc.,

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Tel. 617-222-2202. TWX 710-391-0644.
time. It's available as a 1-k × 9-bit memory or as a memory with two 512-word sections, each to serve as RAM or ROM. It fits on a 6-1/4 × 8-3/4 × 1-in. board.

Sub Mini-ROM, the last of the series, is smaller and slower, with 512 4-bit words, 4-µs access and 5-µs cycle. It fits on a 6-1/4 × 7-7/8 × 5/8-in. board.

Ferrites for old and new

Toko is not alone in nonsemiconductor memories. Many manufacturers are heavily promoting core. Fuji Electrochemical, a major supplier, is making a particular drive for its small-capacity, nonvolatile core RAMs. These include on-board hybrid and monolithic drive, sense and decode circuits. Memories range from 128 × 4-bit RAMs that cost about 3 cents a bit to 4096 × 9-bit units that cost 1.2 to 1.5 cents a bit.

But Fuji doesn't restrict its ferrite efforts to core memories. The company has developed a "Baumkuchen" magnet, which derives its name from the shape, but not the flavor or texture, of a delectable German cake. The magnet is made by rolling, then pressing, thin 0.1-mm sheets of ferrite tape up to 2 m wide into cylinders, then slicing off desired widths.

The unique spiral construction provides radial lines of force with a remarkably high-energy product of 2.5 to 3 × 10⁶, as against a BH of 1 to 1.2 × 10⁶ for conventional, unoriented magnets. The Baumkuchen has about triple the performance of conventional magnets at, initially, about a 70% price premium.

The new magnet has a residual flux density of 3500 to 4000 gs and a coercive force of 2500 to 3000 Oe. It's aimed mainly at applications in stepping motors, brushless dc motors and automotive generators.

Equally unusual are some ferrite products from TDK Electronics, which is known throughout the world for its magnetic tape. The new products include some of the world's smallest cores. Bobbin cores, for example, are available with 1.5-mm over-all length and outer diameter. Sleeve cores have lengths and ODs of 2.79 and 2.16 mm, respectively; rod cores, 2.79 and 0.787 mm; pot cores, 2.6 and 3.3 mm; and poroids have IDs down to 2 mm.

Switches can select ROM, RAM or EROM operation in Toko's Mini-ROM-B, a 1024 × 9-bit woven, plated-wire memory.

TDK has also developed a ferrite electrode with enormous corrosion resistance. At normal temperatures, the electrode is practically undissolvable in aqueous solutions of hydrochloric acid or caustic soda. It has 10 times the corrosion resistance of magnetite, 100 times that of graphite. Aimed at applications like desalination, water treatment and chlorine production, the electrode can be made with the resistivity from 0.01 to 0.5 Ω-cm.

Another example of TDK's work in ferrites is a doppler radar transmit-receive module using a calcium zirconium garnet substrate for the circulator, crystal mixer and filter, and directional coupler. The circulator is formed by printing a gold pattern on both sides of the magnetic garnet, rather than by mounting a YIG circulator on an alumina substrate or in a hole in the substrate.

The calcium zirconium offers much lower porosity and higher density than alumina does. The precise pattern printing made possible by the technique allows substantial cost savings. Initially, in quantities of 10, the new module costs about 150,000 yen ($500), while traditional YIG modules cost about 200,000 yen.

To round out its new ferrite products, TDK introduced two materials—the super-low-loss H68-H3 and super-high-µ H5E. The former has a loss factor less than 1.2 × 10⁻⁶ at 100 kHz and initial permeability (µ) of 1300. The latter has a µ of 10,000 and a loss factor of less than 15 × 10⁻⁶ at 10 kHz.

Advances in materials technology—in a different direction—come from Fujitsu, which is working with single crystals of lithium tantalate, lithium niobate and lead molybdenite. Depending on composition and cutting orientation, these lend themselves to a wide variety of applications because they offer higher time and temperature stability than competing material.

Applications for the lithium tantalate include optical modulators and shutters, acoustic transducers, surface-wave delay lines and filters and pyroelectric devices.

The lithium niobate is intended mainly for ultrasonic transducers,
There's nothing new about a 2N3055 but there's a powerful difference in this one.

That's why we call ours the 2N3055C * "C" designates it as the Cadillac of power transistors.

Compare the specs below and see at a glance why Sensitron's upgraded version of the workhorse 2N3055 . . . the 2N3055C . . . is your best bet for a wide range of power transistor applications.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Conventional 2N3055</th>
<th>RSM Sensitron &quot;Cadillac&quot; 2N3055C</th>
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<td>SOAR</td>
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<td>70 V @ 2.15 A</td>
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</table>

Write or call for more information or applications assistance on the 2N3055C and other RSM Sensitron single diffused power transistors.

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The good test

Two basic types of test equipment have tended to monopolize recent advances—digital meters and graphic recorders. The advances in these instruments come mainly from three vendors: Takeda Riken, Yokogawa Electric Works (YEW) and Rikadenki.

The most impressive DVM comes from Takeda Riken, which, four years ago, developed the world’s fastest pulse generator, a 1-GHz unit with 300-ps rise time and which will soon introduce a super-speed LSI-memory tester with a 50-MHz clock.

The company’s 6501, to be shown at the IEEE show in April, displays up to 11999999 for measurements of voltage, resistance, V or R ratio and temperature. At the most sensitive of its six voltage ranges—100 mV +20% overrange—it offers resolution of 10-nV. On the lowest of five resistance ranges—1 Ω + 20% overrange—it can resolve 100 nΩ. With a suitable transducer, it can resolve temperature to 0.001 C.

At about $20,000, the 6501 is fully programmable and provides automatic zero and full-scale calibration with each reading—once a second for voltage measurement, once every two seconds for resistance and ratio measurements.

Further, the instrument uses microprogramming to provide average readings and standard deviations or to linearize transducers for temperature measurements.

Though lacking the astounding resolution of the Takeda Riken meter, two instruments from Yokogawa are equally impressive in their own way. YEW’s 2503 and 2504 are true-rms meters with maximum readings to 11990 for voltage, current and power. The 2503 provides ranges of 3 to 600 V, 100 mA to 30 A and 300 mW to 18 kW at frequencies of dc or 25 Hz to 2 kHz for voltage and current, and 40 Hz to 1.2 kHz for power.

While providing high-accuracy digital readings of voltage, current and power, the 2503 simultaneously offers analog presentations of voltage and current on small, edge-wise meters so the user can easily observe directions of change. Available in single or three-phase versions—with BCD output and remote control as standard features and analog output as an option—the 2503 recently received an award for excellence from Premier Kakuei Tanaka.

Its sister instrument, the 2504, uses plug-ins to provide a choice of features. A single-input plug-in provides ranges of 100 V, 5 A and 500 W, while a multirange module offers five ranges from 30 to 300 V (with resolution to 10 mV), five ranges from 500 mA to 10 A (with resolution to 100 µA) and, effectively, 25 ranges from 15 W to 3 kW. The 2504 offers specified accuracy (which varies with frequency to a worst case of 0.5% of range from 25 to 50 Hz and 60 Hz to 1 kHz) at voltage crest factors to 4 and current crest factors to 2. Depending on plug-ins selected, the price of the 2504 ranges from 400,000 to 700,000 yen ($1330 to $2300).

Yokogawa has extended the plug-in concept to its line of X-Y recorders, in which the 3083 offers a selection of eight plug-ins, including a de-voltage unit with maximum sensitivity of 5 µV/cm. The instrument accepts roll-chart paper or sheets, and it records on a 250 × 8-mm area with a felt-tipped pen, ballpoint pen, pencil or ink-fed pen. The mainframe costs 250,000 yen ($830), while plug-ins, depending on number of ranges and sensitivity, 14,000 to 70,000 yen ($47 to $235).

More unusual is Rikadenki’s Computing Unit, a powerful accessory for single-pen or multiple-pen graphic recorders. The unit is a mainframe with a built-in power supply and one or more plug-in signal conditioners. These include a preamp with adjustable gain from 10 to 10,000, an adder, a multiplier and divider, an integrator and a differentiator.

Using the Computing Unit with a three-pen recorder, for example, one can record voltage with one pen, current with another and, with the multiplier/divider plug-in, power with the third pen.
When we introduced the SPC-16, we promised it would be the world's most powerful, versatile, cost-effective family of minicomputers.

It was. It still is.

The SPC-16 isn't the lowest priced hardware you can buy. But it will give you the lowest cost solution.

Through advanced systems architecture, simplified interfacing and a powerful instruction repertoire, the SPC-16 allows you to minimize programming, interfacing and memory costs no matter what size your system is.

**Six mighty minis.**

The SPC-16 family consists of six minicomputers offering a choice of three memory cycle times (800ns, 960ns and 1440ns), memory expansion to 128K using efficient 16K boards, and two different packaging configurations.

If you build a system around the SPC-16, it will do more work for less money than any other system you could build.

And that translates into more profits.

We know it for a fact. In the past few years, we helped a lot of OEMs get the edge on their competition by designing our product into their products. We helped a lot of end users solve a lot of tough, tight-budget applications. And, we produced some cost-effective systems of our own.

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Laser technique promises repair of ICs from ‘spares’ on the chip

Repair of integrated circuits on the chip or wafer level is now possible with a new laser technique that uses nanosecond-wide pulses to form connections between the aluminum and diffused silicon layers of a conventional MOS structure. The approach is attractive for read-only memories and programmable logic arrays.

Developed at IBM’s Thomas J. Watson Research Center, Yorktown Heights, NY, the new technique was described at the International Electron Devices Meeting in Washington, DC, earlier this month. Other advances in technology discussed at the meeting included nonvolatile charge-coupled-device memories, Josephson-tunneling logic and electron-beam addressed storage systems.

In describing the laser-connection technique, Stanley E. Schuster, one of the researchers on the project noted that dye laser pulses from 2 to 6 ns wide were used. The shortness of the pulses, he explained, minimizes thermal diffusion normally caused by a laser beam and prevents damage to structures surrounding the contact site.

3 major steps involved

The connection is formed in three steps and involves a number of pulses, he reported. First, a hole is opened in the aluminum layer, with material removed primarily by vaporization. Then the silicon-dioxide insulating layer is removed by a controlled microexplosion, caused by thermal stress, or vaporization, of material at the silicon-dioxide/silicon interface.

Finally, Schuster explained, a conducting path is formed when the molten silicon flows into contact with the aluminum.

According to Schuster, aluminum-to-silicon contact resistance for 5-µm diameter connections is dominated by “spreading” resistance and corresponds roughly to that of conventional contacts. Thermal and electrical stress tests on the laser contacts indicate a reliable process, the researcher reported. Connections have undergone over 2000 hours of testing without any failures.

Schuster sees the primary application of this technique in programmable devices that are needed in small quantities—not enough to justify a special set of masks.

The laser approach has several advantages over the “blasting” techniques currently used to program devices, Schuster said. The major one is that it is possible to connect selectively only the good parts of a circuit. This is easier than disconnecting the bad parts of a blast-programmable device, because it is often difficult to determine exactly where these units failed.

As for repairing defective chips, Schuster noted that this technique would be most appropriate for bus-oriented devices that have several functions connected to one bus on the same chip. If a particular function element is defective, it can be disconnected with a laser pulse and a spare—contained on the same chip—can be used to replace it.

The NOVCAM memory

A new charge-coupled device known as a nonvolatile charge-addressed memory (NOVCAM) was described by Marvin H. White, a CCD researcher from the Advanced Technology Laboratory of Westinghouse Defense and Electronic Systems, Baltimore. The CCD memory is made nonvolatile, White explained, by combining it with an MNOS (metal nitride oxide semiconductor) device.

In initial attempts to combine these two structures, he reported, the MNOS storage site was placed inside a stepped dielectric, two-phase, CCD shift register. This structure, however, had problems. Inadequate charge-handling capability resulted in poor write characteristics, spurious pulses from high-voltage clocks made the write/inhibit operation ineffective,
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and a large access time to the first bit made for a poor read operation.

To overcome these problems, the NOVCAM structure was developed. In this configuration the memory cell is composed of a CCD shift register and a thin-oxide MNOS memory structure in parallel with it. This provides separate locations for signal address and storage.

In describing the operation of the new memory cell, White noted that it is addressed like any other CCD structure. Then voltage is applied to a transfer gate, and charge from the CCD is transferred to the MNOS device. This transfer of charge results in a collapse of the surface potential beneath the MNOS device. Once the surface potential is collapsed, the oxide electric field increases, and the tunneling of signal charge from the surface channel to deep traps near the oxide/nitride interface begins. It is the trapping of charge at this interface that makes the device nonvolatile.

According to White, the write voltage is the same as the CCD clock voltage—20 V. Pulse width is about 10 µs. The reading out of data is nondestructive and typically takes 1 to 2 µs, which is the CCD transfer time. The read voltage required is only 2 V. These read and write voltages are lower than those required for MNOS memories that use conventional transistor structures.

To date, only a 64-bit four-phase shift register has been produced. Work is proceeding, however, on a high-density device, White indicates, and masks will be ready soon. The next step in this project is to produce a demonstration chip that would have 8-k bits of memory. The cell size for such a device would be 15 by 40 µm, for a total of 0.9 sq. mils. Included in the cell is the CCD for transporting the data to the memory site and a parallel stabilized charge injector for high-speed readout.

Beyond the 8-k chip is a 32-k device. The memory, including clock drivers, signal reconstruction circuitry and other supporting circuits, can be put on a chip that measures 200 mils on a side.

Both the 8-k and the proposed 32-k memory chips will use a three-phase clock instead of the four-phase used on the 64-bit device. This switch to a three-phase clock makes it possible to save up to 25% in chip area.

Josephson shift register made

The Josephson shift-register element discussed at the Electron Devices Meeting was covered in a paper by Y. L. Yao and D. J. Herrell of IBM's Thomas J. Watson Research Center, Yorktown Heights, NY. The authors described an experimental 8-bit static shift register that operates with all data patterns at a maximum shift rate of 160 MHz, and with limited patterns at 200 MHz. The average power dissipation was given as only 20 µW per bit.

Josephson-tunneling logic devices are based on the phenomenon of superconductive tunneling between two closely spaced superconductors at a temperature of 4.2 K. Until now, the authors indicated, only Josephson logic gates have been investigated experimentally.

The basic shift register is formed when two three-input gates Q1 and Q2 (see illustration) are cascaded in series and operated in a master-slave mode from externally clocked current supplies, I1 and I2. Data are transferred from Q1 to Q2 and then from Q2 to Q3 under the control of two strobe pulses, IC2 and IC1. The current level of the strobe signals is 2i to ensure that a data ONE condition of i, together with the strobe signal, will exceed the 3i threshold of the Josephson gate.

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Electron-beam memory arrives

Electron-beam memories, which promise high density at high speeds, have been in development for several years. Now, according to John Kelly, a researcher at Stanford Research Institute, Menlo Park, CA, they are ready to go into commercial systems. In a paper on electron-beam addressed memory tubes, Kelly pointed out that a 65,536-bit memory module had been developed and delivered to the Air Force Avionics Laboratory at Wright-Patterson Air Force Base, Dayton, OH. The unit consists of a single-tube system operating from a memory exerciser, which acts as a source of data and addresses for the memory testing.

Although the bit capacity of the tube is small and the delivered system consists of only one tube, Kelly noted that progress to date verifies that tubes of approximately 4 megabits can be made now.

The time is ripe to produce a commercial memory with 18 such tubes, for a system capacity of 64 megabits, Kelly said. Electron-beam addressed memories, he added, promise to become a leading contender for low-cost, large-memory systems, with fast access times, high reliability and data rates.

Referring to the system he developed, Kelly noted that two items were the keys to a successful device: the nature of the storage target and the means by which stored information can be repeatedly located or addressed.

The target used in the Stanford system is an electro-static storage target. It is of metal-oxide-silicon construction with holes etched into the oxide. Two external connections are made—one to a metal gate and the other to the low-resistivity silicon base. A third electrode is deposited in the bottom of the dielectric holes, providing a microcapacitor, or mucap, electrode on which charge can be stored. A major advantage of this structure, Kelly pointed out, is that the electron beam approaching the target sees essentially only the potential of the metal gate, which is normally held at ground.

When data are stored, a binary ONE is represented by storage of a −40 V charge on the mucaps, whereas a ZERO is represented by 2 V. In actual use, more than one mucap is used to store data. This is because it is desirable that a bit location be determined by the point of incidence of the electron beam on the target, and not by the structure of the target. Therefore the structure is made fine in comparison with the beam diameter, and as many as nine mucaps are used for each bit. Occasional missing mucaps do not impede operation. In addition data may be written along a curved path and raster distortion, "within reason," does not affect performance.
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Senator Glenn viewed as R&D proponent

Research and development stands to gain a banner carrier in the election victory of former astronaut John Glenn in the Ohio senatorial race. The retired Marine Corps colonel would seem a natural for a spot on the Armed Services Committee and the Aeronautical and Space Sciences Committee, but being at the bottom of the pole in seniority he will have to be content with what comes his way.

Glenn has left the strong impression that he is more interested in technology than defense, and informants say he wouldn’t be unhappy to take two committee seats now occupied by the Ohio incumbent—Aeronautical and Space Sciences, and Interior. The Interior Committee will oversee the Energy Research and Development Administration, which is slated to take over all R&D of that nature on Jan. 1. This will amount to some $2-billion annually, a hefty bit of which could be in electronics.

Navstar: A navigation system for the 1980s

The Navy has served warning that while no firm decision has been made yet on the future of Navstar satellite navigation system, now under development, users of Transit, or those considering future use, should look toward the 1982-1984 period. If a go decision is made on schedule the Navy says it will be able to start the phaseout of Transit at that time.

The Defense Dept. says it’s unlikely it will maintain both systems. Transit, if it remains, will need support from some other Government agency.

Gen. Samuel C. Phillips, commander of the Air Force Systems Command, recently told an Air Force audience that the Navstar global-positioning system would provide worldwide navigation aid after 1985. The system is to consist of 24 satellites—three groups of eight satellites operating in separate orbits. Position errors are expected to be no greater than 30 feet 90 per cent of the time.

Musical chairs altering U.S. defense setup

Recently announced closings of military bases and realignment of functions by the Defense Dept. will have an impact on the electronics industry, but mostly in transfers of activities rather than cuts in funding. The major changes will affect the Air Force’s Rome Air Development Center in New York State and the Air Force Communications Service at Richards Gebaur Air Force Base in Kansas.

The electronic warfare function at Rome will shift to Wright-Patterson AFB, Ohio, to become a part of the new Wright Technology Center, which will consist of four laboratories: propulsion, avionics, flight dynamics and materials. The Aerospace Research Laboratory there will be deactivated. Rome’s command, control and communication function will move to the Electronic Systems Command complex at Hanscom Field in
Massachusetts.

The environmental research activities of the Cambridge Research Laboratory at Hanscom will move to Kirtland AFB in New Mexico, where the Air Force Special Weapons Center is being deactivated; however, the Air Force Weapons Laboratory will remain active at Kirtland. The Air Force Communication Service will move to the Military Airlift Command at Scott AFB in Illinois.

Other major changes planned by the Defense Dept. include the closing of both the Frankford Arsenal at Philadelphia and Ellington AFB, Houston, TX.

Rises in engineer salaries forecast

While the economic picture at the moment isn't bright, a new report issued by the Washington-based National Planning Association forecasts better days for engineers. The report, “Technical Change and American Enterprise,” by J. Herbert Hollomon, director of the Center for Policy Alternatives, at the Massachusetts Institute of Technology, says that in 1975 salaries of engineers should increase dramatically, because “we will have one-half the annual growth of engineers we had five years ago, and industry will have increased its ability to pay for them and its general need for them.”

According to the forecast, another five to 10 years will be needed to raise the supply of engineers to meet demand and still another five years after that to create a balance of supply and demand. The supply system went out of kilter between 1968 and 1972, when the ratio of engineers to total college students dropped from 23 to 9 per cent. About one million engineers are currently in the nation’s inventory, and the Institute of Electrical and Electronics Engineers estimates that today the average number of annual openings for engineers is around 73,500.

Capital Capsules: NASA has announced the development of a solid-state data recorder that has no moving parts. The agency says the new device may replace magnetic tape recorders aboard spacecraft in the 1980s. The technology is based on magnetic bubbles in specially prepared garnet chips. NASA, which is shooting for a unit with 100-million-bit capacity by 1978, notes that the potential commercial applications are many—such as electronic control systems in mass transit. . . . The Air Force is seeking ways to improve the bandwidth efficiency of digital microwave communications systems. State-of-the-art modulation techniques require excessive amounts of rf bandwidth; the Air Force wants a contractor to investigate cross-polarization techniques. With these, the bandwidth efficiency can be doubled; however, the effects produced can render the performance unacceptable. Developing algorithms is seen as a solution. . . . NASA is in the market for 43 and 85-GHz coupled-cavity traveling-wave tubes for space use. Wanted are designs of 100 and 200-W TWTs with operating frequency ranges of 41 to 43 GHz and 84 to 86 GHz. . . . Two new standards for television monitors have been developed by the Electronic Industries Association. They are “Electrical Performance Standards for Direct-View Monochrome Closed-Circuit Television Monitors 525/60 Interlaced 2:1” and “Electrical Performance Standards for Direct-View, High-Resolution Monochrome Closed-Circuit Television Monitors.”
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Making it tough for European engineers

Associate Editor John Mason, home from a month in Europe, brought back a grim picture. John visited scores of engineers in dozens of plants in 14 cities in eight European countries. Though his main mission was to gather impressions about Electronic Design and Electronic Design's GOLD BOOK, he learned a lot about European attitudes toward American companies. In sum, many Europeans are miffed.

We should understand that no European goes out of his way to buy American. For convenience, if for no other reason, the French engineer would rather buy in France, the British engineer in Britain and the German engineer in Germany. But often these engineers need to buy from the United States because the U.S. product offers some advantages. And that's where American manufacturers make it tough.

The engineer learns about a product in Electronic Design or the GOLD BOOK (which now has more than 11,300 users in Europe), then gets in touch with the local representative. But the rep doesn't know anything about the product. So the engineer writes to the manufacturer's home office in the United States and, if he gets a reply at all, he is referred back to the rep—where he started. Distributors are worse.

"If you can believe it," said one engineer, "distributors don't even know what lines they're carrying. They handle one line today and another tomorrow. And they're not technical, so you can't ask them any questions."

When he places an order, the European engineer runs into further trouble. In one case, an engineer wanted to place an order for some samples worth $100. The local man didn't have the product and knew nothing about it. The home office in the U.S. returned his purchase order; it would not accept an order for less than $1000, though the engineer's company was a giant. If the European works for a company that isn't known to the American, he has an even rougher time—even if his company is vast.

There are exceptions, of course, notably Hewlett-Packard, Tektronix, Motorola and Texas Instruments, whose reputations in Europe are superb. But many U.S. companies sell to Europe in spite of themselves. Some have fine reputations for customer service in the U.S.—but not in Europe.

In general, American engineers design for engineers throughout the world. Too often, unfortunately, their products can be purchased only by those engineers with enough tenacity to overcome the purchasing barriers erected by American companies. Most American manufacturers raise all sorts of hell when they learn of trade barriers erected by other countries. They needn't bother; they are creating their own.
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Displays are unlike most other electronic devices. Often they are chosen for their aesthetic qualities rather than their technical superiority. If you try to get the best of both worlds, selecting the right display for your application can be puzzling.

At least five major technologies are being used to convert electrical data into some sort of digital readout. They include:

- Light emitting diodes.
- Gas-discharge devices.
- Incandescent displays.
- Liquid-crystal readouts.
- Fluorescent tubes.

Deciding among these technologies requires proper interpretation of spec-sheet data and a thorough understanding of the tradeoffs involved.

Since all displays must ultimately be read by people, the first thing to ask yourself is whether the display is pleasing to the eye. Next, determine if it will be used in high ambient light.

Another factor to consider is the contrast ratio of the display. Also: What is the viewing angle? Is the digit big enough to be seen from the normal operating distance? Is ruggedness a key requirement? What color should the display be? Is full alphanumeric capability required? How much data will be displayed at one time? Will the display be operated in the parallel mode or multiplexed? What voltage does the display require? How much power will it consume? How much does it cost?

Watch those specs

As with many other electronic devices, beware of specsman ship. Frequently data are not given over the full operating range but only at the point where the display shows up best. Because display characteristics differ with temperature, be sure you get minimum, typical, and maximum values.

Another spec to check carefully is power dis-
A new trend in large LED displays is to package them as multiple-digit units. The DL 721 and DL 727 from Litronix each contain two 0.5-in. characters, and can be used to form 3-1/2, 4, 5-1/2 or 6-digit displays.

sipation. Sometimes values are given at minimum current or with only five segments of the display lighted. This makes the dissipation look better than it really is. For nominal performance levels, dissipation should be specified at typical current and with all segments lighted.

Here's another thing that causes problems: You're looking at the power-dissipation spec, but what you're really interested in is power consumption. There is a difference. Dissipation refers to the power drop across the display itself, while consumption refers to the power drop across both the display and any associated dropping resistor.

Even if you take care to differentiate between dissipation and consumption and are careful to use typical rather than minimum power specs, you may still have a problem. Your application may require a display of a specific brightness or readability. To fulfill this requirement, it may be necessary to drive the display harder than the typical spec requires. This increases power consumption and may make an alternate technology more desirable.

How bright is bright?

When a spec sheet says that a display is rated at a specific brightness, what does it mean? Not much. The reason is no one really knows what is the best way to specify it. Some manufacturers specify brightness in terms of source intensity—candlepower. This measurement is not related to surface area; it indicates the amount of light—the lumen level—available for viewing by an observer.

Other manufacturers specify brightness in terms of surface illuminance—in foot-candles or lumens per square foot. This measures the amount of light per unit area falling on a surface. Still other manufacturers specify brightness in terms of surface luminance, or footlamberts. This is a complex function describing surface-reflected light, and it includes solid...
angle and area factors.

But brightness is subjective and not directly measurable. It is a response of the human eye to visible electromagnetic radiation. And the eyeball tends to see surfaces—not points or spots, which yield better brightness data.

