Millions of R-C-L discrete still fill new circuits in spite of ICs. And older types serve side by side with the latest chips. But, old or new, they all suffer from the basic problems: Time and stress still take their toll of life and tolerance. And specs still don’t tell all. For a complete update on discretes, see p. 56.
Do you face a make or buy decision on power supplies? **BUY LAMBDAA'S LZ SERIES THE ONLY FIELD REPAIRABLE P-C MOUNTABLE POWER SUPPLY.**

Available in 3 package sizes, in 26 single output and 19 dual output models from $35, up to 28 volts, up to 1400 mA.

**COMPETITOR COMPARISON CHART**

<table>
<thead>
<tr>
<th>Lambda Pak</th>
<th>Competitors' Model</th>
</tr>
</thead>
<tbody>
<tr>
<td>YES</td>
<td>NO</td>
</tr>
<tr>
<td>YES</td>
<td>NO</td>
</tr>
<tr>
<td>YES</td>
<td>NO</td>
</tr>
<tr>
<td>YES</td>
<td>NO</td>
</tr>
</tbody>
</table>

- Fully repairable
- Continuously adjustable voltage
- Multivoltage rated
- Foldback current limiting

<table>
<thead>
<tr>
<th>Lambda Pak</th>
<th>Competitors' Model</th>
</tr>
</thead>
<tbody>
<tr>
<td>YES</td>
<td>NO</td>
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</tbody>
</table>

- Wide input voltage range—105-132 Vac
- Short-circuit proof
- Vacuum-impregnated transformer
- Three different power packages

<table>
<thead>
<tr>
<th>Lambda Pak</th>
<th>Competitors' Model</th>
</tr>
</thead>
<tbody>
<tr>
<td>YES</td>
<td>NO</td>
</tr>
</tbody>
</table>

- Single and dual (tracking) outputs
- Designed for series operation
- Stocked and distributed from Los Angeles, Montreal, Chicago and New York

**LZ SERIES SINGLE OUTPUT MODELS**

<table>
<thead>
<tr>
<th>MODEL</th>
<th>VOLTAGE VDC</th>
<th>CURRENT mA</th>
<th>PRICE</th>
</tr>
</thead>
<tbody>
<tr>
<td>LZS-10</td>
<td>5</td>
<td>450</td>
<td>$35</td>
</tr>
<tr>
<td>LZS-11</td>
<td>12</td>
<td>195</td>
<td>35</td>
</tr>
<tr>
<td>LZS-20</td>
<td>15</td>
<td>300</td>
<td>55</td>
</tr>
<tr>
<td>LZS-30</td>
<td>5</td>
<td>900</td>
<td>65</td>
</tr>
<tr>
<td>LZS-33</td>
<td>15</td>
<td>400</td>
<td>65</td>
</tr>
<tr>
<td>NEW LZS-34</td>
<td>5</td>
<td>1400</td>
<td>95</td>
</tr>
</tbody>
</table>

**LZ SERIES DUAL TRACKING OUTPUT MODELS**

<table>
<thead>
<tr>
<th>MODEL</th>
<th>VOLTAGE VDC</th>
<th>CURRENT mA</th>
<th>PRICE</th>
</tr>
</thead>
<tbody>
<tr>
<td>NEW LZD-12</td>
<td>±15V</td>
<td>50</td>
<td>$35</td>
</tr>
<tr>
<td>LZD-21</td>
<td>±5</td>
<td>300</td>
<td>55</td>
</tr>
<tr>
<td>LZD-22</td>
<td>±15</td>
<td>90</td>
<td>40</td>
</tr>
<tr>
<td>LZD-23</td>
<td>±15</td>
<td>150</td>
<td>55</td>
</tr>
<tr>
<td>LZD-31</td>
<td>±5</td>
<td>300</td>
<td>65</td>
</tr>
<tr>
<td>LZD-32</td>
<td>±15</td>
<td>220</td>
<td>65</td>
</tr>
<tr>
<td>NEW LZD-35</td>
<td>±15</td>
<td>300</td>
<td>95</td>
</tr>
</tbody>
</table>

For additional voltages, send for Lambda's 1973 catalog supplement L-3.

**LZ SERIES AVAILABLE IN 3 NEW MODELS**

- **LZD-12** ±15V, 50mA
  - **$35**

- **LZS-34** 5V, 1400mA
  - **$95**

- **LZD-35** ±15V, 300mA
  - **$95**

**Regulation** 0.15%—line or load; models LZS-10, LZS-30, LZS-34, LZD-21 and LZD-31 have load regulation of 0.15% + 5mV; model LZD-12 has line or load regulation of 0.25%.

**Ripple and noise** 1.5mV RMS.

**Temp. Coefficient** 0.03%/°C

**Tracking accuracy** 2% absolute voltage difference (dual output models only) 0.2% change for all conditions of line, load and temperature

**AC input** 105 to 132 Vac, 57-63 Hz

**INFORMATION RETRIEVAL NUMBER 246**

1-DAY DELIVERY 60-DAY GUARANTEE
We have the broadest chorus line of Phase Lock Loop circuits available today. Take a brief look at our ever-expanding PLL line:

The XR-210 is designed for FSK Modulation and Demodulation and features a self-contained output logic driver, compatible with RS-232C requirements.

Use the XR-215 for FM or FSK demodulation, frequency synthesis and filter tracking. It has a 5V to 26V supply range and 0.5 Hz to 35 MHz frequency bandwidth. What's more, it's bipolar logic compatible.

The XR-567 is a do-it-yourself building block. With this you design your own PLL circuits by selecting external connections and components. You get instant prototypes with minimum fuss and costs.

Moving right along... the XR-567 PLL is designed for tone and frequency decoding. It has a bandwidth adjustable from 0 to 14%, sinks up to 100 mA of load current and has a logic compatible output. Our dual version, the XR-2567, is a real hummer with even better temperature tracking and matching characteristics. Power supply rejection is improved by an order of magnitude over the single version. The dual outputs can switch up to 100 mA at 26 volts.

All together now. We would like to send you the complete musical score on our PLL products. Our data sheets are good and they're filled with applications data. Write now, write.
All 191 flavors of RESNET™ DIPs offer system compatibility because we use the same packages you use for I.C.s; plus you get ceramic dependability at plastic prices.

Whether you're inserting resistors automatically or by hand—call your local Beckman/Helipot representative and ask how you can save money using RESNET DIPs. He stocks locally for immediate delivery.

To request technical data, call your local Beckman/Helipot representative. Or write to Beckman Instruments, Inc., Helipot Division, 2500 Harbor Blvd., Fullerton, Calif. 92634.

<table>
<thead>
<tr>
<th>Flavors</th>
<th>Price (1,000-4,999)</th>
</tr>
</thead>
<tbody>
<tr>
<td>898-1 (15 resistors)</td>
<td>$0.85</td>
</tr>
<tr>
<td>898-3 (8 resistors)</td>
<td>$0.76</td>
</tr>
</tbody>
</table>

**STANDARD RESISTANCE VALUES**

(±2% or ±2Ω)

*Standard in 898-3 only.
†Standard in 898-1 only.

<table>
<thead>
<tr>
<th>Value</th>
<th>Price (1,000-4,999)</th>
</tr>
</thead>
<tbody>
<tr>
<td>22</td>
<td>62 180 510 1.5K 4.3K 11K</td>
</tr>
<tr>
<td>24</td>
<td>68 200 560 1.6K 4.7K 12K</td>
</tr>
<tr>
<td>27</td>
<td>75 220 620 1.8K 5.1K 13K</td>
</tr>
<tr>
<td>30</td>
<td>82 240 680 2.0K 5.6K 15K</td>
</tr>
<tr>
<td>33</td>
<td>91 270 750 2.2K 6.0K 16K</td>
</tr>
<tr>
<td>36</td>
<td>100 300 820 2.4K 6.2K 18K</td>
</tr>
<tr>
<td>39</td>
<td>110 330 910 2.7K 6.8K 20K</td>
</tr>
<tr>
<td>43</td>
<td>120 360 1.0K 3.0K 7.5K 23K</td>
</tr>
<tr>
<td>47</td>
<td>130 390 1.1K 3.3K 8.2K</td>
</tr>
<tr>
<td>51</td>
<td>150 430 1.2K 3.6K 9.1K</td>
</tr>
<tr>
<td>56</td>
<td>160 470 1.3K 3.9K 10K</td>
</tr>
</tbody>
</table>

**899-5-R220/330**

Pulse squaring TTL terminator.

Price (1,000-4,999) $1.45

**899-19**

DIP interface network providing resistors for µA711 core sense amplifier configuration.

Price (1,000-4,999) $1.18

**899-40**

DIP network provides six line terminators and the threshold setting divider for the Intel 3208A sense amplifier.

Price (1,000-4,999) $1.35
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38 A bubble memory-logic chip? IBM heads toward that goal.
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43 Ceramic image-storing device can project data by reflection.
45 Washington Report
49 Technology Abroad

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70 Be on guard when using DVMs. Noise can lead to erroneous readings. Combat it with the proper rejection technique and correct hook-up of the voltmeter.
76 Build stable frequency synthesizers by using off-the-shelf ICs in a phase-locked-loop configuration with variable-modulus control.
84 Unconventional uses for IC timers can be found everywhere. Build anything from car tachometers to program controllers with these simple devices.
92 Program gives FET model from specs. With only one simulation routine written for SCEPTRE, curves can be obtained for all characteristic regions.
100 Consider the part-time engineer, says this small-company manager. You can use him effectively if you learn to use technicians as project 'finishers.'
104 Ideas for Design: Optical isolators provide diverse functions in signal-detector circuit . . . Use a 723 as a switching regulator and get half an amp from a plastic TO-5 transistor . . . Low-temperature-coefficient current source becomes ultra-compliant with two resistors.
110 Design Decision: No-contact dc transformer measures high bus currents.

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Cover: Electric components for color TV sets are being placed into proper sequence for automatic insertion into Dura-Module carrier panels. Photo provided by the courtesy of Zenith Radio Corp.
Enough #10 wire to reach the moon will total about 1 megohm. The GR 1666 DC Resistance Bridge will measure that to within ±0.01%, or the equivalent of ±25 miles. Better yet, if a piece as short as 440 yards is removed from the translunar span, the 1666 bridge will resolve the 1-ohm difference.

Most striking about the 1666 bridge is its wide measurement range. It will measure a piece of the same size wire long enough to reach from here to Neptune, 2.7 billion miles (10 gigohms), or a 1½-inch piece (100 microhms), both within ±2% accuracy. And that feat doesn't really tax the 1666; it has enough resolution and detector sensitivity to distinguish between 0 and 2 microhms and between 00 and 500 gigohms (measured as 2 picohms conductance).

Here, for $950, is a bridge that will measure contact resistance and dielectric leakage, transformer windings and insulation, diode forward and back resistance, relays open and closed... and all with precision.

The 1666 has a fast-responding detector. The 1666 is self-contained. The 1666 has guard and Kelvin connections. The 1666 is essential if you measure resistance.

From General Radio, Concord, Mass. and, in Europe, Postfach, CH 8034 Zurich, Switzerland.
**Instant capacitors**

Complete warehousing in the U.S. providing capacitors for the home entertainment, computer and industrial electronic industries.

**PRODUCTION ITEMS**
- Electrolytic Capacitors
- Ceramic Capacitors
- Film Capacitors
- Oil Filled Capacitors
- without P.C.B.
- Metallized Paper Capacitors
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- Mica Capacitors
- Hybrid IC's
- P.T.C. Thermister
- Trim Pot

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  - Midwest Electronic Sales
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  - H. C. Johnson Agency
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  - Midwest Electronic Sales
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**PENNYSYLVANIA**
- Hall-Mark Electronics
  - (215) 339-7300

**TEXAS**
- Hall-Mark Electronics
  - (214) 231-5101
Did you know that each and every Power/Mate power supply gets 42 separate inspections? A "no" in any one means that your power supply doesn't go out the door.

That's the insistence and emphasis that the new Power/Mate puts on quality. Sure, it costs us more, but that's how Power/Mate makes friends... and why Power/Mate is the world's largest producer of quality power supplies.

Send for the Power/Mate catalog... 32,500 models... most available for same-day shipment.
Turned off by Janice

Janice, the sullen, sultry girl in the Jermy Industries ad, appears to have caused at least one reader to pout, too. He sent the following letter to Jermy:

I take personal offense to your ad in ELECTRONIC DESIGN March 15. Do you have a good quality product to sell, or are you just trying to put down women? An ad such as yours can only give one the impression women are only sex objects.

Never mind sending the catalog. Just tell me how much you paid to "Janice" to prostitute her body for your commercial gain.

Sincerely yours,
H.J.M

(Names withheld)

Jermy's ad agency, Evenett & Desoutter in London, sent H.J.M. the following reply:

Thank you for your letter. Artists, sculptors, illustrators throughout the ages have admired the female form. Who are you and I to change all that?

Yours sincerely,
John D. Evenett
P.S. Janice is well paid.

Janice herself was puzzled by it all. Shown the letter by H.J.M., she jotted down this comment:

—John—We certainly get some strange ones. This I feel is quite unanswerable!

The bare facts urged on encapsulants

Re: Your paragraphs on encapsulants and potting compounds in "Focus on Materials," ED No. 8, April 12, 1973:

You, above all others, should be aware that taking it off is sometimes more important than putting it on. A word or two about the Access process for stripping encapsulants wouldn't have hurt—especially for those readers who are vitally interested in getting right down to the bare facts.

Phoebe Williams, Advertising and Sales Promotion Manager
Amphenol Sams Div.
9201 Independence Ave.
Chatsworth, Calif. 91311

Correction

In the article, "Increase Photo-transistor Bandwidth Without Sacrificing Output Voltage," (ED No. 8, April 12, 1973, pp. 102-104) the following two corrections should be made: The value of $R_t$ in the last equation (p. 102) should be 47 k, not 47 k. The value of $R_L$ in curve d, shown in Fig. 2, p. 103, should be 470 Ω instead of 470 k.

Reader feels burned by regulator advice

I have been reading and enjoying ELECTRONIC DESIGN magazine for about seven years and have found it a useful source of information. It is written at an understandable level and generally avoids the "chest-thumping" articles praising a particular manufacturer's product and written by his own engineers.

But I feel that the article in ED No. 5 by Hnatek and Goldstein ("Don't Get Burned!") March 1, 1973, pp. 72-75) is an example of the type of problems mentioned in your excellent editorial in the same issue. The article's third paragraph gets right to the heart of my complaint: If I, as a user, am to be able to use the regulator in contin-

(continued on page 13)
The NAKED MINI/LSI™
What this country needs is a good $1,000 full-scale computer.

Introducing the computer for everybody. NAKED MINI/LSI™

It's the computer for people who never thought they could afford a computer for their product.

It's also for people who have always been able to afford more, but have always gotten less computer than this.

NAKED MINI/LSI is the first OEM computer designed for widespread, multi-level use. The first computer able to do more jobs than any computer could ever do before.

Jobs that computers were too expensive to do. Jobs that were, consequently, always left to old-fashioned hardwired circuitry. Which meant that products weren't as flexible or immune to obsolescence as they could have been.

Or jobs that were done by more expensive computers. Which meant that products cost more and were less competitive than they should have been.

To make a computer capable of handling this kind of range, we had to give it an unheard of combination: extensive 16-bit computing power and a small price tag. Specifically, NAKED MINI/LSI is the first computer powered to satisfy 90% of all potential minicomputer applications — and yet be priced as low as $990 in OEM quantities of 200.

Imagine it. For a price less than most hardwired circuitry, your product can benefit from a computer having arithmetic capabilities, full byte and 16-bit word processing, and extremely flexible input/output. Without going into all the jazzy widget features, let's just say that the NAKED MINI/LSI gives your product all the intelligence it needs to monitor, sequence, and control effectively.

At this point, you may be wondering why a computer with all this clout was ever named the NAKED MINI/LSI. Actually, the name is very appropriate.

The NAKED MINI means that we designed it without all the over-design found on other minicomputers. All the extra, redundant features that make other minis too unwieldy and costly for OEM use have been purposely left off. (But everything you need has been deliberately built in.)

The LSI stands for large-scale integration, the latest technological advance in electronics. It enabled us to build a complete computer that fits on a single 1" x 15" x 17" card, weighs only 4 lbs., and uses 89% fewer components for unequalled reliability.

All Panel Meters are not created equal.

We try to build an edge into General Electric panel meters. For instance, you won't see a GE panel meter turn yellow, because we use a special white paint that stays white. You won't get eyestrain either. GE panel meters come with extra-wide scales, big numerals, tapered pointers, and shadow-free cover plates for quick, sure readings. We're fussy about things like that.

Once you've installed them, forget 'em. GE's famous reliability just doesn't happen, we build it in! We designed-out a lot of extra parts that might fail, just to give you extra instrument reliability. To make sure, we added a 20% overload capability to our voltmeters and ammeters. Still not satisfied, we decided to measure instrument quality from parts to finished product in order to screen out anything marginal. Now, it's just too tough for a lemon to squeeze through.

GE panel meters come from a good family. They look good individually and they look good together. Choose the rounded BIG LOOK® design for unique style and wide-eyed readability. Or choose the clean HORIZON LINE® case for its behind-panel mounting flexibility (without the usual bezel), and its snap-off mask available in six colors. GE makes panel meters to suit you and to add snap to your application.

You can count on General Electric panel meters. They're built to help you do a better job. At GE, we're not interested in product equality. We want ours to be better than the rest.

For a complete catalog of competitively priced and readily available GE panel meters, see your nearby authorized GE distributor. Or write to General Electric Company, Section 592-43, One River Road, Schenectady, N. Y. 12345.

Specify General Electric... just for good measure.
Within seconds after the match flame was applied to both the epoxy (left) and the silicone ICs (right), the epoxy burst into flame.

The hot issue in electronics today is flame retardancy. While epoxies and other plastics support combustion, silicone-packaged devices are virtually nonflammable. So, they don't need flame-retardant additives that alter the electrical and mechanical properties of epoxies and other materials.

And there are several other good reasons to specify silicone packaging compounds:

- excellent performance under thermal cycling
- low thermal expansion minimizes damage to components and lead wires
- basic electrical, physical, and chemical properties that remain constant over the widest temperature (−55 to 250°C), time, and frequency ranges
- uniform, lifetime electrical characteristics
- superior performance in 85°C/85% RH (biased) test
- total compatibility with all kinds of devices, including ICs, both digital and linear, MOS, CMOS, power transistors, SCRs, high-voltage rectifiers, etc.
- optimum reliability reduces manufacturing and repair/warranty costs
- safe, clean, inert, and require no special handling

Whether you are a device manufacturer or user, these advantages are important in semiconductor devices. Make the switch to nonburning silicone packaging compounds now. Write or call Jack Broser, Product Market Supervisor, Dow Corning Corporation, Department A-3312, Midland, Michigan 48640.

Silicones: simply the best way to protect electronic circuits
Six good reasons why Dow Corning should be your primary packaging-materials supplier.

In addition to the many important advantages of silicone molding compounds, there are other good reasons why it is to your advantage to plan your growth in the electronics market with help from Dow Corning.

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2. Since service is extremely important in helping manufacturers in the development of advanced packaging systems, we have Technical Service & Development men strategically located worldwide to help solve your problems.

3. Your competitive advantage with Dow Corning molding compounds is a complete family of products, totally compatible with each other and with most other materials used in electronic systems, devices, or components.

4. Product-line breadth gives you the ability to design or produce the most reliable and economical packaging to protect any system, regardless of its sophistication or environment.

5. Technical leadership constantly applied in our own laboratories and with our customers results in the development of product modifications and new technologies to handle the needs and requirements of next generation devices.

6. Worldwide delivery from strategically located distribution points enables us to work with you to supply standard or special molding materials as required.

Major commitments like these indicate the kinds of things we are doing to earn your business. We'd like to discuss with you in more detail how we can grow together in this rapidly expanding area. Call or write Jack Broser, Product Market Supervisor, Dow Corning Corporation, Department A-3313, Midland, Michigan 48640.

Phone: (517) 636-9460

Silicones; simply the best way to protect electronic circuits.

DOW CORNING

Information Retrieval Number 11

Electronic Design 12, June 7, 1973

Better idea suggested for counter design

I want to congratulate you on the sense of humor that caused you to print the design idea "Shift Option Improves Handling of Binary Counter Data," by Akavia Kaniel, in the April 1 issue (ED No. 7, p. 84). In case some of your readers missed the subtle joke, here is the proper, modern solution to this design problem:

(continued on page 17)
The AY-5-4007A Four-Digit Display Driver is an LSI subsystem designed for application in counting display systems such as frequency counters, digital voltmeters, digital timers, and event counters using 7 segment numeric displays. It contains a 4 decade up/down synchronous BCD counter, a storage register, multiplexing circuits, internal oscillator for digit selection and 7 segment decoder to count and display to 9,999.

The AY-5-4007A is constructed on a single monolithic chip and is packaged in a 40 lead DIP.

Features
- Minimum interface required to drive most common types of LED, fluorescent, in-candescent seven segment displays
- Large output current capability on seven segment outputs, typically 25 mA at 1V
- Fully synchronous up/down counting operation
- Internal oscillator for operating the digit select counter
- Four-digit select line outputs with inversion control for display driving flexibility
- Serial output of BCD storage register
- TTL/DTL compatible on inputs and outputs
- Economy version available in a 24 lead DIP

The AY-5-4007A FOUR-DIGIT DISPLAY DRIVERS is available through these authorized General Instrument distributors.

For the past 3 years he's been in product marketing with General Instrument and now he's your "Display Man" at GI. Call him any time at the toll-free number below (In New York State call 516-733-3107).

800-645-9247

GENERAL INSTRUMENT CORPORATION • 600 WEST JOHN STREET, HICKSVILLE, L. I., NEW YORK 11802

The AY-5-4007A FOUR-DIGIT DISPLAY DRIVER is available through these authorized General Instrument distributors.
COMPARE THE PHILIPS PM 3400
with any other sampling scope
on the market—
FOR SIMPLICITY, STABILITY, SENSITIVITY

SIMPLICITY is the keynote. The PM3400 is a general purpose, 1.7 GHz, compact instrument that you operate just as you would any ordinary scope, except that you select a sampling mode and you adjust the sampling rate—both with a single control.

The display of the PM3400 looks just like the display of a conventional scope, too; no flicker at all; not even at low frequencies.

It's this low-frequency capability (real time sampling from DC to 10 KHz) that makes the PM3400 a truly universal scope for any application between DC and 1.7 GHz.

STABILITY of the PM3400 is so high that once set up, it stays exactly where you set it—even if you have to shut down and then re-start an hour later. This saves significant time and energy, especially on a production line. And remember—the PM3400 is the sampling scope that's simple enough for anybody to use in a production test environment.

SENSITIVITY is 400 µV/cm over the entire frequency range. Whether you're working with devices having f in the GHz range... or working on AF-modulated UHF signals... or looking for low-level signals in the presence of noise, the remarkable triggering abilities of the PM3400 combine with its high sensitivity and special filtering circuits for significantly clearer, steadier displays.

HIGH SENSITIVITY; GREAT DYNAMIC RANGE
Left, typical double pulses with rise time of 4 nsec; right, peak of one pulse magnified 100X vertically and horizontally, showing fine detail. PM3400 positioning control has range of ±1.6 V at any sensitivity. Note clarity of display achieved by special filtering circuits; total noise is less than 0.8 mV.

ACCURATE INTERNAL TRIGGERING TO 1.75 GHz
Accuracy of PM3400 internal triggering circuits is dramatically demonstrated here. Photo shows AF-modulated 2 GHz carrier along with its 1 KHz modulating waveform. This display is only feasible on a sequential sampling instrument such as the PM3400.

X-Y DISPLAYS AT 100 MHz with <1° PHASE ERROR
Photo shows two displays superimposed. Top traces are the same 100 MHz sine wave applied to both channels with mode selector set to "A and B." Bottom line is obtained when mode selector is switched to "A VERT, B HORIZ." (X-Y display) with same 100 MHz sine wave on both channels. Note accuracy and linearity of display; calculated phase error of less than 1° is not visible in display.

SUMMARY OF IMPORTANT FEATURES:
- Dual trace sampling from DC to 1.7 GHz
- 200X dynamic range
- Input sensitivity 400 µV/cm
- Automatic internal triggering to 1.75 GHz at 3 mV
- Continuously variable sampling rate, 5 to >1000/cm; up to 10,000 samples in any display
- 8 nsec visible delay; you see leading edges, even at high scan rates
- Real-time sampling, DC to 10 KHz, including single-shot phenomena
- Compact; weighs only 40 lb.
- Economical; only $2890, complete...
- no plug-ins or extras to buy

The best way to learn about the versatile and economical PM3400 is to see it in operation. For a demonstration or for full technical details, contact: Test & Measuring Instruments Inc., 224 Duffy Avenue, Hicksville, New York 11802. Telephone: 516-433-8800.
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Bourns LOW-COST FAMILY of industrial TRIMPOT® potentiometers was designed specifically to give cost-conscious industrial electronics equipment manufacturers superior product quality and performance... AT LOWER PRICES.

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INFORMATION RETRIEVAL NUMBER 14

AVAILABLE FOR IMMEDIATE DELIVERY FROM YOUR LOCAL BOURNS DISTRIBUTOR
For over four years we have been selling a monolithic MSI circuit called 9316 that contains all the functions performed by the seven integrated circuits in Mr. Kaniel's design. The 9316 runs faster (> 30 MHz), dissipates less power, occupies less space and costs less than the SSI design. It has been so successful that even our competitors have copied it, calling it the 74161.

Today gates and flip-flops have become the most expensive form of logic. They should be used sparingly only as "glue" between MSI packages. Any digital design that uses more gate and flip-flop packages from MSI packages is inefficient and would benefit from a more imaginative use of MSI.

Peter Alfke
Manager, Digital Applications
Fairchild Semiconductor
464 Ellis St.
Mountain View, Calif. 94040

The tri-flop strikes reader as old hat

The author of the tri-flop article "And Now... The Tri-Flop," in ED No. 23, Nov. 9, 1972, pp. 80-81 says that he researched over 300 relevant periodicals ("The Tri-Flop: Who Got There Fustest?" Across the Desk ED No. 4, Feb. 15, 1973, p. 7) and concluded that the idea had not been published before. Too bad he didn't check ELECTRONIC DESIGN for the following articles:


Robert M. Walker
Fairchild Semiconductor
484 Ellis St.
Mountain View, Calif. 94040

OTHER RESISTORS DO A SLOW BURN UNDER SPRAGUE'S TORCH TEST!

CERON® CERAMIC-INSULATED FLAME-PROOF WIREWOUND RESISTORS are a new development to meet the need for a truly non-flammable resistor in electronic equipment. Unlike some other so-called "flame-proof" resistors, which open-circuit before burning when subjected to high overloads, new and exclusive Sprague Ceron® Resistors are absolutely inert in the presence of heat or flame. They will not ignite under any degree of overload. Actually, they will not burn even when placed directly into the open flame of an oxyacetylene torch! This is clearly indicated in the photo, which dramatizes the protective qualities of the flame-proof Ceron® coating as compared with that of a conventional silicone-coated resistor.

The special coating is completely resistant to standard industrial cleaning solvents. Totally inorganic, it is also immune to attack by fungus. It provides excellent protection against thermal shock, humidity, and vibration. Dielectric strength, measured in a "V" block, is 500 volts a-c.

Series 380E (standard) and Series 400E (non-inductive) Ceron® Resistors meet moisture requirements of Specification MIL-R-26. Resistance values range from 1 to 60,000 ohms, in wattage ratings from 1 to 10 watts. Resistance tolerances as close as ±1% are available. Sizes range from 1/4" D. x 3/8" L. for the 1-watt resistor to 5/8" D. x 1 3/4" L. for the 10-watt unit.


Robert M. Walker
Fairchild Semiconductor
484 Ellis St.
Mountain View, Calif. 94040

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THE BROAD-LINE PRODUCER OF ELECTRONIC PARTS

INFORMATION RETRIEVAL NUMBER 15
Here's a dependable, quick-delivery source for Zero Defect

High Voltage Silicon Rectifiers

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- HIGH TRANSIENT VOLTAGE RATINGS.
- EXTREMELY LOW LEAKAGE.
- WORKING VOLTAGE RANGE ... 200V. THROUGH 50kV.

If you're looking for on-time delivery of miniature and microminiature High Voltage Silicon Rectifiers, look no further than ERIE. You simply can't beat our zero defect rectifiers since these units were first designed for high reliability night vision, lunar and aerospace applications. Their small size makes ERIE rectifiers ideal for thick film substrates, miniature power supplies, airborne displays, CRT displays, color TV, microwave ovens and other industrial and commercial applications where small size, reliability and superior performance are critical. All ERIE High Voltage Silicon Rectifiers feature conservative voltage ratings, fast recovery time, fast turn-on time, wide operating temperature range, high transient voltage ratings, low reverse leakage and unsurpassed reliability.

ERIE also offers double sealed, miniature Full Wave Bridge Rectifiers... perfect for P.C. use, with ratings up to 1000 volts per leg. So think ERIE for your High Voltage Silicon Rectifiers. Write TODAY for our new 24-page catalog...

High Voltage Components and Devices.
U.S. still favors solar cells despite Skylab difficulties

Despite the massive problems caused by the failure of the Skylab 1's workshop solar panel array to deploy, top engineers of the National Aeronautics and Space Administration say most earth-orbital vehicles will continue to depend upon solar panels for electrical energy.

There were a few pangs of regret that the old SNAP (Space Nuclear Auxiliary Power) programs had been killed in the budgetary squeeze several years ago. Both types of SNAP programs—reactors and isotopic generators—were hailed in the early days of space flight as a way to provide huge amounts of power for extended missions.

"When NASA first thought about Skylab [in fiscal 1963], it considered fuel cells, isotopic generators and other power sources," Skylab's director of experiments, Thomas Hanes, explains. "But it was decided that solar cells were the most economical for the time span. Generally speaking, solar cells still are the most economical power plant to use, in terms of weight and volume."

Congressional sources say the SNAP programs were curtailed because the only missions that demanded such large amounts of power would be interplanetary flights past Jupiter or a direct broadcast satellite in synchronous orbit.

Skylab's solar-cell problem was one of mechanics rather than technological. It resulted when a meteoroid shield broke loose during launching and damaged the solar-panel wings on the workshop area.

Four panels arrange in a windmill design on the Apollo Telescope Module section deployed, as planned, and have been performing even somewhat better than expected in providing power. This solar array has produced 2500 W of average orbital power, with the spacecraft pitched up in a 50° angle to reduce temperatures created by exposure to the sun after loss of the shield.

The panels are expected to produce better than 4 kW when the spacecraft is put back into its normal attitude.

Although Skylab originally was planned to have more than 11 kW available, most of the high-priority experiments can be performed with reduced power levels, Hanes said. These include medical, solar-TElescope and earth-resources experiments.

An experiment of high interest to the electronics industry—the growth of crystals in a weightless environment—may be dropped because of high electrical and manpower requirements.

Although the space agency worked to put more oxygen and hydrogen in the Apollo command-module fuel cell to extend its life from 14 days to about 17, none of this power can be transferred to the workshop.

Skylab will require between 3000 and 3500 W for essential housekeeping operations, including refrigeration of spoilables and the operation of crew equipment and communications, Hanes estimated.

Even as NASA struggled with its energy crisis, the House and Senate Space Committees voted to add $10-million to the fiscal 1974 NASA budget to keep some of the advanced nuclear technology work alive.

Magnetic semi urged to widen automation

Probing, sorting and bonding of semiconductor devices—the final steps in assembly that have eluded mass-handling techniques—would be automated under a magnetic approach proposed by Bell Laboratories. But a new type of semiconductor—one with magnetic elements deposited on the chip—would be needed to take advantage of the approach.

The proposal was outlined in a paper presented at the Electronic Components Conference in Washington, D.C., by Dr. M. Herbert Wachs, a scientist with Bell Laboratories in Reading, Pa.