There is no industry standard for measuring brightness. Most manufacturers use either a photometer or a spectrophotometer for measurements. Taken with a spectrophotometer, the measurements can be of questionable worth, since they are made at peak emitting wavelengths rather than at the wavelength of the human eye.

Since there is so much confusion in brightness specs, the best thing you can do is to make an "eyes-on" comparison. Do it with actual devices, not photographs. Photos in data sheets, catalogs and magazine articles are often flattering and sometimes deceptive. Some displays simply do not photograph well; they may look better to the eye than to film. Often manufacturers feel the camera has "lied," so they "help" the picture with an artist's airbrush and imagination.

When comparing different displays, do it under conditions that closely approximate the actual application. Such examinations should include the optical filtering that will be used to increase contrast and reduce reflections from ambient light. No matter what the spec sheet says, the only true test of display brightness is one involving actual viewing.

Get several samples of each device to be evaluated. One sample can disclose much, but several can tell a lot more. It's possible, for example, to see the spread in brightness and color from character to character. And uniformity of character shape and size can also be seen.

Several sets of eyes are also better than one. Ask co-workers to view the displays.

Large dynamic-scattering liquid-crystal displays that vary in height from 4 to 8 in. are available from Transparent Conductors Inc.

The readability of a display does not depend on brightness alone. A high-contrast ratio between the lighted portion of the display and the background is also necessary. Reflection of ambient light from the display background reduces the contrast ratio. Therefore to get the best readability, use either a black, matte-finish background material as an ambient-light absorber or a colored or polarized filter in front of the display. If the filter route is chosen, remember it will decrease brightness a bit.

As for liquid crystals, "forget the data sheet," advises John D. Dunn, product manager for Beckman Instrument's information displays. "I can measure a contrast ratio of from 20:1 to 60:1 for the same device just by changing the measuring setup," he notes.

How long will a display last?

The life expectancy of displays varies from 10,000 hours for liquid-crystal and incandescent units to 100,000 hours for gas-discharge, fluorescent and light-emitting diode displays.

But don't depend on life-expectancy numbers too much. Poorly stated specs can often mislead. For example, a life-expectancy claim for a readout may be based on laboratory life testing on a per-segment basis. In many applications, however, multidigit displays are used, and they may contain several dozen segments. The statistical life expectancy of such a display is significantly lower than that of the individual segment.

Even if the life-expectancy spec is not deceptively stated, you can't always tell how long a display will last—unless you consider the way it will be driven. Certain driving schemes are tougher on displays than others. For many LED applications, the display array is multiplexed and segments are turned on and off at rates exceeding 40 Hz. This switching subjects the LEDs to degrading effects similar to thermal fatigue. Multiplexing is detrimental to gas-discharge displays as well. The high peak currents caused by the multiplexing circuitry can greatly reduce life expectancy.

Viewing angle must be considered

The viewing angle of a display is another spec that must be approached with caution. There is no good definition for it, and therefore it can be misleading. Different manufacturers specify viewing angles in different ways. And even the same manufacturer may use different techniques to specify the viewing angle on different product lines.

Frequently viewing angle is defined as the half-power point—the point at which the lumi-
nous intensity of the display is one-half that of the display when it is viewed straight-on. Sometimes the angle defined by the half-power point is used, and sometimes it is doubled, to get what can be called the total included angle. There is nothing mystical about the half-power point; it is simply a carryover from microwave specs that deal with 3-dB, or half-power, points. In fact, many industry spokesmen feel that the viewing angle should tell the engineer something about when the full display is no longer visible.

This has given rise to another way of specifying viewing angle, a way used primarily for magnified displays, such as those used in handheld calculators. In this definition, viewing angle is the point at which one or more segments of the digit cannot be seen.

There are several points worth noting about magnified digits. First, the viewing angle of the digits changes faster in the horizontal direction than it does for the vertical. Thus while the digit might be visible 40 degrees off the vertical axis, it may not be 40 degrees off the horizontal axis.

Another point to remember: The greater the magnification, the narrower the angle of view. In general, magnified digits have a viewing angle that is limited to between 20 and 35 degrees.

The best way to specify viewing angle—the one that limits the specmanship of manufacturers—is to use a polar plot of constant luminous intensity. This presents information in an unambiguous way and allows you to determine the best viewing angle. Polar plots are now being used on some of the newer LED displays and on liquid-crystal displays.

An important point to remember about liquid crystals is that the viewing angle depends on the display’s contrast ratio, because it is not a light emitter. And since the contrast ratio varies with driving voltage, so does the viewing angle.

You better believe

According to most display manufacturers, the biggest mistake engineers make is not getting in touch with the display manufacturer’s application department. This initial mistake may often lead to more serious ones.

A common problem encountered with LEDs is that users simply don’t want to believe the manufacturer when he says the LEDs must be driven from a current source. Many engineers try to use voltage drivers on LEDs, and they wind up with problems. They fail to realize that if there is a slight difference in voltage from one segment to the next, the lower-voltage diode will draw more current, causing a brightness mismatch. Remember: LEDs require a constant current source.

Another major problem is that environmental conditions are ignored. Customers expect the displays to work under humidity ranges and temperature cycles that the manufacturer does not recommend. Temperature-derating information is sometimes ignored, as are recommendations on soldering and lead length. The problem is particularly acute for LEDs, because they are packaged in clear epoxy.

In the packages used with ICs, opaque fillers in the epoxy give the ICs superior heat characteristics. But fillers can’t be used with clear epoxy. If the package heats up too much, the plastic melts. And this relaxes the pressure on the leads, and some of the thermocompression bonds fly open. Most of these failures are catastrophic.

A common mistake made by designers who use liquid-crystal devices is that they try to use the display for its low power advantage and then put in a backlight to obtain adequate visibility. This results in a display whose power consumption is higher than that of LEDs or gas-discharge types.

Other factors often neglected with liquid crystals are the limited temperature range of operation—sometimes a heater is required—the need for an ac drive signal and the cost of special connectors to make the display replaceable.

A common mistake with gas-discharge displays occurs in power supply and interface design. A good example of this is in multiplexed circuits. A typical circuit has high voltage anode and cathode transistors. The engineer generally over-designs his circuits for high voltage. This can be avoided by use of a voltage-divider network to bias the transistor to a predetermined voltage level. The transistor will not have to swing the full power-supply voltage and cheaper,

An experimental 2-in.-high, 3-1/2 digit dynamic scattering liquid-crystal readout, designed for digital-clock applications, has been fabricated by RCA.
50-V transistors can be used instead of the more expensive 200-V.

Designers don't always understand the features that are built into displays. For instance, some manufacturers use a "keep-alive" cathode that provides an internal ion source. This aids multiplexing, operation in the dark or at low temperatures and applications requiring suppression of zeros.

Another oft-forgotten fact is that since brightness is directly proportional to the average segment current, pulsed power can be used to increase or reduce display brightness.

If you are using a multipackage array of gas-discharge devices, it's essential that you allow for different striking voltages; otherwise one digit might not ignite. In other words, don't base your design on the minimum voltage specified for the display.

Two more points worth remembering: Gas-discharge displays cannot be flow-soldered, because the temperature shock may damage the hermetic glass seal. And current-limiting resistors are necessary.

Users of fluorescent displays sometimes forget, when they are considering the power consumption of the unit, to take into account the current requirements of the permanent filament. Also, since fluorescent units are subject to differential fading of segment brightness, simple field replacement is a must.

**Tradeoffs depend on application**

Since it's highly unlikely that a single display technology will always do everything you want, tradeoffs can be critical. Certain applications will make the decisions easier. They may have a few key specs that virtually dictate which display to use. The digital wristwatch is a good example. It requires a display whose power consumption, size and driving voltage are all low. This eliminates all but light-emitting diodes and liquid crystals.

Other applications don't make the choice so easy. Digital bench-top instruments, for example, don't have a critical power requirement; nor are size or driving-voltage magnitude generally problems. Thus as many as five different technologies can be used. Let's look at each type of display in a little more detail.

**Light-emitting diodes are 'in'**

The most popular display used today is the light-emitting diode. LEDs got their start in 1968 when Monsanto introduced devices priced at $495 and $165. This year, at about a dollar a digit, LEDs will probably account for more digits than any other technology.

As many as 256 alphanumeric characters can be displayed on Burroughs' Self-Scan gas discharge panel. The panel includes all decode, drive and scan circuitry.

There are several reasons why LEDs are popular, the most important probably being that they are solid state. This means that they are inherently more reliable and have a long life expectancy. Another key factor is their low cost. In the last two years prices have plummeted, and they now range from 50 cents to $2 a digit, depending on size.

Basically, LEDs are made by fabricating a p-n junction in gallium-based semiconducting materials. Red, orange and yellow displays are generally fabricated from various combinations of gallium arsenide and phosphorous, while green displays are produced from gallium phosphide.

The types of LED displays available today can be classified into two groups that use three fabrication techniques. The first group consists of small monolithic displays whose character height ranges from 0.1 to 0.2 in. The second group consists of larger digits that use hybrid and light-pipe construction.

The small digits are used primarily for handheld equipment, such as calculators and digital watches, although some are now starting to appear in bench-top instruments, such as the new Hewlett-Packard 1722A microprocessor scope.

Monolithic LEDs are not widely available as single-digit displays; multiple-digit versions, containing between four and nine digits, have proved more popular. They offer the advantage of consistent segment alignment, since all of the segments are etched into the emitting material in a simple, one-step process. Another plus is that like segments on each digit are connected in parallel, making multiplexed operation easy.
Incandescent displays that use directly viewed filaments, such as RCA's Numitron, can be filtered to produce a wide variety of colors.

LEDs are a natural for multiplexing, where each digit is driven at N times its usual drive level for 1/N of the time. The reason is that as the current increases, so does the luminous intensity. Above a certain level of luminous intensity, the eye saturates and cannot recognize digit-to-digit or segment-to-segment differences. The result is a high apparent display brightness with low power consumption.

Another plus for multiplexing of GaAsP LEDs is that as the drive levels go up, the devices become more efficient, so that the same brightness can be obtained for less power than with a dc-driven display. This increase in efficiency is so effective that often displays used in non-multiplexed applications are driven from a pulsed source to reduce power dissipation.

Monolithic LEDs are almost always packaged with a magnifying lens placed over the die. Magnification of the digit size can vary from about 1.5 to 2.5 times normal size. In addition to enlarging the digit, the lens concentrates the light emitted into a narrow cone in the forward direction. Normally this decreasing of the viewing angle would be a distinct disadvantage, but for hand-held equipment it’s not that critical.

LEDs are getting bigger and prettier

Among the new developments in LED technology is a trend toward bigger and better-looking displays. The 0.25 and 0.3-in. devices have given way to the 0.4 and 0.6-in., and the multichip per segment hybrid approach has yielded the reflecting-cavity, light-pipe approach.

Until recently, the most commonly used technique for fabricating large LED displays was the hybrid one in which monolithic LED chips were placed on a ceramic substrate and connected to form a numeric. Often displays, such as Monsanto's MAN 10, use two chips per segment. The hybrid approach has several advantages over the monolithic, including a reduction in the amount of LED material needed and the ability to salvage defective digits by replacement of individual segments.

An improvement on the hybrid approach—one that uses even less LED material and results in a better looking display—is the reflective light-pipe technique.

In light-pipe construction a single, small LED chip is placed in a reflecting cavity, which deflects the emitted light onto a preformed plastic segment bar in the cap of the display. This makes it possible to construct digits that have wider, more evenly lighted segment bars. It also makes it easier and less expensive to produce large digits—such as the FND 500 from Fairchild Semiconductor, a 0.5-in. device.

Another new development is an apparent effort by LED manufacturers to take over many of the applications now being filled by gas-discharge displays. Monsanto has just introduced a new series of 0.4-in. LED displays that feature what the company calls a high readability font. The font looks a lot like the one used on Burrough's gas-discharge Panaplex II, and it uses beveled segment corners to eliminate much of the gappy appearance of other seven-segment displays. Designated the MAN 4000 series, the Monsanto displays are available in neon orange, red, yellow and green. Like other recent entries, the 4000 series uses light-pipe technology.

In another apparent attack on gas-discharge technology, Litronix is extending its multidigit packaging capability to large digits. The first large multiple-digit devices to appear are the DL-721 and DL-727. The DL-721 consists of an overflow function and a seven-segment digit in the same DIP package, while the DL-727 contains two digits. Both units have 0.5-in. characters and are designed to be used together to form 3-1/2, 4, 5-1/2 or 6-digit readouts.

If you want to use LEDs to present alphanumeric information, you can use either 16-bar-segment or dot-matrix devices. The 16-segment display is generally easier to drive, but its characters are slightly distorted. For multiple-character applications, American Electronic Laboratories offers the 5010 series of devices. These consist of 8, 16, 24 and 32-character displays that have self-contained data storage, drive and refresh circuitry.

If you want to use a dot matrix to get better-formed characters and at the same time want the
Attractive gas-discharge displays, like this one from Beckman, can be viewed even in direct sunlight. They use high voltage, but need little power.

flexibility of using as many characters as you want, consider the HP 5082-7100 devices. These feature three, four or five characters per package. The 5-by-7 matrix of LEDs is X-Y addressable and is capable of displaying all the ASCII characters.

Gas discharge displays still being used

Twenty years after Burroughs introduced the first commercial gas-discharge display, the Nixie, that technology is still going strong. But the Nixie is not being designed into much new equipment these days; it's being sold mainly as a replacement part. Today's gas-discharge displays have replaced the individual numeric cathodes of the Nixie with segmented numbers.

The gas-discharge that seems to be the darling of the industry is Beckman's (formerly Sperry's) unit. It comes in 1-1/2, 2, 2-1/2, 3 and 3-1/2 digits and consists of 0.33 or 0.5-in. seven-segment numerics. The segments that make up the number are extended to eliminate side and corner gaps, thereby producing a pleasing display.

Beckman's displays draw between 200 and 500 $\mu$A per segment, depending on digit size. The tradeoff is the requirement for 160 V. This high-voltage requirement is not really significant, especially for equipment that is powered by 117 V ac. But for engineers who think the world runs on 5 V, Beckman offers an economical dc-to-dc converter to operate the displays.

If more digits are required, the Panaplex II displays from Burroughs might be the thing. They are available with as few as four digits or as many as 12. Panaplex II consists of a sandwich of two pieces of glass, on which the seven-segment cathode elements of the numerics and interconnections are silk-screened. The sandwich is then vacuum-sealed with a neon-mercury gas mixture. The big advantage of the display is that it eliminates a lot of external connections.

For example, a 12-digit discrete LED display would require 132 connections, while a 12-digit Panaplex II unit requires only 19 connections. Like the Beckman display, the Panaplex requires high driving voltage.

Another source for plasma displays is Cherry Electrical Products Corp. Its unit, the PlasmaLux, is interchangeable with the Panaplex. National Electronics also makes gas-discharge displays, its Plasmac panel coming in sizes ranging from $1 \times 3$ to $8 \times 15$ in. Plasmac can display unlimited combinations of fixed messages, numeric and alphanumeric characters on a single panel.

Plasma panels bridge the gap

Plasma panels—devices that are capable of displaying large amounts of alphanumeric data via a series of 5-by-7 dot matrices—are aimed at bridging the gap between applications that require single-character readouts and those calling for a CRT that can display hundreds of thousands of characters. The Self-Scan panel from Burroughs is good for applications that require between 10 and 600 characters, while the DigiVue from Owens-Illinois can hold up to 4000 characters.

In the Burroughs unit, a glass plate with an array of holes is sandwiched between top-wire anodes above the glass, cathode strips and bottom-wire anodes below it. The holes form cells for the neon gas. There is one cathode strip for each seven-dot column. The strips are scanned, and the gas in the cell becomes visible when the cathode is switched from 100 V to ground, while the top anode is switched from 130 to 250 V and the bottom anode remains at 250 V.

Whereas the Self-Scan panel is a dc unit, the DigiVue is ac. In operation, a sustaining voltage—not enough to trigger the display—is applied to all elements. To make the gas become visible, a voltage pulse is added to the sustaining voltage to raise it to the breakdown potential of the gas.

Plasma panels are also available from Industrial Electronic Engineers, Inc. Unlike the Burroughs or Owens-Illinois devices, however, the Industrial Electronic Argus dot-matrix panels use a phosphor coating inside the display to achieve a soft green color instead of the conventional orange. But orange is available if desired. Green plasma panels are also available from Okidata, along with red ones.

The latest addition to the plasma scene is a bar-graph display from Burroughs. This device combines the thick-film technology of Panaplex displays with the internal scanning technique of Self-Scan panels to produce a display that can
present analog data with digital accuracy. The display uses what is known as the glow-transfer principle, in which a glow is established at the reset cathode and then transferred up the bars. The height of the bar is regulated by the amount of time that the front anode is on for each bar. When the anode is turned off, the glow stops.

For low power, it's liquid crystals

Eight years ago liquid crystals were a laboratory curiosity with no important commercial future. Today, because of their low power requirements, they have emerged as one of the strong contenders in the display field.

Liquid-crystal displays are constructed from two glass plates that have been coated with an electrically conductive film. For transmissive devices, the films on both plates are transparent; for reflective dynamic-scattering displays, one film is a highly reflective material, such as gold. The films are selectively patterned to produce seven-segment characters, and a layer of liquid-crystal solution is hermetically sealed between the plates.

With dynamic-scattering liquid-crystal devices, application of an electric field causes domains of crystals to form. The domains reflect light at the boundaries and scatter the incident beam. Inactive areas remain transparent.

With field-effect (twisted-nematic) liquid crystals, application of an electric field causes the material to rotate the plane of light polarization that passes through the display. The orientation of polarizing filters determines whether the display is transmissive or reflective.

A new type of liquid-crystal display is starting to appear. It's called a transflective display and is being pushed primarily for watch applications, where people want to be able to tell time in the dark, too. The display has a diffused metallic background. In daylight it's reflective, and in the dark it's transmissive when backlit by a small bulb.

Liquid-crystal displays generally don't tolerate dc driving voltages; the voltages destroy the display by electrolysis. But American Microsystems, Inc., has fabricated a dynamic-scattering liquid-crystal material that allows as much as 20 V dc to be applied without damage. The same concern also makes field-effect liquid-crystal displays, but right now they're mainly for digital watches.

Beckman Instruments is another supplier of field-effect liquid-crystal displays, but don't look for any literature until at least next month. While the company has been in production with liquid crystals for over a year, the work has been primarily custom.

RCA, however, is not limited to custom applications. It has several dynamic-scattering and field-effect displays in 3-1/2, 4 and 8-1/2-digit configurations. These are small devices intended for use in watches and calculators. But a bigger 2-in. display has been fabricated, and units are now being shown to prospective customers.

If you want really big displays, though, you're probably better off with the 8 x 10-in. dynamic-scattering displays from Transparent Conductors Inc. Too big? The company has 4-in. units as well. Both the 4 and 8-in. devices are available as 7 or 16-bar readouts.

Incandescents find limited use

Incandescent displays are the oldest of electrical displays. Their primary advantage is that they produce a very bright display with a broad frequency spectrum. This means they won't wash out easily in direct sunlight, and they can be
Illuminated incandescent displays from Wagner Electric use individual bulbs and light pipes to produce either 7 or 16-segment characters.

Fragility is not a problem with these incandescent readouts from Pinlites because the filament is operated at lower temperatures than those in ordinary lamps.

Comparison of digital display technologies

<table>
<thead>
<tr>
<th></th>
<th>LED</th>
<th>Nixie</th>
<th>Gas Discharge</th>
<th>Fluorescent</th>
<th>Incandescent</th>
<th>Dynamic Scattering LCD</th>
<th>Field Effect LCD</th>
</tr>
</thead>
<tbody>
<tr>
<td>Power/digit</td>
<td>10 to 140 mW, depending on color</td>
<td>350 mW</td>
<td>30 to 100 mW</td>
<td>100 mW</td>
<td>250 mW to 1 W</td>
<td>100 µW</td>
<td>1 to 10 µW</td>
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<tr>
<td>Voltage</td>
<td>5 V</td>
<td>175 V</td>
<td>180 V</td>
<td>15 to 25 V</td>
<td>5 V</td>
<td>18 V</td>
<td>3 to 7 V</td>
</tr>
<tr>
<td>Temperature range (°C)</td>
<td>-55 to 125</td>
<td>0 to 70</td>
<td>0 to 55</td>
<td>-55 to 100</td>
<td>-55 to 100</td>
<td>0 to 80</td>
<td>0 to 70</td>
</tr>
<tr>
<td>Switching speed</td>
<td>1 µs</td>
<td>150 µs</td>
<td>1 ms</td>
<td>1 ms</td>
<td>150 µs</td>
<td>300 ms</td>
<td>100 to 300 ms</td>
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<tr>
<td>Life in hours</td>
<td>100,000+</td>
<td>200,000</td>
<td>30,000</td>
<td>100,000</td>
<td>10,000</td>
<td>10,000</td>
<td>10,000</td>
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<tr>
<td>Colors</td>
<td>red, orange, yellow, green</td>
<td>neon orange</td>
<td>orange, others with filters</td>
<td>blue-green; others with filters</td>
<td>all with filters</td>
<td>depends on illumination</td>
<td>depends on illumination</td>
</tr>
<tr>
<td>Brightness</td>
<td>good to excellent</td>
<td>excellent</td>
<td>good</td>
<td>good</td>
<td>excellent</td>
<td>not applicable</td>
<td>not applicable</td>
</tr>
<tr>
<td>Contrast ratio</td>
<td>10:1</td>
<td>8:1</td>
<td>20:1</td>
<td>10:1</td>
<td>20:1</td>
<td>20:1</td>
<td>20:1</td>
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<tr>
<td>Appearance</td>
<td>good to excellent</td>
<td>fair</td>
<td>excellent</td>
<td>excellent</td>
<td>good</td>
<td>good to excellent</td>
<td></td>
</tr>
<tr>
<td>Viewing angle</td>
<td>150°</td>
<td>100°</td>
<td>120°</td>
<td>150°</td>
<td>150°</td>
<td>90 to 150°</td>
<td>90 to 120°</td>
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<tr>
<td>Font</td>
<td>7 and 16 segment, 5 x 7 dot matrix</td>
<td>individual characters</td>
<td>7 segment</td>
<td>7 segment</td>
<td>7 and 16 segment shaped characters</td>
<td>7 and 16 segment</td>
<td></td>
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<tr>
<td>Vertical size</td>
<td>0.1 to 0.6 in.</td>
<td>0.3 to 2 in.</td>
<td>0.2 to 0.7 in.</td>
<td>0.5 to 0.75 in.</td>
<td>up to 1 in.</td>
<td>0.2 to 8 in.</td>
<td>0.2 to 2 in.</td>
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<tr>
<td>MOS compatibility</td>
<td>small yes; large no</td>
<td>yes</td>
<td>yes</td>
<td>yes</td>
<td>no</td>
<td>yes</td>
<td>yes</td>
</tr>
<tr>
<td>Cost per digit (0.3 to 0.6 in.) 10 k pieces</td>
<td>$1.50</td>
<td>$2.35</td>
<td>$0.60</td>
<td>$1</td>
<td>$1 to $2</td>
<td>$1</td>
<td>$1.50</td>
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<tr>
<td>Ruggedness</td>
<td>excellent</td>
<td>poor</td>
<td>fair</td>
<td>poor</td>
<td>fair</td>
<td>good</td>
<td>good</td>
</tr>
<tr>
<td>Ease of mounting</td>
<td>excellent</td>
<td>good</td>
<td>fair</td>
<td>good</td>
<td>good</td>
<td>poor</td>
<td>poor</td>
</tr>
</tbody>
</table>

Prepared by Symon Chang of AMI.
Optical fibers are used to transmit light from individual bulbs to a viewing screen. The fibers form a 7 or 16-segment character. LEDs or incandescents are used. Standard modules contain from one to six digits.

filtered to produce a display of virtually any color.

Incandescents have some problems in certain applications. They consume a lot of power—anywhere from 250 mW to 1 W per digit. And it's difficult to multiplex them, because isolation diodes must be added.

But incandescent units operate over a very broad temperature range, and they can be run from 5-V logic levels. The expected lifetime of these displays ranges from 10,000 to 100,000 hours. Life, however, is greatly affected by the temperature of the filament, which is a function of the voltage. The lower the voltage, the greater the life.

There are several types of incandescent displays: direct-viewed filament devices, lamp-illuminated and fiber-optic.

Direct-viewed filament displays include RCA's Numitron, the CM 5 Series from Chicago miniature lamp works, the Series 5 from Readouts, Inc., and incandescent units from Pinlites.

Numeric and alphanumeric displays that use individual bulbs and a light pipe are made by the Tungsol div. of Wagner Electric. Another light-bulb display is a transilluminated device from Industrial Electronic Engineers. Fiber-optic displays, which form a seven-segment read-out by attaching several fibers to each bulb that represents a digit segment, are available from Master Specialties and IEE.

Fluorescents look good

One of the better-looking displays is the vacuum-fluorescent, which produces digits with a blue-green color. They still aren't being used too much in the U.S., however. They are available from Wagner Electric, ISE Electronics Corp. and Futaba Electric Industries.

Fluorescent displays contain seven anodes, each coated with a phosphor and a filament. The filament is placed between the viewer and the anodes, which are arranged in the seven-segment configuration.

In operation, the filament is heated to just below incandescence. When an additional 12 to 25 V is applied to the anodes, they glow. A big plus for the fluorescent display is its wide operating temperature range—from -55 C to 100 C.

Another advantage of fluorescents is that since the light they emit has a broad spectrum, they can be filtered to produce displays of various colors. But there are also problems. The devices are packaged in glass and thus susceptible to damage from shock. They require continuous power drain for the filament. Filament breakage can make it necessary to discard a multidigit display, but some manufacturers—like Wagner Electric—minimize this possibility by including two filaments in each tube. ■

(continued on page 62)
Need more information?

The products cited in this report don’t represent the manufacturer’s full lines. For additional details circle the appropriate information retrieval numbers. For data sheets and more vendors, consult ELECTRONIC DESIGN’S GOLD BOOK.