With the new technique, an iron, nickel and cobalt alloy is incorporated into the metallization of the semiconductor chip. The magnetic material, says Wachs, then makes it possible to automatically orient many chips simultaneously into a precise array. This is done with the aid of a special disc magnet that contains a series of alternating north-south pole pairs.

Once formed into an array, the devices can be fed into the mechanized probing and bonding equipment. Electrical or optical measurements, or both together, determine if a device is good or bad. If the device is good, the apparatus moves to the next device; if it is bad, a vacuum removes it from the array.

After this probing and sorting has been completed, Wachs notes, a new matrix of only good devices can be formed quickly and fed to a bonding machine.

Chopper-stabilized amp shrunk by new process

Using a new processing technique that involves one step more than standard bipolar processing, Texas Instruments has shrunk the size of a chopper-stabilized op amp so it can fit in a 14-pin DIP.

The bipolar/JFET process, as described by Michael Callahan Jr., Design Engineer of the TI Dallas Division, involves diffusing a lightly doped p-layer into the epitaxial layer. This step is done just before the base diffusion, and thus it forms the JFET channel. The light p-doping results in a higher JFET G_m, a controlled pinchoff and a higher breakdown voltage. High-quality JFETs can thus be fabricated on the same chip as bipolar circuits, according to Callahan.
The first commercial circuit made with this process is a chopper-stabilized op amp with a differential input and a voltage drift of 0.6 µV/°C. The amplifier is actually two chips, one of which is a combination of bipolar transistors and JFETs and the other all MOS. Both chips are mounted in a single package.

Bipolar transistors and JFETs on the same chip are not new, but TI claims to have increased the JFET breakdown voltage more than fivefold—in excess of 40 V. This chip contains two linear op amps. One—the main amplifier—is an internally compensated, high-frequency, wideband unit. The other amplifier is a low-frequency JFET-input op amp that is used as a low-pass filter and null adjust for the wideband amplifier. The JFET-input main amp has a bandwidth of 3 MHz, a slew rate of 25 V/µs and a CMRR of 80 dB.

The other chip is an all-MOS-FET device described as one of the first commercial applications of linear MOS amplifiers. On the chip are three MOS linear op amps, a clock generator, a flip-flop countdown chain, MOS analog switches and control logic and decoding circuitry. The chip performs the chopper control, synchronous demodulation control and some sample/hold functions.

A better transducer sought for automobiles

Two General Motors research engineers have called for a greatly improved transducer for automotive electronic control systems.

In a paper presented in Detroit at the spring Society of Automotive Engineers meeting, Harry R. Mitchell and Ralph W. McGill of GM Research Laboratories predicted growth in automotive applications of transducers in the next few years.

“Most commercially available transducers,” they said, “are suitable for laboratory, aerospace or industrial-process applications, but do not meet additional, stringent automotive requirements.”

A common misconception, the authors noted, “is that the automotive industry need only translate to automotive needs the transducer technology developed over the last decade in association with the aerospace industry.

“However, this is not the case,” they went on, “because automotive performance criteria will often exceed those for aerospace applications.”

Plastic semi packages may rival hermetics

Plastic packages for semiconductors and microcircuits may start replacing hermetically sealed glass, metal and ceramic packages next year if improvements continue at the current rate, an Army semiconductor specialist believes.

The specialist, Edward B. Hakim, head of the Reliability and Physics Failure Group at the Army Electronics Technology and Devices Laboratory, Fort Monmouth, N.J., gave his views in a paper at the Electronic Components Conference in Washington, D.C. He noted that while plastic devices were still not reliable enough for widespread military use, improvements in bond reliability, moisture resistance and over-all field reliability indicated that by 1974-1975 the failure rates of hermetic and plastic devices would approach each other.

According to Hakim, when the military first considered using plastic, it was interested primarily in moisture resistance. After testing, however, it found that open and intermittent bonds were a more serious problem.

Another big problem with plastic devices, Hakim said, is that vendors are not interested in supplying plastic devices to high-reliability specifications.

When questioned about this, Jack Saddler, Motorola’s manager of federal marketing, Semiconductor Div., said that lot testing was not a problem but production was. Plastic devices for the military, Saddler explained, do not use the aluminum-gold metal systems used on commercial devices. They use an all-gold system.

“When you’re shipping a million devices a week, its uneconomical to switch production to an all-gold system for short runs,” he said.

According to Saddler, the reliability of plastic devices depends more on their hermeticity than on bonding. If a more hermetic plastic were developed, he said, most problems would be eliminated.

Robert McKenna, marketing manager for digital military circuits at Texas Instruments, Houston, disagrees with Hakim. He says that TI’s current line of industrial plastic devices can satisfy military needs. “We use a gold ball-aluminum system and have no problems with bond failures.”

As far as testing is concerned, TI is not at all reluctant to do the testing the military requires, he says.

First hybrid relay line offered for factory use

An integrated line of hybrid relays has been developed finally to meet the rigors of the industrial environment.

Factory installations are tough on theSCRs and triacs used in solid-state relays because of the following:

• The high currents encountered in starting big motors can overheat chips, causing thermal fatigue and eventual failure.
• Heavy line voltage surges tend to damage junctions.
• Line noises and pulses combine with high temperatures and lead to accidental turn-on.
• High vibration levels from machines cause stress failures.

The new line of hybrids, made by the Control Products Div. of Texas Instruments, Attleboro, Mass., is designed to withstand these hostile conditions. The relays are electrically and mechanically equivalent to their electromechanical counterparts and are essentially interchangeable with them.

The 2TI series is designed for switching 120-V inductive and small motor loads. It is said to have a 100-million-cycle life.

The 3TI series will handle up to 10-hp motors and heater loads of up to 45 A at 600 V. This series includes what is, according to TI, the first solid-state reversing motor controller on the market.

At present all the new units are selling for about twice the cost of equivalent electromechanical relays.
NEW SOLID STATE RELAYS

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All the technology that went into making General Electric a leader in couplers and power semiconductors is in our first solid state relay. Two models, 5 Amp. GSR10AU5 and 10 Amp. GSR10AU10, feature

- 120 V line operation
- Zero voltage switching, 5V max.
- $T^2L$ operation – 30 to 100° C
- Operates from 6.3 to 140 V RMS
- 1500 V RMS Photon Isolation

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INFORMATION RETRIEVAL NUMBER 17
Laser-scanner system produces color pictures on black-white film

Black-and-white film transparencies that show up as color pictures when viewed through a simple optical setup are produced by a laser image-recording system.

Developed by RCA for recording multispectral images from earth sensors in the Earth Resources Technology Satellite (ERTS), the system modulates the laser beam with color-carrier signals. Each of the carriers contains color information of a different spectral band ranging from violet to the infra-red.

The modulation scheme produces a synthetic diffraction grating on the film that has both color and image information in it. The laser signals are deflected onto a moving roll of film by a spinning scan mirror that is synchronized with the raster scan of the ERTS cameras or other equipment. The coded images, like those of a hologram, cannot be seen without the playback optical system.

In the playback system, light from off-axis colored sources is diffracted by the encoded transparency, passes through an on-axis spatial filter and emerges as an image on a screen.

Other uses besides ERTS

Steven L. Corsover, senior staff member at RCA's Advanced Technology Laboratories in Camden, N. J.—the system's designer—sees potential use for the basic system in other areas besides ERTS analysis, including these:

- The visual interpretation of IR photos by use of false colors.
- The recording and reproduction of color facsimile photos.
- The distribution of TV color programs by use of low-cost black-and-white film instead of expensive color. As an alternative, prints could be made with RCA's embossed vinyl-film process developed originally for a holographic TV playback system.

The new system is unique, Corsover explains, in that it uses purely electrical inputs, instead of images, to produce the black-and-white, color-coded film. Other systems that can produce a similar film have been developed, but they require optical gratings plus color-photo image inputs.

Color information in the RCA system can be encoded by use of a diffraction grating, Corsover says, because the diffraction pattern impressed on the black-and-white film is the optical Fourier transform of the grating. An inverse transform of the diffraction pattern yields the original grating to-

1. Modulated-laser scanner system records multicolor coded images on black-and-white film. Laser produces synthetic diffraction gratings on the film. They contain the image and color information.

2. Diffraction patterns of gratings can be optically processed to recover impressed information.

3. Synthetic gratings formed by modulating laser with three carriers have a unique white-light pattern.
1953 . . . It was high noon for the bad guys when this famous movie ran. 1953 . . . President Eisenhower had just arranged a truce in Korea. 1953 . . . An American firm successfully demonstrated the first full color video tape recording. And engineering and purchasing were having a hard time getting electronic parts and components. Distributors were taking care of their best customers, and delivery of large piece quantities of discretes was out of sight.

1973 . . . We remember. We’re U. S. Capacitor Corporation (a subsidiary of Globe-Union) and we know history repeats itself. During the intervening years, capacitor technology advanced exponentially, but the component market place still fluctuates with the economy.

Another bit of history . . . after each shortage and pipeline filling, the market place has restored to a higher level of consumption . . . 1953, 1973.

U. S. Capacitor Corporation is preparing to meet the current delivery crunch. We’ve made a substantial commitment to new, automated production machinery so that our customer’s needs will be satisfied, and we’re also expanding our facilities.

We know the history of our industry and we’re investing in it.

We make excellent high-rel and commercial monolithic ceramic capacitors and EMI/RFI filters.

Remember. U. S. Capacitor Corporation.
together with the color and image information that has been impressed on it.

If collimated light is allowed to fall on a blank slide in a simple optical system like that shown in Fig. 2, the light can be focused down to a single spot on a screen.

Substituting a diffraction grating for the blank slide produces a diffraction pattern that is at right angles to the grating lines. If three gratings are superimposed one on the other, the pattern that appears in the focal plane of the lens is the linear addition of all.

In his investigation, Corsover determined that with a laser recorder using a horizontal scan or raster like that of a TV, such gratings can be directly synthesized by modulating the laser output with signals related to the scan rate.

In the first prototype RCA system the scan rate was 24 per second, and three carriers were used: 120 kHz (= 5.10^3 x 24/s), 300.659 kHz (= 12.527472 x 10^6 x 24/s) and 456 kHz (= 19.10^6 x 24/s). These carriers were related to red, green and blue colors, and when all were simultaneously impressed on the film (as in Fig. 4, lower right) this corresponded to a white region of the encoded transparency.

The image information is impressed on the film when the contrast ratio of the gratings is varied in accordance with image brightness. The contrast ratio is changed when the levels of the amplitude modulators are changed.

These carriers have been chosen, Corsover says, with enough differences in their frequency so the diffraction patterns associated with each carrier can be separated.

Because these synthetic gratings are made with a raster scanner, the scan lines are a chopping frequency for the grating. As a result, the synthetic gratings have a diffraction pattern that contains an array of components, as shown in Fig. 3. Here a photo was taken of a pattern formed when the laser beam was sent through a grating region corresponding to white light. The spots formed by each carrier are labeled. The vertical line of spots in the center was formed by the scan raster.

The display system for color-encoded transparencies is most effective with off-axis illumination, as in Fig. 5.

3 point-source lamps needed

To obtain full-color reproduction a minimum of three point-source lamps are needed, one for each of the spatial color carriers (red, green, blue). In an RCA laboratory model the brightness of the individual colors could be adjusted to view a given spectral region.

The original feasibility model, Corsover says, had a single mirror and was used with 70-mm film. The latest model has been improved with a six-faceted scan mirror and a 1250-per-second scan rate (compared with 24 per second). Five-inch film is used.

To provide signals for laboratory testing of the system, a color facsimile system was built. In this, a white-light, flat-field scanner was used to scan a color transparency. The light was separated and fed to three phototubes, one for each of the three primary colors. Signals from the phototubes were applied to the laser modulators.

Basic resolution of the system is good, Corsover says, with 120 line pairs per millimeter for the highest spatial carrier. This is better than conventional TV.

The direct-recording bandwidth of the 24 scan-per-second system is 500 kHz, while that for the latest system is 25 MHz. The video bandwidths for these systems are 100 kHz and 3.2 MHz, respectively. Corsover sees scan rates of 4500 per second and bandwidths of 100 MHz in future systems with 9.5-inch film.

The recording time for the system using 70-mm film is three minutes. ■

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4. Microphotograph of a recorded film shows the synthetic diffraction gratings produced for red, green and blue colors. Their sum is white.

5. Simple optical system transforms the diffraction components of tricolor carrier gratings into a full-color reconstruction of original scene.
New HP logic analyzer solves digital problems

The new 5000A logic analyzer checks digital signals from a correlator.

Until now, bit watchers have attempted to extend their analog oscilloscopes to their digital problems. HP's new 5000A logic analyzer brings a new dimension to the study of logic states vs. time. Now, single-shot bit streams are captured automatically and stored indefinitely. Long digital sequences can be analyzed precisely because the 5000A delay is digital, locked to the clock of the system under test. And a catastrophic event may be used as a trigger source; the analyzer can even display information that preceded this trigger event. The 5000A logic analyzer displays 32 clock cycles for each of two data channels (or 64 clock cycles for a single channel). The display is by bit—i.e., the analyzer's 32 LEDs per
Detect cable faults less than 1 inch apart

Time domain reflectometry is used to check transmission systems, components and terminations. Now, HP makes it easy for you; merely insert a low-cost, 170-ps TDR plug-in into any 180 series oscilloscope mainframe. You get quick, accurate displays on cable lengths up to 1000 ft (300 m).

A time domain reflectometer displays reflected voltages caused by discontinuities in a transmission line. The display shows the location, magnitude and nature of each impedance discontinuity. HP’s 1818A plug-in resolves discontinuities less than an inch (2.54 cm) apart, so you can pinpoint problems in a long cable without having to physically examine the entire cable length. Because it is so compact, this lightweight wideband TDR system is especially useful for checking shipboard, airborne or remote communications equipment.

For details and specifications, check B on the HP Reply Card.

System monitors spectrum automatically

The HP 8580B automatic spectrum analyzer, a fundamental measurement tool for a broad range of applications, can be augmented with optional equipment to optimize spectrum surveillance and monitoring. The 8580B collects and analyzes large amounts of data and can operate unattended.

Performance is further enhanced by a new set of optional preselector/preamplifier units covering 0.1 to 18 GHz in three bands. They increase system sensitivity by 15 to 30 dB, eliminate unwanted responses, and reduce intermodulation distortion caused by strong out-of-band signals. These features also permit the automatic spectrum analyzer to make rapid and accurate EMI/RFI measurements.

For full information, check K on the HP Reply Card.

New multimeter, display for modular instrument

Two new “snap-on” accessories—a high-sensitivity multifunction unit and a 5½ digit display—enhance HP’s 3470 measurement system. The 3470 system consists of five compact instruments that fit together in various combinations to form a digital voltmeter, a multimeter, a battery-operated field instrument, or a digitizer with BCD output.

The new 34703A dc/dca/ohms meter features six dc voltage ranges from 10 mV to 1000 V full scale, six dc current ranges from 1 µA to 100 mA full scale, and eight resistance ranges from 1 Ω to 10 M Ω full scale. Basic sensitivity is 1 µV in dc voltage. Overranging is 100% on all functions and ranges, except 20% on the 1000 V range. Besides over-ranging, the multimeter features fast autoranging (< 250 ms) and a new self-test feature that performs 16 different tests on the internal circuitry.

Snap the new 34750A display module on top, and your answers appear on a 5-1/2 digit display.

For more information, check E on the HP Reply Card.

With these two modules, the 3470 measurement system now has seven different instrument combinations.
New flexible dc power supplies for OEM

OEM supplies come in 1/8, 1/4 and 1/2 rack widths; you can choose any combination up to a full rack width.

Need a multiple output dc power system that you can plug in and forget? HP’s new family of modular power supplies and rack accessories lets you choose from over 50 different standard models (both 62000 series linear and 62600 series transistor-switching types) with ratings from 3V to 48V. That includes the most popular ratings, such as: 5V at 2, 4, 8, 16 and 40A; 12V at 1.5, 3.6, 12 and 23A; and 15V at 1.25, 2.5, 5, 10 and 20A. To supplement these standard ratings, HP uses an interactive computer-aided design system to produce a quantity of supplies with special output ratings.

To complete your power system, just add a 19-in. (48 cm) rack mounting tray, front and rear panels, and slides. The rack tray accommodates any combination of modules totaling a full rack or less. There’s plenty of room behind the front and rear panels to add wiring for meters, switches, controls, terminal blocks and fuse holders. You can choose one of several standard panels, modify low-cost blank panels on your own, or let us build the complete system to your specifications. If you need extra cooling, a compatible cooling unit mounts directly below the rack tray and blows room-temperature air up into the power supplies.

Now, HP offers a minicomputer with built-in “extras” including microprogramming. Extended arithmetic instructions, floating point hardware, dual-channel direct memory access, power fail interrupt, memory parity check, and memory protect—they’re all built into the new 2100S computer. A programmable time base generator, communications control channel, and 16K words of 16-bit memory are also standard.

You can run programs in assembly language, FORTRAN, BASIC or ALGOL. A full range of software systems are available for batch processing, real-time, time-sharing, data acquisition, and automatic testing.

Because the 2100S contains an efficient microprocessor (a computer within the computer), you can write and store microprograms to suit your application and save valuable memory space. With this 196-ns microprocessor, critical subroutines are executed 5 to 10 times faster than if you use conventional software.

For more on our new “mini,” check D on the HP Reply Card.

OEM and quantity discounts are available. For more information, check P on the HP Reply Card.
Powerful new calculator makes statistics easier

Analyze data quickly and easily with this new desktop statistical calculator

Should you need to analyze research data, HP offers a new dedicated statistics calculator that solves many basic statistical problems with a single keystroke. The new 9805A desktop calculator has a solid-state memory similar to those used in computers. The built-in printer uses standard adding machine paper tape; it prints ten digits plus the sign, and up to six places to the right of the decimal point.

With the 9805A, you can:
- Calculate and plot a complete histogram with normal curve overlay.
- Fit curves using linear, parabolic, power, exponential, and logarithmic regressions. The plotting option lets you plot these curves with labelled axes.
- Calculate mean and standard deviation.
- Calculate \( t \) for both paired and unpaired data.
- Calculate one way analysis of variance for any number of data groups.

Other built-in functions include percentage, \( 1/x \), \( x/12 \), \( 1n x \), logarithms, exponentiation, and grand total accumulation. Options include 10-digit display, plotter compatibility, and additional statistical calculations.

For more information, check O on the HP Reply Card.

(Continued from page 1)

channel represent 32 successive clock cycles of the system under test. The LEDs turn on for a logic "high," and turn off for a logic "low".

To view data beyond the first 32 bits after the trigger, use digital delay to bring it into the analyzer's display. (Up to 999,999 bits of delay can be used.) If the data of interest is before the trigger, up to 32 bits of negative delay allows you to look ahead of the trigger event to see what has happened.

You can select any unique system event to trigger the 5000A: either data channel; an external trigger input; or high and low combinations of the three inputs ANDed together for parallel triggering. The 5000A is compatible with all logic families—TTL, ECL, MOS, RTL, HTL and CMOS.

With this new logic analyzer, you can design, test or service digital equipment faster and more efficiently.

For more information, check G on the HP Reply Card.

RF signal generator has synthesizer precision

Fully-calibrated AM, FM and CW signals with synthesizer accuracy, stability and spectral purity are under your fingertip control with the HP 8660B synthesized RF signal generator. Keyboard entry of frequency settings (with LED readout) plus swept and manual tuning provide operating flexibility that's truly unique in signal generators. RF plug-ins are available with these frequency ranges: 10 kHz to 110 MHz, 10 kHz to 160 MHz, and 1 MHz to 1300 MHz. All offer 1 Hz resolution.

Some key performance characteristics are: \( 3 \times 10^{-8} \) day frequency stability, \(-80 \) dB spurious (at most frequencies), \(< 1.5 \) Hz residual FM, and calibrated output levels from +10 to -146 dBm. All functions—frequency, output level, even modulation—can be remotely programmed, which makes the 8660 a natural choice for automatic test system applications.

For details and specifications, check L on the HP Reply Card.

If your requirements call for precision generation of signals in the frequency range between audio and UHF, there's an 8660 configuration that will fill your needs.
New card reader accepts any type card

The new 7260A card reader simplifies record keeping, is quiet enough for the office.

A new optical mark card reader accepts all types of punched or marked tab cards and reads them up to 300/min. You can use tab cards without clock marks or any card length from 7-3/8 in. (18.7 cm) to 11 in. (27.9 cm). It's easy, compact and quiet enough for office use, yet can run unattended under computer control. (An optional stacker is available for computerized operation.)

Data transmission rate ranges from 110 to 2400 baud. The card data is stored in buffers to optimize the feed rate for high transmission efficiency.

Besides saving computer input time, the 7260A is well suited to many applications. In hospitals, patients' lab test results can be recorded on cards then later added to medical records; the costs of the lab tests can be marked on other cards for the billing department. Schools use card data entry for student records, grades, test results, and course registration. The new card reader can also process the results of laboratory and field research.

For more information, check J on the HP Reply Card.

New couplers for wide range swept testing

Two new broadband directional couplers add economy and convenience to swept reflection and transmission coaxial measurements. With their wide frequency coverage (2 to 18 GHz), these couplers can replace several conventional couplers, thereby reducing setup, calibration and measurement time.

Both the 11692D (dual) and 11691D (single) have at least 30 dB directivity from 2 to 8 GHz, 26 dB from 8 to 18 GHz. Coupling variation with frequency is less than ±1 dB, and auxiliary arms typically track within ±0.7 dB.

Precision performance and wide bandwidth make these couplers ideal companions for the HP 8755 frequency response test set, a 0.1 to 18 GHz detection and display system. You can make simultaneous swept measurements of insertion loss and return loss with this versatile microwave measuring system.

For more information, check C on the HP Reply Card.

Make accurate reflection measurements over several octaves (2 to 18 GHz) with the 11692D dual directional coupler.

New pulse generators test fast logic circuits

Two new pulse generators—a plug-in and an independent instrument—test modern high-speed logic circuitry such as TTL-S, ECL-I, ECL-II and MECL 10000. Each has rep rates up to 100 MHz, 5V amplitude, variable transition times, variable offset and several output formats. A constant 50Ω source impedance ensures minimum pulse distortions.

The new stand-alone generator, 8007B, is well suited for measuring propagation delay and testing wideband linear amplifiers. Pulse transition time can be 2 ns to 250 µs; independent control of transition times permits ratios up to 50:1. Slope nonlinearity is below 3% above 20 ns.

Model 1916A plugs into a 1900A or 1901A pulse generator mainframe. Slope nonlinearity is under 5% above 5 ns. Like the 8007B, the 1916A output format may be positive or negative, and complementary or symmetric. In addition, the 1916A features dual output.

For details, check S on the HP Reply Card.
New low-cost core-based real-time system

HP introduces a new real-time computer data acquisition and control system for small, dedicated applications in industry and in research and development laboratories.

Many small laboratory or testing situations require scheduling, multiprocessing and priority interrupt; but they don’t need foreground and background programs or a large data base. The answer: RTE-C, a smaller low-cost version of HP’s real-time executive, that provides concurrent program operations with on-line control by the operator.

System languages are HP FORTRAN and assembly language. Memory capacity is 8K to 32K words; the number of I/O channels vary from 1 to 42. And as your application grows, you can move up to a disc-based system without costly modifications to existing software.

For details, check M on the HP Reply Card.

Distributed systems: one plus one is greater than two

HP distributed systems solve many of the problems confronting multiprocessor system users. In large systems, it is often advantageous to distribute computer processing over a number of independent minicomputers. The HP 91701 distributed system interface kit allocates functional capabilities to multiple remote computers that communicate with a central real-time executive by common carrier telephone lines or by cable (up to 2 miles).

Data collection, sensor-based data acquisition, automatic testing, laboratory automation, and process monitoring and control can be dedicated to the remote computers, while program development and storage, data management, additional data analysis, and report generation occur at the RTE information center. You can program in ALGOL, FORTRAN, or assembly language. And as your application needs increase, additional remote computers can be interfaced.

To find out how distributed systems can fit your particular application, check N on the HP Reply Card.
HP components: new catalog tells all

Send for this complimentary catalog for component users.

If you are a circuit designer, development engineer or instrument manufacturer, the 1973 HP components catalog should be on your desk. This 160-page “Designer’s Catalog” contains complete descriptions and specifications for HP diodes and transistors, including:

- General purpose Schottky diodes
- Microwave Schottky diodes
- PIN diodes
- Step recovery diodes
- IMPATT diodes
- Microwave transistors
- Devices for hybrid integrated circuits.

For a free copy, check Q on the HP Reply Card.

New band switching PIN diodes

PIN diodes for UHF/VHF switches, attenuators

A new low-capacitance device, the 5082-3077 PIN diode is designed for RF switching, modulating and automatic gain control applications. You can use it in RF duplexer, antenna switching matrices, digital phase shifters, analog phase shifters, electronically-tuned filters, and variable RF attenuators.

Effective minority carrier lifetime is >100 ns, resulting in low harmonic distortion in the 100 to 1000 MHz frequency range. Dynamic range is 1 \( \Omega \) to 10 k\( \Omega \); reverse bias capacitance is less than 0.3 pf. CW power switching capability is 2.5 W.

Delivery is from stock.

For more information, check H on the HP Reply Card.

The 5082-3168/3188 planar passivated silicon diodes come in an axial lead, hermetically sealed glass package.

Two new low-cost PIN diodes are available for VHF/UHF switching and general-purpose switching applications that require high performance and mechanical ruggedness. Capacitance is less than 1.0 pf at -20V, and the residual series resistance is typically .35 ohms at 10 mA.

For specifications and details, check I on the HP Reply Card.
Use HP battery-powered storage scopes in the field and in the lab

The 1702A/1703A scopes offer laboratory performance in a rugged portable package, and they're the first storage oscilloscopes that operate on ac, dc or batteries. Both have 35-MHz bandwidths, dual-channel 10 mV/div deflection factors, and 10 ns/div sweep speeds. (The only difference is that model 1702A has a standard time base while the 1703A has a calibrated delayed sweep.) You can use either as a conventional scope, a variable persistence scope, or a storage scope. The 1702A/1703A scopes have a bright, crisp trace. CRT linearity, bandwidth and deflection factors are specified over the entire 6 x 10 division (0.85 cm/div) display, from dc to 35 MHz. The burn-resistant tube requires no more operating care than a conventional CRT.

Need variable persistence? You can retain a trace for over an hour. Variable persistence provides extra brightness for dim traces—such as rep rate pulses—and eliminates flicker, common to slow sweep speeds.

With storage, you can capture single-shot events (e.g., noise-related transients) or infrequently-occurring events (e.g., random-bit dropout). Just push STORE, and your waveform is preserved for up to one hour. Either storage scope replaces a conventional scope and a camera (with all the associated inconvenience).

Applications for these scopes include such areas as acoustics, biology, chemistry, oceanography, pneumatic, fluid, electrical, mechanical and civil engineering. Battery operation enables you to use them for field service applications, as well as in the laboratory.

For more information, check A on the HP Reply Card.

HEWLETT PACKARD

Sales, service and support in 172 centers in 65 countries.
Everything you always wanted to know about Drive Motors.

Into these five booklets we've crammed 156 pages of the latest information on Kearfott's line of Drive Motors.

Kearfott, as you probably already know, is a primary supplier of drive motors. And has a reputation for quality, service and on-time delivery.

We can furnish you with drive motors in individual units or in packages to fit any of your aerospace or industrial applications. From counters to computers. From business machines to printers and tape readers.

Let's take a look at the type and range of motors we're talking about.

**DC TACHOMETERS**
Kearfott Tachometers are designed specifically for precision speed sensing and as rate generators to help velocity servos achieve fast response.
Features include: outputs to 100V dc/1000rpm; minimum ripple at high commutation frequency; high linearity; low friction torque.
These are ideal for computer tape transports where efficient data retrieval is a must. And for business machine and numerical control machine tools.

**DC TORQUERS**
You can get sizes 12 through 42, uncased for gimbal mount applications and cased for direct drive torque motor positioning.
Kearfott can also supply them with a variety of integral feedback elements such as potentiometers, synchros and tachometers—in a single housing.
You've a choice of standard design, inverted construction (inner member is magnetic and transfers power to an outer armature) and brushless Limited Rotation design.

**DC MOTORS**
These are Moving Coil Motors used for high-response DC servos such as High-Speed Printer and Capatan drives.
One of their unique features is that they need less cooling than equivalent competitive units. The reason: low internal impedance which allows a high cooling flow rate at low developed pressures.
Permanent magnet and wound-field types are available for standard aerospace and industrial applications, including high acceleration motors with integral tachometers for terminal printers.

**AC MOTORS**
Kearfott induction or synchronous motors of the hysteresis or reluctance type come in a broad range of frame sizes. And from sub-fractional power to 15 HP.
We can furnish motors that run on up to 440 volts ac, single, 2 or 3 phase.
Induction motors that operate on 2, 4, 6, 8 or 12 pole design. And dual speed motors such as needed for driving memory discs in large computers.
You can also get: high-slip motors for aircraft requirements at 400 cps; synchronous motors for constant rotating speeds with varying loads; gear motors for extremely low speeds or speeds incompatible with the power supply frequency.

**STEPPER MOTORS**
If you want precision control—for example for small peripheral devices, small line printers and tape readers—Kearfott Steppers provide it via discreet steps and high slew rates. And in a wide choice of stepping rates and torque levels.
Typical Kearfott units have 15° stepping angles, compatible with all 24-tooth sprockets. They give high holding torque, high stepping speed and fast response.
Units with other step angles, such as 1.8°, 7.5°, 10°, 30°, 45° and 90° are readily available in frame sizes through 50.
But why not get all the details? Mail the coupon for our new booklets now. The Singer Company, Kearfott Division, 1150 McBride Avenue, Little Falls, N.J. 07424.

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Rush me your new booklets on Kearfott Drive Motors.

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Company _____________________________
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Here are the eight latest additions to our DI/CMOS family—the fastest low-power logic devices on the market. And they're completely free of SCR latch-up problems.

Last fall we introduced our first eight DI/CMOS logic devices. Now, through our continuing development program, we've added eight more. Like the first group, these offer speeds twice as fast as any comparable IC's (typically 10ns with 10-volt power supplies) and extremely low power dissipation. Power dissipation for each of the eight new devices is typically lnW. These units also permit a wide power supply range (3VDC to 18VDC), while providing large noise immunity—typically 45% of supply voltage. And because of our dielectric isolation process, SCR latch-up problems are completely eliminated.

Chip reliability is currently reported at more than 325,000 device hours at +125°C without failure. The first six devices diagrammed here (HD-4000 series) are pin for pin compatible with the CD-4000A series. The last two are Harris proprietary devices (HD-4800 series). All are available in 14-pin DIP's except the HD-4814, which comes in a 16-pin package. For details see your Harris distributor or representative.
OS cont'd:

14 HD-4030
Quad Exclusive OR Gate

Pin for pin compatible with CD-4030A. 100-999 units
- 40°C to + 85°C $2.10
- 55°C to + 125°C $3.80

15 HD-4811
Quad Exclusive NOR Gate

Pin for pin compatible with CD-4011A. 100-999 units
- 40°C to + 85°C $2.10
- 55°C to + 125°C $3.80

A Harris proprietary device.

In case you missed the ad describing our first eight CMOS devices, here they are again. All are high-speed, low-power units. The HD-4000 series is pin for pin compatible with the CD-4000A series. The HD-4009 is a Harris proprietary device.

HARRIS SEMICONDUCTOR
A DIVISION OF HARRIS INTERTYPE CORPORATION
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CALIFORNIA: Anaheim—Weatherford; El Segundo—Liberty; Glendale—Weatherford; Long Beach—HAR (213) 420-7697; Mountain View—Elmar; Palo Alto—Weatherford; San Diego—Weatherford, Western
COLORADO: Denver—Elmar, Weatherford

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INFORMATION RETRIEVAL NUMBER 162

ELECTRONIC DESIGN 12, JUNE 7, 1973
the changing face of time

CAL-TEX digital clock/calendar circuit

If you are one of the people who are causing change, then Cal-Tex has a product of value to you. If you are designing tomorrow's time display and measurement systems today, then our CT 7001 Digital Clock/Calendar circuit has application.

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INFORMATION RETRIEVAL NUMBER 163

34D
Laser system tracks where radar can’t

A laser tracking system for missiles that permits tracking in the low altitudes where ground clutter causes radar to fail is being tested at the White Sands Missile Range, N.M.

The system is reported able to track white-painted targets traveling 1000 mph with four-inch accuracy at up to 0.9 mile. Positions are computed every 5 ms.

Used with radar, the laser system provides accurate tracking of a test missile throughout its flight. The system—called an LRTS, for Laser Ranging and Tracking System—was built by the Autonetics Div. of Rockwell International, Anaheim, Calif., to specifications outlined by the Instrumentation Directorate of the Army Test and Evaluation Command.

A 5145-A beam from a fixed, 5-W cw argon laser is fed to a transceiver head mounted on a precision gimbal. The transceiver aims the beam at the target missile, and an image dissector tube mounted in the transceiver head detects the reflected light. The missiles are painted white to increase their reflectivity.

A Systems Engineering Laboratories SEL-810B computer with an 8-k core memory handles both signal conditioning and gimbal control functions.

“The system is flexible,” explains John A. Roth, Army project manager. “The laser tracker can either scan above the target missile to initiate tracking as it passes or can be locked on before the launch.”

Since it is a skin-tracking system rather than a beacon tracker, no transponders or reflectors need be installed on the test vehicle. Further, no optical or tracking augmentation is required on the ground for the system to work.

The prototype LRTS, costing about $1-million, has been undergoing tests at White Sands for more than two years, and the final phases of testing are taking place now, according to the Army. ■

nimo CRT
THE 64 GUN SALUTE

BOOM... big information in a small package. nimo®, a 1.5” MINI-CRT requiring no internal or external focusing or deflection.

Each of 64 independent guns can display a single letter, number or symbol up to .6” high, or a complete message of up to 3 lines of 6 characters (.187” high). In effect, this ingenious display provides a Read-Only-Memory for your fixed data with extremely simple and inexpensive TTL interfacing; i.e., an 8 x 8 drive structure requires only two SN 7442N decoders, and four MC 1820P Hex inverters to complete the package.

Unmatched legibility (true form characters), and contrast ratio, boom loud and clear, all on a single plane.

Don’t restrict your thinking about the nimo 64’s applications, they’re great for key-to-tape/disc terminals for character entry verifications, digital instrumentation, annunciator systems, computer prompts, optical data scanning systems, teaching machines, and point of sale terminals.

The price? At ease men... 60¢ a message. nimo 64, the ultimate display—GIVE IT A SHOT!

Green LED production spurred by a new process at Ferranti

A new process for greatly improving the batch fabrication of green LEDs is reported by Ferranti Ltd., Chadderton, Oldham, England. "Excellent performance" in the laboratory has been obtained from nitrogen-doped, gallium phosphide devices with an emission peak at 565 nm, the company says.

The process is described in a paper, "Green LED Displays—A Planar Approach," by A. R. Peaker and V. M. Pastore of Ferranti.

The shortcomings of red-emitting, gallium-arsenide-phosphide devices, which now dominate the LED market, were summarized this way by the authors:

"Red LEDs emit at a wavelength of approximately 655 nm—the extreme end of the eye's response—which results in operator problems, such as fatigue after prolonged use, focusing difficulties and high error rates."

These factors, combined with the unacceptable psychological connotations of red displays in some environments like aircraft cockpits, have created a pressing need for green and yellow light-emitting diode displays, with costs and characteristics comparable to those for GaAsP.

Others make green LEDs

Most companies—such as Monsanto of Cupertino, Calif.; Microsystems International of Ottawa; Matsushita of Japan; Opcoa, Edison, N.J., and Siemens of West Germany—use either the liquid-phase or vapor-phase epitaxy process.

The liquid-epitaxy process now widely used to fabricate gallium phosphide diodes produces an emitting region between the individually grown p and n regions. This junction is essentially continuous across the whole slice, so that the emitting areas must be defined by cutting or etching.

This process severely limits the available configurations and makes testing impracticable prior to dicing.

The process that Ferranti chose for fabricating gallium-phosphide diodes commercially, the paper said, calls for a single liquid-epitaxy growth followed by a low-temperature diffusion using a silicon-nitride mask. To obtain the flexibility to make any shape of diode required—and in large quantities—photoprocessing techniques similar to those for making silicon diodes had to be used. This called for very smooth surfaces—with undulations no larger than 1 μm. This smoothness, in turn, put great demands on the epitaxial growth process, causing Ferranti to go to a process that uses horizontal spades, or substrates, in a vertical crucible.

N-type epitaxial layers are deposited on up to 20 slices of 10 cm² each. The layer is doped with sulphur from a solid source and nitrogen from ammonia gas.

After growth, a silicon-nitride layer is deposited on the slice, and normal photoresist techniques are used to delineate the diode areas. Fluorine ions from the tetrafluoromethane plasma are used to etch windows in the nitride, and subsequently zinc is diffused into the gallium phosphide.

The dice can be mounted on the display matrix substrates by alloying, soldering or epoxy-bonding. Consequently, according to the authors, high yields can be obtained with conventional semiconductor equipment—an important point in hybrid displays, where the LED manufacturer is often supplying uncut wafers rather than finished devices.

Special uses cited

One area where green-emitting devices have a large advantage over red LEDs, the authors reported, is in data recording on photographic film. The green device is suitable for recording on orthochromatic and many blue-sensitive films while providing superior results on color, panchromatic and most infrared material. In film applications the transparency of the gallium phosphide enables the light to be taken out through the substrate so that very small characters and dot-spacing can be achieved. The information is relayed to the film via a fiber-optic faceplate for "in contact" marking, or via a lens if further size reduction is required.

A Ferranti spokesman says the company is now capable of producing 10-million green LED chips a year at a cost that is only 20% higher than red LEDs.
Any .025" square post, yours or ours. And Elco's Varipost Box™ connector. For true togetherness in board-to-board and cable-to-board connections. Our new single row (Series 8243) and dual row (Series 8242), connectors will mate with any .025" square posts on the market, even if they're wire-wrapped one level. Which means you can hold with your existing design and still make the connections you need.

Let's peek inside one of our Varipost Box™ connectors and see why they're so receptive. First, the contact surfaces of the spring members are parallel to the surface of the p.c. board, and thus can span post-to-post tolerance deviations in your board. This compensates for misalignment between posts and contacts, so you get a perfect mating every time. Competitive box connectors—on the other hand—have perpendicular contact surfaces that demand tighter post-to-post tolerances to insure the mating of every contact with its corresponding post.

The spring contacts in our Varipost Box™ connector are longer, deflect farther and provide a longer wiping action than competitive connectors. Our contacts extend all the way to the entrance of the connector, so they'll mate with shorter-than-standard posts. And if your posts are longer than standard, a built-in stop prevents the posts from extending out the rear of the connector and shorting out with the upper row of contacts in the dual row version.

There's more. Our contacts can be removed from the housing and replaced without deformation. And sequential mating in dual row connectors—first one row, then the other—reduces insertion forces by half.

A wide range of models is now available... right off the shelf. Cable-to-board units with contact spacing on .100" and .125" centers in single row (with up to 25 contacts) and dual row with up to 50. Board-to-board (.100" centers) versions with up to 50 contacts, and dual row (.100" by .100") with up to 100 contacts.

As companion pieces, we offer our new .025" square posts, Elco Variposts™. And we've the insertion equipment to stake these posts into the board. So we can supply your p.c. board with posts already inserted, ready for mating.

Leave it to Elco, the Matchmaker. Another service in keeping with CONNECTRONICS, Elco's Total Connector Capability.
A bubble memory-logic chip? IBM heads toward that goal

Magnetic-bubble memories would be much more attractive if they could perform logic as well as storage. IBM researchers have taken the first step toward achieving this goal by designing a universal bubble logic element that can perform any logic function.

The development was described at the National Computer Conference in New York by Frank Tung, a staff member at the IBM Research Laboratory in San Jose, Calif. Noting that early attempts at bubble-logic design concentrated on AND/OR gates, he observed: "This is a very primitive form of logic and is inflexible." The early attempts were not sophisticated enough to take advantage of large-scale integration, he pointed out.

The bubble circuit under development at IBM overcomes these problems, Tung reported. It is simply an implementation of the symmetric switching function—a function that has been known for many years. Its use in a design has been limited until now, Tung noted, because it is not easily implemented with solid-state logic. But it is very easy to use with bubbles, he said.

It performs any logic function

Like NOR/NAND logic, the symmetric switching function is a universal operator. It can be made to perform any logic function—such as that of an AND/OR gate, carry-bit generator or sum-bit generator—simply by changing parameters known as A-numbers in the control bubble stream (see diagram).

Generation of logic functions, Tung said, is made possible by the magnetic forces that exist between bubbles. The magnetic force emanating from a bubble, he explained, is adequate to move an adjacent bubble as far as two or three diameters away.

In explaining how the symmetric-function bubble device works, Tung noted that data were first entered into the bubble sifter. The sifter merely separates the bubbles, which represent ONEs, from the voids, which represent ZEROS. When a bubble enters an idler, it remains there unless it is forced out by another bubble. It is this property that permits the sifting, or separating, of bubbles and voids.

The output of the sifter (Z in the diagram) is then fed to the leading bubble detector. This is done by entering additional bubbles known as flushers. The position of the first bubble, which is determined by the time it takes the bubble to be detected, is an indication of the total number of bubbles. This number must be known to perform logic operations.

When the leading bubble enters the detector, it forces a bubble that was loaded into the detector as an additional condition into the AND gate. In the meantime the leading bubble remains in the center idler of the detector and, by magnetic repulsion, forces all subsequent bubbles to be annihilated. Thus the output of the detector stage con-

Jules H. Gilder
Associate Editor
The A-numbers are stored in a recirculating shift register. By proper timing, Tung said, the information coming out of the leading bubble detector stage is required to AND with the A-numbers of the control bubble stream. If both inputs to the AND gate are ONEs, a bubble appears at the output, indicating that the function is true. If, on the other hand, one of the inputs to the AND gate is a void or ZERO, the bubble at the other input goes to the bubble annihilator and the output is ZERO.

In the symmetric-function bubble device, Tung said, the logic operation is performed by counting the number of bubbles. If the A-numbers are chosen as 2 and 3, the device becomes a carry-bit generator. In this case, if the number of bubbles equals 2 or 3, a carry bit is generated.

By changing the A-numbers to 1 and 3, the device becomes a sum-bit generator. The carry and sum functions can be combined to form an adder.

**Blending memory and logic**

The bubble-logic device is fabricated with T and I permalloy patterns, which are very similar to those used for bubble memories, Tung reported. Because of this similarity, it is feasible to blend memory and logic on the same chip. Such a mixture would offer lowered cost and low power dissipation.

Traditionally, memory and logic are packaged separately. For example, the ferrite core memory and semiconductor central processing unit are separate because of different technologies. In semiconductors, memory and logic are separated mainly because read-write memory is volatile while logic is not.

Combining logic and memory on the same chip will also lead to increased reliability and shorter delay times, Tung predicted. With logic and memory on the same chip, the number of interconnections will be reduced and reliability will go up, he noted.

The new capability, Tung speculated, may foster revolutionary changes in computer organization and architecture.

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At The Information Display Show

Liquid-crystal panel overcomes video-rate operating 'barrier'

Until now the operation of a liquid-crystal panel at video rates has not been possible, because of crosstalk between elements and the slow response time of the crystals. A solution to these problems was presented at the Society for Information Display's International Symposium and Exhibition, held in New York City May 15 to 17.

A paper by Lewis T. Lipton and N. John Koda of the Industrial Products Div. of Hughes Aircraft Co., Oceanside, Calif., described a panel design that used thin-film transistors as a switching element and integrated the transistors with other structures required by the cell. Nematic liquid crystals in a reflective mode were employed, but the authors said the design could be adapted to other liquid crystals and to a transmissive mode of operation.

The basic requirement for operating liquid cells, the paper explained, is the application of an electric field across the liquid crystal to orient its molecules. Various modes of operation are then possible. The one chosen by the authors was the dynamic scattering mode, in which increased fields are applied and the corresponding ionic current creates scattering sites.

Photolithography used

Fabrication of the thin-film transistors was achieved by standard photolithography and thin-film deposition techniques. In this approach the gates are chrome and are formed by etching. The insulator is usually silicon monoxide or aluminum oxide, and the semiconductor is cadmium selenide. No masking is required for the deposition of these materials, except at the panel edge, where contacts are made.

The operating panel is completed by sandwiching the transistor array with a suitable liquid crystal, a Mylar spacer and a covering plate that has a tin oxide electrode. The authors' initial effort centered on obtaining the required thin-film-transistor performance. They began by constructing a coarse 2-by-3 array that would solve both the photolithography and transistor fabrication problems.

After the desired array of transistors had been fabricated, the authors constructed the panel by combining the array with a dynamic scattering-mode liquid-crystal material. The panel successfully demonstrated thin-film-transistor control of the individual liquid-crystal elements with no crosstalk, the paper reported. The contrast ratio with collimated light was in excess of 10:1, with 25 V between the source and drain.

The array also demonstrated the concept of rapid address of the liquid crystal via charge storage on the parallel capacitor. The authors said further that a pulse on the gate of the thin-film transistor was able to excite the liquid crystal at a rate approximately one order of magnitude faster than the response time of the liquid crystal alone. The actual rate was controlled by the RC time constant of the transistor ON resistance and the buffer capacitance. The rate is limited by the excessively large capacitance of the coarse 2-by-3 array. Work is now under way, the authors say, to extend the concept to larger panels.

Ceramic image-storing device can project data by reflection

A new type of ferroelectric-photoconductive image-storing device has been developed that allows the stored data to be projected on a screen by reflection from the surface, as well as by light being transmitted through it. Previously similar devices operated only by transmitted light.

There are distinct advantages to the new technique, according to Cecil E. Land and Willis D. Smith of Sandia Laboratories, Albuquerque, N. M., who developed the new reflective device, called the Fericon, and a light-transmission predecessor, the Cerampic. The two men described their findings in a paper at the recent information display show in New York.

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Fericon structure (a) stores images as strain-induced deformations (b) on the surfaces of lead lanthanum zirconate titanate (PLZT) plates.

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Trade reform fight heating up

The President’s proposed Trade Reform Act is headed for a long hot summer of argument. Both the Aerospace Industries Association and the Electronic Industries Association are fighting it. At stake is the Administration’s proposed repeal of Tariff Items 806.30 and 807, which provide duty-free entry—except for value added—of products manufactured abroad with components furnished by U.S.-based companies. The EIA estimates repeal would cost the semiconductor industry alone $5-million a year. The AIA argues that offshore assembly is necessary for American companies to stay competitive in the world market. Without such assembly, the association contends, 37,000 jobs needed to manufacture U.S. components will be lost. But the AFL-CIO, which has strongly favored the highly protectionist Burke-Hartke bill, is adamant that any tax measure must discourage investment abroad by American companies.

Military pressing for laser weapons

All three military services have asked Congress for permission to reprogram more than $10-million in extra funds from other fiscal 1973 accounts so they can step up laser-weapon design work. In heavily censored testimony just released, an Air Force brigadier general, Howard Fish, said a significant breakthrough in laser weapons had occurred since last year’s budget preparation. The Air Force, which appears to favor the gas dynamic laser over chemical types, reportedly wants to design and test high-energy rays for bomber defense. The Navy, the Army and Marine Corps, in a joint effort, also want to test high-energy lasers for anti-air and anti-surface missile use. The cost of development for all three applications is expected to total $500-million.

Minority recruiting for engineering lags

Of all the skilled professions, engineering may be having the most trouble attracting minorities the National Academy of Engineering says. In 1970 Cornell University estimated that only one-half of 1% of all engineers were black. Only 1% of present engineering students represent minority groups.

It could cost the Government as much as $312-million over the next decade to increase minority engineering enrollment, Cornell University’s Donald Dickason told a recent National Academy of Engineering sym-
posium, but the benefit to the nation would be worth the cost, he noted. The money would be spent on special programs, recruiting campaigns and scholarships.

Meanwhile the engineers Joint Council sees a continuing decline in the number of engineering graduates—to about 32,000 in 1975, against 43,000 in 1972—resulting in an annual shortage of 10,000 engineers.

**Defense navigation satellite proposals to be sought**

The Air Force will ask for industry proposals in about a month for the design and definition of the satellite portion of the proposed Defense Navigation Satellite System. The system would give military aircraft, ships and ground vehicles precise positioning information.

The Air Force already is evaluating proposals from four bidding teams—by General Dynamics Electronics, Grumman Aerospace, ITT Avionics and Philco-Ford—for the design of ground stations and aircraft and ship user equipment. The Pentagon is proceeding cautiously on the program and has given approval only for the design of equipment to demonstrate the concept. A final decision will be withheld until all aspects are proven technologically and economically feasible.

**Capital Capsules:** NASA has established a General Aviation Technology Office, with Roger L. Winblade, an engineer and holder of a patent on the X-15 aircraft, as head. . . . Sen. Edward Kennedy (D.-Mass.), chairman of the Senate National Science Foundation Subcommittee, plans hearings on the proposed National Science Policy and Priorities Act and the Civilian Science and Technology Act. Both measures would promote the transfer of aerospace technology to the civilian sector. . . . NASA has invited industries and research organizations that are seeking experienced engineers, scientists and skilled technicians to choose from among the 600 NASA employees whose positions will be abolished by June 30. Employment offices at the Goddard Space Flight Center, Greenbelt, Md., Lewis Research Center, Cleveland and Marshall Space Flight Center, Huntsville, Ala. have details. . . . The Aerospace Industries Association has joined other technical associations in supporting voluntary conversion to the metric system. The AIA asks that the cost of conversion be recoverable in the prices of products. . . . The Air Force is getting ready to contract for yet another study of electro-magnetic pulse (EMP) phenomena and is looking for companies capable of working on the conceptual design of advanced pulse generators. . . . The Naval Ship Systems Command is looking for R&D sources to develop a shipboard data multiplex system. It would handle navigation, ship-control and command-decision data. . . . General Electric's Valley Forge Space Center has won a contract to study earth-resources systems, from data acquisition to applications and to advise NASA on instrumentation, vehicles and procedures. . . . The National Bureau of Standards' Institute for Computer Sciences and Technology and the Dept. of Defense are initiating a COBOL compiler testing service whereby commercial vendors and Government agencies can test compiling equipment to assure compatibility with Government computer operations. . . . The Senate Commerce Committee is holding hearings on the bill which would direct the Secretary of Transportation to study the feasibility of a high-speed ground transportation system stretching from Vancouver, B.C., to the major cities in California.
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AMP microelectronics: doing small things in a big way.

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A pilot production line for liquid-crystal display devices has been started by Thomson-CSF in Paris. The displays fall into three categories. One is dynamic-scattering-mode devices that operate at 15 to 20 V and at frequencies between 25 and 100 Hz; their power consumption is 100 µW/cm², and they have a predicted lifetime of 7000 to 10,000 hours. In the second category are twisted (field-effect) nematic devices, operating at less than 5 V at a frequency of about 1 kHz; their power consumption is about 1 µW/cm², with a life expectancy of 30,000 hours. The third category is variable-color devices. Based on the double-refraction effect, they operate at about 7 V at 10 kHz, with a power consumption of 10 µW/cm²; their estimated life is 30,000 hours. Products are available in the first two categories.

Two MOS integrated circuits for use in an electronic weighing machine have been developed by Siemens of West Germany. The electronic scale calculates the price of a commodity from its weight and unit-weight price. The weight graduations are encoded on a glass disc inside the machine. The disc is rotated by the weighing lever of an inclined balance. Phototransistors keep track of the weight on the disc. The MOS circuits multiply the weight by the unit-weight price, which is fed in through a 10-digit keyboard. The process is repeated up to 10 times per second. The selling price appears on indicator tubes. The MOS circuits are mounted in two 24-pin dual inline packages that contain 1800 and 1150 transistors, respectively.

A new group of triodes by Brown Boveri of Baden, Switzerland, has been designed to meet the severe environment encountered in industrial rf applications while supplying the guaranteed power without drift. The triodes are designed for power outputs ranging from 15 to 300 kW up to a maximum frequency of 120 MHz. A high-perveance, high-stability mesh cathode gives emission reserves to cope with system voltage fluctuations and stresses caused by intermittent operation. A stiffened grid cage provides good stability and can carry rf charging currents of several hundred amperes. The tubes have small inductances and low gains (an advantage when dealing with load fluctuations), low driving power and high grid and anode dissipation reserves.

A continuous-wave dye laser with high frequency and amplitude stability has been produced at the Queen's University of Belfast, Northern Ireland. The laser can be tuned to emit a wavelength of less than 1 Å broad. Operating in the single-transverse mode, the laser can be tuned over most of the visible spectrum. As a result, it can be used in such applications as selective-excitation spectroscopy, saturation spectroscopy and selective-scattering experiments. With second-harmonic generation, the ultraviolet range (2500 to 3500 Å) can also be covered. The laser can be passively mode-locked to produce continuous trains of tunable picosecond pulses. Direct measurements of the pulse trains indicate that the single pulses are less than 5 ps in duration with negligible background radiation.
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INFORMATION RETRIEVAL NUMBER 32
How was Europe?

Having recently returned from a visit to the important electronics powers in Europe—France, Germany, England and Philips—I'm often asked, "How did you find Europe?" My first inclination is to reply that I stepped off the plane and there it was.

The fact, though, is that it's no easier to describe electronics in Europe than to describe electronics in the U.S. Some European companies, with or without government support, just plod along—as do many companies in the U.S. Others are stimulatingly aggressive—exploring ever wider markets, including those in the U.S.

What about Europe's engineers and managers? They're like ours, too. Some are very sharp and imaginative. Others follow tradition; they're competent, but easily lost in a crowd of two. Throw a challenge at one man, and he bubbles with excitement as he starts conjuring up 40 ways to tackle the problem and win the goal. Throw the same challenge at another man and, very methodically and carefully, he tells you why the job can't be done. Armed with 40 reasons, difficulties and problems, he shows you that he doesn't have a large enough staff, that his people don't have enough experience, that he doesn't have adequate equipment and financial resources, that his hands are tied by tradition, bureaucracy and company policy, and that the job should be done by somebody else's department. How typically European! How typically American!

And the products? Like those in the States, most in Europe are "me-too" products, differing only slightly from products already on the market. And a few, which you'll be seeing in these pages, are dazzlers.

What's the conclusion? Companies, and the engineers and managers who give them life, are pretty much the same all over the world. Can we learn from each other? Of course. Regardless of language, pay scales, working environment and social traditions, the wide-awake, dynamic individuals throughout the world are those who give most and, in so doing, receive most in personal achievement, self-respect and personal satisfaction. We should all emulate them.

George Rostky
Editor-in-Chief
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INFORMATION RETRIEVAL NUMBER 33
Unlike the dramatic quantum-jump changes in semiconductor and IC technology, the passive component field has tended to follow a slow, evolutionary path. There have been changes in the last 10 years, but new passive components appear to take more time to develop and the old products longer to die than was originally believed. Comments like these have been bandied about in the marketplace and trade press over the years:

- 1965—“IC manufacturers are designing capacitors and inductors out of their circuits.”
- 1967—“Conventional discrete components are dead.”
- 1969—“Conventional discrete components are holding their own, but are beginning to look less conventional.”
- 1971—“The pallbearers will have to wait a long time. Passive components are alive and well.”
- 1973—“Vendors struggle to meet soaring demands for delivery of discrete passive components.”

A long way from dead

The universal observation at the 1973 IEEE Intercon was that the predicted demise of discrete passive components had discouraged many suppliers from expanding. Then the recent upsurge in electronics sales caught them short. The result: Manufacturers have extended lead times from weeks to months. Advice to customers: Plan ahead, especially for high-quantity needs, and avoid specials.

ICs have certainly made inroads into territory occupied by low-cost, low-stability resistors and capacitors, and IC manufacturers have done their best to avoid the use of inductors and higher-valued capacitors. Yet discrete passive components continue to meet the challenge by changing form.

Changes in form, fit and function

The most obvious change has been the development of the chip, or pellet, component (Fig. 1). Capacitors were the first to take on this form
for use in hybrid ICs. Resistors followed, and now even inductors come in chip form. And chips have led to the DIP network, such as Corning's Cordip line, which uses chip resistors, capacitors and diodes to create, besides a large selection of standard networks, custom combinations of up to 20 components in a 14-pin package and 23 components in a 16-pin package. Circuit interconnections can be made internally in the Cordip line in almost unlimited combinations (Fig. 2).

Fit has also improved. However, in trying to reduce the size of a resistor drastically, the manufacturer is, of course, limited by heat-dissipation ability and permissible temperature rise. Thus further dramatic size reductions can't be expected beyond the present chips and some of the newer, tiny 1/8-W discrete units. But materials of higher dielectric constant and improved packaging methods can materially reduce capacitor sizes—with serious tradeoffs against stability, however. Inductors have also grown a bit smaller with toroids that require fewer turns of wire because of improved cores.

The functional capabilities of passive components have advanced, too—but very gradually. Film resistors can be trimmed to ±0.005% accuracy by lasers, electrolytic capacitors now have ultra-low impedance (less than 0.001 Ω at 10 kHz and less than 0.01 Ω at 1 MHz), and small toroid inductors can carry up to 60 A dc without saturation. Again, nothing really dramatic and no breakthroughs. The surprise dielectric and the super-permeability core material still elude the companies hard at work to develop them.

But improvements or not, design engineers must still specify passive components. And there is no substitute for knowledge here.

Passive, they are not

Though design engineers really know better, many have been lulled into a false belief by the very name "passive components." They accept the devices as truly passive. But are they? The capacitor, in particular, masquerades as an ideal component, and the resistor is only a step behind. But each falls short. Only the inductor seems to be correctly recognized for its deviation from the ideal.

The word passive implies that the component will not change in value with voltage, frequency, temperature, time, radiation or any other influence, and that, therefore, the current is a linear function of the voltage, according to Ohm's Law. But real capacitors are not just microfarads, and real resistors are not just ohms.

Even if a resistor were ideal with respect to all external influences, including applied voltage and current, the circuit of Fig. 3 would still be required to represent it accurately. In fact, the figure depicts a universal component that behaves as a pure resistor only at low frequencies. At high frequencies the capacitive or inductive components may provide the dominant impedance (Fig. 4). In a similar way, at high frequencies, an inductance can behave as a capacitor and a capacitor can appear as an inductance.

Manufacturers' specifications should supply enough data so design engineers can deal realistically with the nonpurity of the ohms, microfarads or henrys they are buying. Most manufacturers give merely the component's value, initial tolerance and power or voltage rating—far from enough data.

Time and stress take their toll

Good data must also include the effects of time, temperature and repeated stress. How well do these so-called passive components resist aging and mechanical rigors? Nothing lasts forever. Even granite erodes in time.

But the time and stress tolerances of passive components are all too frequently omitted from data sheets. And even when they are provided, they present problems when the user tries to draw comparisons; there are no industrywide

1. Chip components, such as American Technical Ceramics' rf capacitors, are the passive-component manufacturers' answer to IC-sized hybrid circuits.
2. For compatibility with popular DIP circuits, passive components are also packaged in DIP form, as in Corning's Cordip line. Custom network designs, and an ever expanding variety of standard configurations, are offered by several manufacturers. As many as 23 components can fit into a 16-pin package.

spec standards to define the parameters.
Along with the initial tolerance at purchase—often the only one supplied by the vendor—the following time and stress tolerances should be included on the spec sheet:
- **Shelf-storage**—Components can drift while merely waiting on the shelf, and after assembly they may drift while stored or turned off.
- **Installation-stress**—Mechanical stress or other assembly treatment, such as heat, solvents and humidity, can cause permanent value changes.
- **Load-stress**—Permanent value changes result from a component's normal or overloaded operation.

These tolerances reflect permanent changes in the value of a component from its initial value to its end-of-life value. Because not every component of a specific type will behave in exactly the same way, a single figure can represent only a dispersion—such as three standard deviations ($3\sigma$), which covers 99.7% of the resistors in a sample group. Fig. 5 shows an example of the cumulative spread of tolerance as TRW resistors progress from initial purchase to 10,000 hours, or five years, of full-power operation. Similar curves could be drawn for capacitors and inductors.

**Coefficients can cause trouble**

Adding to these permanent time and stress changes, and also often overlooked, are reversible changes represented by coefficients that are functions of temperature, voltage and current.

Components that exhibit these coefficients create harmonic distortion, or nonlinear performance. Many baffling circuit problems have been traced to a component's unsuspected sensitivity to voltage or current. Even very small coefficients can cause trouble in some demanding applications. For example, would you suspect that a supposedly passive resistor could generate harmonics or modulation products?

3. **No component can provide a pure impedance**, whether resistive, capacitive or inductive. Each one of the three passive components has, to some degree, the characteristics of the two others.

4. The impedance of composition and film resistors generally drops at higher frequencies because of capacitive shunting. Note that only the Mepco 10-Ω film resistor shows an inductive effect above 150 MHz. Wound resistors, of course, show the greatest inductive effects and film resistors the lowest capacitive effects.

Spec sheets often leave out important parameters such as these, and usually designers fail to ask about them. Yet, the universal cry from component vendors is, “Why don’t they ask?” So why not take them up on it?

**The classic mistakes are still repeated**

There are many other ways in which passive components can create problems in design. Some of the classic mistakes still made are:
- Components are often specified and operated too close to their maximum limits.
- Designers are still trapped by that word
“typical,” which can mean anything from “We once made one unit that met the specs, and we hope we can make another” to compliance with the spec by virtually every unit.

- Derating specs are often ignored.
- Designers still order parts by vendor numbers, thus cutting out competitors who may have better and cheaper products that differ only in minor aspects.

So much for general precautions. Let’s turn now to the specific types of components.

**Film resistors take over**

The common carbon-composition resistor may soon be not so common. The film resistor is overtaking it (Fig. 6)—and in the range where the composition units held dominance for so long, 5 to 20% tolerance and up to 2-W power rating.

Not only are some film types—Piher International’s carbon film, for example—about half the cost of composition types, but the film unit’s also offer four times the shelf life, less noise (roughly 0.5 µV/V), and up to 80% better temperature stability (about 180 to 500 ppm/°C for film vs 1500 to 3000 ppm/°C for composition).

Mepco/Electra’s C and CR series carbon-film resistors have low-precision characteristics that are very similar to Piher’s. And Mepco’s other film-resistor types (metal-film) occupy all the precision and temperature-coefficient ranges from semi-precision (1 to 2% tolerance) to ultra-precision (0.1% tolerance) and zero to selected plus or minus TCs. Also, Mepco’s cermet thick-film GE series provides resistance ranges of 20 to 50 MΩ.

Pyrofilm also has a line of metal-film resistors, with heavy emphasis on MIL-spec conformance. The company claims it is the first to receive approval for an extended resistance range to 15 MΩ in accordance with MIL-R-55182.

TRW/IRC touches all bases with its wide range of types from carbon-composition to wire-wound units, along with a comprehensive line of metal-film types. Many of the TRW film types overlap the Mepco line, and some extend into the ultra-precision region—such as the AR40, which has tolerances to ±0.01%, temperature coefficients in the ±2 to ±5 ppm/°C range and radial-lead mounting.

Thus the film resistor now seems to span almost the total range of resistor applications. Even the power region above 5 W isn’t holding firm against it. Caddock is offering precision, power film resistors for ratings to 15 W with ±1% tolerances.