Acro Electronics Inc., 1551 Osgood St., Dept A, North Andover, MA 01845. (617) 685-4371. (Tom Clark) Circle No. 302

Ametek, 373 South Washing St., Horsham, PA 19044. (215) 348-3260. (J. C. Ryshack) Circle No. 303

Analog Devices Inc., 130 W. East St., Enicinatas, CA 90224. (213) 753-0113. (J. Ross Jr) Circle No. 311

Beckman Instruments, 2500 Harbor Blvd., Fullerton, CA 92634. (714) 894-0525. (T. Chadurjion) Circle No. 577

Burroughs Corp., Elec Components Div., P. O. Box 1226, Plainfield, NJ 07060. (201) 757-3400. (S. Kuchinsky) Circle No. 513

Cherry Electrical Products Corp., 3600 Sunset, Waukegan, IL 60085. (214) 697-7600. (J. U. Derneh) Circle No. 512

Chicago Miniature Lamp Works, 4433 N. Ravenswood Ave., Chicago, IL 60640. (312) 784-1020. (D. Wallach) Circle No. 514

Dialight Corp., 203 Harrison Pl., Brooklyn, NY 11237. (212) 694-6545. (George A. Franco) Circle No. 580

Electrodata Concepts, 69 Connecticut Ave. , Norwalk, CT 06850. (203) 959-3200. (J. B. Gouvion) Circle No. 520

Electro Research Co., Div. Textron, P. O. Box 913, Shrewsbury, MA 01522. (508) 242-1411. (W. T. O'Donnell) Circle No. 556

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INFORMATION RETRIEVAL NUMBER 214
Vylink is the Brand-Rex trade name for its tough irradiated PVC insulated wire and cable. A thermosetting material, it has superior heat resistance, is unaffected when accidentally touched by a solder iron and has outstanding cut-through, abrasion and chemical resistance—all in addition to vinyl’s inherent non-flammability (it meets UL’s FR-1 requirements), high dielectric strength and insulation resistance.

Five important processing and operating characteristics of Vylink and conventional PVC insulated wires are compared in the following panels. Test procedures and Vylink’s properties are detailed in Brand-Rex specification BR-790. Write for your copy to Brand-Rex Company, Willimantic, Conn. 06226. Tel. (203) 423-7771.

**Heat Resistance**
After 96 hours at 350°F, Vylink is unaffected, conventional PVC flows. Vylink wire provides far greater protection against current overloads and high temperature environments. It is recommended for shrink-tubing and wave solder cable terminations where wires are exposed to heat guns or solder baths—an excellent low-cost substitute for the premium-priced “high temperature” wires usually used in this application.

**Solder Resistance**
When a weighted solder iron (1 1/2 lbs. force) is applied to the wire surface, conventional PVC insulation melts almost instantly; Vylink, though it may exhibit slight surface discoloration, shows no substantial change—even after several minutes. Regardless of method—hand gun, solder dip, wave soldering—Vylink insulation will neither shrink back nor melt. Shorts due to soldering are avoided. Circuit integrity is assured.
Cut-through Resistance
The relative resistance of Vylink and conventional PVC insulated wires to penetration may be demonstrated by applying a 90° V cutting edge attached to a weighted plunger perpendicularly to samples of each. To have the specimens cut through in the same length of time, Vylink wire must be subjected to at least 5 times the weight. This extra toughness makes thinner insulation walls possible without compromising physical properties. The result — lighter weight, smaller diameter, but equally reliable, cable.

Abrasion Resistance
In this test, a predetermined weight press a conventional PVC wire sample against a moving 400 grit, aluminum oxide abrasive tape until the insulation has been worn away and conductor exposed. By comparison, more than half the insulation remains when the same amount of tape abrades Vylink insulated wire under identical conditions. This toughness permits the use of thinner insulation which UL recognizes by rating 61/2 mil wall Vylink wire at 125 volts (UL Style 1472).

Chemical Resistance
Electronic bombardment of the specially formulated Vylink compound causes a change in the molecular structure and transforms this PVC material from a thermoplastic to a thermosetting plastic. Vylink, like all thermosets is generally inert to chemicals and solvents. When Vylink and conventional PVC are boiled for two hours in MEK (methyl ethyl ketone), a good solvent for vinyls, Vylink is virtually unaffected; conventional PVC is completely dissolved.

Tests were conducted on 16 (26/30) AWG with 1/32" insulation.
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The case for Liquid Crystal Displays
Dynamic Scattering or Field Effect

Liquid Crystal Displays: light emitting diodes; incandescent and fluorescent displays and "Nixie" tubes are becoming solidly established in circuit design as the trend to digital readout continues. The design engineer faces an unusually formidable task in determining the type of display most suitable and practical for his product. We make liquid crystal displays — dynamic scattering and field effect.

The display of the future? Our displays are as sandwiches of two glass plates, spaced typically about .0005" apart with a nematic liquid crystal solution between them and hermetically sealed at the perimeters.

How they work. When the liquid is not electrically excited, its long cigar-shaped molecules are parallel to one another in a position perpendicular to the plates. The liquid appears transparent. When an electric current is applied, ion activity of the molecules leads to turbulence causing the liquid to scatter incident light. Depending on the type of nematic liquid used, either a dynamic scattering or field effect display results.

Dynamic scattering. We use a nematic liquid crystal solution in our dynamic scattering displays. This nematic liquid crystal is conductive, has negative dielectric anisotropy, and is oriented in either a homeotropic or homogeneous alignment. In either case the liquid is clear in the absence of an electric field. When an electric field is induced, the molecules scatter, giving the visual effect of a frosted piece of glass.

Field effect. These displays also utilize a nematic liquid crystal but with a different molecular orientation. The molecules are arranged in a helical stack, like a spiral staircase. The liquid is also sandwiched between two polarizers which are at right angles with each other. When current is applied the molecules rotate 90° so that they become perpendicular to the front polarizer. Light that passes through them is not rotated and therefore is absorbed by the rear polarizer. The result is a dark image on a light background. The image also can be reversed — light on dark.

Producing an image — digital or other — simply requires a conductive surface the shape of the desired image on the front glass plate. Current flowing from the conductive image through the liquid crystal to the common ground back plate causes the liquid to change from clear to a frosted appearance in the current-carrying areas. The images almost always are in the form of seven segments formed on the front glass with transparent oxide and each with its own electrical lead. Energizing the proper segments produces the desired numerals. Lead-ins connect the segments to external contacts on the sandwich (display).

Consider the advantages. Liquid crystal displays have a number of distinct advantages. Simplicity is the reason for several of these. The elements are few and passive — very little can go wrong with an LCD and this means reliability and long life. Simplicity means low cost too — lower than that of most similar displays. Packaging costs are low because LCD's can be driven directly by MOS and C/MOS circuits. Very narrow character widths are possible and still provide a good viewing angle — 60 degrees in many cases.

Low power consumption makes LCD's a logical choice where power limitations rule other displays out. They do not generate light as do other displays so use no power for that purpose. Watch type field effect LCD's use only 3.5W. for example with all segments energized at 7 Volts.

LCD's offer the greatest flexibility of any display type. Several standard displays, dynamic scattering or field effect, are immediately available from Hamlin's stock. Special displays with virtually any type of image can be produced with surprisingly low preparation or "tooling" cost. Because of the LCD's simplicity, lead time on specials is only a matter of weeks.

DYNAMIC SCATTERING

FIELD EFFECT

A few limitations. LCD's have limitations too. Operating temperature range is one. Liquid crystals slow down and may even cease to function at temperatures below 0°C. Above 50-60°C, crystals go into solution and will not function properly. But extremes do not damage LCD's. Once the temperature returns to normal, operation is automatically resumed. LCD's are somewhat difficult to read under low ambient light conditions. (Side or back lighting can remedy this.) Visibility under medium to high ambient light conditions is excellent.

Conclusion. In the majority of display applications, MOS and C/MOS compatibility, reliability, flexibility and low power requirements are important considerations. No other display can match the liquid crystal display on these jobs. They could be the display of the future. And that's the case for the LCD. For specifications, and application data, write Hamlin, Inc., Lake Mills, WI 53551 • 414/645-2361. Or dial toll-free 800-645-9200 for name of nearest representative. (Evaluation samples are available at moderate cost.)

HAMLIN INCORPORATED

Electronic Design 26, December 20, 1974
Fuses or circuit breakers? They have distinctly different characteristics. What's advantageous in one application can lead to damage in another.

The design calls for a circuit protective device and someone says offhand: "Let's use a 10-A fuse." Slow down. Such flippancy can result in a wide range of problems—from merely annoying blackouts to disastrous damage. The choice of device depends on the application, and it should not be made lightly.

There are three basic circuit protectors: fuses, thermal breakers and magnetic breakers. Each has a different set of properties.

Fuses are the most familiar, simplest in construction and usually lowest in initial costs. But they are one-shot, throwaway devices. Thermal breakers cost a little more, but they have an advantage over the fuse: resettability. Magnetic breakers can also be reset, but they cost the most of all types.

Magnetic vs thermal protectors

A fuse is blown by the I^2R heat generated in its resistance, with the precise current at which this occurs depending on the ambient temperature, the fuse-clip size and mounting, and the length and size of attached conductors. Thus a fuse's tripping current and blowout time can vary widely from published nominal values. Fig. 1 illustrates the typical effect of ambient temperature on blowout time and blowout current levels. Nominal fuse-delay ratings are available in a range from milliseconds to hours.

Circuit breakers are mechanical switches with mousetrap-trigger, circuit-opening action. The usual thermal circuit breaker uses a bimetal or trimetal element to actuate the trigger latch. And like fuses, most thermal breakers are affected by ambient temperature. However, thermal breakers can be ambient-temperature compensated by the addition of a complementary bimetal element; fuses generally can't be.

Thermal devices, both breakers and fuses, are better suited for the protection of long runs of wire and wire insulation than magnetic breakers.

![Diagram showing the effect on carrying capacity rating and blowing time](image)

1. The ambient temperature strongly affects both the blowout point and delay time of fuses.

A thermal device can match the temperature characteristics of the wire. Fig. 2 shows the similarity in curve shapes between the trip time of a thermal breaker and the safe time-current limit of insulated wire.

Though magnetic circuit breakers mechanically trip a circuit open in roughly the same way that thermal breakers do, they operate on ampere-turns of the current rather than heating. This difference allows the use of magnetic breakers in applications that require full operating current without danger of accidental tripping when the ambient temperature rises. Magnetic breakers easily handle a temperature range of -40 to 85 C.

The current-sensing element of the magnetic breaker is an electromagnetic solenoid. Time delay is achieved usually by use of an iron core that moves in a hydraulic dash-pot arrangement (Fig. 3). The speed of core movement, and thus the time to trip, depends upon the amount of overcurrent and the viscosity of the dash-pot oil, usually a silicone. Current ratings and trip curves can be easily adapted by the manufacturer for close correlation with the needs of mixed loads. These ratings can be matched to wiring, PC board, motors, transformers, lights and other

Lyal N. Merriken, Senior Design Engineer, Airpax Electronics, Woods Rd., Cambridge, MD 21613.
components. Magnetic breakers can have secondary applications, too—as in sequencing and remote control.

**Breakers with extra advantages**

An important advantage of the magnetic breaker over other protective devices is its ability to perform functions in addition to protection. This versatility stems from its electrically isolated electromagnetic actuating coil, as in a relay. Thus a magnetic breaker can be supplied with extra independent contacts. And several coils can be combined to make a multipole magnetic breaker, in which a fault current in any one coil will automatically trip all circuits.

In this way a magnetic breaker can provide, in addition to overcurrent protection, the remote indication of a circuit's condition and allow remote, manual or automatic circuit interruption. With two-pole interrupting contacts, both sides of the line are controlled and the unit can be used as an on-off power switch. Though such an assembly costs more than a simple protective device, much can be saved on relays, solenoids and switches that would be needed to accomplish the

**2. Thermal breaker trip-delay characteristics** (a) match the safe-operating time of insulated electrical wire (b) and are thus suitable for the protection of wiring networks as in aircraft power systems.

**3. In electromechanical breakers**, controlled time delay is obtained by means of a moving iron core in a hydraulic fluid.
The time-delay in electromechanical breakers, beyond about 10-times overload, is "instantaneous," because the magnetic flux generated is large enough to trip the mechanism without waiting for the core to advance.

Two-pole circuit breakers can, of course, handle more voltage than single-pole breakers, and the double gap helps rapidly quench the arc, especially on dc.

Circuit breakers with high pulse tolerances are needed for inductive loads like transformers and motors.

Selection parameters

Here are the major parameters to evaluate when you pick a protective device:

Voltage specification. For fuses and circuit breakers in ac applications, the voltages are standardized to those in common power lines. Included are units for power systems such as 120-V single-phase with one side grounded, 120-240-V single-phase and 208-V three-phase. For dc voltages, the choice of voltages is wider. Some generally accepted values are 32, 50, 65 and 125 V. In all cases, the protective device should have a higher rating than the operating voltage.

When the voltage is less than 5 V, however, and the circuit is rated in amperes, get in touch with the device's manufacturer for specific restrictions; this is a difficult combination to implement properly. And milliamperes-rated devices should be checked for minimum allowable operating voltage, because the protective unit may introduce a substantial voltage drop.

Of course, dc is more difficult to switch than ac, because dc doesn't go through zero and extinguish its arc, as ac does. With dc voltages, use a two-pole breaker to break both sides of the line. This provides a longer, more easily extinguished arc gap (Fig. 5).

Tripping current rating. The current ratings of fuses or breakers should be selected approximately 20% higher than the full-load current of the protected device. This allows leeway for manufacturing tolerances and voltage fluctuations of the power mains.

Maximum short-circuit current-carrying rating. It's important that the circuit protector be capable of safely interrupting the maximum-available fault current. "Available" fault current is a theoretical value that generally neglects current-limiting factors, such as source and transformer impedances, terminal resistances and the fault resistance. For example, if a 120-V line that normally supplies 30 A has a 0.02-Ω line resistance, the available fault current is taken as 600 A at the end of the line. Thus a short-circuit breaker rating of 1000 A would be adequate for use at the end of the line.

Power frequency. Fuses and thermal breakers
are not affected by the frequency of the current. But magnetic protectors are sensitive to frequency. The protector's design is usually different for dc, 60 or 400-Hz operation. In some applications, though, multifrequency operation is allowed with a single magnetic protector, provided the trip points and other parameters specification tolerances are broadened. For such special multifrequency operation, consult the manufacturer.

**Trip delay.** This should be matched to the application. The delay should be long enough to allow nonharmful transients of current to pass without nuisance tripping, yet fast enough to open the circuit to protect the system. Trip delays come in four categories:

1. Instantaneous—trip in milliseconds, usually under 100 ms, with most at approximately 15 ms.
2. Fast delay—trip in less than 10 s.
3. Slow delay—trip in 10 to 100 s.
4. Very slow delay—trip in more than 100 s.

Instantaneous delay is used for very sensitive circuits, where low overloads of short duration could be harmful. It's also used as a limiter, when a specific high current should not pass.

Fast delay is used for circuits where temporary overloads of over 200% cannot be tolerated for more than a few seconds. Most dc and electronic applications are in this category.

Slow delay is natural for most large transformer-coupled loads, where an overload of several seconds' duration can be tolerated without damage. The slow delay also allows the turn-on transient to pass without false tripping.

Very long delays are used mostly to protect wiring. A limited overload will usually not cause damage. Some motor loads have normal starting-current surges that can last for a second or more and draw 600% of the nameplate running-current rating.

In all protective devices, the time delay becomes less as the overload increases. At very high fault currents, the mechanical inertia of the mechanism and the arc-quenching properties of the protective device are the only limits to the circuit-interrupting speed. The practical limit for magnetic breakers varies from about 4 to 10 ms. Fuse and thermal-breaker delays vs trip current approximate a logarithmic curve (Fig. 2a) and magnetic breakers combine a logarithmic curve with a step function (Fig. 4). In magnetic breakers, beyond 10-times overload, the logarithmic curve is replaced by the step, where the breaker operates in the so-called “instantaneous” mode.

**Tolerance to pulses.** This is the ability to withstand a short-duration pulse of high amplitude without tripping. For example, a protector with a pulse tolerance of 20 should be able to withstand half of a 60-Hz sine wave pulse with a peak amplitude that is 20 times the trip-current rating (Fig. 6).

Transformers or other highly inductive loads can generate such high turn-on transients. Peak

---

7. Magnetic breakers are relatively insensitive to changes in temperature. Only delay time varies substantially with temperature.
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INFORMATION RETRIEVAL NUMBER 38

values of 30 times rated current, which can last for one-half cycle, are not unusual. And this is a common source of nuisance tripping. Further, it is difficult to observe or measure these transients. Current probes for oscilloscopes often saturate and give an erroneous picture. One of the best ways to examine such transients is across a metering shunt in series with the line and monitored with the oscilloscope’s voltage probe. Special features can be built into magnetic breakers to handle such in-rush transients.

Protector devices with instantaneous delays generally have poor pulse tolerance. The average value is 2 to 3, but always less than five times the nominal trip current. Delay magnetic protectors do much better, with values of 10 to 20. And long-delay units are somewhat better—to about 30.

Special high-pulse-tolerant units have a damping mechanism, called an “inertial wheel” or flux buster, which gives pulse tolerances to 50. Dampers should be used when severe in-rush current transients are encountered, such as with variable-ratio transformers and ferroresonant transformers. Pulse tolerances on fuses are specified in I²t values.

Environmental conditions. High or low temperatures change both the current trip point and the delay time on fuses and uncompensated thermal breakers. On magnetic breakers, only delay time varies with temperature (Fig. 7).

Nuisance tripping because of vibration or shock is generally more frequent with thermal breakers and fuses than magnetic breakers. This is especially true when the current is near the trip rating. A hot fuse element is fragile. And the latch in a thermal breaker near its trip current is very sensitive to external vibration.

Well-designed magnetic breakers can tolerate high vibration and shock conditions better. The trip elements, such as the armatures, are usually balanced. But perhaps most important, there is no sensitive condition prior to trip. The magnetic breaker operates on a step-function basis in the decision to trip, unlike thermal protective devices. Thermal devices accumulate heat and thus easily trip near their rated trip values.

For explosive atmospheres, use a sealed protective unit. And another caution: Some protective devices are sensitive to altitudes above 10,000 ft, especially open or vented units. High altitude lowers arc-quenching ability. Thus voltage and interrupting capacity must be derated.

UL and other agency approvals. Certification from an agency such as Underwriters Laboratory, or a CSA or military QPL listing, is often a spec requirement. But many commercial units are not so certified, though they may meet the requirements. The costs of testing to qualify them may be prohibitive.
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Consider more than power when you select an uninterruptible power system. Internal connections and other factors will determine if the system can do the job.

Don’t select an uninterruptible power system (UPS) solely on the criteria of kVA rating and output voltage and frequency. If a critical load must function continuously, worry also about such short-term disturbances as line-voltage dips, subcycle loss and transients.

And these aren’t all. To evaluate a UPS properly, consider these areas, too:
- Expected power-line conditions.
- Load tolerance to waveform distortion.
- Length of time the UPS must supply power after a primary-power failure.
- Time allowed to recharge the UPS batteries.
- Cost, reliability and maintenance.

An uninterruptible power system ensures that a load is powered properly, regardless of the condition of the power line. In addition it performs several other valuable functions: It protects critical loads, as mentioned previously, against short-term disturbances. And it guards against power-line variations in both frequency and voltage, including brownouts.

Standby or UPS units?

Systems that produce electrical power at the site of some critical load are often classified as standby. The choice between standby and uninterruptible systems generally is dictated by the length of time the load can be without power.

Standby systems are typically activated only in emergencies and for maintenance checks. By contrast, a UPS must operate at all times and must include a supply of stored energy that is accessible instantaneously. Some flywheel/alternator systems are in use for this purpose, but the majority of applications today are served by storage batteries and power inverters of various types.

A number of UPS schemes are in use today. Included are on-line rotating equipment, electro-

1. Four basic elements make up a solid-state UPS. The inverter changes the battery energy to the desired form while the load switch chooses line or UPS power.

mechanical systems, hybrid systems, solid-state units, thermoelectric generators and sunlight-powered systems.

Each type, though widely used, has advantages and disadvantages. For powering electronic equipment, the most popular approach by far is the solid-state UPS. Its popularity can be traced to its available power ratings, size, electrical characteristics, cost and reliability.

In general, a static, solid-state UPS can be considered made up of four subsystems (Fig. 1):
1. An energy storage system (a battery).
2. An arrangement to put energy into the storage system (a rectifier-charger).
3. A system to convert the stored energy into a usable form (an inverter).
4. A circuit to connect and disconnect the UPS from the line and/or load (a switch).

Let’s look at the more important characteristics of each.

A choice of batteries

Four types of batteries are commonly used: the lead-antimony, lead-calcium, gel electrolyte and nickel-cadmium. In the lead antimony, the

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The most important part of a UPS is its inverter. In simplified form, the unit can be broken down to its switching elements, control logic and waveform filters.

Grids are constructed of an alloy of lead and antimony and surrounded by an electrolyte of sulphuric acid. With this construction, cell voltages must be equalized during charge cycles. By contrast, the lead-calcium battery uses calcium alloyed with lead to allow charging without equalizing; it requires very little maintenance.

Of the remaining batteries, the gel electrolyte-lead acid is generally more expensive than liquid electrolyte batteries, but it is usually sealed and maintenance-free. The nickel-cadmium offers high storage capacity in small size. However, it is more expensive than lead acid and needs to be equalized.

While the requirements of an individual application may dictate the battery type, the size of the battery bank will be a function of the current to be supplied and the length of time the load must be supported. These two requirements determine the ampere-hour rating of the battery.

Conductor sizes, and the currents to be handled by the switching semiconductors in the inverter stage, determine the battery bank's voltage. In general, very small systems use low voltages, while large systems use battery banks of several hundred volts. The banks are generally mounted in nearby racks. For the smaller systems, the batteries are often mounted in adjacent compartments or within the UPS in one small enclosure.

When the power line is present, the rectifier circuit supplies all of the power used by the inverter and maintains the battery at full charge. The ratings of the rectifier circuit are determined by the requirements of the inverter and the current to recharge the battery after line power is restored.

Systems that need a very long charging time require a rectifier-charger circuit that is only slightly larger than that of the inverter. In systems where a short recharge time is needed, the rectifier-charger becomes much larger. Expandable systems, which later may assume a greater inverter load or require more batteries, should have rectifier-charger circuits with excess capacity.

The heart of a UPS: Its inverter

In a typical UPS, the inverter accounts for more than half the cost. Inverters generally use three basic kinds of circuitry: the switching elements, the logic circuitry (which controls the switching elements) and a filter to improve the waveform of the output power.

Typically the dc power available from the rectifier-charger is converted to ac by switches that turn on and off in a way that causes a transformer core to magnetize first in one direction and then in the opposite (Fig. 2). Ac power is then drawn from another winding on the same core.

The switching elements in small, low-voltage inverters are generally transistors, while silicon-controlled rectifiers (SCRs) are usually used in higher-powered, higher-voltage systems. Very large systems use banks of parallel SCRs, each operating at well over 100 A. The switching elements are connected and controlled to deliver one of four types of waveforms (Fig. 3):

1. Square wave: The simplest of inverter outputs, it results from alternate opening and closing of two switches at a constant rate. A square-
3. **An inverter's switching elements** can be designed to deliver several types of waveforms. Square waves are satisfactory for many loads (a), but the quasi-square wave with an amplitude of about 140 V is adequate to power many small loads, such as cathode-ray-tube monitors, intermittent-duty printers and many kinds of test equipment. Loads containing both peak-charging filters and averaging filters may not operate satisfactorily from square-wave power. Many computers and data-processing machines use both kinds of filters.

2. **Quasi-square wave**: Similar to a square wave, except that there is a dead time between alternate half cycles to more nearly approximate a sine wave. The relationships between rms, peak and average voltages are considerably improved over the 1:1:1 ratios of the square wave, while the circuitry involved is still relatively simple. Voltage is regulated by control of the duty cycle—longer on time results in higher output voltage.

3. **Stepped waveform**: A further improvement in waveshape is accomplished with inverters whose on and off times are controlled, and whose outputs add together. When none of the switches is on, the output voltage is zero. With all of the switches on, the voltage is maximized. And with some on, there is an intermediate voltage at the output. When the various switches are sequenced on and off, the output waveform can be given a stairstep pattern that follows the general shape of a sine wave. More levels of voltage can be obtained with additionad inverter sections to give a closer approximation of a sine wave.

Voltage regulation in the step approach is generally obtained by generation of two out-of-phase stepped waveforms and the summation of their outputs. When the two waveforms are near-
ly in phase, the output voltage is high; greater displacement produces a lower voltage. The extreme case illustrates the principle: Two equal waveforms displaced 180 degrees produce no output.

4. **Modulated waveform**: In this method, a single set of switches is turned on and off at high frequency in a pulse-width-modulated pattern. This produces a maximum voltage at the peak of a sinusoid at large conduction angles, and minimum voltage near zero-crossing at small conduction angles.

A wide variety of control circuitry is used with the different inverters. While the basic function of the controller is to turn the switches on and off, the control circuitry also may be responsible for the following:

- Frequency stability.
- Voltage regulation.
- Current sensing and current limiting.
- Synchronization of output to power frequency.
- Phase displacement on three-phase systems.
- Soft start capabilities.
- Paralleling capabilities.
- Sufficient drive for load surge conditions.

**Which filter?**

All high-efficiency inverters produce non-sinusoidal waveforms. The primary function of the filter is to shape the waveform by elimination of harmonics. The load generally looks directly into the filter section of the UPS, so filter design may be important to the user’s system. Some of the more commonly used filters are:

- **Ferroresonant transformer**—one of the simplest and most effective of all output filters. When used as the output section of a square-wave inverter, it provides primary-to-secondary isolation, a high degree of noise isolation, inherent current limiting and very good waveform shaping and voltage regulation. Its disadvantages are its bulk, low efficiency and slow response time.
- **Harmonic-suppressing transformer**—an output transformer tuned to resonance at the inverter’s operating frequency. Like the ferroresonant transformer, it performs the functions of isolation and harmonic suppression, but it is considerably lighter and smaller. The heat developed in the harmonic-suppressing transformer limits its usefulness to relatively small systems.
- **LC filters**—various combinations of chokes and capacitors configured to pass the fundamental frequencies and to shunt or trap high-frequency components. LC filters can be used to smooth square, quasi-square, stepped or modulated waveforms. They tend to become smaller and more efficient when the input waveform approaches the output waveform. Large filters tend to affect the response time of closed-loop systems adversely.

Commonly used combinations of inverters and filters include a square-wave inverter with a ferroresonant transformer, a quasi-square-wave inverter with harmonic-suppressing transformers, and stepped-waveform and pulse-width-modulated inverters with LC filters.

To the UPS user, the important inverter considerations are output waveform characteristics and the ability of the inverter to synchronize with the power line and support the load under start-up and other high-surge conditions.

The switch that connects the load to either the inverter or to the power line is the fourth major component of a UPS. Normally the load can be connected to either source; the switch’s primary function is to break that connection and to con-
nect the load to the alternate source of power at the appropriate time. This time is dictated by a monitor circuit that controls the switch position. Though the switch can be an electromechanical device with one or more moving contacts, more generally it is a solid-state device or circuit, such as a triac or a pair of SCRs.

These four basic elements—rectifier-charger, battery, inverter, and switch—are connected to form the UPS. The user's system requirements dictate the most appropriate configuration.

Once the basic parameters of voltage, frequency and power have been specified, and the inverter/filter characteristics have been considered, it is necessary to determine whether the switching circuitry should be fast or slow. The answer should allow complete system specifications to be formulated.

**On-line vs off-line systems**

The most commonly used configuration for medium-power UPS applications is the on-line system (Fig. 4). This allows the UPS to function as a buffer between the power line and the load, and the UPS regulates the voltage as well as eliminates transients and other short-term disturbances. To use this connection, the user must feel that the likelihood of power-line failure is greater than that of the UPS.

Here, again, we define failure as a variation in power that causes the load to perform in an unacceptable way. This is generally the case with data-processing and communications equipment in urban areas, where the more common utility failures consist of transients, noise and brownouts, and complete power outages are relatively rare.

Many computer installations are much better equipped to deal with power outages than with noise or power flickers. Outage causes data to be reloaded and alerts operators to take appropriate precautions: to verify data, monitor processes and the like. A subtle noise-induced error in the data-processing system may escape detection and have later consequences.

The best total system protection is provided by the on-line UPS. The system is generally configured so the ac utility power is applied to a rectifier-charger that converts ac to dc at a voltage level that maintains a proper charge on the battery. The rectifier-charger also powers the dc/ac inverter, which, in turn, powers the load.

The battery is continuously available to supply power to the inverter in the event of utility power outage or brownout. The battery floats, fully charged, across the inverter input and acts like a huge capacitor that absorbs line surges, provides immunity to line dips and absorbs miscellaneous power-circuit disturbances.

In the event of a failure within the inverter, the monitor circuit detects the output change and commands the switch to connect the load to the primary power line.

On-line systems are generally used for computerized data-acquisition, process-control and other real-time operations, as well as for communications systems and medical applications. Usually the on-line unit is used in installations that are characterized by utility lines of doubtful quality and by equipment that responds rapidly to changes in power.

**Connecting to reliable power**

If the critical load is placed at a spot where the probability of utility power failure is extremely low—say, a communications system at a hydroelectric-generating station that has delivered clean, continuous power for 40 years—it would be reasonable to assume that the mean-time-between-failure of the UPS will be considerably less than that of the primary power. In such a case, the load normally is connected directly to the primary power, with the UPS hooked up as shown in Fig. 5.

The switch is connected so that the inverter stands by in an unloaded condition as long as the primary power is present. When a primary-power outage occurs, the monitor circuit detects the condition and tells the switch to connect the load to the inverter output. Many systems are configured so that, after restoration of normal power, the monitor circuit causes the switch to be reset.

The UPS connection in Fig. 5 satisfies many standby-power applications in which switching speed is not critical. In some, a person performs
the monitor and switch functions by noting that
the primary power is out, pulling the critical
load's power cord out of the wall socket and
plugging it into the inverter. When the power
comes on again, the human monitor plugs the
load back into the wall socket.

Many systems of this type contain a manually
operated switch that allows the inverter to
remain off until the load is connected to the output. While this manually switched arrangement is an extreme example of slow monitoring and slow switching, it differs from more sophisticated systems only in speed of response.

A very simple system, which operates in one or two cycles of the line frequency, consists of a switch that is nothing more than a relay or contactor whose coil is powered by the utility line. When the line power is not present, the contacts switch the load from the line to the inverter.

A faster system uses a rapidly responding monitor circuit and a solid-state switch to provide switching time on the order of several milliseconds—fast enough for most data-processing and process-control equipment.

Off-line system is limited

Though the off-line unit has advantages over the on-line system, in terms of efficiency and rectifier-charger cost, it has the inherent disadvantage of being able to protect only against power outages. It offers no buffering against transients and other short-term disturbances, and normally it does not function as a voltage regulator or brownout eliminator. However, these capabilities can be incorporated by design of the monitor so that the switch connects the load to the line only while the line is within certain tolerable voltage limits. At other times the load is connected to the inverter.

Extremely fast monitors and switches are available today that make the off-line UPS ideal for such loads as printers, copying machines, voice-communication systems and remote monitoring apparatus.

For many systems powered by relatively dependable—but noisy—utility lines, an off-line UPS can overcome power outage and brownout problems. An ultra-isolation transformer can be connected between the load and the switch to provide bidirectional common-mode noise attenuation on the order of 1,000,000 to 1—many times more effective than a typical UPS.

In many applications, the power-failure mode is almost entirely noise-related, as distinguished from power-related. The most effective solution in this case may not be a UPS but noise-isolation equipment, installed either at the critical load or at the source of the noise.
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Three of the most common detectors used in gas chromatography are the flame ionization type, which measures ionic current generated by a burning sample; the thermal conductivity type, which measures temperature changes, and the electron capture detector, which measures the electric current generated by a radioactive source.

If you understand the various types of gas chromatographs, you can put their gas-analysis capability to full use. These instruments perform a chemical-to-electrical conversion to help analyze unknown substances introduced into a known gaseous carrier.

In a gas chromatograph, a stream of a carrier (neutral) gas moves an unknown sample gas through the analysis system (Fig. 1). The unknown is usually introduced into the system through an injection port and then swept into a separation column by the carrier. The column is filled with an inert support material such as diatomaceous earth (a porous fossilized skeleton of a coral-like material coated with a thin oil film) or porous glass beads with a thin film (liquid phase). Differences in the attraction between the sample gases and the thin film coating cause the various gas components to slow down by different amounts. Thus they enter the detection chamber at different times. Then a detector produces a separate electrical output that corresponds to each of the gas components. The sequence in which the peaks appear tells you which component it is, and the size of the peak tells you how much of it there is (Fig. 2).

Three basic detector types

Flame ionization detection methods (Fig. 3a) burn a sample in a hydrogen/air flame to create ions. A potential applied to the ion detector section collects the ions, and the current generated by the ions is measured by an electrometer-amplifier.

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The thermal conductivity detector (Fig. 3b) has a heated filament that is within the carrier/sample stream. The temperature of the powered filament is related to the thermal losses of the detector wall as the gas passes by. When a sample component enters the test chamber, the thermal conductivity of the mixture causes a temperature change in the filament. If the filament is part of an electronic balanced-bridge circuit, the change in temperature can be translated into a resistance change and thus an electrical output proportional to the change in temperature.

Electron capture detection (Fig. 3c) uses a radioactive beta source to produce low energy electrons in the detector cavity. The free electrons are collected periodically by a voltage pulse on the detector anode. Sample components with an affinity for electrons reduce the number available for collection, and the output signal is altered by an amount related to the concentration of that component.

Of the three detection methods, the thermal conductivity detector is used mostly for low-sensitivity applications or fixed-gas analysis, like N₂ and CO₂ in natural gas. Applications of the flame ionization detector are, of course, limited to burnable samples, like organic compounds. For such samples, this detector can be 100 times more sensitive than the thermal conductivity detector. The flame method is also used in trace analysis, in drug screening and in testing for...
2. A gas-chromatograph output shows the program (a), the peaks and valleys corresponding to gas concentrations with their retention times (b) and the analysis (c).

3. The three most common gas chromatograph detectors use schemes that operate from flame ionization (a), thermal conductivity (b), and electron capture (c). The electrical output provided by these detectors can be conditioned by electronic circuits for analysis of the chemical compounds in the gas.

---

### Analyze the electrical conditions

Let's start the electrical analysis of chromatograph systems by looking at the flame ionization detector technique. A detector background current of between 10 to 20 pA exists. This current is generated mainly by the thin film coating that evaporates from the porous support material and releases electrons.

The current generated has a shot-noise component that can be described by

$$ I_n = \sqrt{2qI \cdot NBW} $$

In this equation $q$ is the electron charge, $1.6 \times 10^{-19}$ coulomb; $I_n$ is the background current in amperes and $NBW$ is the noise bandwidth in hertz, usually 1 Hz.

Fig. 4 describes the detector noise as a function of background current. The noise bandwidth

### Hydrocarbons as part of pollution in the air.

In some cases the electron capture detector is 20 times more sensitive than the flame ionization detector. But it tends to be selective for halogens. Its primary area of application is in pesticide residue detection.

With the increase in availability of microprocessors to aid analysis, many chromatographs are being redesigned to interface and operate in processor-controlled data-collection systems. Some of the newer instruments include such items as keyboards for functional control and read-only memories for storage of programs and algorithms needed during operation. If the detector is considered as the signal source, you can design the circuitry to enhance the usually weak signal.
4. Shot noise compared with background noise of the flame-ionization detector increases proportionally.

of 1 Hz is common in gas chromatograph work and will be used in the rest of the discussions.

Note that peak-to-peak background noise is plotted, since this shows most closely what is seen by a recording device. Since a low background current would be about 10 pA, the electrometer-amplifiers must have a total current noise under about 7.3 fA to contribute less than 20% to the peak-to-peak noise.

Small geometry JFETs with low leakage (Igs less than 1 pA) can easily meet this requirement. Care must be taken, however, with other aspects of the design, since noise is not only generated here.

The total noise in a system can be approximated as

$$I_{n_{\text{rms}}} = I_{n_{\text{FET}}} + I_{n_{\text{th}}} + (e_n/R_{sh})^2 + (2\pi f e_n C_{in,sh})^2$$

where $I_{n_{\text{FET}}}$ is shot noise due to FET leakage current; $I_{n_{\text{th}}}$ is Johnson noise of the source resistance (this includes the feedback resistor, $R_n$); $(e_n/R_{sh})^2$ is the current noise caused by the FET's voltage noise across the amplifier shunt resistance, and $(2\pi f e_n C_{in,sh})^2$ is the current noise caused by the FET's voltage noise across any shunt capacitance.

The last two FET terms are further complicated by the $1/f^n$ noise power characteristic of the JFET at low frequencies. For the JFET desired, $n$ can be approximated as 2/3. The capacitive term can become quite large because of cable capacitance; the detector is often physically remote from the electrometer. A flame system like the one shown in Fig. 5 also has a floating polarizing supply, which has a shunt resistance and capacitance to ground that adds to the last two terms. If you assume a total capacitance of 100 pF, a 1-Hz bandwidth and a 7-fA contribution from the source, then

$$e_{\text{app}} = I_n / 2\pi f C$$
$$e_{\text{app}} = 7.95 \mu V.$$

5. The electronics needed for the flame ionization detector aren't too complex, but they must be sensitive.

A noise voltage this low is difficult to obtain and often requires a JFET rather than a MOSFET.

When large samples (10% concentration) or solvents are burned, the flame-detector output current approaches 10 µA. The amplifier's dynamic range must be over a billion to one; this is usually achieved with some type of ranging circuit. In a traditional electrometer (Fig. 5) the range of values for $R_n$ would be very large (typically $10^8$ to $10^{12}$ Ω).

If $R_n$ changes to range the electrometer at these high impedance levels, it causes large output transients. These transients make it impractical to range during a sample run. However, a new approach used in some recent systems (Fig. 6) enables operation over $10^9$ dynamic range. This is done by autoranging at a low-impedance node without creating transients.

Transistor $Q_i$ compresses the wide dynamic range of $I_{in}$, according to the following equation (assume that $Q_i$ is forward biased):

$$V_i = -\frac{nKT}{q} \ln \frac{I_{in}}{I_{i1}}.$$  \(1\)

In this equation $I_{i1}$ is the saturation current of $Q_i$; $q$ is the charge of an electron; $T$ is absolute temperature in degrees Kelvin; $n$ is a device...
constant (near unity); and K is the Boltzman constant, \(1.38 \times 10^{-23}\).

The exponential amplifier ranges if you add a range voltage, \(V_r\), to \(V_i\). This yields

\[ V_{\text{out}} = Z I_{\text{out}} e^{q(V_r - V_i)/nKT} \]  

(2)

If you substitute Eq. 1 into Eq. 2 for \(V_i\), you get

\[ V_{\text{out}} = Z I_{\text{in}} \left( \frac{I_{\text{in}}}{I_{\text{in}}} \right) e^{qV_r/nKT} \].

Since \(Q_i\) and \(Q_o\) are a temperature-controlled matched pair, the factors \(q/nKT\) and \(I_{\text{in}}/I_{\text{in}}\) can be considered constants. This results in

\[ V_{\text{out}} = K_I I_{\text{in}} e^{qV_r/nKT} \].

If \(V_i\) is changed in 79 mV steps (at 55°C), hexadecimal ranging results for \(I_{\text{in}}\). Since changes in \(V_i\) occur at a low impedance node, range switching transients are small. Elimination of the range switch also removes a leakage source on the high-impedance input. The amplifier, \(A\), in Fig. 6 is an integrating analog-to-digital converter that digitizes the input current for transmission to a processor.

About half of all chromatographs use the flame ionization detector. Although a number of compounds produce little response when burned, the flame ionization detector is a popular choice for organic mixture analysis. A flame ionization detector that has a sensitivity of about 15 milli­coulomb/gram carbon and a background noise of about 20 fA can detect a level of 4 picogram carbon/s of sample (signal/noise = 2).

Heat-sensitive detectors

The thermal conductivity detector (Fig. 7) is not limited to burnable samples, as in the flame ionization. Therefore it is widely used for gas or air analysis when many of the constituents (nitrigen, sulfur dioxide, carbon dioxide, etc.) are not detectable in a flame-ionization system.

Tungsten-rhenium filaments used in the thermal detector are heated in a short-circuit current bridge by an ac drive. The ac bridge operation avoids thermocouple effects. The heat balance equation for each filament shows\(^5\) that

\[ \frac{I^2R}{J} = G \lambda (T_z - T_i) + S. \]

In this equation \(I^2R\) is the electrical power input (about 1 to 2 W); \(J\) is Joule's constant; \(G\), a constant that describes the geometry of the cell; \(\lambda\), the thermal conductivity of column effluent; \(T_z\), the temperature of the hot element; \(T_i\), the temperature of the detector block; and \(S\), the other sources of heat loss not dependent on \(\lambda\) (end effects, radiation, etc.).

With a constant power input and constant block temperature, \(T_i\), you can prove that

\[ \frac{\partial T_z}{\partial \lambda} = -\frac{I^2R}{JG \lambda^2}. \]  

(3)

The temperature of the hot element is measured as if it were a resistance thermometer. Generally one column is used as a reference, and the other is used for samples. This enables the instrument to treat changes in flow rate and temperature of the block as a common-mode signal that substantially reduces the noise and drift. The noise-limiting factor is not Johnson noise from the source impedance (50 \(\Omega\)), but the thermal limitations of the block temperature and flow changes.\(^6\) From Eq. 3 you can show, for example, that the thermal stability required for a minimum detectable propane sample concentration of 1 ng/ml (one nanogram of sample in a milliliter of carrier gas) is about \(10^{-6}\) C.

The ac signal from the bridge is impedance-matched to a synchronous detector. And an analog-to-digital converter transforms the output of the synchronous detector into a digital signal for transmission to the processor. The converter is
ANALOG SWITCM ------------ FROM SYNCRONOUS DETECTOR

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DUTY CYCLE

8. An analog-to-duty cycle converter takes the output of the synchronous detector and changes it into a digitally compatible signal.

similar to one used in the flame ionization detector and is an integrating analog-to-duty cycle unit (Fig. 8). Since this method conserves charge, it follows that

\[ I_{in} = I_c \left( \frac{T_{ck1} - T_{comp}}{T_{ck1}} \right) = I_c T_0 \]

The system clock measures the duty-cycle interval, \( T_0 \) (Fig. 9). At periodic intervals the counters are loaded into the parallel-in/serial-out shift register for transmission to the processor. Since the registers are not unloaded for every interval of \( T_0 \), they integrate and store the value in the counter until requested by the processor. This feature is important, since it allows the processor to spend less time in the input/output mode.

Radiation measures gas concentrations

The electron capture detector uses a radioactive beta source (frequently Ni63 because of its long half life and high-temperature capability) as a generator of high-energy free electrons. Repeated collisions of these electrons with the carrier gas produce about 100 times as many secondary electrons, which, because of additional collisions, reach thermal energy levels. With no sample (no capture), these electrons are collected and produce a standing current of 9 nA for a 15 millicurie beta source.

Several techniques are used to measure the collected current:
- DC potential.
- Pulsed (constant frequency).
- Constant current (variable frequency).

The first technique applies a dc potential across the cell to collect the electrons generated. When a sample enters the cell, some electrons are captured, and the negative ions that result recombine with positive ions faster than they can be collected.

However, the higher-mobility electrons that have not been captured are collected. The net result is a decrease in current when an electron-capturing gas sample is fed into the detector. This mode of operation has problems with space-charge effects, contact potentials and an exponential relationship of output to concentration (Fig. 10a).

But if a 60-V potential is applied for several microseconds the space-charge and contact-potential problems of the dc mode of operation can be avoided. Sensitivity remains at least as good and usually better, since the electron density in the detector continues to rise during the intervals (5 to 150 \( \mu s \)) between pulses. However, this mode also has a basic nonlinearity in its output, as shown in the following equation:

\[ I = \frac{I_s}{1 + \frac{b}{f} + C \left( \frac{a}{f} \right)} \]

where \( I \) is the collected current; \( I_c \), the standing current (about 9 nA) and \( b \), the cell constants (usually sample dependent); \( f \), the frequency of the pulser and \( C \), the concentration of the sample.

At constant frequencies the output current is inversely proportional to concentration plus a
In the electron capture detector, cell current decreases exponentially (dc operating mode) as sample concentration increases (a). Pulse output frequency increases linearly as the sample concentration increases (b) when the detector operates in the constant-current mode. If this equation is rearranged and solved for frequency then

\[ f = \frac{I}{I_s - I} (aC + b). \]

With the cell current held constant, the output frequency is linear in sample concentration (Fig. 10b). Since \( a \) and \( b \) are not entirely independent of concentration or sample type, the linear range is limited to about 10,000. This is a considerable improvement over the 100-to-1 linear range in the dc and constant-frequency modes of operation.

Fig. 11 is a block diagram of a constant-current, electron capture detection system. This consists of a servo loop, which varies the pulser frequency to maintain \( I_{cell} \) equal to a reference level, \( I_0 \). The pulser generates 300-ns pulses at the servoed frequency with an amplitude of 70 V. These pulses are applied to the cell to collect the uncaptured electrons and maintain the time average of zero current into the input node. The comparator converts the integrated error signal from the amplifier into a frequency that is linear in concentration.

A 15-millicurie source yields \( 5.55 \times 10^8 \) disintegrations per second. Since this is a random process, the signal-to-noise ratio is

\[ \frac{S}{N_{pk-pk}} = \left( \frac{KT}{I} \right)^{1/2} = 2.78 \times 10^3, \]

where \( K \) is the disintegration rate and \( T \) is the time of observation (0.5 s for a 1 Hz NBW).

To translate this into electronic terms: If the collected current (equal to \( I_0 \)) used is 1.5 nA, the noise current is 0.54 pA pk-pk for a 1-Hz NBW. Therefore a FET front end is required, but the leakage requirements are several orders of magnitude easier to meet than for the flame ionization detector. Since the base frequency can be as low as 300 Hz, a resolution of 0.1 Hz is needed to make full use of the signal-to-noise ratio. An interpolating counter increases the resolution of the output counts and stores the results for transmission to the specialized processor.

The electron capture detector is one of the most sensitive detectors available today. It can detect as little as 2 picograms of compounds like carbon tetrachloride or other electron-capturing species. For 1-microliter-size injections, this corresponds to less than two-parts-per-billion concentration.

References
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"We enjoyed every minute we were there," writes Paul R. Saunders, winner of last year's Top Ten Contest. "The islands, the people of those islands and the cruise are wonderful... the hardest part of the whole trip was returning to reality." Paul and his wife are shown, left, at the end of their trip at English Harbour, Antigua. Paul also won $1,000 cash and round-trip air tickets for two to the Windjammer Cruise home port. At the time of the contest Paul was associated with Varisystems Corporation, Long Island, N.Y.

WATCH FOR COMPLETE RULES AND ENTRY BLANKS IN ELECTRONIC DESIGN'S JANUARY 4, 1975 ISSUE
Build counters with calculator chips.
For low counting rates and display of totals, these ICs simplify designs. Use them to replace mechanical counters.

If your application requires counting at relatively low rates and display of the accumulated totals, you probably can simplify the design and cut costs by using calculator chips.

Already designers have found a wide range of counter uses for these LSI circuits—from timers and stopwatches to bin counters, DPMs and table-coordinate counters. Nearly any application that now employs mechanical counters could be upgraded with a calculator IC.

Actually counting is a simple function for these circuits. Repeated additions of a constant to an accumulated total—which can be continuously displayed—represent the basic operation. In its simplest form, a complete counter can be built with only two ICs and a display.

Some of the benefits
Here are the advantages that calculator chips bring to counting applications:

- **Display driving capability.** Most calculator chips have multiplexed outputs that can drive a display directly, or in conjunction with segment and digit drivers. The internal circuitry simplifies drive requirements and reduces the number of external components needed.

- **Switch debounce logic.** Many calculator chips have built-in switch debounce logic that overcomes the most common problem in count-switch or relay-closure applications, especially when the only switches employed are single-pole, single-throw types.

- **Multiple decades of counting in one package.** Even the simplest calculator chips usually have six digits or so and can be used for six-decade counting. Chips with eight to 10 digits are also readily available. Hence a great deal of counting capability is available in a single IC.

- **Counting by various radices.** Since counting is obtained by repeated addition of a constant to an accumulated total, it is possible to count by any desired radix simply by changing the constant. Consequently it is just as easy to build a counter that counts by 2's or 9's as it is to build one that counts by 1's. With a slight increase in complexity, even counts by unusual numbers—like 972 or 11,576—can be obtained.

- **Low package count and cost.** The low parts count offered by a calculator chip can rarely be equaled by medium-scale-integrated components, especially when three or more decades are needed. For example, a six-digit counter that drives a LED display and counts at a maximum rate of about 60 Hz can be built with only two ICs—a calculator chip and a digit driver. Increased counting rates, simplified control and heightened versatility in the display drive can be obtained with the addition of a few components.

- **Low power consumption.** Many MOS calculator chips operate from battery supplies, and they draw very little current. The bulk of supply current is consumed by the display rather than the calculator chip. If CMOS elements are used to control the calculator chip, very little additional supply current is needed.

Tradeoffs in chip selection
The many available calculator chips tend to make selection of the right one difficult. However, the process can be simplified by examination of the major characteristics needed for a good counter. For a particular calculator chip, the key points to check are these:

- Autosummation.
- "Constant" operation.
- Speed of count.
- Wasted capabilities.
- Interface ease.
- Display-drive capabilities.

Does the chip allow autosumming?
A calculator chip has the autosumming feature if, after initial depression, subsequent depressions of the add key result in repeated addition of the first entry to the accumulated total. Chips based on algebraic notation generally do not have...
this feature, while chips based on so-called Polish notation do.

Autosumming offers the best way to make a calculator chip count, since it involves the fewest different types of entries—just 1 and the plus symbol (Table 1). After entry of the first 1, counting takes place each time the plus entry is activated.

Does it have ‘constant’ operation?

Some calculators have a “constant” function that can be used to make repeated additions and so make the calculator count. However, some constant functions work only for “multiply” and “divide” and not for “plus.” Some others work only with numbers stored in memory and not with the working registers.

In addition operation of the constant function might be significantly slower than desired, and more initialization becomes required. Table 2 illustrates how to set up a chip with algebraic notation—National Semiconductor’s MM5738—for constant operation, so the chip will count. This method isn’t as desirable as the autosumming approach, because more initialization steps are required, necessitating increased external logic and heightened system costs.

How fast does it count?

Maximum counting speed is a prime consideration in almost any counting application. Most calculators are relatively slow, as counters go.

Table 1. Autosumming saves entries

<table>
<thead>
<tr>
<th>Key Sequence</th>
<th>Display</th>
</tr>
</thead>
<tbody>
<tr>
<td>C</td>
<td>0</td>
</tr>
<tr>
<td>1</td>
<td>1</td>
</tr>
<tr>
<td>+</td>
<td>1</td>
</tr>
<tr>
<td>+</td>
<td>2</td>
</tr>
<tr>
<td>+</td>
<td>3</td>
</tr>
<tr>
<td>+</td>
<td>4</td>
</tr>
</tbody>
</table>

Table 2. ‘Constant’ counting

<table>
<thead>
<tr>
<th>Key</th>
<th>Display</th>
<th>Action</th>
</tr>
</thead>
<tbody>
<tr>
<td>C</td>
<td>0</td>
<td>Clears chip</td>
</tr>
<tr>
<td>1</td>
<td>1</td>
<td>Enters a 1</td>
</tr>
<tr>
<td>×</td>
<td>1</td>
<td>Stores “×” function</td>
</tr>
<tr>
<td>=</td>
<td>1</td>
<td>Stores 1 in constant register</td>
</tr>
<tr>
<td>+</td>
<td>1</td>
<td>Changes mode to add</td>
</tr>
<tr>
<td>K</td>
<td>2</td>
<td>Repeats add</td>
</tr>
<tr>
<td>K</td>
<td>3</td>
<td>Repeats add</td>
</tr>
</tbody>
</table>

Speeds in excess of several hundred hertz are usually beyond reach, so that chips can’t be used as frequency counters, for example. But all slow counting and display applications are prime targets. These involve man-to-machine interactions, which are limited by human response times.