Caddock’s newest noninductive thick-film resistor line embodies an interesting idea. Until recently, some of the company’s axial-lead film resistors were fabricated with resistive patterns in a helical pattern, to obtain the needed length. But a helix is a highly inductive pattern that can cause problems at high frequencies. Even patterns that are opposingly wound from both ends to the middle, don’t cancel the inductance fully. Caddock therefore hit upon the serpentine pattern (Fig. 7). Opposing flux fields, which are generated by adjacent and closely spaced paths, can more effectively cancel each other. Therefore the resistors have about the same inductance as a straight piece of wire of the same length.

In the area of ultra-ultra precise resistors—with ±0.005% tolerances and TCs of ±1 ppm/°C—Vishay offers a proprietary bulk metal-film type, with some styles direct replacements for wire-wound units. By eliminating such stresses as drawing, winding and stretching—as required in wire-wound resistor manufacturing—Vishay reports that it obtains exceptional stability for this series of resistors. Shelf life of 25 ppm for one year is reported, along with a load life of 0.03% for 2000 hours at 125 °C and generally superior over-all performance. Care is taken so that the resistor material is maintained stress-free during manufacturing. And after final assembly, the resistor is protected by mounting it
in shock-absorbing insulation. In addition the
temperature coefficients of expansion of the vari­
ous materials used to construct the resistor are
matched to minimize deformation of the
resistors.

A thick-film cermet resistor technique is used
to make Bourns' rather different selectable fixed
resistor, the SFR 4002 (Fig. 8). With soldered
jumpers, you can select 90 resistance values with
a 1% definition in a single unit. With only 15
units, you can cover the 33-Ω-to-1.25 MΩ range
in 1% steps, the equivalent of 1350 resistance
values. Selectable fixed resistors can replace vari­
able potentiometers and trimmers in those
adjust-and-forget applications.

Resistor networks spurt ahead

The fastest riser among passive component
products is the resistance network in a DIP. For
example, Beckman's Helipot Div. offers a new
specialty—the Series 898 terminator line, de­
dsigned for the ECL lines of almost all IC manu­
facturers. CTS Microelectronics takes a more
general route with its cermet resistor modules.
CTS has 35 units in its 760 DIP series for pull-up
or pull-down resistors, terminator networks, volt­
age dividers, independent resistors and other
possible network combinations.

And HyComp concentrates on d/a precision
networks. About 13 different styles cover the
HC/HCN line—from 12-bit weighted ladder units
to three-decade BCD ladder networks. HyComp
points out that you can get much better toler­
ances by specifying ratios rather than absolute
resistance values. In d/a ladder networks it is
the ratios that really count.

Sprague, RCL, Ultronix, TRW (Fig. 9), Mepco
types. TRW's charts show the wide range of character­
istics that its various lines cover. Film resistors appear
to overlap more of the ranges than any other type.

and almost every other resistor manufacturer
offers a line of networks—most in DIP, others
in various multipinned packages—to your speci­
fications.

The network-packaged resistor is, of course, a
result of the impact of the dual-inline packaging
explosion which provides component mounting,
wiring and appearance that is compatible with
DIP ICs, like the popular 7400 series.

Chip resistors for microcircuits

The irresistible pressure to small size for
microcircuit applications is met by chip resistors
which are small indeed. Hybrex's 10-Ω-to-511-kΩ
units occupy only 30 by 30 mils of area, with
higher values to 1.6 MΩ in a 50-by-50 mil size.
Power ratings are 250 mW, and the dielectric
breakdown from the chip to its substrate is 400
V. Tolerances are 1, 5 or 10%. The temperature
coefficient, formerly a problem with most re­
sistor chips, is now only ±50 ppm/°C for values
above 1000 Ω in the Hybrex units.

And RCL offers a larger chip of 0.5 by 0.5 by
0.062 inch in its C-1 series—which, surprisingly,
can handle 23 W. The secret of the high-power
capability is, of course, intimate contact with the
large heat-sinking substrate to which it must be
mounted. The heat sink must be maintained at
below 75 C. The C-1 units have a ±5% standard
tolerance and a TC of ±100 ppm/°C.

Pyrofilm, too, recently introduced a chip-re­
sistor line. Some types handle up to 20 W and
operate to 12.4 GHz.

But discrete resistor chips must compete with
integrated, thick or thin-film resistors that are
fabricated directly on the substrate. This seems
to be the cheaper method for now, since laser
trimming methods can economically produce very accurate integrated resistors.

**Capacitor chips are preferred**

But with capacitors, the chip prevails. Integrated capacitors made from semiconductor material, as in some monolithic ICs, tend to be very unstable. And even though circuit designers devote considerable effort to eliminating capacitors from their designs, the resulting cure is often worse than the original problem. Thus discrete capacitors appear here to stay, even in microcircuits.

Capacitors can be made small for IC-sized structures if high-K materials, thin dielectrics and even thinner metal-film plates are used. But high-K materials and good stability don’t go hand in hand. High K also produces high loss at high frequencies.

Thus for rf work, where small valued capacitor chips (1 to 500 pF, with typical dimensions of 50 by 80 by 50 mils) are usually sufficient, low-loss porcelain dielectrics are used for frequencies well through the X band. At audio frequencies, chips having titanate-ceramic dielectrics with Ks to 50,000 can provide roughly 100 to 50,000 pF; these chips are 30 to 240 mils square and 50 mils thick. And for those audio-filtering, decoupling and low-frequency bypassing applications, tantalum chip capacitors fill the bill; they cover a range of values from 0.1 to 100 µF. A 2.2 µF chip measures about 50 by 50 by 100 mils.

American Technical Ceramics specializes in rf capacitors. To educate users, ATC has put together “The RF Capacitor Handbook,” which has an excellent collection of articles, design aids, charts and graphs.

Dielectric materials for rf capacitors should be vitreous and nonporous, ATC says. The company uses porcelain, and the best chip shape, the company adds, is cubic, to minimize the L-to-C ratio. Such items as the capacitor’s Q and its equivalent-series inductance and resistance become especially important in the specification of an rf capacitor. And a few seldom considered effects, such as a piezoelectric coefficient or capacitor hysteresis (nonretrace of a capacitor’s value with temperature), may be important, too, in some high-frequency applications. In addition, of course, temperature coefficient, insulation resistance, voltage rating, temperature range and shelf life are all vital.

Vitramon, another vendor with a line of special microwave chip capacitors, warns against failure to consider aging when capacitors are selected. In an interesting paper entitled “Ceramic Chip Capacitor Reliability,” Vitramon provides details of life testing, age-acceleration methods and environmental testing. The paper is free.

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**7. Caddock’s serpentine film resistors** have a minimum of inductance—little more than that of a wire the length of the resistor.

**8. For those set-once-and-forget applications, Bourn’s SFR selectable, fixed resistors provide a definition of 1% and a resistance range of 33 Ω to 1.25 MΩ with only 15 units.**

**9. Resistor networks,** such as these TRW TanFilm units, are filling industry needs for package-compatible components for hybrid and DIP configured circuits.
Terminations for chip components come in a variety of styles, as illustrated by American Technical Ceramics’ rf capacitors.

General-purpose, chip capacitors from USCC/Centralab fill a wide range of af and rf applications.

Both ATC and Vitramon emphasize that chip terminations (Fig. 10) must be rugged enough to withstand assembly and soldering stresses. Part of the problem here results from differences in the coefficient of expansion of chips, terminating materials, bonding material and the mounting substrate. Another factor is the leaching away of the termination metal during soldering.

General-purpose ceramic-chip capacitors (Fig. 11) are supplied by many vendors including Vitramon, Johanson Manufacturing, Centralab, Erie Tech and Republic Electronics. But though ceramic dielectrics provide high K, you will have to compromise on stability and a poor temperature coefficient. For example, high-K ceramic chip capacitors have a TC of 2000 ±400 to 5600 ±1000 ppm/°C compared with 0 ±30 to 90 ±20 ppm/°C for microwave chips.

National Components Industry specializes in tantalum capacitors in all styles and sizes, as you will quickly find out when you reach for its 162-page catalog. On p. 107 you find its Blue Chip, solid-electrolyte chip line. But before you reach for the order pad and expect off-the-shelf delivery, be warned. The company’s sales manager, Jerry R. Behrens, advises: “Tantalum capacitors will continue in short supply for at least the next 12 to 18 months.” Selection of standard values available at distributors is recommended.

NCI’s Blue Chip line covers sizes from 0.1 µF to 100 µF, voltages from 4 to 50 V, tolerances of ±5% to ±20% and an operating temperature range of -55 to 85 °C.

Conventional capacitor styles survive

In conventional styles, the capacitors of 25 years ago have not changed dramatically (see capacitor-selection chart). The medium-sized, wound, tubular capacitors of yesterday used a paper dielectric for af bypass and coupling work, but today plastic dielectrics and metallized-plastic films have largely superseded paper and reduced the capacitor’s volume by more than 50% in some cases. The wound construction also is giving way. Siemens’ MKM capacitors use a stacked, metallized-polycarbonate film formed into compact, mechanically stable blocks, which further reduces size. Values range from 0.001 to 0.68 µF, with tolerances to ±5% and maximum rated voltages of 100 and 200 V.

Another company, S & EI, also offers a line of metallized-polycarbonate capacitors that emphasizes size reduction. Since low voltages are used for semiconductor devices, the thinner dielectrics permit S & EI to produce a 50-V dc capacitor that is roughly a third the size of more conventional units. For instance, its 20-µF unit is only 0.62 inch in diameter and 1.68 inch long. This is quite small for a 20-µF nonpolarized capacitor.

And mica capacitors are still being made, but they are smaller and generally for lower voltages than in the past. The old molded postage-stamp style has been replaced by the dipped-mica package, such as Cornell-Dubilier’s CD units (Fig. 12).

Since semiconductor circuits are characterized by lower impedances and lower voltages than vacuum-tube designs, capacitor styles and values should be changed accordingly, manufacturers advise. However, both the military and industry often use standards that reflect the high-imped-
Dipped silvered mica-dielectric capacitors, such as Cornell-Dubilier’s CD units, provide more capacitance in less space than the old postage-stamp types, and with better stability, tolerances and Q ratings.

ance, high-voltage requirements of vacuum-tube days. Such old-fashioned rules can lead to unnecessary costs and poor designs according to Matt Simon, assistant marketing manager of AVX Ceramics.

Simon warns of another problem: Some designers insist on specifying ceramic disc capacitors with high Ks, because of their small size, and end up with circuit instability. They do this, he notes, even though in many cases the space for larger and more stable lower-K units is available in the design.

"Because of the versatile nature of ceramics, competitors try to outspec one another," Simon says, but many manufacturers are "trying hard to educate" designers.

Digital circuitry with its many bypassing needs, has provided an enormous market for ceramic disc capacitors. Because most digital equipment operates at room temperature, and tight tolerances and high stability are not required, the bypass function is easily fulfilled by the ceramic capacitor. The result: Multilayer, high-K ceramic capacitors are very popular in the computer industry. For instance, the 0.1-µF, Z5U capacitor is a standard bypass unit used in million quantities. A single computer installation can use as many as 50,000 capacitors of this one size. Companies like AVX, Centralab, Mepco and Siemens, among others, offer ceramic capacitors.

Sprague’s stacked-foil, aluminum electrolytic is a good example of a functional improvement in a conventional passive components. Internal impedance is reduced to below 0.001 Ω and inductance to less than 2 nH—well below most other electrolytic capacitors.
Gradual, almost imperceptible improvements in electrolytic capacitors continue. Packages and seals get better and sizes slowly shrink, but the changes are quite undramatic. However, two new items are worth mentioning.

**Electrolytics are also getting better**

First, there is Sprague's Type 432D stacked-foil aluminum electrolytic capacitor for ultralow-impedance applications (Fig. 13). Capacitors to 100,000 µF, with 5-to-50 V ratings have typical equivalent-series resistances of less than 0.001 Ω at about 10 kHz, and all ratings are guaranteed to have less than 2-nH inductance. Also, maximum safe ripple currents run in the 10-to-50-A range at 85 C. Data-processing, power-supply systems are particularly good applications for these capacitors.

The second new development is Cornell-Dubilier's low-inductance type-UFT aluminum-electrolytic capacitor. A rather interesting four-terminal, feed-through construction produces a decrease in impedance at frequencies above 10 kHz, rather than the usual increase for two-terminal electrolytics. The capacitor forms an H filter configuration, with the four leads. In this way, the capacitor's own internal impedance, even though it is of conventional proportions, has a reduced effect at the higher frequencies. Cornell-Dubilier's No. 1 designer kit, "Low-Inductance Electrolytic Capacitors," explains all the details. The capacitors come in sizes to 16,000 µF at 5 V dc, and to 320 µF at 200-V-dc ratings.

When price is all important, the engineer should select an aluminum electrolytic. If size is the prime consideration, a tantalum is best. For low impedances, of course, the wet electrolytic is the one to use. And solid tantalums are a poor choice for heavy current-surge applications. Wet units, both aluminum and tantalum, also handle reverse voltages better than do solids. But reverse-voltage applications need special considerations that are rarely mentioned in spec sheets. Ask the vendor for his recommendations.

**Use ac-rated capacitors for ac operation**

The reverse-voltage problem brings us to Electro Cube. One of its major capacitor lines is designated specifically for ac operation. F. L. Johnson of Electro Cube puts it this way: "While it is a fact that there are many de-designed and rated units that can, and do, operate satisfactorily in some ac circuits, this fact is a result of a fortunate coincidence for that particular instance."

The use of a dc-voltage rating that is higher than the expected peak ac is not necessarily a solution to the problem. Besides voltage-gradient stress, ac on a capacitor generates other stresses, such as internal heating and tiny corona discharges, which can rapidly cause failure in dc capacitors. Electro Cube's Technical Bulletins 07 and 08 explain what happens in ac-operated capacitors.

The company's ac capacitors are metallized polycarbonate types in a variety of styles. Capacitances range from 0.01 to 2.0 µF in most, and their rating is 115 V ac (rms) at 400 Hz.

While hybrid and IC-circuit designers have been trying to minimize use of capacitors, they have gone all out to eliminate the inductor completely. This attitude has carried over from pre-
IC days, and it has been reinforced by the difficulty of making integrated inductors. This has forced engineers to come up with ways to synthesize the effect of inductance without the use of a real inductive component.

**Inductors are down but not out**

Active RC circuits and mechanical resonators made of quartz or ceramic materials can be packaged in smaller sizes than equivalent tuned circuits that contain inductors. A great deal of research has also gone into new, promising frequency-selective packages—like thermoelectric filters, gyra-tor circuits and resonant-gate FETs. And because of the economics of IC production, several pn junctions are often more economical than a single inductor. Further, although the resulting circuit may seem more complex, the space requirements without an inductor can be less.

But magnetic-component makers are fighting back. They say that a single passive inductive component is more reliable, more stable and can take more extremes of environment than a complex semiconductor circuit. Thus magnetic components are often preferred to active semiconductor circuits for military, space and other high-reliability, high-stability applications. Inductors are more resistant to nuclear radiation, and some core materials give excellent performance over wide temperature ranges.

**Inductor chips help comeback**

Printed-circuit inductors have been used for many years, but they have, hitherto, been limited to only a few microhenries.

In response, San Fernando Electric Manufacturing has developed an unusual chip inductor, the Magna-Chip. The unit is formed from a stack of U-shaped conductor patterns that are screened onto ferrite tape material. The stacked patterns allow inductance that is three orders of magnitude greater than a single-layer PC inductor occupying the same area. Inductances range from 0.2 to 5 µH, and the Q is specified to have a minimum of 20 over roughly 10 to 25 MHz, with a temperature coefficient of less than 500 ppm/°C from -55 to 125°C. The current rating is 1 A at 0.3 W.

Almost any method of bonding or attachment to the precious-metal terminations is possible, and the company says the unit is "virtually indestructible up to 1500° F because of its monolithic fused construction." All this in an 80-mil cube.

Another chip inductor, Vanguard's Super-Q, occupies 0.16 by 0.125 by 0.125 inch, but can provide inductances from 0.1 µH to 10000 µH and Qs from about 25 to 80. For instance, a 10-µH unit lists a Q of 70 at a test frequency of 7.9 MHz, and a 10,000 µH unit lists the Q at 55 at 0.25 MHz. Rated currents vary from 3 mA for the 100,000 µH unit to 750 mA for the 0.10 µH.

The Super-Q's package is suitable for reflow-soldering assembly and can be handled by automatic-insertion equipment. The unit is enclosed in an all-welded housing to resist moisture, and it has an operating temperature range from -55 to 125°C.

**The larger inductors are still around**

To improve the normally sized inductor, many magnetic-component makers have been experimenting with core materials to raise permeabilities and saturation levels and to reduce size. New core shapes are also being offered to overcome the winding problems of toroidal shapes, but the changes have provided marginal improvements so far.

A recent innovation is National Micronetics' new line of SN coils (Fig. 14). They feature a powdered-iron core with exceptionally high-saturation flux densities ranging to 15,000 gauss—which is four to five times greater than the rating of conventional ferrite-core material. The high-saturation feature makes these coils particularly suitable for applications where high-level dc must pass through the coil.

The SN coils come in 36 standard configurations and can carry from 2 to 60 A without saturation. One important application for the coils is in noise-filtering circuits for power lines and in circuits that use thyristors, relays and other switching devices. Besides the improved performance, National Micronetics says that the SN units are less expensive than conventional ferrite or tape-wound cores.

(cont inued on page 66)
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- SN54S/74S66 Quad Exclusive-OR
- SN54S/74S135 Quad Exclusive-OR/NOR
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- SN54S/74S182 Carry look-ahead for SN54S/74S181
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- SN54S/74S03 Quad 2-input NAND gate, o.c. output
- SN54S/74S04 Hex inverter
- SN54S/74S05 Hex inverter, o.c. output
- SN54S/74S10 Triple 3-input NAND gate
- SN54S/74S11 Triple 3-input AND gate
- SN54S/74S15 Triple 3-input AND gate, o.c. output
- SN54S/74S20 Dual 4-input NAND gate
- SN54S/74S22 Dual 4-input NAND gate, o.c. output
- SN54S/74S260 Dual 5-input NAND gate
- SN54S/74S261 Dual 5-input NAND gate
- SN54S/74S262 Dual 5-input NOR gate
- SN54S/74S263 Dual 5-input NOR gate
- SN54S/74S265 Dual 5-input AND-OR-INVERT gate

**Recent introductions**

For new 54S/74S applications report, Bulletin CA-176, write on company letterhead to Texas Instruments Incorporated, P.O. Box 5012, M/S 308, Dallas, Texas 75222.
Be on guard when using DVMs. Noise can lead to erroneous readings. Combat it with the proper rejection technique and correct hook-up of the voltmeter.

Like most sensitive, high-resolution instruments, digital voltmeters are prone to erroneous readings from noise at the input terminals. This becomes especially severe in system applications of DVMs, where leads tend to get long and coupling between adjacent leads is common.

To avoid erroneous readings—and to prevent possible damage to the DVM—the user must do two things: First, select a DVM that can handle the anticipated sources and types of noise. Second, know how to connect the DVM input terminals to the measurement points. To do these two things, it's important to understand both the noise mechanism and the measures taken by manufacturers to protect DVMs from both damage and errors.

Two error modes exist

Noise can be split into two general modes, depending on its origin relative to the DVM signal input lines: (1) Normal-mode noise, which enters with, and is superimposed on, the signal to be measured, and (2) Common-mode noise, which is common to both the high and low signal inputs.

Normal-mode noise may stem from power-line pickup and stray electromagnetic fields, or it may originate within the device being measured. Whatever its origin or mode, noise can take on many forms—such as sinusoids, spikes or even white noise.

If there is such a thing as typical noise, it might look like that depicted in Fig. 1. Here, a periodic ripple, combined with noise spikes, is superimposed on a dc signal. Such noise can cause errors of 100% or more in a typical DVM, unless the instrument is protected in some way.

Two techniques are used to reduce normal-mode noise: integration and filtering. In integration a measurement is made over a fixed time interval during which unwanted amplitude variations are averaged out. If the integration period includes an integral number of periodic noise cycles, the noise will be averaged out to zero.

Larry Potter, Product Manager, DVMs, Hewlett-Packard, Loveland Instrument Div., Loveland, Colo. 80573.
For example, a DVM with a 1 / 60th-second integration period would average out one 60-Hz noise cycle, two 120-Hz cycles, four 240-Hz cycles, etc. In North America, the line frequency is subject to short-term frequency fluctuations, typically less than ±0.15%. An integrating DVM with a 1 / 60th-second integration period achieves 56 dB of rejection for a 0.15% deviation from 60 Hz (Fig. 2). This magnitude of rejection is more than adequate for most measurements.

In the filtering technique, ac noise is rejected or attenuated by one or more active filters in a DVM's front end. But DVMs using such filters become progressively slower with increasing amounts of filtering. Quite often different degrees of filtering are switch-selectable, thus giving the user the flexibility of trading noise rejection for measurement speed (see table).

An obvious question is, Which technique is better? The answer depends on the type of noise expected. Integration is better for rejecting line-related noise; filtering is better for broadband noise.

Take two DVMs with almost identical characteristics, except for the noise rejection technique (Fig. 3). Both instruments have a reading speed of, say, two to three readings per second. Note that the integrating DVM has a 1 / 10th-second integration period, with cusps at 10, 20, 30 Hz and higher. At 60 Hz, integration gives higher rejection. But to either side of 60 Hz, filtering wins out.

For the “typical” noise (Fig. 1), part is periodic and part is random, or non-line-related. A combination of both filtering and integration might work best in this situation.

Common-mode noise is hard to eliminate

Floating dc-voltage measurements are usually plagued by common-mode noise. Often this noise is ac line-related noise stemming from grounding differences between the DVM and the voltage source being measured. The magnitude of common-mode noise can range from a few millivolts to hundreds of volts.

Common-mode currents usually cannot be eliminated by the DVM, but they can be made to flow around the measuring circuit. In this regard, a DVM's first line of defense is passive shielding. However, once the common-mode current gets into the input terminals, the DVM's normal-mode rejection becomes the second line of defense.

A floating input is one in which the low input terminal is isolated from ground (Fig. 4). In this case there are now two potential sources of noise: one from grounding differences ($E_{cm1}$) and the other from the floating measurement ($E_{cm2}$).

A floating DVM significantly reduces the errors of common-mode currents, because $Z_2$ is usually high. In other words, the instrument's low input is well isolated from the ground. However, since

![Diagram of noise sources and DVM](image)

4. Two sources of noise—$E_{cm1}$ and $E_{cm2}$—can appear in a floating measurement, in which neither source terminal is grounded.

### How to specify CMR

Rejection of either normal-mode or common-mode noise is specified in decibels as follows:

$$\text{dB} = 20 \log \frac{\text{noise voltage}}{\text{voltage error}}$$

Both the numerator and the denominator must be measured in the same way. For example, if a 10-V peak noise signal is applied to a DVM and its readout deviates 100-µV peak, the noise rejection equals 100 dB. The calculation is as follows:

$$20 \log \frac{10 \text{ V peak}}{100 \times 10^{-6} \text{ V peak}} = 100 \text{ dB}.$$ 

This measurement is usually made with zero signal input, so that any observed deviation is roughly zero. The noise affects the DVM by introducing changes in the last digit or digits. By looking for the maximum excursion in the display, the user can determine the peak voltage error.

The CMR specification includes the condition of a 1-kΩ unbalance in the low lead, which represents the worst case between the two leads. This lead resistance is critical to common-mode rejection. If its size is decreased by a decade to 100 Ω, the common-mode rejection appears to improve by 20 dB.

There are really two types of common-mode rejection. The ratio, in decibels, of the common-mode signal to the normal-mode signal it produces is pure CMR and results strictly from shielding or guarding. The effective CMR is a combination of pure CMR and NMR, and this is what actually affects a reading.
good instrument design will keep $Z_1$ and $Z_3$ higher than $Z_2$, most of the common-mode current will still flow through the low input-lead resistance, $R_b$.

The floating connection is usually satisfactory for bench DVMs. But for DVMs used in a system—especially where resolution and sensitivity are important—the floating input may not yield enough common-mode noise rejection (CMR).

This is especially true for transducer bridge measurements, where the output level may be in millivolts and the source resistance may be high. To increase CMR in such cases, an additional shield—called a guard—is used around the measuring circuit. The guard is brought out to the front panel as an additional terminal.

A guard effectively increases the impedance between the low input and ground, thereby reducing the effect of common-mode currents. The real strength in guarding, however, comes from what the guard can do if it is properly connected to the circuit being measured.

Contrasting connections (Fig. 5) show how the guard works. The situation in Fig. 5a is similar to that of the floating input, except that the low-to-ground impedance is higher. In the second connection (Fig. 5b), the guard shunts common-mode currents at the source. Here, the current caused by $E_{cm}$ finds a path through $Z_4$, the path of least resistance. The low input and guard are kept at about the same potential, so little current flows through $Z_2$.

**Use the guard terminal**

For best results, the guard terminal should always be used. Here are rules for connecting the guard:

1. Connect the guard so that it and the low terminal are at the same voltage, or as close to it as possible.
2. Connect the guard so that no common-mode current or guard current flows through any resistance across the input terminals (especially the low source resistance).

Physically the guard is nothing more than a sheet-metal box surrounding the measuring circuits, and itself surrounded, in turn, by the outer chassis of the DVM. The guard shield often passes through the windings of the power transformer. Information generated “in-guard” must be passed “out-guard” in a manner that maintains isolation: for example, via pulse transformers, reed relays or photo-isolators (Fig. 6).

Sometimes a pulse transformer is time-shared for a two-way flow of information. At other times the reading is passed serially and reconstructed on the out-guard side to reduce the number of pulse transformers.

It’s not enough to know just the basic rules for connecting a guard. For instance, there are three ways to connect a guard to a source (Fig. 7). The device being measured in the figure is assumed to be a floating dc power supply with low source resistance. Lead resistances $R_a$ and $R_b$ form the bulk of the source resistance.

Of the three connections, the top one is the best. The guard here is at practically the same potential as the low input terminal and no common-mode current passes through $R_a$ or $R_b$.

In the middle example, the bar provided with most DVMs is used to short the guard to low. This is the easiest connection, and may very well be the one most commonly used. Although low

**Tradeoffs: CMRR vs reading speed for a typical DVM**

<table>
<thead>
<tr>
<th>Filter position</th>
<th>60-Hz rejection</th>
<th>Readings/second</th>
</tr>
</thead>
<tbody>
<tr>
<td>Out</td>
<td>None</td>
<td>1000</td>
</tr>
<tr>
<td>A</td>
<td>&gt; 30 dB</td>
<td>5</td>
</tr>
<tr>
<td>B</td>
<td>&gt; 80 dB</td>
<td>1</td>
</tr>
</tbody>
</table>

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*Electronics Design 12, June 7, 1973*
6. Guard-shield isolation must be maintained when information is passed from one side of the guard to the other. Pulse transformers are often used for this.

and guard are at the same potential, all of the common-mode current flows through $R_b$. The drop across $R_b$ becomes part of the input signal and must be rejected by the DVM as a normal-mode signal. Also, since $Z_2$ is shorted and the low-to-ground impedance is lower than in the top connection, more common-mode current flows. In a system where the leads are long, the value of $R_b$ becomes significant. The middle example, then, is not a good way to connect the guard.

The lower example gives two additional connections. The solid line shows the guard connected at the source's ground. This can be a good connection because it shunts common-mode currents originating between the grounds. However, guard and low may not end up at the same potential. And common-mode currents originating within the source would not be shunted away from $R_b$.

Note, too, that on most DVMs the breakdown voltage between guard and low is usually a lot less than that between guard and chassis. This may impose a limitation on the measurement.

The dotted line in the lower figure shows the guard shorted to chassis. Again, the impedance between low and ground is reduced by shorting $Z_3$.

There is one other alternative—leave the guard open. Just about any connection is better than this. The values of $Z_2$ and $Z_3$ are usually unequal, and if a floating measurement is made, the guard will seek its own division ratio. A 500-V floating measurement could easily result in over 200 V between the guard and low. This would damage many DVMs.

7. A source and guard can be connected in three ways. In the preferred connection (a), no common-mode current flows through $R_a$ or $R_b$. In the other two connections (b, c), some current may flow in $R_b$. **
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Build stable frequency synthesizers
by using off-the-shelf ICs in a phase-locked-loop configuration with variable-modulus control.

If the design calls for many narrowly spaced, stable frequency channels—and today’s communications systems often do—don’t use a collection of quartz-crystal oscillators to generate the frequencies. With the availability of suitable, inexpensive ICs, a more economical approach is now possible.

With a single crystal and a few ICs, all the channels for any system can be generated easily, with a stability approaching that of crystals and with minimum complexity and size. This approach makes use of the newer synthesizer circuits, which employ phase-locked loops (PLLs). And the relative simplicity of these circuits eliminates the need for extensive production testing and alignment.

Such circuitry is needed in systems intended for operation in the FM band, with its 100 channels spaced 200 kHz apart over an 88-to-108-MHz span. Another example is the Citizens Band, with its 23 channels occupying the spectrum between 26.96 and 27.23 MHz.

The traditional way of generating the various frequencies with the required accuracy is to use a quartz crystal—usually with a multiplier chain to bring the crystal into the 10-to-50-MHz range. For just one or a few channels, this is an economical and proven route. But a large number of channels would require a correspondingly large number of crystals, with attendant high circuit costs. Therefore phase-locked loop synthesizers using ICs usually provide a better approach.

Building a PLL frequency synthesizer

A basic PLL circuit is shown in Fig. 1a. The VCO output frequency need not be the same as the input frequency. All we really have to do is compare a reference frequency to some frequency that is representative of the output. Thus we can use any harmonic or subharmonic of the VCO’s frequency.

One good way to do this is to add a suitable digital divide-by-N circuit between the VCO and the phase detector (Fig. 1b). Suppose we use a 1-MHz crystal as the reference and let N = 10. Then the VCO should run at 10 MHz. If it deviates from this frequency, the resulting error voltage will force it back to the desired 10-MHz output.

But suppose we vary N. Then we can generate a wide range of frequencies, depending on the VCO’s range. The long-term stability of every output frequency will be as good as that of the crystal, while the short-term settling time and noise will be determined by the filter and the
VCO stability, over the temperature range.

If we were interested in building an accurate 1-to-10-MHz signal generator, we could do it with a circuit like that shown in Fig. 1c. This circuit would generate around 9000 discrete frequencies under direct crystal control. For instance, if we use a 1-kHz reference derived from the crystal, and if we set our thumbwheel switches to 4531, the output frequency will be 4.531 MHz.

By suitable switching, we can generate any megahertz-range frequency with a 1-kHz resolution. One obvious use for such a device is in ham radio, where the 40, 80 and 160-meter bands can be covered and crystal stability can be achieved on any 1-kHz frequency increment in any band. By offsetting the switch settings properly, we can easily allow for the receiver's intermediate-frequency difference. Typically, three ICs would be needed for the divider, one for the phase detector and one or two for the VCO. Thus the whole circuit can be built for the price of a few crystals. A similar PLL synthesizer system can be used for an airborne direction finder.

Using the PLL approach with hf and vhf circuits

Unfortunately it is not very reasonable to extend this technique to circuits operating at several megahertz. While the VCO poses no problem, the divide-by-N becomes difficult. Thus in our 10-MHz synthesizer, the divide-by-N counter had around 100 $\mu$s in which to re-enter the number to be divided. But for a frequency range of, say, 148 to 172 MHz, we have less than 6.7 ns in which to determine that the counter has finished its sequence and to set up a new division sequence. While 100 $\mu$s is feasible for this type of circuit, 7 ns is not.

Before turning our attention to a new and versatile approach—variable-modulus synthesis—it will be useful to consider a few other accepted methods for solving this divide-by-N problem. One obvious one is to run the VCO at one-ninth the output frequency and add two triplers in series with the output (Fig. 2a). The triplers multiply the VCO frequency by nine, while the VCO and the dividers operate in the 10-to-20-MHz range.