Consequently most calculator chips are loosely spec’d with regard to execution times. This allows the semiconductor manufacturer a wide range of process variation, which reduces costs. Reference to calculator-chip data sheets reveals an unusually wide range between the minimum and maximum execution speeds that are guaranteed. These speeds may be a long way from either the mean or the median. But a designer must either live with these speeds or ask the manufacturer to perform special sorting to separate the faster chips.

The time required for each count involves both that for the actual addition and the time to enter the function that causes each addition—either “plus” or “constant.” Usually the time required for entry consists of both a key-depression debounce time and a key-release debounce time. Also to be determined is whether the addition time overlaps one or both debounce times. This sort of information is not always available from an ordinary data sheet and may have to be obtained from the manufacturer’s applications department.

National Semiconductor’s MM5736 calculator chip, for example, has a debounce time-out for key depression and key release of eight word times each. The data sheet indicates that a word time—
a basic cycle—varies from 420 µs to 1.60 ms. Thus the time taken to enter any key depression and get ready for the next one runs from 6.7 to 25.6 ms. The time to execute the addition overlaps the key-release debounce time-out, so that the maximum speed varies from about 40 to 150 Hz. However, the MM5736 has a feature that allows these speeds to be doubled.

Choose the simplest chip

Obviously the more capability left unused when a calculator is used as a counter, the less economical the solution becomes. Don't use a 12-digit, floating-point calculator with memory and constant if you only need a six-digit counter. Choose the simplest calculator chip that satisfies the counting requirement. In general, look for a fixed-point unit with the necessary digits and with Polish notation. Such a chip should yield an economical solution, provided you don't have to count too fast.

The calculator should interface with other logic elements without additional components, if the total component count is to be kept low. If the calculator chip runs off a single supply of less than 15 V, CMOS logic elements can control the calculator. CMOS circuits usually drive the calculator directly, and vice versa. If the calculator requires a voltage higher than 15 V, additional interface elements have to be built, and this requirement can rapidly erode the economic advantages of a calculator chip.

Some calculator chips drive the segment inputs of some LED displays directly, without any buffers. This is clearly ideal. However, some displays require more current than an MOS chip can supply without emitter followers or Darlington buffers. Again, the addition of buffers increases the component count and system costs.

Does the calculator chip require a voltage that is not readily available? Will a dc-to-dc converter be needed? Does the chip draw too much current? How well regulated must the supply be? If the counter is to be battery-powered, what battery life can be expected? All of these questions should also be considered before a calculator chip is selected. The answers affect end-product cost.

A typical calculator for counting

One of several commercially available calculator chips that can be used for low-speed counting is the MM5736, a six-digit, five-function unit with no decimal point. The five functions consist of Add, Subtract, Multiply, Divide and Clear. Three inputs—K1, K2, and K3—are designed to be used with a keyboard matrix and the chip's digit outputs.
eight consecutive word times. Before another entry can be made, at least eight word times must elapse, during which none of the digits' outputs are applied to the K inputs. This requirement limits the speed of the calculator, but it is needed to provide an adequate debounce time-out.

The MM5736 operates from a single voltage in the range of 6.5 to 9.5 V, which allows battery supplies. The calculator chip itself draws about 6 mA. If a LED display is driven directly, without segment drivers, the current that drives the display must come through the calculator, so the total power supply current can be as high as 110 mA; typically it's about 50 mA.

The power-supply voltage must come up to an operational level fairly quickly, since a slow ramp doesn't always initialize the calculator properly. If the chip is used with a heavily filtered power supply, some provision should be made to allow the \( V_{ss} \) terminal of the calculator to rise abruptly. After power up, the calculator should be cleared twice to ensure that all registers are reset to zero. The first Clear operation affects only the display register, while the second Clear affects all other registers.

The calculator chip is directly compatible with standard CMOS circuits. The maximum CMOS load that the calculator can drive depends on capacitive loading. Loads of 200 pF or less should present no problem to the digit outputs, but the segment outputs should not be loaded with more than about 50 pF. As a result, fanout should be limited to about 10 on the digit outputs and four on the segment outputs.

Two ICs make a counter

A six-decade counter that drives a display and requires a minimum of components appears in Fig. 2. The circuit uses two ICs and has a maximum counting rate that is typically 60 Hz. Some chips may run as slow as 40 Hz, while others count as fast as 150 Hz. This is because of inherent variations in the internal oscillator from one IC to another.

The counter in Fig. 2 requires manual reset, which consists of two steps: Clear the calculator and enter a "1" into it again. (Only one Clear operation is needed after an arithmetic operation.) The two steps are accomplished by depression of \( S_1 \) and \( S_2 \).

Two variations of this counter are shown in Fig. 3. The circuits indicate how to build the same counter but with segment drivers. The driver in the circuit of Fig. 3a must be mask-programmed to source a specific value of current. Generally available currents range from 5 mA up to about 17 mA per segment. Hence fairly large displays can be handled.

Different segment drivers are employed in
4. Additional components yield further improvements. With CMOS gates, a self-starting counter (a) is obtained. Another package of CMOS gates and a diode produce increased counting rates (b).

Fig. 3b. External current-limiting resistors determine the current drive to the LED.

With the addition of only one package of CMOS gates, a self-starting counter can be built (Fig. 4a). The counter does not require a separate start operation to enter an initial 1 into the calculator chip. When the Reset switch is returned to its normal position after the calculator has been cleared, the additional components generate a delayed pulse that gates digit output 2 into the calculator, thereby entering a 1. The counter resets in a single operation.

The circuit in Fig. 4a can be made to count at a higher rate if the additional components in Fig. 4b are included. The maximum counting rate with the new circuit ranges from about 80 Hz up to about 300 Hz, depending on the version of the calculator chip. A typical speed is 120 Hz. The circuit can also be used with segment drivers, as indicated in Fig. 3.

The increase in counting rate is obtained when digit output 6 is fed back to the digit-4 output, thereby "fooling" some internal logic. However, a resulting double pulse on the digit-4 output must be gated back to a single pulse at the normal digit-4 time. This requires one diode and one additional package of CMOS gates. In operation, the input must be high for at least four word times and low for four word times. Word time varies from 420 µs to 1.6 ms, with 1 ms typical.

Counters can also be made to count down by use of successive subtractions rather than successive additions. And both features can be combined to build an up/down counter. Fig. 5 shows a circuit that counts up and down by 4's. Such a counter might be used to keep track of inventory in a bin, in which case the components to be inventoried must be packaged in groups of 4's. When a package is put into the bin, switch S1 is activated and the counter adds 4 to the accumu-
6. A calculator or a counter? Use of external MOS transistors for isolation from the keyboard permits the circuit to operate in either mode. Hence the full capabilities of the calculator chip can be retained.

Retention of full use of the calculator

Counters also can be built to retain full use of the calculator. This requires that the usual keyboard arrangement of the calculator be undisturbed by the counting logic. Fig. 6 illustrates a circuit that uses MOS transistors to achieve this. The usual calculator operation is retained when \( S_2 \) is in the calculate position, since all four MOS transistors—\( Q_1 \) through \( Q_4 \)—are off (gates are at \( V_{ee} \)). With the Reset switch activated, \( D_1 \) connects to \( K_1 \) and the calculator clears. Capacitors \( C_1 \) and \( C_2 \) discharge, while \( S_1 \) activates. But as soon as \( S_1 \) is released, \( C_1 \) and \( C_2 \) charge to generate a delayed pulse (negative going) on the gate of \( Q_2 \). Then \( D_2 \) gates into \( K_1 \) and causes a 1 to be entered into the calculator. The delay caused by \( C_1 \) allows the Clear function to be debounced.

Maximum counting rate doubles through a reduction of the internal debounce time-out. With \( S_2 \) in the Count mode, \( Q_1 \) turns on and \( D_1 \) ties to \( D_2 \). The count input is now enabled, and an input pulse turns \( Q_1 \) on. Then \( D_2 \) gates into the \( K_1 \) input and causes the calculator to perform an addition. Each subsequent input pulse causes 1 to be added to the sum. When \( S_2 \) is returned to the calculate position, the count input disables and \( Q_1 \) turns off—an action that returns the keyboard logic to its normal state.

The circuit of Fig. 6 also can be built with NOR gates instead of NAND gates. Then the MOS transistors can be replaced with a CMOS switch.
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Electronic Design 26, December 20, 1974
Project success: the main concern in '74.
Eight interviewees tell how they forecast, schedule, design, manufacture and service a product in this year-end roundup.

Richard L. Turmail, Associate Editor

Eight of the 20 engineering managers we interviewed this year for ELECTRONIC DESIGN told us how to manage a project better. Shortages, inflation, recession and keener competition were responsible for their overwhelming concern on how to save time and money through better forecasting, scheduling, design, manufacture and servicing of a product.

To compete in today's market, they've learned that they must:
- Be more cognizant of what the customer needs rather than what he wants.
- Be more attentive than ever to design detail.
- Be more aware of the total project effort from product forecast to product servicing.

Here's a roundup of ideas on project management from the engineering managers who were interviewed in 1974 for the series "Challenges to the Engineer Who Manages."

Tightening the loop on forecasts

With a shorter and shorter lead time to get the product to market, the tricks of successful design forecasting and subsequent follow-through take on greater importance for both top management and the designer.

To improve the forecasting ability of Airpax

Harold Goldberg, President, Data Precision, Wakefield, MA.

Bernard Schmidt, Manager CMOS Production and Design, Motorola, Phoenix, AZ.

L. J. Seiden, Manager, Engineering, T-Bar, Inc., Wilton, CT.
of Fort Lauderdale, FL, Herb Cook, president, uses the computer models of the U.S. economy.

"I've found these models to be quite accurate and a lot more bullish on America than the stock market has been," Cook says.

Cook also believes in sending his engineers back to school. He's found that it helps to sit at the feet of an experienced physicist, someone who can help the designer take a very long-range look at the state of the art he's in. Such an expert can answer questions like: Is there anything fundamental in the art that's going to change? Is a product line going to become obsolete? If so, why?

Cook says, "An engineer also has to be willing to do some of the dirty work." He has to be able to do the layout for a draftsman and have the draftsman clean it up. That's the trick today—to translate a problem into a commercial reality.

But according to Cook, there aren't enough engineers today who can do printed-circuit-board layouts. An experienced engineer can lay one out in about 35 hours. It would take a technical draftsman maybe 400 hours to do the same thing. It takes personal discipline on the part of the engineer because it's a laborious task. Cook says that it pays off.

But discipline alone, of course, is not enough.

The times also call for the engineer to be shrewder and more informed. The specific reasons for this, says Harold Goldberg, president of Data Precision, Wakefield, MA, is that the ground rules for design have changed in the last few years in the following ways:

- Because of the vagaries of the component market today's designer must be more concerned than ever about their price and availability.
- Unlimited design changes and improvements are a thing of the past; unlike the old aerospace market, in the commercial area it's still a question of price and field service.
- Customers don't want versatility any more. They are looking for small, inexpensive dedicated instruments, and complex ICs are fulfilling the need here.
- Engineers must learn to interface with all departments to be better informed about customer problems.
- Engineers must keep up with current events, particularly where they relate to overseas technology and competition.

"The older engineers resist change," Goldberg says. "The newer designers don't resist as much because they think that computer technology is a panacea, and that's not realistic either."

Goldberg says that engineers should accom-
pany his firm's salesmen on their field trips to hear first hand the user's complaints. He also believes that engineers can no longer afford to ignore the parts salesman or rely on only one vendor or one technology to see them through a project.

Staying loose on design

"And remember," Peter G. Bartlett, president, Automation Systems, Inc., Eldridge, IA, says, "the designs that sell require compromise."

According to Bartlett, when a designer visits a customer to talk about a new product concept, he's often so concerned about losing a prospective sale that he tells the customer he'll give him anything he wants.

"That's a mistake," Bartlett says, "because the customer may be wrong. What the designer should do is analyze the customer's requirements and understand them well enough to know what he needs, instead of what he wants. When the designer is finished, he should know the product better than the customer does."

To reach that point, Bartlett says that a designer must show his ignorance, which he's usually afraid to do. He should realize that he's there to learn what his prospective customer's business is. The customer will most probably be impressed by his candidness.

Three of the traps of compromise that Bartlett says designers should consider are:

*Experimenting on the customer's product*—Should the designer use an integrated circuit that is higher priced than the old standbys because he wants to use the newer technology? Bartlett advises not to use it unless there's a definite need for it.

*The 'not invented here' syndrome*—Even if the designer hasn't invented it, he must let the customer know when there's an item on the market that's very similar to the product that the customer wants.

*Upgrading and downgrading the customer's specs*—Maybe the guy doesn't need gold-plating, or maybe he should have it because of environmental considerations. Maybe paper circuit boards can't be used because they'd have to be repaired frequently, and glass epoxy would be better.

"The designer must use common sense and not always let the specs dictate the design," Bartlett says.

And if you're Tom Beling, vice president, engineering, Sigma, Braintree, MA, you believe that it's most important to review that design constantly to test how practical it is.

Beling says: "The market changes and the designer must constantly review his product to determine if it's worth developing further."

Beling knows that charts and reports and planning methods are valuable to keep track of what's going on. But he feels that the danger in using established methods exclusively is that people use them to meet milestones directly and to develop the product indirectly.

To keep his design as current as possible, Beling does two things: He sticks to his initial design approach most of the time and solves the most difficult technical design problem first.

To start or not to start a new design approach is a difficult question.

"It's hard to see the problems in a new approach as opposed to the problems you already know about in the old approach," Beling says.

"My experience tells me: I had a plan and I expected troubles... now what's really wrong with that plan? Sometimes that really sobered me up. But 70% of the time I'm better off sticking to my first approach."

Beling never bases his decision on how much money has been spent; he feels there's no way he's going to get it back. He has tried both ways often enough and most of the time he has found that if he tries the second approach, the first approach starts to look pretty good again.

Two of the managers we talked to had interest-
Bernard Schmidt, manager, CMOS Production and Design, Motorola, Phoenix, AZ, says that by cross-fertilizing his staff, hiring support personnel before the designers and giving engineers freedom to invent, he was able to finish a large project fast.

**Beating the project clock**

Schmidt believes that a common problem of many project managers is to try to pick up experienced talent in the particular field of the project design.

"That's a mistake," he says, "because the engineers you pick tend to be narrow-minded, which leaves little chance for cross-fertilization within the group. Quite often these people just don't have the broad perspective that's needed to generate new ideas."

So Schmidt cross-fertilized ideas in the IC design game. He hired a systems man, a bipolar IC design man, an engineer who was experienced in the PC-board business, a military designer and an R&D engineer.

"That's quite a hodgepodge," he says, "but it was a very creative group."

Schmidt also puts a lot more emphasis than is normal on selection of the leaders of the support personnel—the leader of the drafting group and the leader of the technicians—and trains them before he completes the hiring of the engineering staff.

Delays in time mount against a project while the manager tries to find that one key engineer who's going to make his project successful.

Schmidt says that it's better to look for people with basic engineering ability and count on the training function and experience on the job to make them productive. The manager can afford to do this if he has experienced support personnel.

Schmidt also believes that the manager must constantly reinforce the creative urge of his engineers:

"When there's a creative challenge," he says, "I've found that you can manage the project better by asking your staff to come up with a number of patentable ideas."

Another supervisor, L. J. Seiden, manager, engineering, T-Bar, Inc., Wilton, CT, completes his projects by designing and manufacturing parts for the same project simultaneously. The idea is to send a design drawing to the manufacturing department rather than to make a prototype. This means that he can package a job about as fast as it can be conceived. It also means that the designer has to think fast and make few mistakes.

Most companies, when faced with production of a product in a hurry, design, build, test, then render production drawings of it. But Seiden's approach is to render a set of production drawings first and then test the concept. He's committed to design and development, not research and development. He's not looking for new principles; he's looking to apply known principles—and as rapidly as possible. To do that, he has to get all the needed information on the drawings on the first go-around.

"I remember reading somewhere that no one is more liable to mistakes than he who acts only on second thoughts," Seiden says. "I think of that whenever I use the principle of concurrent design and manufacture to help me manage my projects, because with it, the engineers' first thoughts are the ones that count."

With the concurrent approach, Seiden designs the entire unit at the start as best he can, based on his experience. Less rework is required. They end up with some minor bugs, but they don't end up scrapping the product. They've thought out the problems in advance and made a lot of generalized ground rules that they've decided to live with.

"They may not always be the best rules," Seiden says, "but they're adequate, and we get
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**Jack Alford, Director of Product Planning, ILC Data Devices Corp., Bohemia, NY.**

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But no matter what management method is used, small companies often have trouble completing projects simply because they cannot always afford to hire both good designers and good project engineers.

Sumner Weisman, section manager, Modular Products, Electrodyne, Sharon, MA, says that learning to wear two hats on the job is one of the most important responsibilities of an engineer in a small company.

"You must remind them constantly of that responsibility," Weisman says.

What happens, according to Weisman, is that designers will occasionally revert to their small world of circuits and components, temporarily forgetting the larger "project world" around them. After some of his designers were becoming less project-oriented and unwilling to consider the broader aspects of a program, he recently distributed a memorandum specifying the requirements for a project engineer as follows:

1. Interface with the section manager and with project management, drafting, manufacturing and quality control, where necessary.
2. Generate, update and test the product specification.
3. Provide backup to publications, which means checking the product specification, operator's manual and maintenance manual, as well as writing the theory of operation section of the
maintenance manual.

5. Provide complete information to drafting whenever necessary.

6. Provide backup to manufacturing before and during pilot run, by answering their questions, helping define test fixtures and assisting with component problems such as substitution.

Minimizing later customer problems

Most project managers in companies large and small realize that if their company is going to service its product, they must provide a design capability that minimizes later problems with the customer.

Such is the charter of Jack Alford, director of product planning, ILC Data Devices Corp., Bohemia, NY.

Alford says, “As a company whose goal is to do complete servicing for every product we design, we’re acutely aware of a problem that nearly all electronics manufacturers face: How to design products that won’t give trouble to the end user—or, if they do, that can be serviced easily.”

His engineering staff aims to do it by meeting the following challenges:

- Providing full product characterization.
- Using long-life components.
- Realizing that compromise designs are possible.
- Providing complete documentation.

Any company that is going to service its own product must determine the full characterization of the products, according to Alford. It must find out everything its products can do—not just the minimum and maximum specs, but everything. That will also provide a complete list of applications for potential customers.

After growing from a small company to a larger one, Alford says that they initiated a unilateral engineering review of all new-product designs. As they progressed, they found that the best method was a joint review of design among management, design and manufacturing personnel. This helped to uncover some more of the difficulties that come up in any normal design, and it eliminated the bulk of them.

“Engineering must always realize,” says Alford, “that its job isn’t done until manufacturing is capable of producing the design with minimum assistance from engineering.”

And a company might as well stay away from the ballpark altogether if its engineers are hooked on designing only products that are technological milestones.

“Engineering managers should make it clear to their staffs,” says Alford, “that the idea for new products is only as good as the market will accept.”

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**Industrial Electronic Engineers, Inc.**

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Phone: (213) 787-0311

European Office: 6707 Schifferstadt, Eichendorff-Allee 19, Germany.
Optical coupler helps transmit data and clock signals on single wire pair

Both data and clock signals can be transmitted on a single pair of conductors through the use of optically coupled isolators. The circuit concept can be used on party lines.

Selection of the optically coupled isolators depends on the application. When the isolators, OC, and OC,, have sufficient drive, the designer can eliminate inverters G,. A good isolator choice is the HP 5082-4370. For the circuit shown, 1-kΩ and 330-Ω resistors are recommended for R, and R,, respectively.

Here's how the system works: When the clock-in signal is LOW, the outputs of the line drivers, G,, are both HIGH, the output transistors from the optically coupled isolators, G, and G,, are both OFF and the clock-out signal is LOW. When the clock-in signal goes HIGH, one of the line driver outputs goes LOW and the other remains HIGH. If the data-in line is HIGH when the clock-in line goes HIGH, the output transistor of G, turns ON, the output transistor of G,, remains OFF, the clock-out line goes HIGH and the data-out line goes HIGH.

The clock-out line always follows the clock-in line. The data-out line follows the data-in line when a HIGH clock-in signal is present. When the clock-in signal goes LOW, the data-out line remains in the state prior to the last clock transition. The data-out signals can be fed into a serial-in shift register, which shifts data in on the trailing edge of the clock-out signal.

Richard Gunderson, Senior Project Engineer, ADC Products, 4900 W. 78th St., Minneapolis, MN 55435.

In this data transmission system, the values of resistors R, and R,, depend on both the data-transmission application and the type of optically coupled isolators that are used.
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Tester A (above) was designed to give auto mechanics a simple, rugged tester for "go/no go" tests that would otherwise be measured in electrical units unfamiliar to them.

Tester B is a modification of a standard Triplett tester incorporating only the specific ranges needed by the field service engineers for whom it was designed.

Tester C has special ranges and special input connectors and cables to permit a single-point connection for trouble-shooting and servicing all the circuits of a complex business machine.

Several other buyers of standard Triplett test equipment request their company name on the dial to personalize their testers.

If you think a custom tester may solve some problems for you, contact your Triplett representative. He'll put you in touch with the Tester Designers and Engineers at Triplett who'll help you analyze the problem and suggest the optimum cost/result solution. Triplett Corporation, Bluffton, Ohio 45817

INFORMATION RETRIEVAL NUMBER 49
Circuit warns automobile driver when he exceeds preset speed

Conventional automobile speed-warning devices require the addition of a multipole electromagnetic transducer in the transmission or the speedometer cable as a source for the speed signal. Here is a circuit that uses as the engine-speed signal the existing voltage pulses available at the primary of the spark coil. A switch in the transmission that is closed only in high gear is also needed.

The lowest-cost display could be simply a LED warning light. But more elegant is a set of two NSN71, 1/3-in.-high, seven-segment numeric displays that can be hard-wired to display speed at a preset limit. For best effect, this visual warning is accomplished by an audible alarm, which uses a tone generator to drive a miniature moving-coil loudspeaker.

The circuit in the figure employs a quad LM-2900 Norton op amp to perform all the functions. Amplifier A₁ amplifies and limits the signal from the spark coil. Amplifier R₂ converts frequency to voltage, so its output is a voltage proportional to engine rpm. This signal can directly drive a tachometer. Amplifier A₂ compares the voltage output from A₁ with a reference voltage and turns the output transistor on at the set warning speed. About 2% positive feedback in the circuit of A₁ prevents annoying chatter near the set speed, by providing hysteresis as in a Schmitt trigger. Amplifier A₃ generates an audible tone whenever the set speed is exceeded. Resistor R₁ calibrates the system. It is adjusted to account for the gear and axle ratios, number of cylinders, wheel and tire size.

The circuit is powered so the tachometer output is always available with the engine on. When the transmission moves to top gear, switch S₁ closes and connects the output light and speaker to the power source. When the vehicle speed exceeds the set value—about 56 mph, for the values shown—the display and tone are energized. To extinguish these warnings, the driver must slow the vehicle below the value determined by the hysteresis in A₃ (roughly 1 mph).

The integrating 10-µF capacitor on the frequency-to-voltage converter, A₂, can be increased so the alarm is not sounded for momentary excursions above the set speed.

David Long, National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, CA 95051. CIRCLE NO. 312
...and when it arrives, take special note of pages 42 and 43. They contain a factual—and useful—discussion of Acopian's long-standing 3-day-shipment policy. You'll find that "3 days" is not just an advertising slogan. It is a firm commitment that we have never failed to meet. You'll learn that, in an emergency, we may be able to do better than 3 days. We've also commented on the "stock delivery" claims of other power supply manufacturers, and what happens to delivery when the units ordered are out of stock.

The remaining pages provide complete specifications and prices for a comprehensive line of power modules and systems. Included are mini modules for powering IC's and op amps, as well as other supplies with ratings to 60 Amps and regulation to ±0.005%. The Acopian catalog also lists redundant output power systems, narrow profile and plug-in modules, and unregulated supplies.

Ask for the new Acopian 1974-1975 power supply catalog.
Circuit provides slow auto-wiper cycling, with one to 20 seconds between sweeps

An all-solid-state automobile wiper-control circuit allows the windshield wiper to sweep at selected frequencies from once a second to once every 20 seconds. The circuit uses one IC, two silicon transistors and seven discrete components.

Circuit timing is determined by a 555-timer IC and its external parts, R\textsubscript{A}, R\textsubscript{B} and C. Transistor Q\textsubscript{1} is switched on when V\textsubscript{1} goes LOW, and npn transistor Q\textsubscript{2} also turns on. The mechanical park switch takes over and conducts the motor current until one cycle of wiper motion is complete. At wiper park, the park switch opens and stops the wiper.

Transistors Q\textsubscript{1} and Q\textsubscript{2} conduct for only about 0.5 s. They do not conduct again until the next timer pulse. The delay between pulses is adjusted with the 500-k\textOmega delay resistor.

Resistor R\textsubscript{1} limits the current into Q\textsubscript{1} and the base of Q\textsubscript{2}. The peak collector current into Q\textsubscript{2} is about 3 A. Since the duty cycle is normally very low, little heating occurs.

This circuit is in use on a GM-Delco rectangular-motor wiper system.

Paul Galluzzi, Electrical Engineer, P.O. Box 352, Beverly, MA 01915.

CIRCLE NO. 313

In this windshield wiper system, voltage V\textsubscript{1} is a 0.5-s pulse—just long enough to move the wiper off the park switch. The wiper then executes one sweep and reparks until the next pulse occurs.

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Radar chain to cover Netherlands waterway

A radar chain covering the entire Westerschelde estuary, a Dutch waterway that also serves ports in Belgium, is being constructed by Philips Telecommunicatie Industrie in the Netherlands.

The chain on the eastern part of the Westerschelde will have two unmanned radar towers and a central station using two 3-cm radars. Telecommunication channels will be provided for command and return signals. One tower, the Saaftinge, is to be built on an artificial island in the estuary.

The 3-cm radar has high resolving power, and the antenna rotates at 20 rpm. Except for the magnetron, the equipment is solid-state. The pulse-repetition frequency is 3000 Hz and the peak power 30 kW.

A time-division-multiplex circuit combines the video signal, the synchronizing signals and the antenna-angle data into a signal with a bandwidth of about 13 MHz. This combined signal is passed to either of two transistorized radio-relay transmitters operating in the 7 GHz band.

One of these two transmitters is always connected to the antenna, while the output power of the other is dissipated in an artificial load. The antenna has a parabolic reflector of 2.4 m and a gain of about 42 dB. On each tower the antenna is pointed at two identical antennas of the radar center.

Each of these antennas is connected to two 7-GHz wide-band receivers, the output signals of which are continuously compared on the space-diversity principle. The strongest signal is selected automatically.

The time-multiplex signal selected is passed on to a circuit in which it is demultiplexed into a radar video signal, a synchronizing signal and an antenna angle-data signal. These signals are passed on to the display units.

The complete radar chain will have eight or nine unmanned towers.

Strain gauge senses pressures inside body

An electronic system has been designed for the measurement of multiple parameters inside the body, such as the intestinal tract, the circulatory system or the cervical tract. Developed at the Dept. of Biophysics of the Bulgarian Academy of Sciences in Sofia, Bulgaria, the system monitors biomedical pressure waves.

A special silicon strain gauge known as a “rosette” was developed. Twenty-one of these gauges each $1 \times 1 \times 0.05 \text{ mm}$, are mounted at 3-mm intervals on a probe with a 70-mm-long active section and a diameter of 3.5 mm.

The gauges sense pressure variations, and the outputs from the matrix of gauges show the speed of biomedical waves. Temperature compensation is provided by a non-active strain resistor in a bridge circuit which uses 21 active gauges. Multichannel tensiometric equipment records the outputs of the gauges in parallel or in series, depending on the propagation speed of the phenomena being examined. Patterns of normal biomedical waves can be obtained, so the system can distinguish abnormal circumstances.

The apparatus is useful for clinical and research applications and can also be a helpful adjunct to surgery.

Contact resistances too low to measure

Metal-to-semiconductor contacts that have resistances too low to be measured have been obtained at the University of Newcastle-upon-Tyne in England. Even when subjected to liquid-nitrogen temperatures, these contacts show no indication of the energy barrier that is typical of grown liquid-epitaxy types.

Usually a thick, high-conductance layer must be grown by costly and complex processes. If strict control is not maintained on the thickness of such a layer, it has excessively high thermal resistance and, at a certain stage, electrical-contact resistance reappears.

The difficulty in growing a layer of GaAs or InP lies in the volatility of the As and P components. The thin, high-conductance layers are formed by one of the metals acting as an ionizable shallow impurity. At low alloying temperatures, this can be achieved only by regrowth of the semiconducting material after it has been dissolved by metal-layer saturation. The loss of the volatile As and P components results in a regrown layer that is substantially thinner than the dissolved layer. This leads to unwanted contact resistance and an energy barrier.

To avoid out-diffusion of the volatile component, a certain amount of the volatile material is introduced into the alloying chamber, so that its vapor pressure can be carefully controlled. By use of an “overpressure” of As in the growth of contacts on GaAs, a very slow alloying cycle is achieved, and full control is maintained of the growth of the layer thickness.
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8-bit a/d converter module cuts size and price in half

Intech, 1220 Coleman Ave., Santa Clara, CA 95050. (408) 244-0550. $199 (1 to 24); stock.

Priced at less than $200 and offering an 800-ns max conversion time in a package only 2 x 2 x 0.4 in., the Intech A-857 analog-to-digital converter shrinks both size and price, compared with its closest competition, the ADC-G8B from Datel Systems (Canton, MA).

The $385 Datel module, packaged in a 2 x 4 x 0.4 in. case, is almost twice the price and twice the length of the Intech A-857— with about the same conversion time (but for more bits).

Both modules are linear to within ±0.5 LSB, offer at least 8-bit resolution (the Datel unit provides 10 bits) and have an accuracy of about ±0.1% ±0.5 LSB. The modules also share the same successive-approximation conversion technique—the source of their high conversion speed.

Power-supply requirements for both modules are +15, −15 and +5 V dc, but the A-857 needs only +35, −35 and +75 mA, respectively, while the ADC-G8B needs 50, 30 and 280 mA. Supply regulation is less critical for the A-857, since it has internal regulators.

The Intech unit also has an edge on operating and storage temperature ranges: −25 to +80 C and −55 to +125 C, respectively, compared with 0 to 70 and −55 to +85 C for Datel's unit.

The noise immunity, input impedances (2 to 2.5 kΩ), temperature coefficients (50 to 100 ppm/°C) and long-term stabilities (about ±0.1%/6 months) of both modules are comparable.

In a space formerly occupied by an 800-ns a/d converter, a pair of A-857s can provide 400-ns conversion time. This can be done if the converters are multiplexed and allowed to sample input voltages. These voltages are then converted and outputted alternately. The relatively low price of the converter makes this an attractive option.

For Intech
For Datel


The series 872 d/a converter is designed for low-power applications. Features include CMOS switching, an R-2R binary ladder network, a micro-power type 4250 output buffer amplifier and an internal ±10 V precision reference. Typical power dissipation levels are 4.5 mW for the DAC portion of the hybrid, and 40 mW for the precision reference section, which can be operated separately or disconnected. Two models are available, which differentiate between levels of linearity and precision reference specifications. Model 872-D1 accuracy code guarantees ±1/2 LSB in 10 bits over a temperature range of −55 to +125 C. Model 872-D2 guarantees ±1/2 LSB in 9 bits, over the same temperature range. Both units have a typical offset specification of ±1 mV and can be connected for 0 to +10, or −10-V-scale range by external connections.

Retroreflective control has range of 60 ft

MEKontrol, 56 Hudson St., Northboro, MA 01532. (617) 393-2451. From $180 (single qty.); stock.

The MEK-55-RD81-AAF LED reflective control has a 60 ft. operating range when used with a 3 in. diameter reflector. Ambient light does not affect the unit's operation, whether bright sun or total darkness. The LED light source and alignment indicator have an expected life greater than 100,000 hr. Plug-in relays, reed relays, logic, solid-state ac and dc outputs and five plug-in timing functions are available to provide maximum design flexibility. The unit is available in an "O" ring gasketed NEMA 3, 4, 5 and 12 die cast housing.
DIP-ended multipliers give accuracies within 0.25%


Tighter specs, lower cost and a smaller package are combined in the Burr-Brown 4204J and 4204K hybrid analog multipliers. These units housed in 14-pin hermetically sealed DIPs can deliver pretrimmed 0.5-to-0.25% accuracies at a maximum cost of $69.

Both multipliers are laser-trimmed for four-quadrant operation. No external components or amplifiers are needed for operation. Output accuracy drifts only 0.019%/°C vs temperature, while vs voltage, it drifts 0.02%/%. When connected to standard ±15-V supplies, the multipliers have a 1 V/μs slew rate, a 250-kHz, small-signal bandwidth and a 20-kHz, full-power response. Output noise over a dc to 10 kHz bandwidth (zero input) is a low 300 μV rms. Signal feedthrough at 50 Hz is 10 mV, pk-pk, for the 4204J and 5 mV, pk-pk, for the 4204K.

The internal output amplifier in either model can deliver ±10-V output swings at up to ±5 mA. Output impedance is a low 1 Ω.

Burr-Brown says these units are the most accurate DIP-sized multipliers available. The closest competitor in package size is Analog Devices, Norwood, MA, with its $26 Model 532, which has 1% accuracy. Modular units, though, are available from: Function Modules, Irvine, CA; Intronics, Newton, MA; Teledyne Philbrick, Dedham, MA, and Analog Devices, to name a few.

The Function Modules 511 has an accuracy of 0.25% and temperature drift of ±0.015%/°C. It measures 1.5 x 1.5 x 0.4 in. and costs $98—double the cost of the Burr-Brown 4204J and more than double the size. The M611 from Intronics has about the same specs but costs even more—$125. The Teledyne Philbrick 4455 is comparable to the Intronics unit—at least for the specs mentioned.

The 435K multiplier from Analog Devices costs $98, is internally trimmed to an accuracy of 0.1%, has a tempco of 0.002%/°C and is in a 1.4 x 1.4 x 0.65-in. case.

The Burr-Brown multipliers, the 4204J and 4204K, have accuracies of 0.5% and 0.25%, and cost $49 and $69, respectively. Delivery is from stock.
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Siemens Corporation
Components Group
P.O. Box 1390, Scottsdale, Arizona 85252
(602) 947-2231   TWX 910-950-1292   Telex 667-406
INTEGRATED CIRCUITS

Hex MOS/TTL sense amps have programmed levels

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. (408) 732-5000. $3.70 (100-up); stock.

Hex sense amplifiers that interface MOS to TTL now include programmable input thresholds. These devices—the DS 3605, 6, 7, 8 series—use a current-sensing input to provide wide flexibility, good speed and noise immunity. The four types available include inverting and noninverting outputs and bi-state and Tri-State inputs.

Input current sensing permits greater output speed for MOS memory systems by allowing the designer to pick the earliest possible point for detection of the input pulse to the sense amp. The input voltage to the circuits is clamped (0.8 V for 3605-6 and 1.6 V for 3607-8), thereby minimizing line capacitance effects. Input impedance is equivalent to one or two diodes.

A grounded programming pin gives a 100-µA threshold, an open pin a 300-µA threshold, and other values can be provided with a single resistor. From 100 to 300-µA, a resistor is connected between the pin and ground, and for values above 300 µA the connection is between the pin and \( V_{cc} \).

The 3605 version has a bi-state input and noninverting Tri-State output. The 3606 also has the bi-state input but an inverting output. The 3607 and 3608 follow similarly but have Tri-State inputs. The inputs of the 3607-8 can be forced to a high impedance state, permitting the MOS memory output to be sensed by another MOS device tied to the same line. A bipolar bus driver can interface with the MOS memory via the same line, with the sense inputs presenting no load.

The circuits can sink a maximum of 50 mA at 0.4 V and source 5.2 mA at 2.4 V. In the high-impedance state, the outputs will not source or sink more than 40 µA, max.

Other specifications include a 4.75-to-5.25-V operating range for \( V_{cc} \), a temperature operating range of 0 to 70 °C and typical propagation delays in the 16-to-28-ns range. Being current-sensing devices, the parts do not require the resistor in each input, as used for

(continued on p. 118)
6 ways you can get design flexibility with Panasonic miniature aluminum electrolytics.

1. **Panasonic L Series** gives you a complete range of standard miniature electrolytics for commercial, industrial and entertainment use. Wide range, from 4.7 µF to 10,000 µF. 6.3 through 100 volts. Available in axial and radial design, with temperature range of -40°C to +85°C. Panasonic L series mini's can be ordered in standard capacitor tolerances of ±10%; ±20%; or -10%, +75%.

2. **Panasonic MS Series** can be used to replace larger, more costly mylar capacitors. Their small size reduces space and weight on your PC boards. And because of their extremely low leakage and ESR ratings the MS series can be used to replace dipped tantalums at considerable cost savings. Panasonic MS electrolytics have a capacitance range of 0.1 µF through 100 µF. 6.3 to 100 WVDC.

3. **Panasonic 2H Series** gives you top performance under wide temperature conditions. Temperature characteristics from -55°C to +105°C. They have long product life and are available in radial and axial types. These electrolytics can be ordered in a choice of tolerances; ±10% and ±20%.

4. **Panasonic 3H Series** incorporates very wide temperature range (-55°C to +125°C) and attractive low temperature stability characteristics. The 3H Series can also meet most stringent environmental conditions. Available in axial and radial lead configurations with a choice of tolerances; ±10%; ±20%.

5. **Panasonic Z Series** are designed specifically for high stability over a temperature range of -40°C to +85°C. These miniature electrolytics have exceptionally smooth performance curves for temperature vs. capacitance, temperature vs. impedance and D.F. vs. temperature. Both in radial and axial type.

6. **Panasonic High Voltage Electrolytics** rated up to 500 volts (axial type) and up to 350 volts (radial type). Temperature range from -25°C to +85°C. Panasonic High Voltage Electrolytics are available in capacitance tolerances from -10%, +100%; -10%, +75% or ±20%.

Panasonic miniature electrolytics can meet most tough design specifications that call for very close tolerances, demanding ESR and leakage specs. We invite your special requirements. Panasonic's wide range of miniature electrolytics may be the answer to that special application problem you are trying to solve.
New and improved General Electric lamps provide for increased design flexibility.

**Two new sub-miniature halogen cycle lamps ideal for miniaturization.**

These new T-2, 6.3V, 2.1 amps, 75 hour GE halogen cycle lamps are the smallest of their type (.265") and set industry standards for size and light output (16-20 candlepower). They are perfect for miniaturization of equipment such as reflectors, housings and optical systems. They also save on overall cost of equipment and are less than half the cost of the #1973 quartz lamp they replace.

Two terminal configurations are available. #3026 (20 candlepower) has wire terminals. #3027 (16 candlepower) has a new two pin, ceramic base that plugs in to make installation and removal a snap. Samples of the #3027 lamp are available in limited quantities now; production quantities will be available in the first quarter of 1975. These lamps have an iodine additive that creates a regenerative cycle that practically eliminates normal bulb blackening. They will produce approximately 95% light output at 75% of rated life.

**An expanded line of Wedge Base Lamps for simple, low-cost circuitry.**

Now you can have greater design freedom than ever before with wedge base lamps. GE now offers six large lamps in its line of T-1 3/4 (.230" max.) all-glass, sub-miniature wedge base lamps. In addition to our three 14V lamps (#37, #73 and #74), we now also offer two 6.3V lamps (#84 and #86) and a 28V lamp (#85).

These lamps are ideal for applications where space is at a premium. Their wedge-based construction allows you to design for low-cost sockets and virtually ends corrosion problems because they won’t freeze in the sockets. And the filament, which is always positioned in the same relation to the base, offers more uniform brightness.

**Green Glow Lamp has been improved over previous lamp.**

Now our G2B Green Glow Lamp, the only domestic green lamp on the market today, gives a more uniform, purer green light than our previous model. It’s bright enough for your circuit component applications. With appropriate current limiting resistors, it can be used for 120/240 volt green indicator service. Or used together with our high-brightness C2A red/orange/yellow glow lamps to emphasize multiple functions with color.

All GE glow lamps give the benefits of small size, rugged construction and low cost — 12¢ each for the G2B, 4.4¢ each for the C2A in 100,000 quantities.

**Send today for newest literature.**

For the most up-to-date technical information on any or all of these lamps, write: General Electric, Miniature Lamp Products Department, #7412L, Nela Park, Cleveland, Ohio 44112.

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**INTEGRATED CIRCUITS**

(continued from p. 116)

such units as the 3208A and 75108.

The series can be used with a wide variety of MOS RAMs—including most 1-k and 2-k memories, such as the 1103, 1101, 5262 and 6003—and can interface CMOS to TTL. Even with some 4-k RAMs equipped with TTL outputs, the circuits can increase the over-all memory speed.

All versions are packaged in 16-pin DIPs, and a military series is available (DS 1605-8) in ceramic packaging for $8 in quantities of 100 and up.

**INQUIRE DIRECT**

**Gates, inverters extend low-power S-TTL line**

**INQUIRE DIRECT**

**Electronic Design 26, December 20, 1974**
Scientific calculator comes on single chip

MOS Technology, Valley Forge Corporate Center, 950 Rittenhouse Rd., Norristown, PA 19401. (215) 666-7950. $17.50 (250,000 up).

A single-chip calculator array (MPS2529) combines algebraic problem entry with parenthesis together with a full range of advanced scientific functions. Initially the array will be offered in three versions for operation with keyboards having 40, 35 or 20 keys. Besides the parenthesis capability, which permits two-level nesting, all versions also have these features: full-range scientific rotation for entry and result data, 12-digit display (8-digit mantissa); improved accuracy using 10-digit internal precision; memory with store, recall and accumulate keys, and full-chain calculation with any function sequence. In addition all versions handle basic arithmetic, exponential, and logarithmic and anti-log functions. Also, included are trigonometric, inverse trig and several convenience functions. Each array comes in a 28-lead DIP, and each contains internal clock generators on the chip.

CIRCLE NO. 325

256 and 128-bit RAMs use ECL 10,000

Motorola Semiconductors, P.O. Box 20924, Phoenix, AZ 85036. (602) 244-3466. $35 to $40 (100-999).

Two ECL-10,000 RAMs, the MCM10144L/AL and MCM10147L, are available in 256 x 1 and 128 x 1 formats, respectively. Address-input-to-memory-output access time, for the MC10144, is typically 18 ns, with a maximum of 30 ns. Address-to-output access time for the MCM10147 is typically 10 ns with a maximum of 12 ns. Maximum chip-enable-to-memory-output access times are 10 ns and 8 ns, respectively, for the MCM10144 and MCM10147. Both devices have open-emitter outputs, allowing wire-ORed connection to data busses. Chip Enable inputs permit memory expansion without additional decoding. Operating over a temperature range of -30 to +85 C, the memories are housed in 16-pin ceramic DIPs.

CIRCLE NO. 326

Before you order switchlights, we challenge you to compare our low cost

“Persuader Line” feature for feature with other leading brands

We're the kind of firm that believes in more than one gun barrel and plenty of ammunition. So when you add our familiar S410* series to our new S190* series, you'll find we have a very convincing line of general purpose switchlights indeed. It's “The Persuader” —the line we invite you to compare for low cost, quality and versatility with that of any other manufacturer. Just check the list below, then get in touch with your local distributor for exact specifications. And we're easy to find ... located in major cities world wide.

<table>
<thead>
<tr>
<th>Standard Features</th>
<th>Clare-Pendar &quot;Persuader&quot;</th>
<th>Micro</th>
<th>Dialight</th>
<th>Other</th>
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<tbody>
<tr>
<td>1. Low Cost</td>
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<td>2. Distributor Stock</td>
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<td>3. U.L. Listed</td>
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<td>4. 2 Form C</td>
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<td>5. Wiping Contacts</td>
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<td>6. Snap Action Contacts</td>
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<td>7. 10 amp Rated</td>
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<td>8. 2 amp Rated</td>
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<td>9. 100,000 Cycle Life</td>
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<td>12. Solid/Proj. Displays</td>
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<td>13. 5 Adapter Shapes</td>
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<td>15. Snap-In Mount</td>
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<td>16. Rear Panel Mount</td>
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<td>17. Gang Frame Mount</td>
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<td>19. Engraved Legends</td>
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<td>20. Alt. Remain-In</td>
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<td>21. Mom./Alt./Indicator</td>
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'S190 $1.62 in quantities of 1000 See distributor listing Vol 1/568
'S410 $2.53 in quantities of 1000

CLARE-PENDAR

CLARE-PENDAR a GENERAL INSTRUMENT CO. Box 785, Post Falls, Idaho 83854 (208) 773-4541

INFORMATION RETRIEVAL NUMBER 59
Low profile mini-relays can handle up to 26.5 W


The 911 series of hermetically sealed low profile relays is designed to fit on densely packed printed circuit boards. The flat packaged, rotary armature type relays measure only 0.25 in. high and have rigid, 0.25 in. long, 0.025 in. diameter, terminal mounting pins.

Relay contacts are arranged as double-pole, double-throw (dpdt) to give two independent circuit switching actions.

The relays are available in coil voltages of 6, 12, 26.5, 48 and 76 V dc. Other coil voltages are available on special order. The series 911 relays meet or exceed all the performance requirements of MIL-R-5757D. They can withstand 50 g shocks for 11 ms and 20 g peak vibrations from 10 to 2000 Hz.

The low height of the relay permits closer board spacing, while the plug-in, solder dip terminals simplify self-mounting. The terminals also eliminate the need to fish free leads through PC board holes or use mounting brackets with screws or rivets. Contacts are rated for low-level dry circuit loads of up to 1 A at 26.5 V dc, resistive (maximum). The contact life expectancy is specified for more than 100,000 operations at full rated power to the load.

The operating temperature range for the relays spans -65 to +125 C.

Prices for the 911 series relays start at $7 to $8 when ordered in 1000 piece lots. Delivery for the relays is from 8 to 10 weeks.

CIRCLE NO. 302

10MHz 5” scope with easier calibration and voltage measurement

Here are some B&K extra touches. Besides DC-to-10MHz bandwidth, triggered sweep, automatic sync, 16.6mV/cm vertical sensitivity, DC-coupled amplifier and front-panel Vectorscope capability, Model 1465 also has 5X magnification to increase sweep speed to 0.2usec/cm for complex waveform analysis. And Cali-Brain®, which collapses horizontal sweep to let you measure instantaneous peak-to-peak voltage easily while simultaneously displaying the full-scale voltage range. Now in stock at your local distributor or write Dynascan.

Model 1465 $400

Your quality work deserves digital convenience

Model 282’s DC accuracy of reading of 0.5% ± 1 least significant digit makes it 6 to 13 times more accurate than the industry’s most popular bench-type VOM. And it’s much easier to read Model 282’s bright digital display. Also features automatic polarity, clear out-of-range indication, automatically positioned decimal point, full overload protection, 100% overrange capability, 10 megohm input and isolation probe. Now in stock at your local distributor or write Dynascan.

Model 282 Multimeter, $200

INFORMATION RETRIEVAL NUMBER 60

INFORMATION RETRIEVAL NUMBER 61

120

ELECTRONIC DESIGN 26, December 20, 1974
Precision potentiometer features low cost

Beckman Instrument, 2500 Harbor Blvd., Fullerton, CA 92634. $5.50 (1-9); stock.

Model 7286 precision potentiometer is a high-performance, low-cost unit. Some features of the 10-turn, 7/8-in-dia, bushing-mounted resistance element are: 2-W power rating at 70 C, independent linearity within 0.25% and ambient temperature range from -55 to 125 C. A separate contact position guide decreases coil wear. Several other features available on order are: center tap, linearity tap, flatted shaft, slotted shaft and shaft lock.

CIRCLE NO. 327

Pushbutton switches assemble to 50 stations


The simple basic design of CG-7700 pushbutton switches allows many variations. It is possible to have a continuous bank of up to 50 stations, lighted or unlighted. Contacts are either leaf-type springs with cross-bar contacts, open snap-action contacts or enclosed snap-action contacts. Contacts can be stacked in assemblies from 4PDT to 12PST. Standard construction allows interlatching and lock-out actions between all stations on a single bank assembly of up to 50 stations.

CIRCLE NO. 328

Introducing Shelly's TRANS-EYE

the microminiature front-relampable indicator light with a built-in solid state amplifier.

Built-in Hybrid Drive Amplifier

Another good reason why Shelly sells more T1 incandescent indicators than anyone. It's our Trans-Eye with built-in hybrid amplifier. Configurations (NPN or PNP) include internal base current limiting resistor, pull-up resistor, diode in series with base to increase noise immunity, and a unit which is compatible with positive inverted logic.

We've put the drive circuitry into the lamp so you don't have to mess around with it on your boards.

Just Snap Into Panel

Trans-Eyes are easiest to use too. Just insert into .191” hole and press into position. Front panel relamping is also a cinch.

No tools needed. Just remove snap-on cap, remove lamp, insert new one, replace cap. Takes just seconds. Trans-Eyes are just right for contemporary panels where space is at a premium.

Mounting on .225 centers, they offer clean design and high illumination. The modern look.

CIRCLE NO. 329

Digi-Caps Too

Imagine. One or two letters, numerals or symbols imprinted on a tiny Trans-Eye indicator. A great way to give added dimension to your display.

Send for our free "How To Order" brochure or phone 800-645-9200 EEM Dial-A-Source.

shelly associates

A Subsidiary of Datatron, Inc.

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MAILING ADDRESS: P.O. BOX 11427, SANTA ANA, CALIFORNIA 92711

INDICATORS • MULTI MESSAGE DISPLAYS • FIBER OPTICS • ANNUNCIATORS
"Okay, okay.
You tell me where we can find twenty thousand RAMs a week for that much less than the 2102 and I’ll tell you where to find the Easter bunny."

Give him
the good news:

You can find all the 1K RAMs you need right now—right here at AMI. We have 4006, 4008 and 4008-9 RAMs ready for immediate delivery. They’re pin-for-pin with Mostek’s. But you can get more of ours—faster. (Stands to reason that when you have larger production facilities you can produce more.) The price is right, too. For example, the 4008-9 is yours for just $3.50 in quantities over 1000. You get the advantages of a 2102 system, while saving a bundle with our 4006 family. You can get an application note on how to do it, and a free sample, by writing to Frank Rittiman, AMI, 3800 Homestead Road, Santa Clara, CA 95051. Phone: (408) 255-3651. Or ask your distributor.
The charge of the 1K RAMs.

No more waiting for your 4006 family.

You have a perfect combination of price/performance for your 1024 bit MOS RAM applications. Use them for buffer or scratch pad memories. Or for peripherals, terminals, displays, programmable calculators, cash registers, optical scanners, spectro-analyzers.

And we give you more than fast deliveries. We give you specs like these:

P/N S4006 S4008 S4008-9

| No. of Bits | 1024x1 1024x1 1024x1 |
| Access Time | 400 ns 500 ns 800 ns |
| Cycle Time | 650 ns 900 ns 1000 ns |
| Power Supply | +5V, +5V, +5V, -12V, -12V, -12V |

And this is how the S4006/8/8-9 looks on paper:

Intelligent controller aids remote data-acquisition

With an intelligent controller called PROCOM 1, remote measurement and control systems can speak the language of your computer—even in a hierarchy. The microprocessor-based unit, from Computer Products, is supplied with communications firmware (PROM programs) for serial asynchronous IBM 2260 protocol—one that is available with most minis as well as the IBM 360 and 370 Series.