But there are several disadvantages. The tripler design gets sticky, particularly if we need bandwidth—and we are back with analog circuitry and production adjustments. We do, of course, eliminate the need for high-frequency dividers, thus reducing our power requirements. But we also increase the noise and settling time of the loop, since it now takes nine times as long to get an error signal as it did before.

Another traditional method employs a mixer to add a high-frequency offset (Fig. 2b). For instance, if we are covering a 148-to-172-MHz range, we might use a 140-MHz offset and have the basic synthesizer cover frequencies from 8 to 32 MHz. But this technique involves a high-frequency reference and a mixer output filter—meaning more analog circuitry and production problems with calibration and alignment. However, we have eliminated the need for division of the reference (which is now set to the channel separation), so that errors are corrected nine times faster, and we thus have a tighter and cleaner loop.

Another variation of the same approach is to mix down (Fig. 2c). The only difference here is that the VCO now runs at the output frequency. For instance, the VCO could cover the 148-to-172-MHz range, while the 140-MHz offset would reduce the divide-by-N frequency to 8 to 32 MHz. We have exactly the same advantages and disadvantages as when mixing up. However, the VCO design is usually simpler, because the circuit uses smaller components and it operates over a narrower bandwidth.

Neither of the mixing schemes requires high-frequency, premium ICs, and neither consumes the supply power required by other circuits. Thus
either of the mixing circuits represents a good approach when micropower operation is essential, such as in portable equipment.

One of the newer approaches (Fig. 2d) is to prescale the VCO output with a high-frequency counter and then use a low-frequency divide-by-N. Prescaling by a factor of 10 is popular.

In Fig. 2d the high-frequency prescaler is an ECL device (MC1678). It divides by 10, and thus reduces the frequency seen by the divide-by-N to 17 MHz or less. The rest of the divide-by-N can be built with low-cost TTL or CMOS programmable dividers. The only two real disadvantages of this circuit are the need to divide the reference by 10 and the fact that we sample the error only one-tenth as often as we would like to (which leads to more noise and longer settling times).

Variable-modulus prescaling does the trick

Looking at Fig. 2d, we see that if we could trick the high-frequency prescaler into doing more than one task at one time, we could eliminate the need for the extra divide-by-10 section. This would also improve the error and noise performance of the circuit by a factor of 10.

Thus suppose that, instead of a divide-by-10, we use a prescaler that we could teach to divide either by 10 or 11 (Fig. 3a). Also, suppose that the input to the divide-by-11 persists for \( A \) cycles and is then switched to the divide-by-10 for the rest of the divide-by-N sequence. Furthermore, for each \( A \) cycle, one extra count is added to the total division—that is, if \( N = 40 \) and \( A = 3 \), the high-frequency prescaler cycles four times. During the first three cycles it runs for 11 counts each; in the final cycle it runs for 10 counts. The total is 43 counts. If \( N = 40 \) and \( A = 2 \), we get \((11 + 11 + 10 + 10) = 42 \) counts. Similar \( N \) and \( A \) sequencing is used to produce other needed total counts.

For every 10 \( N \) counts, \( A \) extra counts are generated. The output frequency is:

\[ f_{\text{out}} = (10N + A)f_{\text{in}}. \]

Thus we see that division by any \( N \) is possible and is not limited to the decade increments, as is the case with straight high-frequency prescaling. With the variable-modulus method (using the MC12012, for example), error detection and correction run 10 times faster—even with a single high-speed, high-current divider. A control IC (such as the MC12014) is required for sequencing the high-speed divider and to change from a divide-by-11 to a divide-by-10 count. But this command is needed only once for each divide-by-N sequence; consequently it does not present any speed problems.

A frequency synthesizer using the variable-modulus approach (Fig. 3b) has two counters: an \( A \) and an \( N \). Both start out in the zero state. The controller lets the two-modulus scaler run as a divide-by-11 counter for \( A \) counts. After \( A \) counts, the \( A \)-counter reaches zero and is held in the reset condition by the controller. The variable modulus prescaler is then switched to divide by 10 for the rest of the \( N \) count sequence. At the end of \( N \) counts, counter \( A \) is released and the sequence repeats.

Thus the variable-modulus synthesizer uses only two high-frequency ICs, eliminates the division below the channel spacing and gives us the best possible error-response time. There is, however, one restriction with this method: \( N \) must be greater than \( 10A \).

One minor problem is that the numbers on the thumbwheel switches may not correspond to the numbers required for the division, particularly if we are dealing with channel numbers instead of actual frequencies. One way to overcome this problem is with special switches.

A more universal solution is to use a read-only memory (ROM) as a look-up table to change from numbers that mean something to the operator to numbers that mean something to the synthesizer (Fig. 3c). Ordinary BCD thumbwheel switches can then be used.
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Unconventional uses for IC timers can be found everywhere. Build anything from car tachometers to program controllers with these simple devices.

Timing functions are at work everywhere—in monostable multivibrators, voltage-to-pulse-duration circuits, speed-warning devices, error-detector circuits, liquid-level detectors, display-time controls, motor-speed controls, car tachometer circuits and, of course, in electronic timers. In whatever form they appear, timers are important elements in signal-conditioning and control.

Until recently, bulky thermal relays and electromechanical devices have dominated this field. Now the 555 monolithic timer IC is available from several manufacturers in an eight-pin DIP for less than a dollar. This circuit largely overcomes the size, weight and cost limitations of other timing devices.

Low-cost IC timers are opening up many unusual applications where it would have been impractical to use older devices. One cost-sensitive area is automotive electronics, where mechanical tachometers and speed controls are slowly being replaced by the solid-state devices. Instrumentation and systems control are other areas where IC timers are making inroads.

Besides low cost, the new ICs offer the following advantages:

- A time-delay repeatability of 1%
- A maximum operating frequency of 200 kHz when connected as an oscillator
- A maximum output current of 200 mA, either as a source or sink
- A delay instability of only 40 ppm/°C with temperature changes
- Operation from 4.5 to 18 V dc at a maximum current drain of 15 mA

Here are a few design examples of how IC timers can be used in new application areas.

**Speed-warning device**

To obtain speed information, an electronic pickup is mounted on the brake backing plate. A magnet, attached to the brake drum, induces trigger pulses in the pickup coil. Each time the wheel rotates, a pulse triggers the first of two timers connected as missing-pulse detectors. If the pulses occur at a low enough frequency (Fig. 2a), the output from the first timer will alternate between its high and low states. The second timer, IC2, is then driven from the output of the first (Fig. 2b). If pulses continue to appear at the input to IC2, the second detector's output remains high. When the speed setting is exceeded, pulses occur too rapidly for the RC time constant of IC1 to react, and its output remains in the high state. After the delay, this, in turn, causes the output of IC1 to go to its low state and turn on a warning indicator.

The necessary time constants can be calculated from tire size. A tire with an outer diameter of 25 inches covers a distance of \( \pi D \) or 78.5 inches. One mile per hour equals 1.467 ft/sec; hence each revolution can equate to mph. The time constant of IC1 is then calibrated to, say, multiples of 5 mph. Resistor R1 can then be either a calibrated potentiometer or several fixed resistors and a rotary switch.

**The car tachometer**

Pulses generated by the opening and closing of the distributor points are fed into the input
The 555: How it works

The 555 monolithic IC contains two comparators, a flip-flop, a high-current output stage, a voltage reference and a resistive divider. The flip-flop is controlled by the comparators, and the comparators are referenced to $V_{cc}$. Comparator II sets the initial state of the flip-flop. It is controlled by an external threshold signal (referenced to one-third of $V_{cc}$) that is applied to pin 2. The flip-flop, in turn, controls the state of the output. A negative-going pulse (of magnitude less than one-third $V_{cc}$), applied to the trigger input, sets comparator II and the flip-flop.

Two of the fundamental modes of operation are as a monostable one-shot and as a free-running multivibrator (astable). For the monostable mode, a negative going pulse from $V_{cc}$ to less than one-third of $V_{cc}$ at pin 2 changes the flip-flop state. This sends the output high and removes a short-circuit from capacitor C. The capacitor then starts charging—the time, $t_1$, required for C to charge equals $0.685(R_a + R_b)C$. When $V_c$ reaches two-thirds of $V_{cc}$, the output goes low, and C discharges through $R_b$ and pin 7 until it reaches one-third of $V_{cc}$. The discharge time, $t_2$, equals $0.685(R_bC)$. Thus the total period, T, equals $t_1 + t_2$ or $0.685$ times $(R_a + 2R_b)C$, and the frequency of oscillation is given by the inverse of T. The pulse duty cycle, D, equals $R_b$ divided by $(R_a + 2R_b)$.

of the tachometer circuit, Fig. 1, and are shaped and clamped by $R_1$ and $CR_1$. They are then passed on to the trigger terminal of the timer by $C_1$. Triggering of pin 2 causes the output of the timer to go high for a period determined by

$$T = 1.1 \times (R_C C_2)$$

During this time diode $CR_2$ is back-biased and resistors $R_4$ and $R_6$ provide a calibrated current to the meter. After the time duration elapses, pin 3 goes low, shunting all current around the meter. The ratio of the time for which current flows through the meter to the time for which it is shunted to ground provides an accurate meter reading of engine rev/min. For a V-8 engine, the frequency of pulses at the ignition points is four times the engine rev/min—since the points close eight times per revolution of the camshaft and the engine runs at twice the speed of the distributor shaft. A constant current must be applied to the meter during the one-shot period. This is supplied by the vehicle's electrical system via $R_7$, $C_3$ and a 9-V zener, $CR_3$.

**Voltage-to-pulse-duration converter**

The circuit in Fig. 3a can convert a voltage level to a pulse duration by integrating the input voltage and comparing its value with the charge...
The timer is set up so that it operates in a monostable mode when no voltage is present at the input. When the input voltage increases, the width of the output pulses increases, but the frequency of the pulse train input to pin 2 remains the same (Fig. 3b). Basically this circuit is a dual-slope integrator and has an accuracy of better than 1%. Possible uses occur in data-acquisition and telemetry.

**Servo system controller**

In the motor controller shown in Fig. 4, the transmitter consists of a timer connected as a variable-duty-cycle oscillator. Diode CR 1 and potentiometer R 1 provide the charge current to C r, which sets the duration of the positive portion of the output cycle. Potentiometer R, can vary the time duration from 1 to 2 ms. During the negative portion of the cycle, CR 1 is back-biased and a discharge time of 16 ms is set by resistor R 2.

Servo drive is generated by the IC servo-amplifier (WE3141). This IC receives the pulse-width modulation from the transmitter and compares the 1-to-2-ms pulse width with the duration of an internally generated pulse. If the pulse widths are not of equal duration, the difference is stretched and applied to the output stage of the WE3141. Depending upon whether the input pulse is longer or shorter than the generated pulse, the motor will be driven either clockwise or counterclockwise, to adjust the internal pulse width to match that of the transmitter.

Resistors R 4 and R 5 set the null point of the amplifier. The 33-Ω values allow a null period of about 4 to 5 μs. This hysteresis is necessary to prevent the system from hunting. This type of circuit is useful in a wide range of remote-control systems.

**Reference**

1. Signetics Data Sheet for NE555 timer.
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Program gives FET model from specs.
With only one simulation routine written for SCEPTRE, curves can be obtained for all characteristic regions.

When designing with the help of the computer, most engineers use several models to calculate field-effect-transistor characteristics. But with a new program, written for SCEPTRE, one model covers all regions of FET operation. And the program accepts FET parameters that are readily obtained from manufacturers' spec sheets.

The three regions of FET operation—triode, pinchoff and cutoff—are shown in Fig. 1a. To fuse the three, it's imperative that boundary transitions not overlap. Our model uses a translation technique developed from device physical characteristics to maintain piecewise continuity through all boundaries.

A complete n-channel junction-FET model is presented in Fig. 1b. For p-channel devices, all polarities and the diode are reversed. A corresponding model for MOSFETs would not require the junction diode. The FET model is valid for any gate-to-source voltage, so long as the drain-to-source voltage is less than the avalanche level.

Spec sheets provide basic input

The basic parameters, readily available from manufacturers' specification sheets, consist of the following:

- \( V_p \) = pinchoff voltage, normally given as gate-to-source cutoff voltage, \( V_{gs} \) (CUTOFF).
- \( I_{dss} \) = zero-gate-voltage drain current.
- \( G_m \) = transconductance, normally found in the form of forward transadmittance, \( Y_{gs} \).
- \( G_{gd} \) = gate-to-drain capacitance, generally given as the reverse transfer capacitance, \( C_{rgd} \).
- \( C_{gs} \), the gate-to-source capacitance, is found from the input capacitance, \( C_{iss} \), and \( C_{rss} \) from the relation \( C_{gs} = C_{iss} - C_{rss} \).
- \( G_{do} \)—the slope of the \( V_{gs} = 0 \) curve on the \( I_d \) vs \( V_{gs} \) plane—is calculated from the relation \( G_{do} = \frac{\Delta V_{ds}}{\Delta I_d} \) at \( V_{gs} = 0 \).
- \( R_s \)—the drain-to-source resistance when the FET is off—is generally so large that it can be left out with little sacrifice in accuracy. Hence it often doesn't appear on spec sheets. In our model its inclusion allows for software voltage development.

The model parameters include the following:

\[
R_s = \frac{1}{G_m}, \quad D_{gs} = \text{junction diode, and} \quad I_{dss} = \frac{1}{V_{gs}/V_p}, \quad [1 - \frac{V_{gs}}{V_p}]^2, \quad \text{the drain current at pinchoff.}
\]

Voltage \( V_{translate} = V_p - V_{gs} \), the drain voltage at pinchoff used to translate the origin of the \( V_{gs} \) curve along the pinchoff line. Resistance \( R_{ds} = \frac{1}{G_{ds}} \left( 1 - \frac{V_{gs}}{V_p} \right) \). And the triode equation, defining current \( I_{dtr} \), is given as \( I_{dtr} = \left( I_{dss} \frac{V_{ds}}{V_p} \right) \left[ 2\left( \frac{V_{gs}}{V_p} \right) - 1 \right] \).

Software selects region of operation

To apply the model, we use software to delete the parameters not being used in each region of FET operation. Boundary equations provide the criteria for switching parameters in and out. On a boundary line, either region's parameters will give identical values.

---

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The model for each region is shown in Fig. 2. The boundary equations between regions were used to derive the inequalities.

The boundaries determine how the operation point moves from one region model to another, and they also allow the region models to be fused into one FET model. The pinchoff region was modeled by use of a slope-origin translation scheme to allow the region conductance to originate at pinchoff.

**Region boundaries provide continuity**

To be piecewise continuous, the boundary between the triode and pinchoff region must have the same drain current when approached from either region. Therefore the boundary equation should evolve from simultaneous solutions for the drain-current equations for each region.

The commonly used equation for drain current at pinchoff,

$$I_d = I_{dss} \left(1 - \frac{V_{gs}}{V_p}\right)^2,$$  \hspace{1cm} (1)

is valid only for drain current at the physical pinchoff.

For a drain-current characterization that applies over the full triode region, including pinchoff, we use the following triode equation:

$$I_{dtr} = \frac{I_{dss}}{V_p} V_{ds} \left[2 \left(\frac{V_{gs}}{V_p} - 1\right) - \frac{V_{ds}}{V_p}\right].$$  \hspace{1cm} (2)

At the boundary between the triode and pinchoff region, the drain-to-source voltage is given by the following:

$$V_{ds} = V_{gs} - V_p.$$  \hspace{1cm} (3)

This equation can be derived by simultaneously solving Eqs. 1 and 2. Piecewise continuity results between regions, since both region models have identical values along the entire boundary.

The equation that defines the boundary between the pinchoff and cutoff regions is

$$V_{gs} = V_p.$$  \hspace{1cm} (4)

The slope of the characteristic curves in the pinchoff region result from space-charge limiting. The slope for these curves is modeled by conductance:

$$G_{ds} = \frac{\Delta I_d}{\Delta V_{ds}}, \quad V_{gs} = \text{constant}$$  \hspace{1cm} (5)

The slope angle differs for every constant $V_{gs}$ curve. Since an infinite number of $V_{gs}$ curves are possible, measuring all of these varying slopes is impractical. In our model, constant $V_{gs}$ curve slopes are normalized to the $V_{gs} = 0$ curve slope, defined as $G_0$, at $V_{gs} = 0$ (see Fig. 3). The value of $G_0$ can be interpolated from manufacturers’ curves.
3. **Conductance in the pinchoff region** is normalized to the $V_{gs} = 0$ curve slope, $G_0$. This conductance can be interpolated from manufacturers' curves.

4. The model for the $G_{ds}$-slope at origin variation presumes that the $G_{ds}$ curve begins at the pinchoff boundary. The difference between the actual origin and the boundary origin is accounted for by source $V$-translate.

The general conductance, $G_{ds}$, can be seen in Figs. 1 and 2 in its inverse form, $R_{ds}$, which is derived as follows: From semiconductor physics, we see that

$$G_{ds} = \frac{C_{dc} \mu_{eff}}{t} (V_{gs} - V_p),$$

where $\mu_{eff} = \text{effective channel mobility}$, $C_{dc} = \text{effective drain-channel coupling capacitance}$, $t = \text{total channel length}$ and $V_p = \text{pinchoff voltage}$.

Define $K_t = -\frac{C_{dc} \mu_{eff}}{t}$.

Then $G_{ds} = K_t (V_{gs} - V_p)$ and $G_x = K_t (-V_p)$.

Since $K_t = -\frac{G_x}{V_p}$, $G_{ds} = G_x \left(\frac{V_{gs}}{V_p} - 1\right)$.

With $R_o = 1/G_x$ and $R_{ds} = 1/G_{ds}$, we get:

$$R_{ds} = \frac{R_o}{1 - \frac{V_{gs}}{V_p}}. \quad (6)$$

The $G_{ds}$ slope does not have an origin until pinchoff, and subsequent space-charge limitation, occurs. Beginning the conductance slope at pinchoff gives a drain current defined by Eq. 1. This maintains the needed continuity along the boundary. It also means that the current $I_{ds}$ (Fig. 4) is zero at pinchoff and becomes a function of the differential voltage across $R_{ds}$ beyond pinchoff. Therefore, at pinchoff, $I_d = I_{ds} \left(1 - \frac{V_{gs}/V_p}{V_{ds}/R_{ds}}\right) + \Delta V_{ds}/R_{ds}$.

Since the point at which pinchoff is reached varies for different values of $V_{gs}$, every $V_{gs}$ curve will have its own origin. And the origins translate along the pinchoff boundary line for a changing $V_{gs}$.

5. The origin of any $V_{gs}$ curve is set at the pinchoff boundary to maintain the needed continuity along the boundary. Voltage source $V_{dspx}$ is used to account for the difference between this origin and the actual one.

To derive this translation, the origin of any $V_{gs}$ curve is set at the pinchoff boundary, with the difference taken up by voltage source $V_{dspx}$ (see Fig. 5).

In the following development for the origin translation, subscript $p$ denotes a value along the pinchoff boundary. Subscript $x$ denotes a value on the $V_{gs} = x$ curve.

Given any $I_i$ in the pinchoff region,

$$I_{dsx} = I_{dspx} + \Delta I_{dx}.$$

Since slope $G_x = \frac{\Delta I_{dx}}{\Delta V_{dsx}}$, then

$$\Delta I_{dx} = G_x \cdot \Delta V_{dsx} \text{ and } \Delta V_{dsx} = V_{dspx} - V_{dspx}.$$

Combining the last two equations gives

$$\Delta I_{dx} = G_x (V_{dsx} - V_{dspx}).$$

Combining this with the first equation gives

$$I_i = I_{dspx} + G_x (V_{dsx} - V_{dspx}). \quad (7)$$

This equation shows the need for two branches in our modeling scheme. The first is $I_{dspx}$, which is the drain current at pinchoff, as described by Eq. 1 (it is shown in Figs. 1 and 4 as $I_d$). The second part of the equation—$G_x (V_{dsx} - V_{dspx})$—describes a current caused by drain-to-source voltage, translated by $V_{dspx}$, through a conductance, $G_x$.

Voltage $V_{dspx}$ refers to the drain voltage at pinchoff, which is described by Eq. 3 as $V_p - V_{gs}$. The translation of the drain-to-source voltage across $R_{ds}$ is accomplished by $V$-translate in Fig. 4.

If we neglect stray capacitance and assume that the total input capacitance is lumped as gate-to-drain and gate-to-source capacitance, we find...
SCEPTRE listing calculates $I_d$ vs $V_{ds}$

SCEPTRE’s commonly used computer-aided circuit design program can be used to generate $I_d$-vs-$V_{ds}$ curves for constant $V_{gs}$. The program listing is shown in Fig. 6, with the accompanying schematic illustrating the software development.

In the schematic, the following applies: RSHT is a short-circuit resistor to sample $I_d$ for display, EDS sweeps the drain-to-source voltage for a curve-tracer mode display; EGI sets the $V_{gs}$ voltage for each sweep, and JFET, ETRAN and RDS depend on the region of operation.

Switching software in the program makes JFET become $I_d$, in the pinchoff region and $I_{tri}$ in the triode region. ETRAN is shorted out in the cutoff and triode regions and becomes V-transform in the pinchoff region. RDS becomes a finite $R_{ds}$ only in the pinchoff region. And PSIGN reverses the generator when the FET is used in the reverse mode—that is, when EDS goes negative.

Three regions of operation are obtained with a special software switching scheme that was used to stay in the SCEPTRE format. In the pinchoff region, for example, $|V_{rd}| \geq |V_{CGS}-PVP|$ and $V_{CGS} < PVP$. Moreover $P1 = 1$, $P2 = 0$, and $P3 = 0$.

In the switching scheme, PA gives a positive value in the pinchoff region and a negative value in the triode region. $P1B$ will be 0 if PA is negative; otherwise it will be a very large positive value. P1 uses $P1B$ in an exponential to switch. If $P1B$ is 0, then $P1 = 0$, and if $P1B$ is a very large positive value, then $P1 = 1$, as required for the triode region.

The parameters in this region are given by the following: $PJJ = I_{dp}, PR1 = R_{ds}$ and $PRD = 1/G_{dm}$. The switching conversion criterion is controlled by PERROR.

References:
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INFORMATION RETRIEVAL NUMBER 154
Consider the part-time engineer, says this small-company manager. You can use him effectively if you learn to use technicians as project ‘finishers.’

Small electronics companies—those grossing $1-million to $10-million a year—usually can’t afford the salaries of senior engineering talent or the time to train new engineering graduates properly. But they have a good alternative: They can hire engineers who have been in the field for three or four years and are extremely competent—but who want to work part-time only.

That’s only half the battle, however. Using part-time engineers presents two major problems to management: completing projects on time and building an R&D capability. To meet these challenges, it’s necessary to employ the second half of the one-two engineering punch for small companies: Use the part-time engineers strictly for the creative aspects of the project, and let technicians carry the work to completion as “product finishers.”

I once got a call from an engineer I was ready to hire. He told me that he wanted to work only 25 to 30 hours a week so he’d have enough time to counsel drug addicts. Right then I realized that for a company our size to complete a project successfully, we’d have to organize the schedule so that the person in charge could finish it without spending his life on it.

Some small companies might be able to do this by using a lot of part-timers, but that depends on whether the company is in an area where technical talent is plentiful. Our company is situated where the pool of technical talent is not very deep.

The part-time engineers who are available to us are professionals who want to design exclusively. They’re interested in a small-company atmosphere, and they like a great deal of freedom to come and go as they please. They like to choose the projects they work on, and they like to see the results of their work quickly. We recently hired two designers who had one or two years in a large company and who didn’t want to get stuck with the red tape of a project.

How did I use these designers effectively?

A senior manager of the local technical community gave me an idea. He said that one problem small-to-medium electronics manufacturers had was that they didn’t train people to do their jobs. They always go out and look for someone to fit the job.

Refining the raw talent

So I got to thinking that it would be a very good investment for us to train people off the assembly line or from the test department—people who weren’t engineers but who had the raw talent to carry a program or at least to work into a technical position. I figured they’d be a great help to engineers who didn’t want project responsibility after they had completed the design function.

So we organized into two-man project teams, with a technician (called a product engineer) and a designer on each team. The technician typically did not have a degree. This spot could be handled by a draftsman or a mechanical engineer. The basic qualifications were these: He should be capable of mechanical and printed-circuit design. And while he could not design circuits, he should be able to read and draw schematics for a simple d-to-a converter—a typical product that a company like ours makes.

Today our product engineer follows up all those detail jobs that the designer is usually heir to. He buys the parts for the product, calls meetings, orders the PC boards, checks the accuracy of the art work on the PC boards and, in general, helps keep the designer on schedule.

Prior to this system we had virtually no support for the designer, just a pool of service. Now, for each designer, we assign two men through the design phase. The third man handles product releases. He takes the product at the conclusion of the second pilot run.

When the breadboard is complete, the product engineer starts taking control of the project by acquiring the material for the prototype. The designer does the actual evaluation and investigation of the prototype, while the product engineer virtually peers over his shoulder, writing down changes and updating the paperwork and order-

Donald L. Peinetti, Director of Engineering, Zeltex, Inc., Concord, Calif. 94520.
ing parts for the second prototype. The second prototype should be a finished product, barring really serious design problems. Depending on the project, we may make as many as 10 to 15 prototypes units.

Then we go into our first “A” revision of all the documents. The product engineer sees that these documents are filed as a revision “A” for pilot production only. The product engineer sees further that the first pilot run is billed under an engineering number, which joins the finished-goods inventory at the completion of the pilot run. The product engineer organizes the assembly labor and sees that all of the test equipment is available. He also assists in testing the product with a third member of the team who is now added—another technician. The designer will have been assigned another project by now.

Wherever there are changes in documents, the product engineer makes sure that the changes are incorporated into the product for the second pilot run. He also makes sure that the long-lead parts for it are on order, and he transfers the second pilot run to what we call a release-product group. The technician of this group keeps track of component evaluation and does most of the testing. He sees that the second pilot run gets built in manufacturing.

Before the product engineer leaves the project, he stocks replacement parts and files the documents.

The part-time designer is also the key to building up the company’s R&D potential. With his creative freedom, he can concentrate on the innovative, while the technician follows through on the nitty-gritty of building the prototype.

Whether building an established product or developing a new one, the designer—or project engineer—is the only one who is an electronics engineer; he phases out of the project earlier than he used to because others are doing the “finishing” work.

Benefits of the system

The other people were always here; they aren’t new people. They’re just taking on more responsibility. They did the same jobs before but they weren’t responsible for them in any kind of time frame. Now they’re more responsible to the project. In the past the design engineer had to see that all the finishing work was done. The product engineer would do the work when he was told, but he was never motivated to do the work on his own.

The new system has other benefits, too.

It allows more people to become involved in the project.

It gives the manager visibility on the projects. I can go to the product engineers of each project to see how a project is going. And I can get schedules from a man who’s more interested in drawing them up than the designer was.

It allows the part-time designer freedom to design. In the old days when I worked as a project engineer, I ran around all day, shuffling papers and getting parts ordered and checking to see if Joe was making boards for me and checking to see if the girl on the line could build them for me. Then I spent all night designing the circuit. Now, the engineer with the camper can design in his garage if he wants to. • •

Education: San Diego State College, math and physics; graduate studies in electronics engineering.

Responsibility: Direct electronic, process and mechanical engineering efforts in the development of hybrid and modular amplifiers and conversion products.

Experience: Ten years electronics engineering including three years engineering management. Lectured in solid-state oscillator design. Developed 24 solid-state electronic test instruments including function generators, oscillators and measurement equipment. Designed 17 amplifiers, analog-to-digital and digital-to-analog conversion products.

Personal: Married; two children, a boy 10 and a girl 9. Hobbies include handball and golf.

Employer: Zeltex, Inc., was founded in 1962 as a manufacturer of analog computer components. It pioneered the manufacturing of general purpose modular operational amplifiers. In recent years it has become a leader in modular a/d and d/a conversion products.
Delco’s new DTS-4000 series Darlings with \( V_{CEO} \)s of 400V and 600V are triple diffused mesa units built for rugged duty. They come to you with a practical 15 Ampere rating that you can depend on all the way up to the high voltage requirements of ac motor speed controls, for instance—or the 1.5 kW switching regulator in the illustration.

And they offer new possibilities in circuit design where dc drive conditions may have created awkward problems when using SCR’s.

Our new Darlings can save you space and give you more design flexibility. The high energy capability of the DTS-4000 series is

<table>
<thead>
<tr>
<th>TYPE</th>
<th>( V_{CEO} )</th>
<th>( I_C ) (Cont.)</th>
<th>( V_{CEO} ) (Max.)</th>
<th>( V_{CEO(sus)} )</th>
<th>( I_C ) (com. base)</th>
<th>( P_D ) (max.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>DTS-4040</td>
<td>400V</td>
<td>15A</td>
<td>20V</td>
<td>325V</td>
<td>250/3A</td>
<td>0.25( \mu s ) 100W</td>
</tr>
<tr>
<td>DTS-4045</td>
<td>400V</td>
<td>15A</td>
<td>20V</td>
<td>325V</td>
<td>500/3A</td>
<td>0.25( \mu s ) 100W</td>
</tr>
<tr>
<td>DTS-4060</td>
<td>600V</td>
<td>15A</td>
<td>20V</td>
<td>400V</td>
<td>250/3A</td>
<td>0.25( \mu s ) 100W</td>
</tr>
<tr>
<td>DTS-4065</td>
<td>600V</td>
<td>15A</td>
<td>20V</td>
<td>400V</td>
<td>500/3A</td>
<td>0.25( \mu s ) 100W</td>
</tr>
</tbody>
</table>

NPN—Triple diffused Darlington transistors packaged in solid copper TO-204MA (TO-3) cases.
backed by safe operating curves up to 600 volts, as shown at left. And to further aid your circuit design $h_{FE}$ is plotted continuously from 15mA to the maximum collector current rating of 15A.

As you expected, the new DTS-4000's are in stock and ready for delivery. Contact us or your nearest Delco distributor for complete details. Ask for Application Note 52 on the switching regulator.

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Optical isolators provide diverse functions in signal-detector circuit

Optical isolators provide a simple way to detect ultrasonic frequencies. And the isolators can also be used for other circuit functions.

A bandpass filter (Fig. 1) extracts the desired range of frequencies from a wideband input signal. The LM318H op amp delivers an output signal like that shown in Fig. 2a. This signal is then full-wave rectified by the light-emitting diodes in the optical isolators. Since the op amp delivers a bipolar signal, the LEDs will be successively turned on with increasing intensity up to a predetermined maximum. Therefore the phototransistors, too, are successively driven harder and harder into conduction. This in turn causes the 0.1-µF capacitor to charge up to the trigger level of the voltage comparator (Fig. 2b). Once the voltage comparator triggers, the NAND gate (or other TTL logic) is enabled, and an indicator can be activated.

When there is no input signal in the filter passband, the emitter-follower phototransistor pair presents a low output impedance and the 0.1-µF capacitor discharges very rapidly.

Compared with conventional detectors, this circuit eliminates the two 0.7-V diode drops that would be present in each branch of a full-wave rectifier. Also, it avoids the need for special high-frequency transformers.


CHECK NO. 311

2. Typical output signal from the bandpass filter (a) contains only the desired ultrasonic frequencies. Peak-detector output voltage (b) builds until it reaches $V_{REF}$, the trigger level of the comparator.

1. Ultrasonic detector with optical isolators avoids need for a transformer and bridge rectifier.
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Model 4228-N

1. 2½ digits — Provides double the accuracy (0.25% of reading ± ½ digit) and double the resolution at lower cost.