The controller’s firmware manages the routing, scanning and blocking of data to and from the manufacturer’s RTP 7400 analog/digital measurement and control equipment. At the remote site, the unit can also support a TTY or TTY-compatible terminal via a second serial port.

Each controller supports up to eight 7400-Series acquisition and controller units on its 16-bit parallel I/O bus. These devices include a universal controller (analog and digital I/O), a high-level analog controller (four to 64 channels, ±5 mV to 1.0 V) and a wide-range unit (eight to 512 channels, ±2.5 mV to ±10.24 V).

The PROCOM 1 is a microcomputer based on the 8080 microprocessor from Intel (Santa Clara, CA). The controller’s chassis contains room for six cards—four standard cards (CPU, parallel I/O; serial I/O and power supply) and two optional cards in a 3-1/2-in.-high RETMA rack-mount panel.

With the polled communications protocol used, one host computer port can manage up to 16 controllers on a single full-duplex line. The host can initiate a variety of channel selections for scan control as well as send and receive data with each unit. For private lines the Computer Products 7420/30 remote serial link (limited-distance modems) provides data rates up to 19,200 bit/s between host and controllers. Or the user can use standard modems such as the Bell 202 or 103 or their equivalents. The Bell modems have data rates of 1800 bit/s or 300 bit/s, respectively. At the maximum rate of 19.2 kbit/s, the controller can handle 450 samples/s of 16-bit words.

System prices vary with the configuration. A universal controller (Model 7430) PROCOM 1 and two modems list for $8669. A private-line system that includes the 7430 and 7480 wide-range analog unit lists for $11,069; the controller with 2048 bytes of PROM and 512 bytes of RAM costs $2995. Substantial OEM discounts are available. Scientific Systems Services (Melbourne, FL), which developed the firmware, also plans to offer Fortran applications modules for host use.
DATA PROCESSING

Low-cost disc drives offer 6.2 Mbit capacity

Diablo Systems, 24500 Industrial Blvd., Hayward, CA 94545. (415) 783-3910. See text; stock.

Features of the Series 10, Model 12 flexible disc drives include copy capability, 612 Mbit capacity, IBM 3740 compatibility and ceramic/ferrite heads for longer diskette life. These units are said to provide two drives in about the same size package as most single units. Price for single units is $1100, which drops to under $600 for large quantities.

CIRCLE NO. 329

Adapter mates mini to maxi as a peripheral

Austron, Inc., 1915 Kramer Lane, Austin, TX 78758. (512) 836-3523. See text.

The Model 8001 is a buffered adapter that performs all interfacing between the IBM 360/370 multiplexer channel and a bidirectional 16-bit minicomputer I/O channel. Either single byte or multibyte transfers are accomplished (four-byte maximum). A sequence buffer relieves the mini of channel response requirements. Transfer speed depends on mini cycle time. A 1-µs mini can achieve 42 kbyte/s; for minis with 750 ns or less, the rate goes to 50 kbyte/s. The adapter plugs into the channel cable and conforms with the interface standard for IBM peripherals. Software is free, and the mini can appear as a card reader, line printer to the maxi. Price varies with quantity from $8500 (for a single unit) to $4000 for large purchases.

CIRCLE NO. 330

TTY-compatible terminal has 132 print positions

Sperry Univac, P.O. Box 500, Blue Bell, PA 19422. (215) 542-4213. $2592; stock.

A communications terminal named the DCT 475 includes a data entry keyboard and an incremental printer for operation at 10 char/s. The TTY-compatible unit prints the full 63 ASCII characters and provides up to 132 print positions. Communications can be full or half-duplex.

CIRCLE NO. 331

THE MAXI KEYBOARD FAMILY

Shopping for keyboards? Don't buy more — or less — than you need. Maxi can supply keyboards to your mechanical and electronic requirements, in standard or custom configurations.

Economy? Our 3100 Series encoded keyboard with mechanical contacts is priced as low as the $50.00 range in quantity. Dual bifurcated gold contacts have a life of over 10^7 operations under load.

Need the option of glass reed switching? The Maxi 2700 Series keyboard combines low cost and high reliability. All reeds are pre-tested before assembly, and switch modules are machine-adjusted for accurate operating point.

Special key actions? The Maxi 1800 Series keyboard offers more action options than any other keyboard on the market. Interlatch and lockout, accumulative latch, solenoid hold and release to name a few. Even illuminated buttons if you need them. Its metal frame construction makes the 1800 Series the strongest keyboard of the market.

The Maxi keyboard line includes double-shot and engraved buttons in a variety of sizes and colors. Encoding is another flexible Maxi option. Specify USASCII, EBCDIC or special codes in up to nine bits. The Maxi keyboard family has a member exactly suited to your needs. Call or send your specs for a firm quote on cost and delivery.

THE

(See Maxi in EEM)

Maxi-SWITCH CO.

9697 East River Road • Minneapolis, Minnesota 55433 • (612) 755-7660

INFORMATION RETRIEVAL NUMBER 65

Electronic Design 26, December 20, 1974
Our advanced hi-speed CRT’s now available with color.

- high sensitivity, short length, electrostatic deflection.
- up to 15" diagonal and 16" diameter tubes.
- up to 850 MHz bandwidth.
- ruggedized types available.
for oscilloscope, radar and data display.
Sealed disc made for OEMs is rugged and inexpensive

Tri-Data, 800 Maude Ave., Mountain View, CA 94043. (415) 969-3700. $1325 (unit quantity); 60 day.

A sealed, fixed-disc subsystem from Tri-Data, the Model 100, is designed to operate for up to five years with no maintenance. The subsystem is sealed against dust and can withstand a 10-g shock (11 ms, 1/2 sine wave) while operating, or up to 15 g during transport.

The unformatted data capacity of the disc is 2.9 million bits, with 2400 bits for each of 16 sectors. Access time is 10 ms, track-to-track, with a 10-ms settling time and 16.7-ms average latency. The unit has a recording density of 1600 bpi (inner track), 64 tracks per head (total 128), and the number of sectors is variable from 1 to 16.

The hard-read error rate is one for every 10⁹ bits read, with one seek error in 10⁶ seeks. The drive-and-disc assembly is in a 20-lb casting that is 6.5 in. high and has a diameter of 13 in. The power requirements are 75 W at 105 to 125 V ac, 50 to 60 Hz. Since the system is designed for the OEM, it is difficult to determine precisely what the electronics would cost to support the memory, but costs are estimated at about $750 to $1500.

Although not intended to compete with floppy discs, the Model 100 does compare in many ways with such units as the SA 900 diskette storage drive from Shugart Associates, Sunnyvale, CA. The SA 900 has an unformatted capacity of 3.1 megabits, data-transfer rate of 250 kilobits per sec and access and settling times the same as the Model 100, with an 83-ms latency.

The diskette uses an IBM-compatible recording format that permits data to be transferred from machine to machine—which, of course, a sealed disc cannot do. A diskette drive does require periodic maintenance, ranging from every few weeks to a few times a year, depending on use. And the diskette is designed to last over a year under most conditions, over five years when treated more carefully.

The SA 900 from Shugart Associates will not operate properly with a 10-g applied force, but it can operate with about 2 g's. It has no dust filter but will work in most offices or light-industrial environments.

The disc in the Tri-Data Model 100 is a 9-in. nickel-cobalt medium with a protective overcoating. It rotates at 1800 rpm and is sealed in an airtight housing (continued on p. 128)
Go ahead because Ise lights your way to smaller, snappier equipment with a new wafer-thin multi-digit display. Then in addition to lighting the way, gives you a choice of two displays to work with. The DP-AS Multi-Digit Display with nine, eleven or thirteen digits. Or the FG type Multi-Digit Display with nine or twelve digits.

Digits on (FG) models measure a mini 5mm high to help you be as small in your thinking as you want. Both new displays are glass-enclosed all around. And have easy-mounting pin connectors. But mounting isn't the only thing that comes easy with these trimmed-down displays. Reading the indication they give comes easy, also. Because Ise keeps with the past. Gives these new multi-displays the same eye-easy green glow and planer construction that make their forerunners so popular. In addition, they also give you low-voltage advantages for direct LSI drive.

If you've been holding back on a headful of ideas simply because the right multi-digit display wasn't available, it's time to stop.

Creator of Fluorescent Digital Display:
ISE ELECTRONICS CORP.
P.O. Box 46 Ise city, Mie Pref., Japan
Tel: (05963) 5-2121 Telex: 4695623

ISE CORP. OF AMERICA
1472 West 178th Street, Gardena, Calif., 90248 U.S.A.
Tel: (213) 532-0470 Telex: 230674910

Representative: Paris, Munich, Amsterdam, Stockholm, Vienna, Milan, Bombay, Hong Kong, Taipei

INFORMATION RETRIEVAL NUMBER 68
Unique versatility from a non-destructive read-out memory, (NDRO), thanks to special TOKO woven plated wire design.

This system is ideally suited for use as a random-access memory (RAM), an electrically alterable read-only memory (EAROM) or a fixed read-only memory. EAROM is suitable for micro-computer applications.

The MINI-ROM A has either 1 kW/8-bit or 2 kW/4-bit capacity, using only a single board, with a cycle time of 3 µs and access time of 2.4 µs. Mounted on small removable RAM board, which is not required for read-only (ROM) functions.

MINI-ROM B has a 1 kW/9-bit capacity, with a 1 µs cycle time and 500 ns access time. Its capacity comes from four 256W/9-bit units, each of which can be used individually for ROM or RAM.

<table>
<thead>
<tr>
<th>Specifications</th>
<th>MINI-ROM A</th>
<th>MINI-ROM B</th>
</tr>
</thead>
<tbody>
<tr>
<td>Capacity</td>
<td>1 kW-8 bit (2 kW-4 bit)</td>
<td>1 kW-9 bit</td>
</tr>
<tr>
<td>Access Time</td>
<td>2.4 µs (1.2 µs)</td>
<td>0.5 µs</td>
</tr>
<tr>
<td>Cycle Time</td>
<td>3.0 µs (1.5 µs)</td>
<td>1.0 µs</td>
</tr>
<tr>
<td>Power</td>
<td>+5V, -5V, 10.5W (ROM), 15W (RAM)</td>
<td>+5V, 10.5W (ROM), 15W (RAM)</td>
</tr>
<tr>
<td>Dimensions</td>
<td>2000 x 250W x 29mmH</td>
<td>2000 x 200W x 24mmH</td>
</tr>
<tr>
<td>Interface</td>
<td>TTL Negative Logic</td>
<td>TTL Negative Logic</td>
</tr>
<tr>
<td>Memory Element</td>
<td>NDRO type Plated Wire</td>
<td>NDRO type Plated Wire</td>
</tr>
</tbody>
</table>

Eight 2.5-Mbyte discs added to PDP-11

Computer Labs, 1109 S. Chapman St., Greensboro, NC 27403. (919) 292-6427. $8950 (two discs); 30 to 45 days.

The Series M3000 disc memory consists of a moving head, rotating mass memory, controller, and all necessary cables for connection to the UNIBUS of the DEC PDP-11 computer family. This disc Memory System—at what is said to be substantial savings—offers complete software and hardware compatibility with the PDP-11. The single platter is changeable with the DEC RK05. The self-contained controller can access up to eight 2.5 Mbyte discs. Models are available in single (removable) platter, dual (fixed and removable) platter, front and top-loading systems. All have 35 ms (average) positioning time for random moves and 9 ms for track-to-track positioning.
MICROWAVES & LASERS

Rf transformers operate up to 600 MHz

Mini-Circuits Laboratory, 2913 Quentin Rd., Brooklyn, NY 11229. (212) 252-5252. $2.95 to $3.45 (10-49); stock.

The company's T-Series compact rf transformers cover the 0.015-to-600-MHz frequency range. The new units operate with impedance levels of 12.5 to 800 Ω, and they feature typical insertion losses of less than 0.5 dB. A typical unit—the Model T4-1, for 4:1 impedance ratio based on 50 Ω—list a maximum insertion loss of 1 dB over the 2-to-100-MHz band. From 5 to 100 MHz, it has a maximum unbalance of 0.1 dB in amplitude and 1° in phase.

CIRCLE NO. 333

Sources generate L-to-X band signals

Polarad Electronic Instruments, 5 Delaware Dr., Lake Success, NY 11040. (516) 328-1100.

Four modular signal sources—the 1205 through 1208—cover L through X bands in overlapping ranges from 800 MHz to 11 GHz. The 5-1/4-in-high units contain modulation capabilities for FM and square wave. For widely adjustable pulse modulation, the company offers the Model 1020 modulator. The four new sources have minimum output power ratings of 35 to 80 mW. Stability and freedom from harmonics are reportedly provided by the sources' lightly loaded cavity-tuned oscillators. The company offers a one-year warranty without component exclusions.

CIRCLE NO. 334

If you don't require all the electrical performance built into SMA type connectors, why pay for it? Up to 3 GHz for flexible cable assembly and even beyond 6 GHz for semi-rigid assembly, our new JCM series gives you the same electrical performance as the far more expensive SMA types. The series includes connectors for both panel and PC mounting. All are interchangeable and intermateable with the standard, expensive SMA connectors. So you can use them without making any changes... and without compromising required performance. There are JCM connectors to accept virtually any miniature size cable, so you don't have to stock a big variety. It's worth looking into, isn't it? All it costs is a stamp.

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Please check for technical information or test samples of our new low-cost series 142-0200-001 JCM connectors.

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E. F. JOHNSON COMPANY
INFORMATION RETRIEVAL NUMBER 70
Harmonic rejection filters work to 12 GHz

Cir-Q-Tel Inc., 10504 Wheatley St., Kensington, MD 20795. (301) 946-1800.

A broad line of low-pass harmonic rejection filters spans a cutoff frequency range of 250 MHz to 12.4 GHz. The new units have a rejection ratio of at least 60 dB at 1.4 times the passband high frequency. They are tubular in shape and available in 13 standard models. Frequencies from 250 to 1000 MHz are covered by Models 1L, with a diameter of 1/2 in. and power capacity exceeding 15 W cw. Higher frequencies from 1500 MHz to 12.4 GHz are covered by 2L Models that are 1/4 in. in diameter, with power handling capacity exceeding 2 W cw.

Cascadable amps have 35-dB NF


Two low-noise cascadable amplifiers—the WJ-A3 and A4—offer gains of typically 15.5 dB and VSWRs of less than 1.3:1 across a 5-to-500-MHz bandwidth. Each can be used in 50-Ω microstrip rf and i-f systems, and each model has a noise figure of 3.5 dB typical. The new units are intended for use as first stages for reduced system noise figure. The WJ-A3 comes in a hermetic, four-pin, TO-8 package, while the WJ-A4 is housed in a hermetic, eight-pin flatpack.

Optical gate selects pulse

Hadron, Inc., 2520 Colorado Ave., Santa Monica, CA 90404. (213) 829-3377. $9200 to $9800.

The Model KQS4 optical gate can be used at the output of either ruby or Nd:Glass Q-switched laser oscillators, operating in either the normal giant pulse mode or in a mode-locked configuration. When used with normal giant pulse oscillators, the KQS4 can gate out pulse widths as narrow as 3 ns. When used with mode-locked oscillators, the KQS4 is capable of gating out a single sub-nanosecond pulse from a train of pulses. The KQS4 contains the electronics for powering the unit, and the optics assembly.
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CONTINENTAL CONNECTOR CORPORATION • WOODSIDE, NEW YORK 11377
INFORMATION RETRIEVAL NUMBER 73

Electronic Design 26, December 20, 1974
from SPECTRUM.... for emi CONTROL.
The 1 MF. FEED-THRU CAPACITOR.

The combined technologies of SPECTRUM CONTROL, INC. and ALLEN-BRADLEY CO. have produced this exciting line of multi-layer feed-thru capacitors. Their tubular design and coaxial construction gives low inductance with capacitance values to 1 MF. The operating temperature range is -55°C to +125°C at 10 amps and 50 VDC. They are ideally suited for bypassing, filtering and coupling applications. Write today for our complete catalog.

<table>
<thead>
<tr>
<th>Part No. (Threaded)</th>
<th>54-785-005</th>
<th>54-786-006</th>
<th>54-786-007</th>
<th>54-786-013</th>
<th>54-786-014</th>
<th>54-786-015</th>
</tr>
</thead>
<tbody>
<tr>
<td>DC Working Voltage</td>
<td>100</td>
<td>50</td>
<td>50</td>
<td>35</td>
<td>35</td>
<td>35</td>
</tr>
<tr>
<td>Capacitance, MF. at</td>
<td>0.05 GMV</td>
<td>0.3 GMV</td>
<td>0.5 GMV</td>
<td>1.0±20%</td>
<td>1.0±20%</td>
<td>1.0±20%</td>
</tr>
<tr>
<td>O.1 VRMS, 25°C, 1 KHz</td>
<td>16</td>
<td>32</td>
<td>36</td>
<td>40</td>
<td>40</td>
<td>40</td>
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<tr>
<td>Insertion Loss (db)</td>
<td>50</td>
<td>70</td>
<td>70</td>
<td>80</td>
<td>80</td>
<td>80</td>
</tr>
<tr>
<td>Thread Size - Bolt</td>
<td>8-32</td>
<td>10-32</td>
<td>10-32</td>
<td>10-32</td>
<td>10-32</td>
<td>10-32</td>
</tr>
<tr>
<td>Mounting Hole Size</td>
<td>.140 ±.015</td>
<td>.171 ±.015</td>
<td>.171 ±.015</td>
<td>.171 ±.015</td>
<td>.171 ±.015</td>
<td>.171 ±.015</td>
</tr>
</tbody>
</table>

Available now from these authorized distributors:

- HALL-MARK ELECTRONICS 215-355-7300
- METUCHEN CAPACITOR 201-442-0500
- MIRCO ELECTRONICS 602-944-2281
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PH. 814-474-5593 TWX 510-699-6848

POWER SOURCES

Isolator/Regulator gives 100 MΩ/250-pF I/O

Datel Systems, 1020 Turnpike St., Canton, MA 02021. (617) 838-8000.

The UPM-5/500-D5 is a dc/dc converter with 100 MΩ isolation and only 250-pF capacitive coupling from input to output. It is designed for local circuit board transformation of a 4.5-to-5.5-V noisy or unregulated logic power into regulated and isolated 5 V. The unit can also be used to develop negative 5-V power from a positive 5-V power bus. The output voltage has a 200 ppm/°C tempco and is short-circuit protected with foldback current limiting. Output ripple voltage is less than 1 mV rms. Other specs include 500-mA output and 0.05% regulation. Size is 2 × 2 × 0.432 in.

CIRCLE NO. 338

DC/dc converter works under high CMVs

Data Translation, 109 Concord St., Framingham, MA 01701. (617) 879-3595. $149; stock to 2 wks.

Model DT-5750 dc/dc converter is designed for use where high common-mode voltages are prevalent. This completely floating module converts ±5 V to ±15 V and +5-V power despite voltage differences of 500 V between input and output. The converter supplies 165 mA from each side of the 15 V and 750 mA from the 5-V output. All outputs are floating and isolated, multiple input/output isolation is less than 150 pF and greater than 1000 MΩ, and breakdown voltage between input and any output is greater than 500 V.

CIRCLE NO. 339
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ELECTRONIC DESIGN 26, December 20, 1974

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INFORMATION RETRIEVAL NUMBER 78

133
Op-amp supply delivers ±100 mA

Optical Electronics, P. O. Box 11140 Tucson, AZ 85706. (602) 624-8358. $66; stock.

Model 8430 dual ±15-V power supply can deliver continuous current of ±100 mA. The unit is protected against overload currents, short-circuits, and high ambient temperatures. The 8430 is also protected against reverse currents driven into the power supply from the load. The unit can operate at line-voltage frequencies of 50 to 400 Hz and line voltages from 125 V ac down to 90 V ac. Size is 3.5 \( \times 2.5 \times 1.25 \) in.

CIRCLE NO. 340

Voltage standard is accurate to 0.005%


Model TE2004 dc voltage standard provides four full-scale operating ranges from 11 mV to 11 V with better than 1-ppm resolution. The precision output voltages within each range are set by six digiswitches. Two portable models with specified setting accuracies of 0.01% or 0.005% are available. No standardization is required because a high-stability reference is included in the unit. Other built-in features are a sensitive microvolt null-balance potentiometer and an output-polarity reversing switch. The battery/line power unit makes possible field operation independent of line power.

CIRCLE NO. 341

20-W dc/dc converter delivers triple outputs

CellMate Div., 1405 Civic Center Dr., Santa Clara, CA 95050. (408) 249-8400. $149; 60 days.

Claimed to be the first triple-output dc/dc converter to deliver 20 W, the Model 100 offers practically universal output voltage selection. One output is 5 V. The other two outputs are of opposite polarity, and each is individually adjustable from 0 to 15 V. The unit operates from any voltage source within the range of 10 to 32 V and features a unique inward-folded case design which provides over 100 square inches of heat-dissipating surface. Size is 4-1/2 \( \times 4 \times 1-5/8 \) in. and weight is 15 ounces.

CIRCLE NO. 342

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INFORMATION RETRIEVAL NUMBER 79
Logic supply reads ONEs and ZEROs

Grumil Corp., 4626 Idlewilde Lane SE, Albuquerque, NM 87108 (505) 265-2320. $84; $105 with option.

This 5-V, 1-A laboratory supply features a seven-segment direct-readout logic-probe option. Standard specs include: output fully protected against overload, floating output (±300 V dc) load regulation of 0.01% NL-FL, line regulation of 0.01% NL-FL, ripple and noise of 1 mV pk-pk and tempco of 0.02%/°C. The logic probe option provides direct readout of ONE, ZERO and "H" for high-impedance or open-collector three-state logic, and flashing display to indicate a fast pulse.

CIRCLE NO. 343

Compact hv unit can be programmed

Sierra Systems, 650 Vaqueros, Sunnyvale, CA 94086. (408) 733-1040. $100; stock to 2 wks.

Series 774 high-voltage module is encapsulated for full environmental protection. Input voltage is 28 V dc; ripple and regulation is 0.1% pk-pk and 0.5%, respectively. Output voltages for the nine variations of the Series 774 range from 500 to 18,000 V. The unit is solid-state and resistance and voltage programmable.

CIRCLE NO. 344
INSTRUMENTATION

Modules manipulate & send test data at 150 Mbits/s


Engineers who use Tau-Tron equipment to make error-rate measurements can now do so at 150 Mbit/s and with increased data-manipulation capability. Two additions to the company's modular TMI instrument line make this possible.

The ME-1, called a bit-rate extender, serves as a companion to the year-old pseudorandom generator and error detector, or receiver, that form the foundation of the test line. With the ME-1, data can be zipped through the system under test at twice the original rate of 75 MHz.

The second module, the MM-1, takes the pseudorandom stream, searches for a particular sequence in the stream up to 20 bits long and then, upon detection of the sequence (or upon external command), modifies a number of successive bits up to 99. Modification can involve injection of errors (logic complements) or the forcing of a byte to ZERO or ONE.

The first bit of the modified sequence can be selected anywhere from four bits before detection to four bits after. Front-panel toggle switches plus a two-digit thumbwheel select the desired sequence and the number of bits to be manipulated.

Thus the MM-1, which can operate at 75 MHz, makes the pseudorandom sequence less random as special test codes—or a preamble, if desired—are inserted.

Preambles up to 99 bits can be inserted when the sync pulse—generated upon detection of the unique incoming sequence—is used to trigger an external, fixed-word generator. The output of the generator is connected to the MM-1's preamble input jack, and the fixed word appears in a selected, blanked (all ZER Os) portion of the pseudorandom sequence.

Since the modules in the Tau-Tron transmission/detection system operate synchronously with a system clock, provision is made in the ME-1 rate extender to prevent races and allow alignment between the data and the clock. Adjustments are made with indicators and slide switches that can be set for various phase delays from 0 to 5 ns. The indicators tell when the data input is properly latched and when the data and clock have proper phase.

Delivery is stock to six weeks.
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- Lamp Indicator
- Exponent Key
- Change Sign Key
- Reciprocal Key
- Square Root Key
- X^n Key
- Y^n Key
- Natural Log Key
- Common Log Key
- Common Antilog Function
- Natural Antilog Function

Compact Size: 3⅛" x 6" x 1⅞"

The exciting new "1400" instantly computes natural and common logs and antilogs as well. It calculates sines, cosines, and tangents, and their respective inverses. It expertly handles quantities as small as 1.0 x 10^-10 up to 9,999,999,999 x 10^9. It features special parenthesis keys, prefers non-scientific notation, and has a 14 character display. The "1400" is quite comparable to units selling for $150-$225. Order now for immediate delivery.

Please send me Commodore 1400 Scientific Electronic Calculator(s) at $99.95 each. (plus $3.95 shipping, handling, and insurance) If not completely satisfied, I can return it within 2 weeks for an Immediate Refund.

INFORMATION RETRIEVAL NUMBER 85

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INFORMATION RETRIEVAL NUMBER 86

Technology Marketing, 3170 Red Hill Ave., Costa Mesa, CA 92626. (714) 979-1100. $20,000 to $29,000; 60 days.

Model 2160 computer-controlled system simultaneously tests logic states and timing for up to 160 I/O lines. The system is designed for high volume production tests of circuit cards and other electronic devices and assemblies. No languages are required. Operator oriented front-panel controls and technician-oriented programming methods allow the lowest possible level of skills. Costly software maintenance expenses are avoided. Fault isolation down to node and individual ICs are easily attained. Major specifications include: test rate of 6400 bytes/sec.; read/write memory of up to 16K bytes.

CIRCLE NO. 345

IC tester draws battery power
Fut-heuristic Devices, Box 1117, Reseda, CA 91335. (213) 348-9188. $300; stock.

The Evaluator is a portable digital IC tester that measures 8 x 11 x 4-1/2 in. and weighs about 4 lb. The unit will test approximately 10,000 ICs on a fully charged set of NiCd batteries. An inexperienced operator can easily test 500 ICs per hour, including 100% testing of all TTL, DTL, CMOS and many other ICs. This includes the popular 7400 series, 74, 74L, 74H, 74S, 74LS, etc. It can test these ICs under load if desired.