2. Instantaneous Response — 16-millisecond display rate with 60 times per second sampling rate.

3. Foot-proof Numeral display blurs beyond over-range and with negative polarity.

The Model 4228-N is a real value at $140, so call your local Triplet Sales/Service/Modification Center or Triplet sales representative right now. Either will also be pleased to demonstrate two companion products: Triplet's Model 4225-N at $125 which merely omits the neon lamp “1” (thus reading to 995) and offers ± 0.50% ± 1 digit accuracy; and the Model 4220-N at $110 — a 2-digit instrument (reading to 99) with ± 1% ± 1 digit accuracy.

Mounted in the same size case and boasting the same low power consumption and positive over-range indication, Triplet's 3½-digit Model 4235-F adds auto-polarity (with polarity indication) display hold capability, high input resistance (from 10 to 1,000 megohms depending on range) and a 3½-digit single-plane seven-bar fluorescent display. For many users, the wide-angle viewing capability — enhanced by a green, circularly-polarized viewing window that eliminates confusing internal reflections — will make the 4235-F the obvious choice.

Boasting a voltage accuracy of ± 0.10% (current ± 0.15%) of reading ± 1 digit, Triplet's Model 4235-F sells for $240. Its companion, the 3-digit Model 4230-F is $220. More information, or a free demonstration of both models, is available from your Triplet Sales / Service / Modification Center or your Triplet sales representative. Triplet Corporation, Bluffton, Ohio 45817.

TRIPLETT
Manufacturers of the World’s most complete line of V-O-Ms.
Use a 723 as a switching regulator and get half an amp from a plastic TO-5 transistor

Convert batteries, op-amp supplies or MOS supplies into +5 V to drive TTL or DTL circuitry. By using a µA723 IC regulator and some other components, you can build a switching regulator that is immune to overloads and short-circuits, free of starting overshoot and undervoltage burnout, and has an efficiency of more than 70%.

The circuit shown is designed for a nominal load current of 0.5 A, but it can deliver from 150 mA to a 1 A maximum—at which point it current-limits. Input voltages can range from 9.5 to 40 V.

The output current is limited by Q2, which senses the voltage across R1. The hysteresis provided by positive feedback at the emitter of Q2 keeps Q1 switching under overload or short-circuit conditions. Because it continues to switch at moderate rates and current levels, Q1 rides through load faults and startup transients. The current limit also prevents startup output overshoot.

The current-limit transistor built into the µA723 controls the drive to Q1. This drive, set by R1, varies with the regulator output load to maximize operating efficiency.

Resistor R5 also provides a main control-loop signal that is proportional to the current ramp in L1. Thus operating frequency and peak transistor currents are almost unaffected by any load capacitance in parallel with C5.

Diode CR2 in the reference-voltage feedback path fixes the amplitude of the control-loop hysteresis voltage and makes it independent of the input voltage. The combination of this fixed hysteresis with the inductor current feedback through C5 stabilizes the operating frequency. As a result, the frequency changes by less than 2 to 1, while the input voltage varies by more than 4 to 1.

At any given input voltage, the operating frequency is an inverse function of the inductance of L1. The inductor may be modified to vary the operating frequency if sufficient current-carrying capacity is provided. The unit described here operates between 4 and 8 kHz. The inductor begins to saturate above 500-mA output current; therefore the frequency will increase for heavy loading. Saturation is gradual, so the current-limit circuit retains control. Winding the inductor with fewer turns of larger-gauge wire will result in better high-current performance, but at the expense of higher operating frequency and reduced efficiency at lower currents.

The resistor values shown provide a nominal output of 5 V. Resistor tolerances and individual differences in µA723 ICs can cause an unacceptable regulated voltage. The optional resistor, Rs, can be connected to raise or lower the output voltage, as required. The value given for Rs should, when properly connected, bring the regulator into the voltage range required for TTL. By making Rs a "select-at-test" component, you can trim the regulator output to a tighter tolerance.

A. Paul Brokaw, Group Leader for Advanced Development, Nova Devices, Inc., 829 Woburn St., Wilmington, Mass. 01887. **CHECK NO. 312**
The DigiTec line of digital voltmeters offers a selection that will enable you to choose the perfect instrument for your needs. Each unit provides its own special features. You select the instrument that has the functions you require, and you'll pay for only the useful features you want. For digital voltmeters with guarded inputs, isolated BCD outputs, LED displays and basic accuracy of .02%, you can select from:

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Low-temperature-coefficient current source becomes ultra-compliant with two resistors

New low-voltage, low-temperature-coefficient reference diodes are making it possible to perform circuit functions that previously would have been awkward or impossible to do. Among these are high voltage-compliance, low-temperature-coefficient current sources that can take advantage of the low reference voltage to improve circuit efficiency.

Shown in Fig. 1 is a basic high-compliance current regulator, arranged to source current and operate from a single supply. The current $I_s$ supplied by transistor $Q_i$ is $V_{ref}$ divided by $R_i$, where $V_{ref}$ is the 1.2-V breakdown voltage of $CR_1$.

The availability of the low reference voltage allows the voltage compliance of $Q_i$ to be maximized through an increase in the portion of the supply voltage made available to the load. In this case the compliance is

$$V_{comp} = V_{cc} - (1.2 V + V_{CE(sat)} Q_i).$$

If a low-saturation voltage transistor is used for $Q_i$, the loss of voltage will be negligible in comparison with the 1.2 V dropped across $R_i$.

An ultra-high-compliance version of this circuit can be built if the 1.2 V reference is reduced to an even lower potential to decrease further the drop across $R_i$. This is shown in Fig. 2. Resistors $R_s$ and $R_r$ reduce the reference voltage applied to the op amp, $A_{op}$, to 120 mV. This is possible with the 101A op amp because it continues to operate linearly as its positive common-mode range extends to the supply potential. This allows $R_i$ to drop only 120 mV for regulation of $I_s$.

In both circuits the level-shift zener, $CR_2$, is used to ensure turn-off of $Q_i$, since the output swing of $A_{op}$ does not reach a sufficiently positive voltage to drive $Q_i$ directly.

This technique reduces the loss of compliance to a point where the regulation drop and the $V_{CE(sat)}$ of $Q_i$ are comparable. A side benefit of the low reference voltage is the decrease in power dissipated by $R_i$. This enhances the resistor’s stability and makes selection easier.

Reference


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Electronic Design 12, June 7, 1973

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No-contact dc transformer measures high bus currents

Here’s a tough problem: Measure a bipolar dc current of up to 10,000 A without breaking or touching the line and without loading. And do this to within a linearity of 0.015% and with a circuit that’s not affected by temperature changes, line-voltage variations, magnetic fields or aging.

The Transrex Div. of Gulton Industries solves the problem with its Transrector—a dc-current transformer that uses bias and feedback windings to achieve the desired performance.

As shown in the figure, the Transrector has seven windings. They are as follows:

- Two pairs of toroidal, or main, windings that measure the magnitude and direction of the dc current by sensing the magnetic field produced by the monitored current.
- A pair of bias windings that allow the output of the main windings to be a balanced, differential voltage. This cancels temperature drift, noise, line-voltage changes and other undesirable variations.
- A feedback winding that reduces the operating flux levels and thereby makes it possible to monitor large currents within the linear core region.

The two toroidal windings of each main pair are connected in opposition and excited by an ac source \( E_{ac} \). When dc current flows in the bus, one core becomes magnetically saturated, while the other remains in the linear region. These magnetic states alternate with each half-cycle of the supply frequency.

The current in the toroidal windings is given by \( I_s = I_{bus}/N \), where \( N \) is the number of turns on each toroid. A second winding, called the bias, is added to each core pair.

Bias current flows in a direction that enhances the magnetic effect in one pair of cores and reduces the effect in the other. The output signal, \( E_o \), is taken as the difference between the voltages of each core pair, and its polarity thus depends on the direction of the bus current.

With this configuration, the transfer curve, \( E_o \) vs \( I_{bus} \), flattens at high current levels. To extend the linear region, a third winding, called the feedback winding, is added to the cores.

Voltage \( E_o \) is now applied to a high-gain amplifier, whose output is connected to the feedback winding. As a result, \( E_o \) is driven to null. Any undesirable variations in the difference voltage produce a large feedback current, which unbalances the core pairs in a direction that minimizes the variations and restores \( E_o \) to null. Consequently the feedback current is proportional to the dc-bus current.

The technique achieves high isolation, since there is only magnetic coupling between the dc bus and the measuring head, not direct contact. In addition tight coupling between the bus and head produces fast response: The 3-dB bandwidth is 1000 Hz.
WORLD'S FIRST PRODUCTION CCD
Our 500-Element Linear Image Sensor: World's First Production CCD.


The CCD101 Linear Image Sensor uses charge-coupled technology and a buried-channel structure to create a rugged, monolithic, self-scanned, 500-element sensor designed for high sensitivity conversion of images to analog signals. For slow-scan TV, facsimile, and other high-resolution linear imaging applications. The impact of CCD on imaging is analogous to that of the transistor on vacuum tubes. It has been called by one high-level government scientist "the most important breakthrough in semiconductors since the development of MOS."

CCD101 Linear Image Sensor

The array is a 500-element photo-sensing chip, 60 x 635 mils. It includes, in addition, charge transfer gates, two 250-element CCD analog shift registers, a 2-element output register, and a preamplifier. The device allows sequential reading of the 500 imaging elements with a typical dynamic range of 1000:1 at 1 MHz. Sensitivity is typically 15 x 10^6 footcandle-seconds. Operating voltages are under 20V. On-chip preamplifier allows a low-impedance interface. The 24-lead dual in-line ceramic package—1 ¼" long x ½" wide x ½" high—has a sealed anti-reflectance glass window and non-reflective interior.

99.999% Transfer Efficiency

Key to CCD101 high sensitivity imaging is the buried channel structure which reduces charge-transfer loss, thus permitting greater image element density. The result is demonstrated above. The 4 photos illustrate the device's capacity for generating a clear video picture of a single frame at
widely varying levels of illumination. The photos show the face of a CRT displaying the output of a CCD101 sensor clocked at 1 MHz scanning a black-and-white photo on a rotating drum. Increasingly dense filters were inserted between the sensor and the scanned photo. The intensity dropped, but the image remained usable.

CCD Imaging Advantages
CCD technology provides the first high-performance method for solid state imaging. The CCD101 is the first CCD product, and thus the first to clearly demonstrate its high performance advantages, high reliability and dimensional accuracy, with lower noise video, low-voltage operation and self-scanning that eliminates much external control circuitry. All made possible by our CCD buried N-channel technology.

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**Monolithic s/d converter boasts high reliability**


Monolithic analog switches, linear ICs, MSI logic and thin-film resistor networks have been combined by Analog Devices to produce the SDC series—a new family of reliable synchro-to-digital and digital-to-synchro converters. The company has calculated a 200,000-hour MTBF, at 25 °C, for the 1602—the 400-Hz, 14-bit member of the tracking s/d family.

Eight basic models are offered, with price depending on the choice of resolution, the temperature range and the frequency. For example, the 14-bit unit—operating over the standard 0 to 70 °C range—costs $680. A 10-bit version, the 1604, is identical to the 1602 except for resolution. The 1604 sells for $480.

Either unit can be ordered at additional cost for 60-Hz operation, or with an extended temperature range of −55 to +125 °C.

The 14-bit 1602 has a listed accuracy of ±4 minutes of arc, while the 10-bit 1604 is accurate to ±30 minutes. And the stated accuracy applies not only over the temperature range but also for variations of ±10% in signal and reference amplitude, for variations of ±10% in reference frequency, for 10% harmonic distortion in signal and reference, and for ±5% power-supply variations. The tracking rate of both models is specified as 1440 deg/sec.

Although they are a new product line for Analog Devices, tracking s/d converters in modular form are offered by at least a dozen manufacturers, including North Atlantic Industries and ILC Data Device Corp. In fact, the Analog’s SDC appears to be pin-for-pin compatible with DDC’s ESDC series. However, Analog Devices appears to be the first to use monolithic, rather than discrete, circuitry in its converters.

DDC’s 14-bit version, the ESDC H3, tracks at 360 deg/sec, has 4-minute accuracy and sells for $695.

North Atlantic’s Series 780 is another competing module that has 14-bit resolution, ±3-minute accuracy and a tracking speed of 4000 deg/sec. It sells for about $650.

Other features and specs of Analog’s SDC series include an acceleration of 180 deg/s² for an error of 1 LSB, a 179-degree step response of 300 ms for a 1-LSB error and a power dissipation of 2.5 W, maximum. The outputs are TTL/DTL-compatible, with a fanout of four TTL loads. The seven-ounce 1602 measures 3-1/8 × 2-3/8 × 0.8-in.

For Analog Devices **CHECK NO. 250**

For ILC Data Device **CHECK NO. 251**

For North Atlantic Industries **CHECK NO. 252**

---

**Temperature controller is compact and accurate**

*Heinemann Electric, 132 Magnetic Dr., Trenton, N.J. 08602. (609) 882-4800. $37.50 (50 up).*

The model-TB temperature controller is a 4.4-in² board with built-in power supply and triac output, matched precision setpoint potentiometer, dial-plate, and encapsulated RTD sensor. The unit operates from any 120/240 V, 60-Hz power source. Controlling range is from room ambient temperature to 650 °F using the 100 Ω nickel RTD sensor—but can be extended to 1000 °F by substituting an optional platinum sensor. Sensors can be remote-located up to 200 ft from the control module. With “burst-fire” proportioning the unit can remain stable to within 0.1 °F for 24 h at ambient temperatures to 130 °F. Accuracy is unaffected by voltage variations from +10% to −15%. Setpoint resolution is 0.5% of full-scale; setpoint control is a single-turn, 280 Ω, 3-W pot supplied with the controller.

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2021 W. Valley View
Dallas, Texas 75234
Phone: 214/243-4321
TWX: 910/860-5542

INFORMATION RETRIEVAL NUMBER 52

MODULES & SUBASSEMBLIES

Peak detectors have adjustable hold time


The MDL2 series will hold a peak reading on a DVM or DPM for an adjustable time period after occurrence of the peak value. The series includes models MDL2-20MV-1, MDL2-100MV-1, MDL2-1V-1, MDL2-10V-1 and MDL2-100V-1, with ranges of 20 mV, 100 mV, 1 V, 10 V and 100 V dc, respectively. All models have hold times that are variable to 10 s or infinite, automatic or manual reset, max operating temperature of 50°C, and input impedance of 10 Mn min. Dimensions are 4-1/4 w x 7-1/4 l x 1-3/4 h in.

CHECK NO. 254

Replace many interface modules by one package

Analogic, Audubon Rd., Wakefield, Mass. 01880. (617) 246-0300. $695; 4 to 6 wk.

The MP6912 12-bit a/d system provides all the scanning, signal-conditioning, a/d-conversion and program/control/timing circuitry needed for multichannel, high-speed operation. Maximum resolution/throughput combinations on the MP6912 are 100 kHz for 12-bits or 500 kHz for 4-bits. The module is 0.375 in. high, thus compatible with the 0.5 in. card spacing of most racks. Internal shielding from electromagnetic and electrostatic interference allows close proximity to high-energy noise sources. The MP6912 can operate in the “overlap” mode, permitting selection of a new channel while the analog value from the preceding sample is being held for conversion.

CHECK NO. 255

Digital lock uses a five-digit enabling code

Elesis Laboratory, P.O. Box 387, Chillicothe, Ohio 45601. (614) 773-1414. $40 complete system (1-9); stock to 3 wk.

The series-L “Touch-Latch” system consists of an input keyboard and an epoxy encapsulated control module, interconnected by a 12-conductor cable of convenient length. A pin-plug termination at the module end permits the user to program a five-digit enabling code. Both a momentary output (high while the last code digit remains depressed) and a latched output are provided. The system operates from a +5-V-de supply or from any supply between +6 and +30 V with the addition of an external resistor.

CHECK NO. 257
NOW MAKE THE BIG MOVE TO MINIATURIZATION WITH CUTLER-HAMMER.

As you miniaturize your products, rely on these space-saving new Cutler-Hammer ultra-miniature switches. They deliver additional quality, together with a full choice of style, color, and shape.

You get full current-carrying capacity at 115 V.A-c in toggles or pushbuttons. One or two poles in 5 different circuits.

Superior construction details include: a 1/4-inch bushing for convenient one-hole mounting, silver-alloy contacts with initial contact resistance of only 0.010 ohm maximum, a polyestal base partially jacketed in steel for extra switch-mechanism protection, and either solder-lug or PC terminals.

Cutler-Hammer's remarkable application flexibility continues externally with a wide range of decorator caps, buttons, and bezels in many colors.

And all circuits are in stock for fast delivery.

To learn more about how this highly adaptable new line can add function and style to your products, check with your nearest Cutler-Hammer Sales Office, or Authorized Stocking Distributor.
D/a converter resolves to 16-bits for only $89

Datel, 1020 Turnpike St., Canton, Mass. 02021. (617) 828-6395. $89 (unit qty).

Model DAC-169-16 is available in either a B or D version. The B unit will convert 16-bit straight or offset binary and the D model can handle a four-digit BCD code. Both models offer either a current or voltage output and are in a 2 x 2 x 0.375 in. case. Output settling time is 750 ns or 30 µs for the current or voltage outputs, respectively. Full-scale outputs for the binary version are 0 to +10, 0 to –10, or ±5 V at ±5 mA. The current output can be selected for 0 to +2 mA or ±1 mA. In the BCD version, the voltage output can be either 0 to 10 V or 0 to –10 V at 5 mA while the current output can be pin strapped for 0 to 1.25 mA full-scale. All digital inputs are TTL/DTL compatible, and offset and gain adjustments are provided to compensate for long-term drift. Linearity of either model is ±0.005% of full scale while the temperature linearity is ±0.0005%/°C over an operating temperature range of 0 to 70°C. Accuracy is adjustable to 0.005% of full scale, and the resolution is 150 µV (1 LSB) for the binary model and 1 mV (1 LSB) for the BCD version.

CHECK NO. 259

Card switch operates 25k times before cleaning

Hickok, 10514 Dupont Ave., Cleveland, Ohio 44108. (216) 541-8060. $75 (unit qty); 30 days.

Model 50B offers 50 card-programmable contacts for economical system programming or personnel identification. The programming cards are 1-1/2 by 3-3/4 in, and are made from either Mylar or vinyl. Each card contains a 5-by-10-hole matrix on 0.25-in. centers. The switch can be programmed by punching holes in the card with a simple hand punch and will read cards 0.007 to 0.03 in. thick. Environmental operating specifications are –40 to +65°C for temperature and from 0 to 99% for humidity. The model 50B will perform more than 25,000 operations, when switching 115 V, before contact cleaning is necessary. Size of the model 50B is 1 x 2-1/8 x 3-1/2 in.

CHECK NO. 261

SPST switch driver has only 10-ns delay

LRC Inc., 11 Hazelwood Rd., Hudson, N.H. 03051. (603) 373-6930. $56 (100 qty); stock to 2 wk.

A single-pole, single-throw switch driver has less than 10-ns delay (total switching time). It is compatible with TTL logic. Model SD-1201, used with shunt and series switches, provides positive and negative outputs. Ten switches can be driven from each TTL gate. Supplied in a flatpack configuration, it meets MIL-STD-883 specifications and operates over a temperature range from –55 to +125°C.

CHECK NO. 258

Sinewave oscillators are resistively tunable

Frequency Devices, 25 Locust St., Haverhill, Mass. 01830. (617) 372-6930. $56 (100 qty); stock to 2 wk.

Series 440 quadrature oscillators are tuned by two external resistors. The oscillators provide buffered low distortion (0.08%) quadrature outputs (90° ± 0.1°) with amplitude-ratio tracking to better than 100 ppm/°C, and output amplitudes externally adjustable from 2 V to 20 V pk-pk. They are externally tunable over a 1000:1 range with 2 equal resistors. Models 440, 442 and 444 cover a total range of 0.05 Hz to 20 kHz and the maximum frequencies are 50 Hz, 500 Hz and 20 kHz, respectively.

CHECK NO. 259

CHECK NO. 260

Precision voltage-ratio dividers meet MIL specs

Singer Instrumentation, 3211 S. La Cienega, Los Angeles, Calif. 90016. (213) 870-2761.

Series-CRT coaxial ratio transformers are precision ac voltage dividers that are only 2-1/2 in. diameter (for the military version) and 3-1/2 in. (for commercial versions). All units are certified to MIL specs for vibration, shock, salt spray, fungus and humidity. Terminal linearity is from 0.001%. Accuracy is grouped in two frequency ranges and depends upon model. The two ranges are 50 to 3000 Hz and 3 to 10 kHz.

CHECK NO. 262

ANALOGY

BEAT THE BAD GUYS WITH THE A-BIGG A/D HIGH SPEED CONVERTER. RESOLVES 1:65,536 WITH CONVERSION SPEED OF 8µS. THAT'S 125,000 SAMPLES PER SECOND! TEMPERATURE STABILITY OF ±5 ppm/°C LINEARITY ±10 ppm.

INFORMATION RETRIEVAL NUMBER 54
Designing a hybrid circuit shouldn’t be all work and no play.

If you want to make sure the circuit you’ve designed really plays, you need to do more than see a schematic of it.
You need to see the real thing.
And that’s what the new KEMET® Hybrid Circuit Chip Kit allows you to do.
Containing 280 tantalum and ceramic chip capacitors with high temperature capabilities, plus supporting technical literature, it’s the industry’s first kit covering the complete capacitance range used in hybrid circuits.
All of which gives you the freedom you need to build a prototype of the schematic you’ve been working on.
So fill out the coupon and order your Chip Kit today. Or, for more information, get in touch with us at Union Carbide, Components Department, Box 5928, Greenville, S.C. 29606. Phone (803) 963-7421.
All work and no play makes a dull career.

☐ I want to play. Enclosed is $99.00 in check or money order for your KEMET Hybrid Circuit Chip Capacitor Kit.
☐ I do not wish to play right now. But please send me more information on your Chip Kit anyway.

Name ____________________________________________
Title ____________________________________________
Company _________________________________________
Street ___________________________________________
City _____________________________________________
State __________ Zip ______________

In Europe: Union Carbide Europe, S.A., 5 Rue Pedro Meylan, Geneva 17, Switzerland

INFORMATION RETRIEVAL NUMBER 55
Need rotary switches?
2-million combinations, 72-hr. delivery from your Oak Moduline™ distributor.

Quick-and-easy ordering of Oak-quality rotary switches in lots of 1 to 99. The Moduline system lets you specify switch components by number (no drawings needed). Your order is shipped within 3 days. Contact these Moduline distributors:

- **DRW**
  - MASSACHUSETTS, Watertown. (617) 922-1900*
  - NEW YORK, Farmingdale. (516) 248-2660*

- **HALL-MARK**
  - ALABAMA, Huntsville. (205) 539-0691
  - FLORIDA, Orlando. (305) 865-4020*
  - GEORGIA, Atlanta. (404) 363-9728
  - ILLINOIS, Chicago. (312) 437-8800
  - KANSAS, Kansas City. (913) 889-4747
  - KANSAS, Wichita. (316) 582-2973
  - MARYLAND, Baltimore. (301) 265-8500
  - PENNSYLVANIA, Philadelphia. (215) 355-7300
  - TEXAS, Dallas. (214) 352-2601*
  - TEXAS, Houston. (713) 785-5205
  - WISCONSIN, Milwaukee. (414) 476-1270

- **INDUSTRIAL COMPONENTS**
  - MINNESOTA, Minneapolis. (612) 925-2974
  - MINNESOTA, Minneapolis. (612) 925-2944
  - MARYLAND, Baltimore. (301) 265-8500
  - MARYLAND, Baltimore. (301) 265-8500
  - MINNESOTA, Minneapolis. (612) 925-2944
  - MISSOURI, St. Louis. (314) 521-3800
  - OHIO, Dayton. (513) 278-6963
  - OKLAHOMA, Okla. City. Enterprise 50094
  - OKLAHOMA, Tulsa. (918) 835-8458
  - PENNSYLVANIA, Philadelphia. (215) 355-7300
  - TEXAS, Austin. (512) 454-5439
  - TEXAS, Dallas. (214) 231-6111
  - TEXAS, Houston. (713) 781-6100
  - WISCONSIN, Milwaukee. (414) 476-1270

**MODULES & SUBASSEMBLIES**

Pulse-to-tone encoder is less than 0.6 in.

Alpha Electronic Services, 8431 Monroe Ave., Stanton, Calif. 90680. (714) 821-4400.

The AE-50 produces a burst of tone on any frequency between 20 and 3000 Hz. The burst or pulse duration can be varied from 100 ms to 15 s. Or the circuit can be strapped for continuous encoding. The size is 1-1/4 x 15/16 x 1/2 in. The unit works over a temperature range of -40 to +100 C; current drain is 4 mA at 12-V dc. Frequency stability is ±0.5% over the temperature range. The output level is adjustable to greater than 7 V pk-pk into a high impedance load.

Pressure sensor detects decay of 0.1 psi/min

Bourns, 1200 Columbia Ave., Riverside, Calif., 92507. (714) 684-1700.

Model 811 rapid-pressure-loss detector provides a calibrated output signal proportional to rate of change of pressure as well as a calibrated output proportional to the absolute pressure of the atmosphere within a chamber. The transducer detects pressure-decay rates of 0.1 psi/min, or greater. Signal conditioning for pressure-analog and rate-analog signals is provided within the 811 by a high density circuit. Also, a decision circuit within the instrument provides discrete relay closures when a pre-selected rate trigger level is reached.

**Digital tachometer and counter has LED display**

Airpax Electronics, 6801 W. Sunrise Blvd., Fort Lauderdale, Fla. 33313. (305) 587-1100. $275 (4-digit version); 8 to 12 wk.

The series-77 digital tachometers and counters are in 5-3/16 x 3-3/8 x 5-9/16 in. cases with unblinking LED displays. They can be used for "event-per-unit-time" (tachometer) or "accumulation" (counter) applications. The systems operate from signals produced by magnetic, analog or digital transducers and signal sources such as proximity sensors, switches, photo cells, flow meters, etc. Other specifications include: input sensitivity, 50 mV rms with adjustable threshold for noise; input frequency to 250 kHz; contact closure or standard TTL; 3-to-6 digit LED display (0.25-in. char height).
SPECTRA-BOTH

Side-Arm and Coaxial. We swing either way.

We're in two classes by ourselves. Our design capability makes us the only company that can deliver both side-arm and coaxial tubes.

If you need a tube that will go in a small package, we can provide a coaxial. If size is not a problem, we can provide a side-arm tube at considerable savings. Example: a 2.0mW, TEM00, coaxial tube in quantities is $90.00; a 2.0mW, TEM00, side-arm tube in quantities is $85.00.

Our capability gives us the broadest line of Helium/Neon plasma tubes in the business. Over 30 different standard plasma tubes, from 0.5mW to 50mW. Most off the shelf. With internal or external mirrors. All internal mirror tubes and lasers warranted for 18 months.

Moreover, if you need a Helium/Neon laser specially designed, we can design it just for you—using the same parameters that we have tested to 26,000 hours MTTF and 15,000 hours average lifetime. We can even handle such special requests as a modulated laser to 50 KHz, or a .01% noise laser, or you name it.

One more Both to brag about. We make more lasers than anybody, and so we have the expertise that brings you both high quality and low cost.

Home office: 1250 West Middlefield Road, Mountain View, CA 94040. 415/961-2550.

Spectra-Physics

INFORMATION RETRIEVAL NUMBER 57
MODULES & SUBASSEMBLIES

Keep centers even when pushbuttons are stacked

Grayhill, 565 Hillgrove Ave., La Grange, Ill. 60525. (312) 354-1040.

Six, three and one-button versions of a PC-mount push-button switch can be stacked horizontally or vertically while maintaining 11/16-in. centers between buttons. Choice of available contacts includes standard spst (N.O.) to 4pst (N.O.) sections: internally shorted sections which connect several poles in the down position; and sequential contacts which ensure that the common terminal makes last. A one-button module is 0.75-in. high off its PC board mount and 0.683-in. square. Each switch is rated to make and break 100 mA at 5 V dc, for an anticipated life of 250,000 operations.

CHECK NO. 267

THE INSIDE STORY...

ON A CONSTANT VOLTAGE TRANSFORMER THAT LOOKS AS GOOD AS IT PERFORMS.

Computer-assisted design plus quality construction. Designed to meet the requirements of UL-478 for Data Processing Equipment. For additional information contact Magnetics Division, ADC Products, or send for Bulletin 9-3.

ADC PRODUCTS
4900 West 78th Street, Minneapolis, Minnesota 55435
Tel: (612) 835-6800 — TWX: 910-576-2832 — TELEX: 29-0321

INFORMATION RETRIEVAL NUMBER 58

THE INSIDE STORY...

ON A CONSTANT VOLTAGE TRANSFORMER THAT LOOKS AS GOOD AS IT PERFORMS.

Computer-assisted design plus quality construction. Designed to meet the requirements of UL-478 for Data Processing Equipment. For additional information contact Magnetics Division, ADC Products, or send for Bulletin 9-3.

ADC PRODUCTS
4900 West 78th Street, Minneapolis, Minnesota 55435
Tel: (612) 835-6800 — TWX: 910-576-2832 — TELEX: 29-0321

INFORMATION RETRIEVAL NUMBER 58

Buy power supplies with or without transformers

Essex Data Information Systems, 17 Arthur Rd., Lincoln Park, N.J. 07035. (201) 696-8788. With transformers from $19.95 (100 up); stock.

The TS-100 series power supplies are small (4 x 4 x 2-1/2 in.) and have predrilled mounting-holes to ease installation. Five models are available. They are designated 15105, 15112, 15115, 15124, and 15212. Output voltages for these models are 5, 12, 15, 24 and ±12 V dc, respectively. Each unit has a 100,000-h MTBF, built-in short-circuit protection, current limiting, line and load regulation better than 0.2%, and a ripple voltage of 2.2 mV rms max. Overvoltage protection is available on all models. As a user option, all supplies are available with or without the transformer.

CHECK NO. 268

Functional module is a "Jack-of-all-trades"

Intech, 1220 Coleman Ave., Santa Clara, Calif. 95050. (408) 244-0500. $70 (1 to 9); stock.

A multiple-function mathematical module, the A-733, can be programmed to multiply, divide, square root, square, square of a ratio, and raise voltage ratios to an arbitrary power. The output error is essentially independent of input signal levels. Input levels from 100 mV to 10 V can be processed with a maximum output error of less than 0.5% of full scale. The module has a gain drift at full scale of ±1 mV/°C maximum and an output offset drift (at zero input) of ±1 mV/°C maximum. The A-733 is made up of four sections: a log ratio circuit, log circuit, an antilog amplifier, and a reference-voltage source.

CHECK NO. 269

INFORMATION RETRIEVAL NUMBER 58

Electronic Design 12, June 7, 1973
MULTI-CHANNEL GRAPHIC DISPLAY SYSTEMS

MULTI-TERMINAL SYSTEMS

COLOR OR GRAY SCALE DISPLAY

FORM OVERLAY DISPLAY

YOUR COMPUTER

DISPLAY GENERATOR

YOUR COMPUTER

DISPLAY GENERATOR

YOUR COMPUTER

DISPLAY GENERATOR

Choose one from column A, two from column B

Or choose all from column C, or...

Because this is a multichannel graphic display system, you can choose most any combination you wish. And like a Chinese dinner, any way you order it, you get an excellent buy.

This system uses a common display generator and a disc memory refresh to drive up to 16 independent, high resolution channels.

For multiterminal applications, use each channel to drive a low cost, daylight viewable TV monitor. Cost for a 16 terminal monochrome system, complete with 14" monitors, keyboards, and typical computer interface, works out to just under $4000/terminal.

If you want color or gray scale displays, just combine channels. Two channels give you three colors and black; four channels give you 16 colors plus black. And for a full color display (4095 levels) use twelve channels. Color can make even the most complex graphics understandable.

You can also use multiple channels for convenience in editing or data entry. Put a standard grid or form on one channel, your graph or data on another. Then superimpose the channels on a single display monitor. Because you don’t have to regenerate the grid when you change the data, you can have more efficient software.

These systems have all the capability you need for most applications—there are over ¼ million individually addressable points in the graphic display. You can selectively erase any rectangular area of the screen; write up to 51 lines of 85 alphanumeric characters. And because the displays are disc refreshed, the CPU need generate each display only once.

So think of the multichannel display system when you need computer graphics. Call your Data Disc representative for more information, or contact us at 686 West Maude Avenue, Sunnyvale, California 94086; 408 / 732-7330.

And for dessert, have a fortune cookie.
An alternative to the use of ROMs is available when the application is random logic generation or a microprogram store. A faster and more economical approach uses a bipolar programmed logic array (PLA).

National Semiconductor is offering a mask-programmable PLA in a 24-pin DIP. Depending on a user's specific requirements, the circuit accepts a number of data inputs and produces outputs each of which is represented by a logical expression with the data inputs as variables. National's PLA has up to 14 inputs and 8 outputs. Each output can contain as many as 96 partial product terms.

The circuit comes in four different versions—the DM7575/DM8575 and the DM7576/DM8576. The difference between the 75XX models and the 85XX models is that the former has conventional outputs, while the latter has inverted outputs. The XX75 models have TTL-active pullups on the outputs, whereas the XX76 models have open collector outputs. The circuits use bipolar technology which results in a 90-ns input-output delay for the PLA. Typical power dissipation is 550 mW.

The National PLAs have 2112 bits of mask-programmable memory to define the outputs. A comparable ROM to perform the same function would require 131,072 bits of memory.

If more inputs or more outputs are needed, the PLA is readily expandable. The outputs need only to be wire-ANDed together. However, regardless of the number of inputs gained through expansion, any output may still use only 14 input variables.

The arrays come in both plastic and ceramic 24-pin DIPs. Maximum storage-temperature range is -65 to +150 °C and the maximum operating temperature range is -55 to +125 °C.

The PLA requires just a single 5-V power supply. All data inputs and outputs are at TTL levels.

National plans to introduce a field programmable version of these PLAs at a later date. Some additional applications of the PLA include code conversion, address mapping in the micro-instruction control portion of a microprogrammed computer and the implementation of specialized arithmetic functions that are not readily available in integrated form.

INQUIRE DIRECT
a tool kit full of measurement solutions...

Now there's a 3-pound scope that can be carried in your tool kit, suitcase, briefcase, coat pocket, glove compartment... almost anywhere.

It's the 211, our first laboratory-quality miniscope. Size is only 3 x 5 1/4 x 9 inches. Bandwidth is 500 kHz. A lot of scope in a small package.

The 211 is easy to use. You spend your time solving measurement problems, not studying scope operation. Deflection factors from 1 mV/div and sweep rates from 5 μs/div are read out from controls easily related directly to the CRT. One rotary control does all the triggering.

Ever wanted to float a scope? Here's one that floats to 500 volts RMS when operated from its internal batteries.

Price? It's lower than you might expect. Only $545, FOB Beaverton, Oregon.

For a demo, just contact your local Tektronix Field Engineer. He probably has a 211 in his briefcase. Ask him for complete information or write Tektronix, Inc., P.O. Box 500, Beaverton, Oregon 97005. In Europe, write Tektronix Ltd., P.O. Box 36, St. Peter Port, Guernsey, C.I., U.K.
Dialight sees a need:

(Need: A large 5/8" high LED readout at a low $4.95* price.)

See Dialight.

Each digit in this bezel assembly contains a Dialight light-emitting diode, decoder/driver, and resistor network that produces a bright, highly visible readout that can be easily installed in a panel. The readout display is supplied with discrete gallium phosphide or gallium arsenide phosphide diodes arranged in a seven-segment format. These generate a bright, highly legible red character (0.625 inch high—the largest size character in the industry) with the lowest power consumption for a character of this size. Ideal for mounting on a control panel, or in a digital clock, meter, credit-card verifier, TV channel indicator, or hospital room status-board indicator. The contrast ratio between the illuminated and non-illuminated segments is further enhanced by a one-piece red nonglare window.
Dialight is a company that looks for needs and develops solutions. That’s how we developed the industry’s broadest line of LED light sources, indicator lights and readouts. No other company offers you one-stop shopping in LED visual displays. And no one has more experience in the visual display field. Dialight can help you do more with LEDs than anyone else because we have done more with them. Talk to the specialists at Dialight first. You won’t have to talk to anyone else.

Here are a few products in this family: 1. Multidigit readout assembly in 0.205” character height 2. Status display module with 6 LEDs with adjustable light cells 3. LED readout in character height 0.625” 4. Alphanumeric display complete with code generator/driver character height 0.300” 5. 5 x 7 dot matrix alphanumeric display in character height 0.300” 6. Hexadecimal display with logic character height 0.270” 7. Single digit LED readout module in 0.125” character height. 8. Numerical display with integral TTL MSI circuit chip with counter character height 0.270” 9. Single digit LED readout module in 0.270” character height (MAN 1 equiv.). *1000 lot quantity for 730-1003

Solid State Devices Inc., 14830, Valley View, La Mirada, Calif. 90638. (213) 921-9660. See text; stock to 4 wk.

Rectifiers built with a new ion-implantation process called Epion, switch currents of 1 to 30 A in 25 ns or less—reportedly five to ten times faster than other devices on the market. These switching times hold for peak reverse voltages of 10 to 100 V.

Rectifiers with six different current ratings are presently available from Solid State Devices. The 1-A model is packaged in a miniature radial-lead package. The 1.5, 3, 8, 20 and 30-A models come in stud-mounted packages. The three lowest-current models all switch in 10 ns or less, The three higher current models switch in 15, 20 and 25 ns, respectively. Forward recovery time for all models is about 1 ns, maximum.

For a 1-mA conduction, the forward threshold voltage of all types is less than 0.45 V. And, for full-rated conduction, the forward voltage drop is less than 0.95 V.

For a 1-μs surge pulse of current, the rectifiers can tolerate from a 100 A surge for the low current rectifiers to 100 A for the 30 A stud-mounting model.

The maximum storage temperature range of all models is −55 to +175 °C with a maximum operating temperature range of −55 to +150 °C. They are also said to have “high rectification efficiency” to operating frequencies of 10 MHz and above due to their very high switching speed.

Pricing varies with quantity and peak reverse voltage for each current rating. Typical prices at the 100-V, 1000-unit level vary from $4.05 for the 1-A model to $67.05 for the 30-A model.

Major areas of application for the rectifiers are expected to be high-efficiency power supplies, shunts, clamps and switching regulators.

CHECK NO. 270
HyComp Addresses the Problem of Inflation

What is better than two for the price of one?

..,_,,

~

~

Using one instead of two for the price of one!

WHEN YOU USE PRECISION THIN FILM RESISTOR LADDER NETWORKS WITH CURRENT SWITCHES AS INTERSILS 8018A THRU 8020A AND FAIRCHILD'S µA 96SO FOR A/D AND D/A CONVERSION, YOU CAN REDUCE COSTS AND SIZE SIGNIFICANTLY!

HOW? WITH HyCOMP'S HC-130 AND HC-135 SERIES 12 BIT WEIGHTED LADDER NETWORKS WHICH ARE MADE ON SINGLE 110 x 190 MIL GLASS SUBSTRATE CHIPS AND REPLACE THE PREVIOUS STANDARD TWO CHIP NETWORKS THEY PROVIDE SUPERIOR T.C. TRACKING AND OTHER CHARACTERISTICS AND COST AS LITTLE AS $24(1-9) and $17(1K). AVAILABLE IN 24 LEAD DIP OR FLAT PACK, HERMETIC OR NON-HERMETIC . . . OR IN CHIP FORM. HC-130 SERIES USED WITH INTERSIL SWITCHES. HC-135 SERIES USED WITH FAIRCHILD'S.

THE THREE DECADE BCD WEIGHTED LADDER COUNTERPARTS, DESIGNATED HC-130A AND HC-135A, HAVE THE SAME EXCELLENT SPECS AS THE OTHER HyCOMP RESISTOR LADDER NETWORKS WITH THE EXCEPTION THAT RATIO ACCURACY IS 0.05% AND MAXIMUM ACCUMULATED POSITIVE OR NEGATIVE ERROR IS 0.05% F.S.

IF THE OLD STANDARD TWO PACKAGES HAVE ALREADY BEEN FROZEN INTO YOUR DESIGNS . . . THEN USE THE HC-420 AND HC-430 SERIES WITH THE INTERSIL SWITCHES. AVAILABLE IN 14 LEAD DIP OR FLATPACK.

AND WHEN YOU USE THIN FILM R-2R LADDER NETWORKS, GET THEM ON THE SMALLEST SINGLE CHIPS AND AT THE LOWEST PRICES!

HC-1000 SERIES 12 BIT LADDER NETWORK WITH STANDARD RESISTANCE VALUES OF 5K, 10K, and 25K IN 16 LEAD DIP OR FLATPACK, HERMETIC OR NON-HERMETIC . . . OR 100 x 150 MIL CHIP AS LITTLE AS $23.20(1-99).

HC-210 SERIES 12 BIT LADDER NETWORK WITH A RESISTANCE VALUE OF 50K for MOS OR ANY ANALOG SWITCH WITH A HIGH SATURATION RESISTANCE AS LITTLE AS $25(1-99) AVAILABLE IN 16 LEAD DIP OR FLATPACK, HERMETIC OR NON-HERMETIC . . . OR 100 x 190 MIL CHIP.

SPECIFICATIONS FOR 12 BIT THIN FILM LADDER NETWORKS (unless otherwise noted).

T.C. TRACKING: < 1 PPM/°C RATIO ACCURACY: 0.01%
MAXIMUM ACCUMULATED POSITIVE OR NEGATIVE ERROR: 0.012%
10 AND 8 BIT MODELS ALSO AVAILABLE

In addition to supplying many other standard precision thin film resistor ladder networks and hybrid D/A and D/S converters with a normal delivery time of two weeks, HyComp is pleased to consider modifications to standard products and customized circuits whenever economically feasible.

HyComp

the Hybridic

Hybrid Company

146 Main Street, Box 250 Maynard, Mass. 01754 (617) 897-4578

INFORMATION RETRIEVAL NUMBER 63

ICs & SEMICONDUCTORS

MOSFETs have very low feedback capacitance

Texas Instruments, P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-2011. $0.90 (3N211 & 212), $0.95 (3N213) (100-999); stock.

Designated the 3N211, 3N212, and the 3N213, these depletion-type MOS transistors have a low feedback capacitance of 0.05 pF maximum and a high forward transconductance (g_m) of typically 25 micromhos. Typical commonsource spot-noise figure for these MOSFETs is 2 dB at 200 MHz. Power gain is 28 dB at 200 MHz. Integrated back-to-back diodes between gates and source protect inputs against static charges. The 3N211 has extremely low feedback capacitance, the 3N212 provides low-noise operation and the 3N213 has higher breakdown voltages to provide more power output for linear detection.

CHECK NO. 271

2k-bit SR has 10-MHz rate

Hughes Microelectronic Products, 500 Superior Ave., Newport Beach, Calif. 92663. (714) 548-0671. $36 (100); stock.

A 2048-bit multiplexed dynamic shift register provides a 10-MHz shifting rate over the −55 to +125 C temperature range. The new MOS circuit, called HDSR 2048, uses ion implantation to achieve its high rate and is structured as a dual 1024-bit shift register. Power dissipation is typically 300 mW at 25 C with 50% duty-cycle clocks per 1024 bits. Bipolar circuits may be driven by the 2048.

CHECK NO. 272
ECL quad D-type latch has gated outputs

Signetics, 811 E. Arques Ave., Sunnyvale, Calif. 94086. (408) 739-7700. $5.90 (100 up).

A high-speed, low-power ECL quad latch consists of four bistable latch circuits with D-type inputs and gated Q outputs. Typical clock or data-to-output time is 4.0 ns; typical enable-to-output time is 2.0 ns, and typical setup and hold time is 0.7 ns. Dissipation is typically 290 mW per package with no load. The circuit can drive four 50-Ω lines.

Hockey-puck SCRs rated up to 1500 V

Motorola Semiconductor Products, P.O. Box 20924, Phoenix, Ariz. 85036. (602) 244-3466. $15 to $300 (5-9); 4 wks.

A line of high current SCRs, in 1/2-inch hockey-puck packages, are offered as the MR 235, 380 and 470 (device number gives rms current). The slower speed devices are available with voltage ratings up to 1500 V; high speed devices, from 600 to 1200 V. Switching speeds range from 10 to 40 μs.

100-W Darlington transistors feature a gain of 750 at 4 A. Called the 2N6055 and 2N6056 the new devices have 60 and 80-V ratings and are manufactured with a double-epitaxial construction for a high forward and reverse secondary breakdown capability.

The smallest 180° tuning air variable capacitors just had babies!

Right. Johnson's exclusive subminiature type "T" air variable capacitors (PC mounts) now come with stripline terminals for microwave applications, either vertical or horizontal tuning. These space-savers are only about 1/2 the volume of a "U" capacitor, but they offer extraordinarily high mechanical and electrical performance for critical applications.

Rotors and stators are as stable and uniform as precision machining from solid brass extrusion can make them. A high 1 1/2 to 8 ounce-inches torque holds the rotor securely under vibration. Temperature coefficient is very low plus 30±15 ppm/°C. Q is high, typically 1800 at 200 MHz. Three capacitance ranges span from 1.3 pF to 15.7 pF.

Our 45 years of experience really shows up in these new capacitors. But why take our word for it when a stamp will get you a couple of freebees and you can check them out for yourself.

E.F. JOHNSON COMPANY /3306 Tenth Ave., S.W. / Waseca, Minnesota 56093

Check type and range of sample(s) needed: Capacitance range

Horizontal tuning 1.3 to 5.4

Vertical tuning 1.7 to 11.0 1.9 to 15.7

Name_____________ Phone________

Firm__________Title________

Address________________________

City__________State________Zip________
You gain fundamental design advantages with General Electric infrared SSL's (LED's).

For example, General Electric guarantees* every SSL-55B and SSL-55C infrared lamp for:
- Precision beam alignment, to within 3 degrees of the mechanical axis of the lamp.
- Power output of each lamp will be within the less than 2 to 1 range, as published; the SSL-55B output ranges from 3.5 mW minimum to 6.0 mW maximum; the SSL-55C from 4.8 mW minimum to 7.5 mW maximum.
- Both types are available for immediate delivery, as are most other General Electric infrared SSL's. For prices and complete SSL infrared data write or call today.

Green Glow Lamp for Flexibility.

This GE broad spectrum bright green glow lamp gives you greater design flexibility than ever before. It also emits blue, with suitable color filter. Called the G2B, it is directly interchangeable electrically and physically with GE's high-brightness C2A red/orange/yellow glow lamp. You can use the G2B alone for 120 volt green indicator service. Or together with the C2A to emphasize multiple functions with colors. For example: for safe/unsafe functions, for dual state indications and to show multiple operations in up to 5 colors.

They should be operated in series with an appropriate current limiting resistor. Both the G2B and C2A save money because of low cost, small size and rugged construction.

Now Wedge Base Lamps in two sizes.

If space for indicator lights is your problem, the GE T-1 1/2 size all-glass wedge-base lamp is your solution. It measures only .240" max. diam. The wedge-base construction virtually ends corrosion problems; it won't freeze in the socket. Like its big brother — the T-3/4 wedge base lamp with a .405" max. diam., the filament is always positioned in the same relation to the base. And it makes possible simplified socket design.

For free technical information on any or all of these lamps, just write: General Electric Company, Miniature Lamp Products Department, #4454-L, Nela Park, Cleveland, Ohio 44112.

*Lamps not meeting published specifications will be replaced or money refunded.

ICs & SEMICONDUCTORS

Darlington transistors can handle high currents

Solitron, 1177 Blue Heron Blvd., Riviera Beach, Fla. 33404. (305) 484-4311. (1-99) $5 (TO-66), $3 (TO-5); stock.

The SDM 3100-3400 series Darlington devices are packaged in three-lead TO-66 and four-lead TO-5 cases. Typical features include: $V_{CEO}$ from 40 to 80 V, multiple gain selections at 2.5 or 5 A, typical 5 A $I_{FE}$ of 1000 min, 1 A $I_{FE}$ of 10,000 min, low-leakage planar construction (less than $\mu$A's at 80% of $V_{CEO}$, $V_{CEO}$ high speed ($f_s$ is 40 MHz typical, rise and fall times 200 ns typical) $\frac{Q_{2C}}{C/W}$ less than 5 °C/W (TO-66) and 25 °C/W/TO-5).

Quad line receivers provide own hysteresis

Silicon General, 7382 Bolsa Ave., Westminster, Calif. 92683. (714) 892-5531. SG1489J: $4.00 (100 up); stock.

The SG1489J and SG1489AJ quad line receivers offer built-in threshold hysteresis. The hysteresis in the A version exceeds that of the SG1489J by more than 2:1. Both types offer logic threshold shifting and input noise filtering capability. Input resistance ranges from 3 to 7 kΩ and input signal range is ±30 V. Package style is 14-pin cerdip.
Tiny bridge rectifiers can handle 1.5 A

Edal Ind., 4 Short Beach Rd., East Haven, Conn. 06512. (203) 467-2591.

Subminiature silicon single-phase bridge-rectifiers sealed in epoxy provide a low silhouette, for stacking miniature circuit cards. Units contain double-diffused passivated junction diodes in a cold case design. Voltage ratings of 50 to 1000-V PIV are offered with a current rating of 1.5 A in open-air mounting. Special ratings and other circuit configurations available on request.

CHECK NO. 277

15-V dual regulator tracks within 50 mV

Ratheon, 350 Ellis St., Mountain View, Calif. 94040. (415) 968-9211.

$2.18 (100 up).

A dual-tracking voltage regulator in a standard eight-pin mini-DIP delivers positive and negative 15-V outputs that track within 50 mV. Called the RC4195, it provides line regulation of 2 mV and load regulation of 5 mV with only 0.005%/°C drift per degree centigrade. The circuit provides 100 mA at each output and requires only two bypass capacitors. It also includes thermal shutdown at junction temperatures exceeding 175°C. The miniDIP dissipates 600 mW.

CHECK NO. 278

Low voltage avalanche diodes need only 50 µA

TRW Electronic Components, 14520 Aviation Blvd., Lawndale, Calif. 90260. (213) 679-4561. $15.40: PS1314A (OEM qty); 6-8 wk.

Types PS1300A through PS1314A are reference elements featuring temperature compensation and very low current levels. The zener voltage is 6.5 V ±5%. The diodes provide a stable reference at currents as low as 50 µA and temperature coefficients as low as 0.0005%/°C. The avalanche diode is said to have a very sharp knee. The unit can therefore operate at far lower current levels than are possible with a conventional zener diode.

CHECK NO. 280

CTS CORPORATION, a pioneer in cermet network packaging, HAS WHAT YOU NEED TO SOLVE "CUSTOM" RESISTOR REQUIREMENTS! Complete thick film facilities save in-house investments: existing tools speed production—cut costs... capabilities you can't afford to overlook. Resistors and resistor networks are our business... not just a sideline.

Whatever your needs, from standard in-line and DIP networks to custom high power/high voltage packages, you can rely on CTS experience and know-how.

Unmatched field reliability, high volume mechanization, and over a decade of cermet thick film-technology make CTS resistors "the engineers' choice". We have what it takes for both standard and custom resistor packages. Call on CTS EXPERIENCE...today! CTS CORPORATION, 905 N. West Boulevard, Elkhart, Indiana 46514, Phone: (219) 293-7511.

CTS CORPORATION
Elkhart, Indiana

A world leader in cermet and variable resistor technology.

INFORMATION RETRIEVAL NUMBER 66
Electronic Design 12, June 7, 1973

**COMPONENTS**

**RC networks can suppress noise and EMI**

Potter, 10441 Roselle St., San Diego, Calif. 92121. (714) 453-6610. From less than $0.30; 4 to 8 wk.

Bluseal RC networks have capacitance values ranging from 0.25 through 2 µF and resistor values from 10 Ω through 1 MΩ. Units operate in environmental temperatures from -40 C to +85 C. Series-4909 units have radial-lead construction and are encased in rigid flame-retardant epoxy; series 4900 have axial leads with cases of thermosetting polyester film and end fills of epoxy; series 4902 also is constructed with axial leads, but have rigid phenolic cases and flame-retardant epoxy end fills. The smallest networks are only 0.78 (l) x 0.33 (w) x 0.63 (h) in.

CHECK NO. 281

**Program panel features removable patch boards**

Sealectro Corp., 225 Hoyt St., Mamaroneck, N.Y. 10543. (914) 698-5600.

A quickly removable 7 x 10 program panel provides ready access to circuits for testing and program changes. The unit features Teflon-insulated jumper wires and silver-plated contact surfaces. Mating is controlled by oversized guide pins.

CHECK NO. 282

**20-yr life claimed for wet electrolytics**

Philips, Elcoma Div., P.O. Box 523, Eindhoven, The Netherlands.

Philips' new 108-series of wet aluminum electrolytic capacitors has a rated working life of over 20 yr, at 40 C and rated voltage, with no change in parameters. Rated voltages range from 6.3 V to 63 V and capacitance values from 33 to 2200 µF with a -10 to +50% tolerance. Life drops to 10,000 hr at 85 C and rated voltage.

CHECK NO. 283

**Terminator networks serve ECL circuits**

Beckman Instruments, 2500 Harbor Blvd., Fullerton, Calif. 92634. (714) 871-4848.

The Series 898 line of DIP terminators is specifically designed for use with new emitter-coupled logic such as ECL 10,000 and 9500-series ECL. The five standard configurations now available include: -2.0 V units (Series 898-41), -5.2 V units (Series 898-42), Thevenin-equivalent terminators (Series 898-43), series-line terminators (Series 898-44) and TTL-to-ECL translators (Series 898-45). The networks include ceramic 0.01 µF capacitors to decouple the supply busses.

CHECK NO. 284

**See-through switches allow new design ideas**

Industrial Electronic Engineers, Inc., 7720 Lemona Ave., Van Nuys, Calif. 91406. (213) 787-0311. $0.30 per switch plus cost of hardware; 6 wk.

Finger-tip pressure switches, called Cue-Switches, are made of matricesd conductors embedded in transparent plastic membranes. The switches operate without mechanical linkages, springs or buttons. Because of their transparency, the switch elements do not obscure the readability of printed, silk-screened or projected data. Products now available are a line of lighted push-button assemblies on 0.8-in. centers, bezel units that combine with rear-projection readouts and a line of 3 x 4 switch matrices with telephone or adding-machine formats.

CHECK NO. 285
New Sperry Clock Display lowers the cost of electronic clocks!

This unique Sperry Clock Display not only helps cut engineering expense, reduce assembly time and lower component costs, it looks a lot better than other displays now on the market. This new unit, the SP-151, has the same bright, clear, continuous, easy-to-read characters that have made Sperry a major supplier of readouts in only two short years. It's ideal for eye appealing home and auto clocks of all kinds as well as a clock and/or frequency readout for radios and television sets.

And, the new displays are low in cost. Just $7.00 each in 1,000 unit quantities. That's less than $1.75 per digit. In large OEM quantities, the cost is under a $1.00 per digit. Interfacing with MOS/LSI clock chips, these planar gas discharge displays can be used in all dc or multiplexed applications, with or without blanking zeros. Character height is 0.50" with centerline spacing of 0.160". The display's face is only 1.593" x 1.120". Depth is just 0.255" plus 0.260" for the pins.

The units can be viewed easily at distances over 30 feet and have a viewing angle of 130°. The natural color is an eye-pleasing orange. Other colors are available with filters.

SPECIAL EVALUATION KIT AVAILABLE

So that you can have the time of your life and evaluate the SP151, Sperry is offering a special Evaluation Kit complete with one clock display, connectors, MOS/LSI clock chip, printed circuit boards, 9-page application note and detailed assembly instructions. You supply the capacitors, resistors, diodes, transistors and power transformer.

AVAILABLE FOR LIMITED TIME ONLY FROM YOUR SPERRY DISTRIBUTOR — $19.95 PER KIT. ONLY ONE PER CUSTOMER. Offer ends July 1, 1973.

FOR THE NAME OF YOUR LOCAL SPERRY DISTRIBUTOR SIMPLY DIAL EEM TOLL FREE (800) 645-9200 (in N.Y. State call collect 516-294-0990).

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Sperry Information Displays, a division of Sperry Rand Corporation, P.O. Box 3579, Scottsdale, Arizona 85257. Telephone (602) 947-8371.
PDQ from your Triad Distributor

TRIAD'S low cost, wide range adjustable, 40-watt power supplies.

Triad's WR Series of 4 models feature open top construction, extruded integral heat sink housing, all silicon semiconductors, 10-year life computer grade capacitors, FR glass epoxy pc boards, and electrostatically shielded transformers. All units are convection cooled, have automatic current limiting, and are designed to meet UL-CSA requirements. In stock and available now from Triad distributors.

B size slot supplies for OEM systems.

NCB Series in 5 voltage ranges delivers 25 to 45 watts of precisely regulated DC power at extremely low ripple. With built-in overvoltage protection, automatic fold back current limitation and reverse polarity protection. Lower in cost, they retrofit many models on the market today. In stock now at Triad distributors.

COMPONENTS

Phase sensitive relays protect 3-phase devices

TimeMark Corp., 4586 E. 29th St., P.O. Box 15127, Tulsa, Okla. 74114. (918) 939-5811. $21 (100 up); Stock.

The Series 250 phase-sensitive relay senses if the three phases are connected in the correct rotating sequence. The unit contains a SPDT relay with 5-A contacts and it plugs into a standard eight-pin octal socket. The contacts close when the correct sequence is applied.

Small thermocouple can test electronic parts


Hy-Cal's Zig/Zag TC-2345 thermocouple is small, only 1/4 x 1/4 in., and has a 20 ms response which makes it suitable for electronic and semiconductor application. The small couple mounted on a patch is easily attached to TO-5 cans, diodes, DIPs and other electronic components. Only finger-tip pressure secures the patch to most surfaces, and the couple can operate over a temperature range of -320 to +350 F. All the base metal thermocouple types such as J, K, T and E are available. Six inches of 28-gauge, fiberglass-insulated thermocouple leadwire is standard.

CHECK NO. 286

CHECK NO. 287
Thumbwheels set predetermined counter

Kessler-Ellis Products, 120 1st Ave., Atlantic Highlands, N. J. 07716. (201) 291-0500. $14 (100 up); 2 wks.

It looks like three thumbwheel switches, but it functions like an electrical predetermined counter. You first set in the desired number manually. Electrical pulses fed to the counter cause it to count down to zero where a SPDT switch is actuated. An adding version counts upwards from any preset number, but this unit has no built-in switch. The counter is supplied with snap-in mounting clips. Standard models are available for 12, 24 and 110 V, dc or ac.

CHECK NO. 288

Thermoelectric module provides heat or cold


Thermoelectric module, Model 801-2001-01, can supply heat, or cool water, a small refrigerator or an electronic component. Its ceramic construction and metalized plates allow both good thermal transfer and electrical isolation. Maximum current is 8.5 A at a nominal voltage of 3.5 V dc. The unit can provide a max temperature differential of 60 C when little or no heat is transferred, and the max heat transferred is about 19 W at small temperature differentials (1 to 2 C).
The Elegant Transformer Kits


Six materials: fluorocarbon, nylon, glass-reinforced nylon, DAP, polyester and epoxy. For stability at temperature ranges from 105 to 200 °C.

The complete collection expresses the craftsmanship you expect from EPC as an EAi component company. Look to EAi also for custom-molded parts. Or to EAI for thick-film audio amps. Capacitors. Custom coils. Solenoids. Active filters. Analog/digital converters and other special function modules. Plus a growing list of other elegantly crafted etceteras.

COMPONENTS

Sector switch skips circuits when switching

Sealelectro Corp., 22 Hoyt St., Mamaroneck, N.Y. 10543. (914) 698-5600.

Slide’N Switch circuit selector skips unwanted circuits when switching to any one of 11 contacts. A pull-slide-push action operates the modular switch. The unit also provides a buss contact during switching that can actuate a make-ready circuit. Gold-plated terminals on the switch fit a standard PC card connector or they can accommodate solder connections. The switch is 2-5/8 x 11/32 in. and extends 1-23/32 in. behind the mounting panel. It is rated for 250,000 operations per contact when switching 250 mA.

CHECK NO. 290

Trimmer pot is 1/4-in. high, yet handles 3/4 W

CTS Corp., 406 Parr Rd., Berne, Ind. 46711. (219) 589-3111. $1.37 (100 up); stock.

The miniature 345-series trim pot has a TC of ±100 ppm/°C, which is standard for most resistance values. The cermet resistance element is in a completely enclosed package (sealed resistance element). The trimmer also offers: 0.18 in. high profile, 0.03% settablility, a resistance range of 50 Ω to 1 MΩ and resistance tolerance of ±20%. Power rating is 3/4 W at 25 C derated to no load at 150 C.

CHECK NO. 291

Multipole DIP switches come in five styles

American Components, Inc., 8th Ave. at Harry St., Conshohocken, Pa. 19428. (215) 828-6240.

DIL 16, dual-inline switches, come in five multipole and multi-position styles. They provide break-before-make operation and positive wiping action. All styles are 0.779 L x 0.330 W x 0.335 H in. A 16-lead configuration is standard.

CHECK NO. 292

Scott-T transformer is smaller than 1/3 in.

Magnetico, 10 Richter Ct., E. Northport, N.Y. 11731. (516) 261-4502. $19 (100 up); stock to 3 wk.

The model 12393 converts synchro information into resolver information. Its size is 0.75 x 0.75 x 0.6 in. and it comes in a molded type unit with PC pins (0.025 dia.) on a 0.1-in. grid. It operates over a temperature range of -55 C to +125 C and with MIL-spec environments. Other specifications include an input of 11.8 V rms line to line, 400-Hz synchro information, and a standard output of 6-V sine/cosine. Accuracy is typically 30 arc seconds to 3 arc minutes, where output loading is 100 kΩ. The unit can also be supplied in a low-profile configuration (0.75 x 1.75 x 0.375 in.).

CHECK NO. 293

EPC

Electrical Plastics Corporation
500 Long Branch Avenue
Long Branch, New Jersey 07740
Tel. (201) 870-9500
A Subsidiary of Electronic Associates, Inc.

INFORMATION RETRIEVAL NUMBER 71
X-1284 is a pressure-sensitive polyester film tape that handles like "Scotch" 56. However, the color is red, and because of its outstanding self-extinguishing characteristics, it can be used on radio and TV components and wiring involving fire or shock hazards.

It passed the rigid test outlined in U/L Subject No. 492, No. 510 and No. 94 with flying colors. ASTM D-635 was passed. Federal Highway Administration Safety Standard #302. Passed. ASTM D-1000-70a extinguishes in less than 3 seconds. Passed. 3M Cello Fusee extinguishes in less than 3 seconds. Passed. The reason "Scotch" brand flame retardant X-1284 tape won't support combustion is that the "Scotchpar" polyester film backing and the unique adhesive system are both flame retardant. One of the key technological advantages, included in the "Scotchpar" Type 7300 polyester film backing, is that the flame retardant properties are built in directly. They cannot delaminate or flake off.

X-1284 provides excellent tear resistance. It's ideal for coil holding and coil covering applications, high temperature harness wraps, color TV flyback transformer insulation and yoke coil assemblies.

For more information write Dielectric Materials & Systems Division, 224-64, 3M Company, 3M Center, St. Paul, Minnesota 55101.

See our product data in EEM.
COMPONENTS

Hybrid transformer can terminate 4 wire lines

Magnetico, 6 Richter Ct., East Northport, N.Y. 11731. (516) 261-4502. $12 (1000 up); stock to 4 wk.