CIRCLE NO. 346
6-digit DPM counts to 1 GHz

Amtex Research, P. O. Box 1714, Rockville, MD 20850. (301) 424-6112. $799; stock to 8 wks. LPM 1000 is said to be the smallest 1000-MHz frequency counter. The unit is a six-digit panel meter. Sensitivity is 50 mV rms. The logic panel meter is completely self-contained and includes a high-stability crystal oscillator, time base, counter, decoder and LED display in a 3 × 1.4 × 2.45-in. case. Weight is 3.5 oz. Other frequency versions are available at 10, 120 and 600 MHz. The LPM 1000 is fully programmable for time-base expansion, frequency multiplication or division, internally programmable three-decade offset and BCD outputs available.

CIRCLE NO. 347

Thermocouple meters come in 40 models

Omega Engineering Inc., Box 4047, Stamford, CT 06907. (203) 359-1660. $200 to $450; stock.

Over 40 different portable thermocouple readout meters having built-in, high-gain amplifiers are available in a choice of three accuracy categories. Class I meters come in both battery-powered portable units and 115-V-ac units with an accuracy of 1°C throughout the entire range of -120 to 1800°C in 12 to 18 steps. For greater accuracy, Class II units can measure temperatures below -100 up to 1800°C. Class III meters work to an accuracy of 0.1°C from levels as low as -200, up to 1300°C.

CIRCLE NO. 348

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DIPPED . . .

SPRAGUE TYPE 196D

Small size economical capacitors that utilize high-quality tantalum pellet construction. Conformal epoxy resin coating is highly resistant to moisture and mechanical damage. This capacitor has found wide usage in consumer and commercial electronic equipment. Operating temperature range, -55°C to +85°C. Available in all popular 10% decade values from 0.1µF to 330µF. Voltage range, 4 to 50VDC. Standard lead spacing, 0.125" and 0.250". For complete data, write for Engineering Bulletin 3545B.

MOLDED . . .

SPRAGUE TYPE 198D

Economically priced, molded-case Econoline™ capacitors. Standard lead spacing, 0.100", 0.200", and 0.250". Tough, flame-retardant, crack resistant case has flatted section and polarity indicator for easy-to-read marking and error-free insertion. Fixed external dimensions allow increased productivity during assembly of PC boards. Designed for severe vibration and shock environment, where lead support alone is not adequate. Operating temperature range, -55°C to +85°C. Capacitance values from 0.1 to 100µF. Voltage range, 4 to 50VDC. For complete data, write for Bulletin 3546.

INFORMATION RETRIEVAL NUMBER 298

Call your nearest Sprague district office or sales representative, or write for the bulletins mentioned above to Sprague Electric Company, 347 Marshall Street, North Adams, Mass. 01247.

INFORMATION RETRIEVAL NUMBER 299

THE BROAD-LINE PRODUCER OF ELECTRONIC PARTS

Electronic Design 26, December 20, 1974
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1. **IF YOU KNOW THE MANUFACTURER**, you will find his U.S. distributors included under his listing in the MANUFACTURERS DIRECTORY. Name, city, and phone numbers are provided.

2. **IF YOU KNOW THE DISTRIBUTOR'S NAME**, you can find his complete address, zip, and phone number in the alphabetic section of the DISTRIBUTORS DIRECTORY. In most cases annual sales volume or net worth, year established, and names of key officials are included.

3. **IF YOU WANT TO FIND OUT WHICH DISTRIBUTORS ARE LOCATED NEAR YOU**, check the geographical section of the DISTRIBUTORS DIRECTORY. You enter the section by state, then find your city — or one nearby — and the distributors located in that city. You can then go back to the alphabetic section to learn more about them.

Electronic Design's GOLD BOOK

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10µV resolution, $279
Model 6355 is a portable DMM having a 10µV (DC voltage) resolution. It is comparable to DMM's for laboratory use, priced at an economical $279, and sets a new standard of performance for portable DMM's.

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Operation is as simple as selecting the function and signal connection. The measured value is displayed through the automatic selection of 5 functional modes: range selection, unit display, polarity, overrange indication and overload protection.

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Request Bulletin PS-301
115 Marine St., Farmingdale, N.Y. 11735 • (516) CH 9-2336
IMC introduces fan for cooling sandwiched areas

IMC’s new, high performance FULMAR fan features maximum efficiency for cooling high power density enclosures and rows of printed circuit board arrays. Unique design of this fan allows for convenience of “Side by Side” mountings for maximum airflow distribution and stable motor performance under low voltage (brown out conditions). Fulmar’s low noise level is a natural for computer room use.

4-3/4" diameter by 5-29/32"

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INFORMATION RETRIEVAL NUMBER 95

DISCRETE SEMICONDUCTORS

Quad power transistors designed for CATV use

Communications Transistor, 301 Industrial Way, San Carlos, CA 94070, (415) 591-8921. $33.50 (1 to 99); stock.

The Quad 1 transistor array has four rf power transistors in one package. Quad 1 offers high gain over the 40-to-300-MHz CATV band. Other performance features include return loss input to output, more than 18 dB; cross-modulation +50 dBmV, 12 ch flat = -65 dB; second IM distortion, +50 dBmV, -80 dB (typical); and triple beat distortion, +50

CIRCLE NO. 351

LED lamps in four colors include limiting resistor

Xciton Corp., Shaker Park, 5 Hemlock St., Latham, NY 12110, (518) 783-7726. From $0.50 (1000 up); stock.

A series of resistor-LED lamps is available in three different plastic lens styles and in four colors—red, green, yellow and orange—rated for either 5 or 12-V-de operation. Each of the 24 LED lamps is in popular epoxy-molded, radial-lead cases. Each lamp is rated for luminous intensity at a forward current of 16 mA. Basic specifications for the resistor-LED styles are: XC209 lamps have viewing angles of 75°. Lamp lenses have diameters of 0.125 in. and heights of 0.21 in. Luminous intensity is 0.6 mcd minimum and 2 mcd typical. XC5053 lamps are wide angle indicators with viewing angles of 80°. Lamp lenses have diameters of 0.2 in. and heights of 0.34 in. Luminous intensity is 0.5 mcd minimum, and 1.5 mcd typical. XC22 lamps also have viewing angles of 80°, diameters of 0.2 in. and heights of 0.24 in. Luminous intensity is 0.5 mcd, minimum, and 1.5 mcd, typical.

CIRCLE NO. 352

INFORMATION RETRIEVAL NUMBER 95

ELECTRONIC DESIGN 26, December 20, 1974
LED panel lamps have large lens diameter

Data Display Products, 5428 W. 104 St., Los Angeles, CA 90045. (213) 641-1232. $1.45 (100-up); stock to 3 wk.

The 460 series LED displays use high-brightness LEDs to provide large (0.39 in.) diameter lighted areas. The lamps are available with green, yellow, amber or red LEDs, with lenses tinted clear or translucent in any of the four colors, or water clear. All lenses have an internal fresnel pattern for optimum light diffusion even in clear. The lens style is cylindrical with either standard projection or low-profile (1/16 in.) fresnel panel projection. Lamps mount in 0.25 in. diameter holes and can be positioned on 0.5 in. centers. They may be mounted directly in the panel with supplied hardware (neoprene washer and retaining clip) or they may be ordered as a cartridge type for front panel replaceability. All lights have wrapped-wire type gold-plated terminals, and are available with voltage ratings of 2 to 28 V at currents from 9 to 35 mA.

Darlington transistors handle up to 100 W

RCA, Route 202, Somerville, NJ 08876. (201) 722-3200, 1000-up prices: 1B07 ($1.30); 1B08 ($1.60); stock.

Two complementary npn and pnp Darlington transistors, types RCA-1B07 and RCA1B08, are designed for audio-amplifier applications. The transistors have a sustaining voltage (V_{CBO(max)}) of 80 or -80 V and a gain (h_{FE}) of 1000 to 15,000, with a dissipation rating (P_{T}) of 100 W. The RCA1B07 and RCA-1B08 are supplied in the JEDEC TO-3 hermetic package.
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application notes

Nitrogen lasers

"Nitrogen Laser Requirements for Successful Dye Laser Pumping" discusses nitrogen laser parameters. The note stresses the importance of pulse width, power and beam characteristics and compares spark gap vs thyatron switching of the laser. Molelectron, Sunnyvale, CA

CIRCLE NO. 355

FET input op amps

An 18-page note discusses the advantages of FET input stages over the bipolar transistor stage, pointing out that low input and offset current characteristics of matched FET pairs are three-to-five orders of magnitude lower than those of bipolar-driven op amps. Siliconix, Santa Clara, CA

CIRCLE NO. 356

Flat ribbon cable

A series of six "How To" data sheets illustrates the techniques of terminating bonded and laminated round-conductor flat ribbon cable. Spectra-Strip, Garden Grove, CA

CIRCLE NO. 357

Temperature measurement

An application note describes the use of highly matched transistor pairs to perform accurate temperature measurement without requiring expensive reference junctions or linearizing circuitry. Precision Monolithics, Santa Clara, CA

CIRCLE NO. 358

Thermoplastic resins

Design, fabrication and performance data of thermoplastic resins are covered in a 56-page manual. A fold-out section provides easy reference for formula symbols and notations. Detailed illustrations of techniques, design equations, application data and performance characteristics are included. General Electric Plastics Dept., Selkirk, NY

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Rogan, 3455 Woodhead Dr., Northbrook, IL 60062

PC card ejector set
A PC card ejector set, featuring self-lubricating nylon material, consists of two ejectors and mounting pins. Scanbe Manufacturing.

Mini temp recorders
Self-adhesive miniature three and four-increment temperature recorders indicate overheating of electronic circuit board components. The recorders are accurate to ±1% over the 37-to-260°C temperature range in increments of 5°C. When exposed to the rated critical temperature, the indicators turn in sequence from silver to black for a direct readout, which is both permanent and irreversible.
William Wahl, Temp-Plate Div.

Ferrite cores
A small kit offers power-circuit designers a simple way to discover the advantages of ferrite cores in a converter circuit. The kit includes a ferrite core and a diagram for a converter circuit that can be built in a few minutes. The circuit converts 12 V dc to 150 V dc at an efficiency of over 80%. Ferrox-cube.
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Capacitor chart

An 18-page Established Reliability Tantalum Capacitor Conversion Chart compares the electrical, acceptence inspection tests and marking requirements between MIL-C-39003D and MIL-C-39003C. Union Carbide.

CIRCLE NO. 363

Minicomputer template

A computer-programming aid is offered to users of the company’s D-116 and the Data General NOVA 1200 series minicomputers. The paper data lamp decoder template affixes to the front panel and provides the system programmer with an easily read interpretation of the computer’s data lamp instructions. Digital Computer Controls.

CIRCLE NO. 364

Calibration chart

A stability/calibration chart gives the calibration laboratory man the data needed to determine how often a local standard must be recalibrated. The oscillator drift rate or stability is used as the determining factor. True Time Instrument.

CIRCLE NO. 365

Aluminum standards

“Aluminum Standards & Data” is a basic reference to mechanical, physical and other properties of aluminum. The Aluminum Association.

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ELECTRONIC DESIGN 26, December 20, 1974

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General relays

Electromechanical, dry reed and mercury-wetted relays, time delay and interval timer relays, hybrid and solid-state relays, precision snap-action switches and custom control assemblies are shown in a catalog. The catalog contains electrical specifications, mechanical requirements and wiring diagrams for each model. Potter & Brumfield, Princeton, IN

CIRCLE NO. 367

Custom ICs

A 16-page publication describes the company's unique custom IC concept. The key to the concept are three standard bipolar chips that contain a large number of standardized IC components. Interdesign, Sunnyvale, CA

CIRCLE NO. 368

Laboratory products

Descriptions, applications information, prices and illustrations of equipment used in scientific, industrial and research laboratories are presented in a 32-page catalog. Science Essentials Operations, Anaheim, CA

CIRCLE NO. 369

Capacitors

A revised guide to MIL-style CSR09, CSR13 and CSR23 capacitors abstracts all important data from MIL-C-39003 established reliability “D” revision in an easy-to-use format. Sprague, North Adams, MA

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NEW LITERATURE

Film resistors

A four-color film resistor catalog showcases metal, cermet or carbon-film resistors. Easily understood descriptions of the standard packaging offered are included as well as a special section aimed at easing the job of ordering the components. Mepco/Electra, Morristown, NJ

CIRCLE NO. 371

Vinyl tapes

A guide to plating systems for PC board manufacturing lists and describes vinyl tapes for use during solder stripping and gold-plating procedures. It also describes polyeester and polyethylene protective tapes. A chart lists properties for each tape—total caliper, adhesion to steel, available colors and elongation. 3M, St. Paul, MN

CIRCLE NO. 372

Gas regulating equipment

"How to Safely Operate Gas Regulating Equipment" explains how to select, install and operate gas regulators for specialty gases, including flammable, oxidant, corrosive, inert, toxic and high pressure gases. Air Products and Chemicals, Specialty Gas Dept., Allentown, PA

CIRCLE NO. 373

Environmental equipment

A 40-page catalog illustrates and describes environmental simulation equipment designed to perform under the most rigorous government and commercial specifications. Technical configurations and drawings are included. Associated Environmental Systems, Lawrence, MA

CIRCLE NO. 374

3-D displays

Three-dimensional display system comprised of building-block modules is described in an eight-page catalog. The catalog graphically illustrates the various capabilities of the 3-D system. Specifications and prices are provided. Optical Electronics, Tucson, AZ

CIRCLE NO. 375

Microwave instruments

An 84-page illustrated catalog describes features and specifications of sweep oscillators and instruments for the measurement of microwave parameters. Details on over 80 instruments are given. Twenty-three pages contain applications, techniques and theory on microwave sweepers, attenuation measurements and rf power measurements. Weinschel Engineering, Gaithersburg, MD

CIRCLE NO. 376

Photoelectric scanners

Completely self-contained photoelectric sensors, two-part sensors and photoelectric system components are detailed in a 24-page catalog. Block diagrams and wiring diagrams for sensor units, timing diagrams for time-delay modules, schematic diagrams of output switching devices and dimensional drawings are included. Warner Electric Brake & Clutch, Beloit, WI

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Holographic laser systems

Pulsed holographic lasers operating at 0.532 µm are described in a two-color, four-page brochure. Included with the brochure is a data sheet entitled, “What’s Coherence Length,” which defines this often misunderstood parameter. Also presented is a discussion of how to measure coherence length. International Laser Systems, Orlando, FL

CIRCLE NO. 378

Plastics guide

An updated edition of “Standard Tests on Plastics” is illustrated with photos, drawings, tables and charts. The brochure describes test procedures in six categories: mechanical, thermal, optical, permanence, analytical and electrical. In each specific test, the specimen, procedure and significance are discussed. Celanese Plastics, Newark, NJ

CIRCLE NO. 379

Transistors, Darlinsgtons

Power transistors and Darlinsgtons using glass passivation techniques for improved performance are described in a series of nine data sheets. Each data sheet contains curves, specifications and ratings and applications information. Dimensional drawings and a photograph of each device are provided. International Rectifier, Semiconductor Div., El Segundo, CA

CIRCLE NO. 380

Printer/plotters

Statos electrostatic printer/plotters are covered in a 10-page catalog. The catalog shows maps, charts and graphs generated on Statos units. Varian Data Machines, Irvine, CA

CIRCLE NO. 381

CB radio accessories

CB and amateur radio replacement parts, accessories and “step-up” items are illustrated in a catalog. The eight-page catalog features such items as power base and mobile unit microphones, dual power SWR meters, noise filters and suppressors and microphone and antenna plugs and connectors. GC Electronics, Rockford, IL

CIRCLE NO. 382
The NEC V222 transistor is a low noise amplifier with a minimum gain of 8 dB at 4 GHz. The V222 is available with three noise figure selections at 4 GHz: 3.5 dB, 4.0 dB, and 4.5 dB. The package is the popular 100-mil square stripline. California Eastern Labs, Inc., One Edwards Court, Burlingame, Calif. (415) 342-7744.

The Proven Incandescent Readout Standard 16 Pin DIP Flat Pack. All units 5 Volt 100,000 hrs. plus 3015F-BM 08ma/seg 700 ft/lam 3015F-BM10 10ma/seg 1700 ft/lam 3015F-BM15 15ma/seg 4500 ft/lam Field tested over 4 years in many applications. READOUTS, INC. P.O. Box 149, Del Mar, Ca. 92014 Tel. 714-755-2641 Telex 69-7992.

Scott T Transformer. 11870: 60HZ, 90v, L-L in. 1.1x2.1x1.1. 50460: 400HZ, 90v, L-L in. 7.8x1.5x1.8 x11/16. 50642: 400HZ, 11.8v, L-L in. 7.8x1.5x1.11/16. 10472: 400HZ, 11.8v, L-L in. 3.4x1.1/2x3/8. All with 6v RMS sine & cosine output. MAGNETICO, INC., 182 Morris Ave, Holtsville, N.Y. 11742 516-654-1166.

Introduction To Defense Radar Systems Engineering. Excellent introduction and practical reference to radar systems design and applications. #9194, 260 pp., $20.00. Circle the Info Retrieval No. to order 15-day exam copy. When billed, remit or return book with no obligation. Hayden Book Co. 50 Essex St. Rochelle Park, N.J. 07662

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UV Blue Response Photodiode: United Detector Technology now offers blue, super blue, and UV enhanced silicon photodiodes with near theoretical responsivity in the range from 200 to 550 nanometers. Available in both the Pin-5 .5 cm² and the Pin-10 1 cm² configuration. United Detector Technology, 2644 30th St., Santa Monica, Ca. 213 396-3175.

INFORMATION RETRIEVAL NUMBER 619

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INFORMATION RETRIEVAL NUMBER 622


INFORMATION RETRIEVAL NUMBER 617

THE LOGIC NEWSLETTER—Free sample copy of low cost publication that emphasizes logic, Minicomputers, Microcomputers and microprocessors. A special offer is included for all of those who failed to keep-up with microprocessors in 1974. THE LOGIC PRESS, 260 GODWIN AVENUE, WYCKOFF, N. J. 07481.

INFORMATION RETRIEVAL NUMBER 620

PDP-11 General Purpose Interface. The MDC-11C provides all features of a DEC DR11C plus additional 16 bit register, 4 selectable interrupt control levels, 16 decoded device addresses, takes only one quad slot has maximum Unibus load of 1. Also, 20 wirewrap positions are provided. $390. MDB Systems, Inc., 981 N. Main Street, Orange, CA 92667.

INFORMATION RETRIEVAL NUMBER 621

Solid-State Voice Systems for audio readout of numbers and words. Whole-words are stored in ROMs with natural sounding voice reproduction. Standard models offer 10 numeric words (0 - 9). Master Specialties, 1640 Monrovia, Costa Mesa, Calif. 92627. (714) 642-2427.

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Design Data from

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NOISE/VIBRATION MEASUREMENTS

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Demo, circle 170
Lit., circle 171

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CIRCLE NO. 173

PRINCETON APPLIED RESEARCH CORPORATION
P.O. Box 2565
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New Kepco Power Supply Catalog and Handbook

Kepco, Inc. has published a new 1974 Power Supply Catalog and Handbook. In 130 pages, there are schematics and mechanical drawings of more than 30 power supply designs, encompassing several hundred separate models. The Kepco Catalog and Handbook includes applications material on high speed-fast programming models, digital control systems, measurements and power supply combinations. A comprehensive glossary is also included.

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by Fennimore N. Bradley

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**MODEL S14R-1**

**FREQUENCY TOLERANCE:** ±0.1% from -25°C to +75°C

**FREQUENCY RANGE:** Available 4 MHz to 20 MHz

**OUTPUT WAVEFORM:** TTL

Logic 0=0.4V
Logic 1=2.4V

Risetime and Falltime ≤50 ns

Duty Cycle 30/70 or better

Fanout of 10

**SUPPLY CURRENT:** 1 ma to 5 ma

**TERMINATION:** 14 pin DIP socket

pin diameter .02"

**SUPPLY VOLTAGE:** 5Vdc ±20%

**DIMENSIONS:**

0.3" H x 0.5" W x 0.8" L

* SMALL SIZE
* LOW COST
* HIGH FREQUENCY

CONNOR-WINFIELD CORP

West Chicago, Illinois 60185
Phone: (312) 231-5270

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HIGH Q CHIP CAPACITORS

High Q multilayer capacitors feature very high quality factors at microwave frequencies. Superior dielectric properties and structure permit operation at high voltage and high current at microwave frequencies through the full temperature range with minimum dielectric loss. Offered in 4 standard sizes from .040" x .030" to .125" x .095". Applications include UHF-microwave hybrids and MIC's.

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HEAT PIPE
‘Break-through’ by astrodyne

Major fabrication “break-through” by astrodyne makes HEAT PIPES available at prices that permit serious consideration of these remarkable heat transfer devices. HEAT PIPES are ideally suited to transfer heat from ‘black boxes’, compact assemblies and similar restricted areas to remote heat sinks.

astrodyne has the capability and “know-how” to fabricate complete transfer systems — from heat source to heat sink — to meet your application.

Demonstration kits, available from Astrodyne at $8.00, compare the fast heat transfer of HEAT PIPES with a solid copper conductor.

Contact your Astodyne representative for further information or assistance with your application.

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(617) 272-3850 TWX 710-347-0704

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grabber

SIMPLIFIED ASSEMBLY
Rapid assembly or replacement of damaged lead.

MODEL 3925
hooks onto components or slips over square Wire-Wrap pins

Model 3925
Mini Test Clip
Shown Actual Size

This test clip with gold plated hook is excellent for rapid testing of components and Wire Wrap pins. Clip is completely insulated to point of connection. Build any combination of test leads with wire up to .090 dia. Easy and comfortable to operate. Molded of rugged Lexan to resist melting when soldering. Write for literature and prices.

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A Division of ITT
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INFORMATION RETRIEVAL NUMBER 108
Electronic Design 26, December 20, 1974

INFORMATION RETRIEVAL NUMBER 109

*Lexan is a General Electric trade-mark. tRegistered trade-mark of Gardner-Denver Co.
THE ONLY 4PDT, 5 A RELAY IN ITS CLASS OK'D BY UL, CSA, & VDE.

You can go only to Arrow-M for a 4PDT relay of this small size: 1.079"L x 0.827"W x 1.280"H with a 5 A, 240 VAC resistive rating approved by UL, CSA, and VDE for unqualified industrial use. Check these great design features: arc barriers, debris wells, one-piece molded contact blocks, gold-flashed AgCdO contacts, and hermetic sealing in plastic. They make for the quality and long-lived reliability that approval demands (10⁶ mechanical operations). This HC relay series also contains DPDT (7 A, 240 VAC) and SPDT (10 A, 240 VAC) versions. All approved. Send for your full specs.

Relays for advanced technology.

Arrow-M Corp. 250 Sheffield St., Mountainside, N.J. 07092 U.S.A. Telephone: 201-232-4260


Hoffman ELECTRICAL ENCLOSURES

Hoffman Engineering Company
Division of Federal Cartridge Corporation
Anoka, Minnesota, Dept. 8056

INFORMATION RETRIEVAL NUMBER 112

Here's a low cost load cell that's not afraid of water

In the past, low cost load cells could only be used in closely controlled environments. That meant no water splashes, no steam, and no condensation. Times have changed. With the new Sealed Super-Mini Load Cell from Interface, you don't have to worry about outdoor environmental conditions, and you don't have to worry about a high price either.

The rugged Sealed Super-Mini is designed to replace all those costly load cells you've been using and provide you with guaranteed performance of ±0.05% non-linearity, ±0.03% hysteresis, ±0.01% non-repeatability, ±0.03% creep, and a list price of just $295. Standard ranges are 0 to ±500, and 0 to ±1000 pounds and they can be provided with either a rugged electrical connector or an integral cable.

For complete information on these load cells and others in ranges from 5 pounds to 100 tons, call or write Ted Johnson at Interface, today.

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Telephone (602) 948-5555

INFORMATION RETRIEVAL NUMBER 113

Electronic Design 26, December 20, 1974

INFORMATION RETRIEVAL NUMBER 110

INFORMATION RETRIEVAL NUMBER 111

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Electronic Design 26, December 20, 1974

INFORMATION RETRIEVAL NUMBER 110

INFORMATION RETRIEVAL NUMBER 111
Magnecraft's BIG TIMERS come in all shapes, sizes, and timing ranges for your applications. Time delay relays with slow operate or slow release and time repeat accuracy ±1%. Each relay is designed to function with absolute reliability, for long life at lowest cost. Versions offered include: solid state hybrid, copper slug, thermal, air dashpot, telephone type, mercury displacement, and solid state-static output. The photo portrays just some of the endless features, mountings and packaging characteristics available with Magnecraft built-in quality and integrity.

Over 100 different stock time delay relays are available through our nationwide network of distributors. But, if you don't find what you need in stock we will custom build it for you!

Free!
TIME DELAY RELAY CATALOG

To help specify your time delay relay needs, ask for Magnecraft's Seventh Edition of the Time Delay Relay Catalog. It offers suggestions on how to specify, testing procedures, comparisons of the types available, principles of operation and a glossary of terms. This super, 52 page catalog is yours for the asking.

Find Magnecraft Relays in EEM sec. 4500 and the Gold Book sec. 1600.
We've put together an assortment of 20 different devices that cover most of the things you want to do with op amps. With this package at your elbow you will be able to reduce your idea-to-breadboard time from days, or even weeks, to minutes.

Here are some of the reasons we think it will be useful to you:

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Second, you will have a number of RCA versions of industry standard types that will let you evaluate and compare them with what you are now using.

Third, you can get first-hand experience with some of the new devices that could soon become industry standards — they’re the types we’ve developed over the past 12 months to help you design for improved performance and lower cost.

In addition to general-purpose, precision and high current types you will get wideband and operational transconductance amplifiers, as well as RCA micropower programmable op amps.

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For specific information about the Op Amp Selector, contact your local RCA Solid State distributor or write RCA Solid State, Box 3200, Somerville, N.J. 08876. Phone (201) 722-3200, Ext. 3142.