Designed to meet telephone company requirements for data and voice access, model 50819 contains a hybrid pair for converting a four-wire terminal into a two-wire voice path, or the reverse. Its frequency response over 300 to 3500 Hz is ±1/2 dB, over levels from -45 dBm to +7 dBm. Longitudinal balance is 45 dB minimum and return loss 26 dB minimum. The transhybrid loss exceeds 50 dB and impedance match is within ±10%. The unit can also be supplied, to tolerate without degradation, the normal 120-mA dc current unbalance typical of signal or hold current in a switched telephone line.

CHECK NO. 294

Now there’s a big name in miniatures.

It’s Raytheon. And you know with Raytheon on a miniature switch you get quality, dependability and most important — availability. Popular toggle, push-button, proximity, rotary and rocker-type designs carry the Rayswitch name and Raytheon’s reputation for excellence in electronics.

Whatever your application, from test equipment to computer peripherals, there’s a Rayswitch for your panel. Switch to the big name in miniatures.

Call your Raytheon representative. Or for a FREE copy of our Rayswitch catalog write Raytheon Company, Fourth Avenue, Burlington, Mass. 01803.

Raytheon

INFORMATION RETRIEVAL NUMBER 73

Mini load cell claims to be lowest cost unit

Interface Inc., 7210 E. Acoma Dr., Scottsdale, Ariz. 85254. (602) 948-5555. $99 (11 up); stock (small qty).

A standard miniature load cell has guaranteed specifications of ±0.03% linearity, ±0.2% hysteresis, and ±0.01% nonrepeatability. Rated output of the MB-50/75/100/150 is 3 mV/V. Full-scale deflection is 0.005 in. It is available in standard ranges of 0 to ±50, 0 to ±75, 0 to ±100, and 0 to ±150 lb. Over-all dimensions of the Minibeam are just 2-3/8 (I) x 1 (h) x 1/2 (w) in.

CHECK NO. 295

Small cathode-ray tube provides 0.6 mil spot

Video Products, 7550 San Fernando Rd., Sun Valley, Calif. 91352. (213) 767-0748.

A miniature cathode-ray tube, type VPI-1, is 1 in. OD, has high resolution, a small spot size (0.6 mils) and comes complete with deflection yokes and a Mu-metal shield. It operates over a 5-to-10-kV range, can handle 850 lines and is capable of 350 ft-L output. The tube weighs only 39 g, is 5.5-in. long and has a flat face.

CHECK NO. 296

ELECTRONIC DESIGN 12, June 7, 1973
ANNOUNCING A LOT LESS TO GO WRONG.

We've got a 50 MHz frequency meter with simpler circuitry and better performance than anything anywhere near its price range. It's the Newport 730 Counter-Timer and it only costs $299.

The new 730 offers 50 mV input sensitivity. A count range from 10 Hz to 50 MHz. Frequency, accumulate and digital stopwatch modes. Five selectable gate times. Six-digit LED readout. Internal crystal controlled time base.

It also has many features you wouldn't expect in a low-cost instrument. Including readout display storage with storage override control. Precision crystal oscillator accurate to two parts per million. And a multi-range time base selector switch which permits maximum resolution of the frequency being measured.

For easy maintenance, we made the ICs socket-mounted. For ease of replacement, we offer an optional IC spares kit.

For more information, just circle reader service number 232 or write Newport Laboratories, Inc., 630 East Young Street, Santa Ana, California 92705. For immediate information, call collect. Dial (714) 540-4914.

Ask for Walt Boris. Or TWX: 910-595-1787.
MORE THAN THIN-FILM METALLIZED SUBSTRATES, RESISTOR NETWORKS & CUSTOM HYBRIDS

LRC, Inc. is providing a variety of thin-film substrates and devices with two important advantages: A Quick-Reaction Capability for custom resistor networks and hybrid circuits. Complete LRC facilities for testing and screening all devices to MIL-STD-883.

Thin film metallizations include chrome/gold, tantalum-tantalumnitride/gold, chrome/copper, chrome/copper/gold and many other combinations. Unique LRC trimming methods and heat treatment assure highly reliable, stable resistive elements. Standard packages include DIP, TO- and Flatpacks.

TYPICAL PERFORMANCE

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For your copy of the new LRC THIN FILM brochure, call or write:

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140 MORE THAN THIN-FILM METALLIZED SUBSTRATES, RESISTOR NETWORKS & CUSTOM HYBRIDS

MICROWAVES & LASERS

CATV transistor lists
8-dB NF at 210 MHz

Solitron/Microwave, 1440 W Indianatown Rd., Jupiter, Fla. 33458. (305) 746-8311. $5.40 (1-99); 3 wks.

The SC3000 CATV transistor has a broadband noise figure of 8 dB at 210 MHz and a cross-modulation figure of -95 dB at +35 dBm for 20 channels. Intended primarily for bridge and trunk amplifiers, the SC3000 comes packaged in a stripline TO-117 case.

CHECK NO. 297

Rf linear amp delivers 40 W

Electronic Navigation Industries, 3000 Winton Rd. S., Rochester, N. Y. 14623. (716) 473-6900. $1450; 60 days.

The Model 240L solid-state instrumentation amplifier can supply up to 40 W of linear rf power or up to 150 W of saturated power over the 20-kHz-to-10-MHz frequency range. The unit supplies its rated output to any load regardless of the impedance value. The 240L has a gain of 50-dB, with variations limited to ±1.5 dB. Harmonic distortion is typically more than 30-dB below the fundamental at an output power of 40 W, while maximum noise figure is 8 dB.

CHECK NO. 298

Laser system has 5-wavelength output

International Rectifier, 1521 Grand Ave., El Segundo, Calif. 90245. (213) 322-4987.

A high-power, high rep-rate laser system offers outputs at 1.06, 0.53, 0.6943 and 0.3472 µ. The five wavelengths are obtained by interchanging ruby and Nd-glass laser rods. The system's power control operates at a peak current of 75 A and switches at zero voltage level. Voltage to the charging circuit can range up to 12 kV, and is maintained within 1/2%.

CHECK NO. 299

Power-chip resistors cover 40-MΩ range


Power-chip resistors for S-band applications range from 1 Ω to 40 MΩ. Available tolerances are 0.5, 1, 2, 5 and 10%. The chip resistors are offered in these configurations: Size E—0.10 × 0.10 × 0.02 inch and 3-W dissipation—and Size F—0.10 × 0.20 × 0.02 inch and 5-W dissipation.

CHECK NO. 300

Double-balanced mixer has 2-to-500-MHz range


A double-balanced mixer operates in the 2-to-500-MHz frequency range. Called the DBM-500/BNC, the mixer's i-f output covers frequencies from dc to 500 MHz. Typically the mixer exhibits 15 to 50 dB of isolation between ports and a conversion loss of 5 to 10 dB (SSB N.F.), with a +7 dBm LO input-signal level. And the use of Schottky-barrier diodes permits a total power input of +23 dBm over the temperature range of -54 to +71 C.

CHECK NO. 301
We're everything you need in cermet trimmers.
We're TRW/IRC Potentiometers.

These infinite resolution pots cover the complete size range from $\frac{1}{4}''$ round to $1\frac{1}{4}''$ rectangular in the industry's widest selection of mounting configurations.

The exclusive Metal Glaze® element results in a cermet trimmer with higher power rating and wider temperature range than other manufacturers' units of the same size. Maximum temperature coefficients of ±100 ppm/°C. are standard, with TCs of ±50 ppm available on most types.

For fast delivery, from stock, call any TRW/IRC Potentiometer distributor listed on the adjacent page. For information of the complete line, contact your distributor or TRW/IRC Potentiometers, an Electronic Components Division of TRW Inc., 2801—72nd Street North, St. Petersburg, Florida 33733; phone (813) 347-2181.

ELECTRONIC DESIGN 12, June 7, 1973
INFORMATION RETRIEVAL NUMBER 76
with the industry's broadest line of subminiature T-2 lamps.

Specify A lamp with the light output at the business end of the bulb. Maximum end viewing in signalling applications is assured with our T-2 flat top bulb construction.

Specify Simplicity A .250 O.D. lamp in over one hundred types assures design continuity and consistency.

Specify Versatility You can trade off design economy, light output, voltage, current and size with a choice of pilot, indicator and telephone lamps in up to 5 base styles.

Specify the Total Package We have the hardware to match the light source - a complete line of pilot and indicator sockets and lenses.

Specify Reliability The most widely used light source in telephone industry signalling applications. Specify telecommunications reliability.

Get the designer's edge - write for specification data.

MICROWAVES & LASERS
Log amp accuracy varies over temp by ±1 dB

Circuit Technology, 160 Smith St., Farmingdale, N.Y. 11735. (516) 293-8686. From $650 (unit qty); stock to 14 wk.

With a 60-MHz center frequency and a bandwidth of 25 MHz, models CTL60s-1 and -2 provide logging accuracies of ±1 and ±2 dB, respectively. The log accuracy applies over the operating temperature range of -20 to +65 C and -75 to -5 dBm input dynamic range. Rise time is a minimum of 50 ns. Gain scale factor is 30 mV/dB with a video output drive capability of 0 to +2.1 V into 100 Ω. The matched dual log amps measure only 4.88 x 3.35 x 0.68 in. and the single units are only 2.44 x 3.35 x 0.68 in. The CTL60D-1 and -2 models are dual versions of the CTL60s-1 and -2.

CHECK NO. 302

Avalanche diodes have 20 kV PIVs at 1 A

AFI Ind., 400 Warburton Ave., P.O. Box 476, Long Branch, N.J. 07740. (201) 229-8300. From $1.50 ea.

Designated the 500A series, the avalanche rectifiers have an 8 to 20-kV PIV and are specifically designed for use in commercial or industrial type microwave cooking ovens. The rectifiers feature output currents from 300 to 1000 mA.

CHECK NO. 303

ONE SOURCE, ONE CATALOG. GET THE EDGE.
Send for our new 28-page catalog.
Sylvania Miniature Lighting Products Inc., West Main St., Hillsboro, N.H. 03244 (603) 464-5533

GTE SYLVANIA
INFORMATION RETRIEVAL NUMBER 77
Stripline hybrid has quadrature output

Technical Research and Manufacturing, Grenier Field, Kelly Ave., R.F.D. #3, Manchester, N.H. 03103. (603) 668-0120. $25 (1-4); stock to 2 wk.

The miniature stripline hybrid Model HQ 502-1 for direct installation into microstrip circuits uses strip transmission-line construction. Power handling is on the level of 100-W cw with 3-kW peaks. Typical specifications for model HQ 502-1 are: frequency range 225 to 400 MHz; isolation, 20 dB (min.); VSWR, 1.20:1 (max.); amplitude balance, ±0.5 dB; phase balance, ±1.5°; insertion loss, 0.25 dB (max.); size 1.25 in² × 0.11 in. thick.

CHECK NO. 304

Cavity oscillator has 0.25% stability

Solid State Technology, 3650 Charles St., Santa Clara, Calif. 95050. (408) 247-8620. $595 to $1176 (small qty.); 60 days.

The SSC-0204 cavity oscillator features a frequency stability of 0.25%, at temperatures greater than 100 °C, during 12 hours of operation after 15 minutes of warm-up. The oscillator can replace phase-locked oscillators and has a voltage-tuning capability over a 0.4% bandwidth at rates from dc to 10 MHz. Mechanically tuned bandwidths of typically 10% can be obtained from 500 MHz to X band. Harmonic and spurious rejection are −30 and −60 dB, respectively.

CHECK NO. 305

Power dividers work from 2 to 18 GHz


A series of broadband two and four-way power dividers, Model 3300 and 4300 series, can be used in the 2-to-18-GHz frequency range. The new stripline units provide equal in-phase division of input powers, with low VSWRs ranging from 1.2 to 1.35 (typical). Output-port isolations are typically about 20 dB.

CHECK NO. 306
Cover the 5 to 200-MHz range with 3 attenuators

Radiation Devices, P.O. Box 8450, Baltimore, Md. 21234. (301) 665-2764. (Unit qty) $42 (VCA-1) $38 (-2), $35 (-3); 30 days.

A series of three voltage-controlled p-i-n-diode attenuators covers the frequency range of 5 to 200 MHz—model VCA-1, 40 dB, 5 to 100 MHz; VCA-2, 30 dB, 5 to 100 MHz; VCA-3, 20 dB, 5 to 200 MHz. Maximum insertion loss is 6 dB. VSWR varies from 3.0 to less than 1.5 depending on attenuation setting. Units require up to 105 mA supply current and less than 5 mA control current. Connectors available include BNC, JCM (SMA compatible) and TNC. Unit size is 5.8 \times 5.3 \times 3.1 \text{ cm}.

CHECK NO. 307

He-Cd laser offers 10 mW in radiated blue

Coherent Radiation, 310 Porter Dr., Palo Alto, Calif. 94304. (415) 493-2111. $1,950; stock.

The helium-cadmium Model 90 laser provides greater than 10 mW at the 441.6-nm wavelength (visible blue). Tube life, according to the company, exceeds 1000 hours and the tube can be replaced in minutes. Lasing action is obtained within two minutes after turn-on and full power is obtained within eight minutes.

CHECK NO. 308

Dye lasers achieve 0.001-nm resolution

Molecotron, 930 Thompson Pl., Sunnyvale, Calif. 94086. (408) 738-2661. DL-300: $9,265; 3 months.

Dye lasers are offered in the DL-Series with resolutions reaching 0.001 nm in the 350-to-740-nm range. The series starts with the DL-100 that provides 0.2-nm resolution in the wavelength range. The DL-200 adds a beam-expanding telescope to the DL-100 and provides 0.01-nm resolution. By adding an intracavity etalon to the DL-200, the DL-300 resolution reaches 0.001 nm. The lasers are nitrogen laser pumped and built on the Hansch principle.

CHECK NO. 309
A flexcircuit for electronic pocket camera control.

We did it for Kodak.

The Kodak Pocket Instamatic, one of the major marketing successes of the decade.

Many of the pocket Instamatic® cameras, Model 50 and 60 pack the Schjeldahl flexcircuit you see above. One circuit containing two integrated circuits, all other electronics and flexed into 12 planes. That's using flexcircuirty as it should be used.

But there's more to the Schjeldahl circuit than that. It is only 8 mils thick yet it's fully insulated on both sides. Components mount directly to the flexcircuit and they can be hand or wave soldered. It replaces all wire and all circuit boards and provides the entire interconnection function.

To help make its great new camera possible, Kodak needed a compact, sophisticated flexible circuit that could be produced at the rate of thousands per week.

Schjeldahl did it for Kodak.

And we can do it for you.
**PIN diodes have low insertion loss**


The VSD-300 series p-i-n diodes feature SiO₂ passivation and are available with breakdown voltages of 50, 100, 200 or 500 V. Performance characteristics obtained with the VSD-300 series include: junction capacitances ranging from 0.05 to 0.75 pF and series resistances from 0.3 to 2 Ω. Typical, minority carrier lifetimes for VSD-300 diodes are between 5 and 350 ns. The diodes will withstand operating temperatures from −65 to +150 C, and storage temperatures from −85 to +300 C.

**Ion laser line offered**

Coherent Radiation, 3210 Porter Dr., Palo Alto, Calif. 94304. (415) 493-2111. $8350 up; under 30 days.

The CR-Series of ion lasers consists of argon, krypton and mixed-gas (argon and krypton) types. The argon lasers delivers 2, 3, 5 and 8 W; the krypton lasers, 500 and 750 mW at 647.1 nm; and the mixed-gas lasers, 250 mW at 488 nm, 514.5 nm and 746.1 nm. All lasers have an amplitude noise that is less than 0.5% rms and single frequency stability that is better than ±8 MHz. According to the company, the lasers will operate in excess of 6000 hours.

**Entire S-band paramp provides 45-dB gain**

Micromega Div., 12575 Beatrice St., Los Angeles, Calif. 90066. (213) 391-7137.

An S-band paramp with built-in power supply and temperature stabilization circuitry provides low-noise amplification of rf signals in the 2.2-to-2.3-GHz band with a nominal insertion gain of 45 dB. Other specifications include noise temperature of 125 K max and gain stability of ±1.0 dB/24 hours over the 0 to 125 F temperature range. The bandpass ripple is 1 dB pk-pk max and gain compression is 1.0 dB max with input signal level at −40 dBm.

---

**How flexible can you get?**

Ultra-flexible with ultra fine wire stranding, combining wires as slim as .001 of an inch in diameter. Super supple pliability makes it a must for in-movement service.

**WOVEN ELECTRONICS**

P.O. Box 189
Mauldin, South Carolina 29662

INFORMATION RETRIEVAL NUMBER 81
5.4-5.9 GHz Gunn VCO drifts 10 MHz typical

A Gunn-effect oscillator, the ETO-217, exhibits a typical frequency drift of 10 MHz (20 MHz worst case) over the temperature range of -10 to +60°C while varactor tuned anywhere in the 5.4-to-5.9-GHz band. Minimum power output is 40 mW with tuning and temperature-induced variations of ±2 dB. Tuning voltage is 5 to 60 V and the bias is 14 V dc at 1/2 A. The oscillator measures 1/2 x 1 x 2-1/4 inches and weighs less than 2 ounces.

CHECK NO. 893

Panoramic/sector rcvr covers GHz range

Watkins-Johnson, 6006 Executive Blvd., Rockville, Md. 20852. (301) 881-3300.

Full panoramic or sector coverage of the 2-to-1000-MHz frequency range is offered by the 208 series of receivers. Seven receivers are required for complete coverage, however 11 receivers with various band coverages are available. In the panoramic mode, the full frequency band of the receiver is swept at an adjustable rate varying from 0.1 to 25 sweeps per second. The sector mode permits a sector scan variable from zero to full band, continuously adjustable by front panel control.

CHECK NO. 894

WE OVERSHADOW THE COMPETITION

Our stack is on the right. It's quite an assortment. After all, we're the largest manufacturer of terminal boards, blocks and strips in the world. And we offer more variations than anyone else. "One" meets your specific requirement. Delivery? Allow a few weeks for our good old standards, longer for the oddballs. So plan ahead and get the best.

Kulka
A NORTH AMERICAN PHILIPS COMPANY
Kulka Electric Corp., 520 South Fulton Avenue, Mount Vernon, New York 10551
Dual-trace storage scope offers 50-MHz bw

Test & Measuring Instruments, 224 Duffy Ave., Hicksville, N.Y. 11802. (516) 433-8800.

Designated PM3251, This 50-MHz dual-trace storage scope offers all the features of the Philips PM3250 high-sensitivity broadband scope and also provides continuously-variable storage time up to 2 hr in addition to continuously-variable persistence from 0.3 s to 15 min. The PM3251 has a sensitivity of 2 mV/cm at 50 MHz or 200 µV/cm at 5 MHz. Like the PM3250, the PM3251 allows simultaneous display of trace A-B vs ±B, chopped or alternate, and allows X vs Y display with 2-mV sensitivity on the X axis and 200 µV on the Y axis, with phase shift of only 3 deg at 100 kHz.

CHECK NO. 502

3-1/2-digit LED DPM takes 200 readings/sec

Datel Systems, 1020 Turnpike St., Canton, Mass. 02021. (617) 828-6395. $99; stock.

Model DM-2000 3-1/2-digit DPM (LED display) contains a true differential input. Both inputs and the analog common can sustain up to ±2 V, common-mode, with respect to the digital-output common. Other features include a choice of input range, ±1.999 mV or 1.999 V, a common-mode rejection ratio of 70 dB at 60 Hz, input bias current of 20 nA and an input impedance of 100 MΩ, plus automatic polarity. Model DM-2000 has a specified accuracy of ±0.05% and can resolve to 100 µV over 0 to +70 C. Input settling time is 50 µs and up to 200 readings can be made asynchronously or synchronously.

CHECK NO. 503

Automated test system is easy to use

Julie Research Labs, 211 W. 61st, New York, N.Y., 10023. (212) 245-2727. $25,000 to over $100,000; 8-20 wks.

LOCOST-106, Labor Optimized Computer Operated System Test facility, can be operated by a laboratory technician. The control system consists of a calculator with a 10 to 12K capability, coupled with a data terminal, high-speed thermal printer, and a 32,000-word, programming-cassette memory. The system, which uses BASIC language, has an alphanumeric keyboard and an interactive 32-character display, as well as a 15-k byte mainline memory. Pre-programmed software makes it possible to generate, store and carry out test programs for new instruments.

CHECK NO. 504

Units detect, categorize power-line transients

Programmed Power, Inc., 141 Jefferson Dr., Menlo Park, Calif. 94025. (415) 323-8454. $2995 to $3600; 8 wks.

The 3200 Series is a family of three power-line disturbance monitors. The portable instruments simultaneously detect, count, categorize, time and record overvoltages, undervoltages, fast transients and frequency variations on single or three phase power lines. Provided are audio/visual alarms and hard-copy printout indicating day, hour and minute, plus a code digit correlating to the specific power anomaly noted. The latter feature permits unattended, remote applications. Transient response ranges from 0.5 to 100 µs and transient amplitudes range from ±50 to ±600 V.
Switching technology vs. series-pass.
Now there's a choice.

Series-pass regulation offers great advantages in compact size, established design technology and exceptionally clean output. While switching technology is theoretically even more compact, it's virtually impossible to produce because of the inherent high noise and RFI problems.

Right?
Wrong. Sorensen's STM series of modular power supplies prove the point. First, for a given power rating, STM's offer twice the efficiency, half the size and lower price than equivalent series-pass units (and all STM's have built-in over-voltage protection). Plus a big plus. Low RFI and noise. We ran conducted interference tests and fully met the requirements of MIL-STD-461A above 20KHz.

The STM series presently consists of 30 switching transistor power supplies — with 10 models to follow shortly. STM efficiencies approach 75% keeping dissipation low. In many systems applications these high efficiencies obviate the need for forced air cooling systems.

Switching technology is no longer a bugaboo. It works. Beautifully. Send for our complete catalog and see for yourself (and see our great series-pass supplies too). Write Sorensen Company, a unit of the Raytheon Company, 676 Island Pond Rd., Manchester, N.H. 03103. Telephone (603) 668-4500. Or TWX 710-220-1339.

STM: twice the efficiency, half the size.

<table>
<thead>
<tr>
<th>Specification</th>
<th>Sorensen STM5-24</th>
<th>Brand &quot;X&quot;</th>
</tr>
</thead>
<tbody>
<tr>
<td>Size</td>
<td>3¾&quot; x 5½&quot; x 9½&quot;</td>
<td>4½&quot; x 7½&quot; x 9¾&quot;</td>
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<tr>
<td>Volume</td>
<td>160 in³</td>
<td>344 in³</td>
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<tr>
<td>Price</td>
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<td>$235</td>
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<tr>
<td>Efficiency</td>
<td>58%</td>
<td>29%</td>
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<tr>
<td>Regulation (line &amp; load combined)</td>
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<td>0.2%</td>
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<tr>
<td>Temperature Coefficient</td>
<td>0.01%/°C</td>
<td>0.03%/°C</td>
</tr>
<tr>
<td>Overload Protection</td>
<td>Current limiting-adjustable electronic</td>
<td>Optional @ $30 (except built-in, fixed, on 5-volt model only)</td>
</tr>
<tr>
<td>Overvoltage Protection</td>
<td>Built-in adjustable, all models</td>
<td></td>
</tr>
</tbody>
</table>

Compare this point-by-point spec-check between Sorensen's STM5-24 and Brand "X".
**D/A SETTLES IN 15 NS!**

Unretouched photo of scope traces showing settling time for Computer Labs MDS-0815 under worst-case conditions of MSB switching out of phase with all other bits.

Now you can get D/A's with 8-bit settling time as low as 15 ns; 10-bit settling in 20 ns! The Computer Labs MDS/MDP Series offers a complete range of 8 and 10-bit converters with cost/performance tradeoffs in speed and temperature coefficients. All settling times are specified at full current output of 15 mA or ±1.5V for unipolar operation; and ±7.5 mA at ±1.1V for bipolar output. That makes these D/A's ideal for applications requiring ample driving currents and exceptionally fast conversion. Call or write now for complete information on the fastest and most economical 8 and 10-bit D/A's available.

**INSTRUMENTATION**

**Digital storage scope has internal memory**

Nicolet Instrument, 5225 Verona Rd., Madison, Wis. 53711. (608) 271-3333. $4800; 4-6 wks.

The 1090 digital storage scope has a nonvolatile magnetic-core memory with the capacity to store a waveform to a resolution of one part in 4096 on both voltage and time axes. It's comprised of a main frame and plug-in units. Moveable crosshairs are used to select any region of the stored waveform for closer inspection. This selected area can then be expanded in voltage and/or time dimensions, in steps of two, up to a factor of 64X. A touch of a button allows the present, preceding, or following signal to be held (whichever is desired) and another touch returns the operation to real time. Several waveforms may be stored and superimposed. Pen recorder drive and binary output are included.

**VOM measures current to 12 A, ac/dc**


Features of the Model 265 include high ac and dc current capability, to 12 A, and the ability to take ac voltage and ac current measurements almost simultaneously. The 265 is housed in the familiar Simpson 260-style case and is equipped with a single, central-range switch and adjust-a-vue handle, which doubles as a meter stand.

**INFORMATION RETRIEVAL NUMBER 85**

**CHECK NO. 506**

**CHECK NO. 507**
4-3/4-digit DMM offers 300% overrange

Hickok Electrical Instrument Co.,
10514 Dupont Ave., Cleveland, Ohio
44108. (216) 541-8060. $595; 60
days.

With optional 300% overrange,
the Hickok 3400 offers five-
digit accuracy for measurements
up to a maximum display of 39999.
The Hickok 3400 contains 26
ranges: Five each for dc and ac
volts and dc and ac current, and
six for ohms. A three-year war-
ranty is standard. The 3400 is
3-1/2 x 8-3/8 x 13 in. and weighs
10 pounds.

CHECK NO. 508

Digital printer mates
to many sources

Beckman Instruments, 3900 River
Rd., Schiller Park, Ill. 60176. (312)
671-3300. $750; stock.

Model 1453B digital printer can
accept data from a wide variety
of sources. The instrument offers a
1 to 12-column printout capacity,
and is designed to replace exis-
ting Beckman Models 1453 and
1453A printers. Adding appropriate
input modules provides the
1453B with flexibility of input
codes, levels and format. These
modules include BCD or 10-line
input, and vacuum tube, transistor
or integrated circuit levels. A con-
tinuously rotating print drum,
spring-loaded print hammers, paper
advance system, print color selec-
tor, and dc motor are the instru-
ment's only moving parts.

CHECK NO. 509

The fast and easy way
to troubleshoot

This unique, automatic ranging, ac/dc digital multimeter
puts the data right at your fingertips.

The Model 167 Auto-Probe DMM:
• measures dc voltage - 1 mV to 1000 volts
• measures ac voltage - 1 mV to 500 volts rms
• measures resistance - 1 ohm to 20 megohms
• measures current - with optional shunts
• battery operated (line adapter optional)

It's fast (saves time!), it's accurate, and its readout is right
in the hand-held probe.

The Model 167 Auto-Probe DMM — only $325. Send for
more details.
why go to the far places for a miniature IF Filter under $4*? It's right at your doorstep from Vernitron... (the filters people)

If you're after miniaturization, performance and low cost—and think you have to go to overseas sources to get them—you don't!

Here's Vernitron's new TAF-02A encapsulated ceramic filter for today's compact Comm receivers and transceivers. Gives you performance equal to four IF cans in a space smaller than one. Sharp clean selectivity to beyond 40 dB. Good resistance to shock, vibration, humidity. Immune to magnetic fields—so you can eliminate shielding. That's design flexibility!

Made for automated assembly—and produced right here at home, where you have full design assistance right on tap. And you can't beat the price.

* In production quantities

Complete application info is yours for the asking

Vernitron Piezoelectric Division
232 Forbes Road / Bedford, Ohio 44146 / (216) 232-8600

INSTRUMENTATION

Four-digit DMM sells for $595

Systron-Donner, 10 Systron Dr., Concord, Calif. 94518. (415) 882-6161. $595; 5 days.

Model 7004A 4-digit DMM offers 25 measuring ranges: ac V, dc V, amps and ohms. Dc accuracy is 0.01%, and ac response covers the range to 100 kHz. Color-coded push-buttons simplify selection of desired function and range. Inputs are fully guarded for highest common-mode operation. An optional rechargeable battery pack can be mounted internally and a BCD output option makes it possible to record measurements on an associated digital printer.

CHECK NO. 510

3-in. portable scope gives 2-MHz bw


The B & K 1403 "MiniScope" is a general-purpose 3-in. scope with a bw of dc to 2 MHz, and direct-deflection terminals for viewing waveforms to 150 MHz. It's 100% solid state and has dc amplifiers on both horizontal and vertical axes. Over-all size is 5-1/4 x 7-3/8 x 11-1/4-in., and weight is only 8.5 lb. Vertical sensitivity is 20 mV/cm and input impedance is 1 MΩ shunted by 30 pF.

CHECK NO. 511

INFORMATION RETRIEVAL NUMBER 87
Lock-in amplifier is sensitive to 100-nV fs

Princeton Applied Research, Box 2565, Princeton, N.J. 08540. (609) 452-2111. $2295; 90 days.

Model 186 lock-in amplifier measures amplitude and phase angle of signals obscured by noise. It provides 100-nV fs sensitivity and handles transient noise overloads as much as 300,000 times fs. A unique feature is the lock-in’s ability to yield low drift under high overload conditions. Stability to 10 ppm/°C is possible with overloads to 3000 times fs and 100 ppm is typical with overloads to 30,000 times fs. Operating frequency range is 0.5 Hz to 100 kHz but the signal need not be frequency stable; it can drift and the lock-in will automatically track.

CHECK NO. 512

Purchase 3-1/2-digit multimeter in kit form

Nobex Electronics, P.O. Box 4865, Burlingame, Calif. 94010. (415) 344-7691. $149.95 (unit qty); stock.

Nobex Model 8700K digital multimeter, when assembled, has an accuracy of 0.5% by using an internal oven-controlled voltage reference. The kit is engineered for easy sequential assembly. Ranges include 1, 10, 100, and 1000 V dc with 300% overrange, 1, 10, 100, and 1000 V ac with 100% overrange, 1 k, 10 k, 100 k and 1 MΩ with 300% overrange and 300-V fuseless input protection. The unit can be calibrated, with its internal voltage standard, using only a screwdriver.

CHECK NO. 513

...YOU’LL LIKE IT!
TRUE RMS VOLTMETER RESolves 0.01 dB

PROGRAMMABLE ■ SENSITIVE ■ WIDE BANDWIDTH

These important features, usually extra-cost or unavailable, are standard with the 3½ digit 93AD at its $1200 base price:

■ 300 µV sensitivity usable over the full 20 MHz bandwidth.
■ Full remote control.
■ Digital and analog outputs.
■ Auxiliary analog meter.
■ Selectable bandwidth and response time.

Several options and accessories are available for special requirements:

■ Digital dB display and outputs.
■ Automatic ranging.
■ High impedance probe.

Boonton Electronics
ROUTE 287 AT SMITH RD.
PARSIPPANY, N.J. 07054
TEL.: 201-887-5110
TWX: 710-986-8241

Information Retrieval Number 88

Electronic Design 12, June 7, 1973
NEW Super Small, 12-Bit D/A Converter

DAC371I-12
- ±0.025% Linearity
- Complete and Ready-to-Use
- Binary or BCD Coding
- All Hermetic Components
- TTL/DTL Compatible

$35. in singles

The current output DAC371I-12 — the smallest 12 bit D/A converter on the market — has been especially designed for the size and price-conscious engineer. The unit is so small (1.1" x 1.7" x 0.4") that it only takes up the size of two standard 16 pin IC sockets. And, it's priced right too, selling for $35.00 in singles.

The DAG uses some significant new proprietary breakthroughs in component technology to achieve this size and cost. Nonetheless, the unit is complete with precision resistor ladder, switches, and a high accuracy internal reference, and just requires ±15V power for operation. Contact us for full details.

HYBRID SYSTEMS CORPORATION
87 Second Avenue, Northwest Industrial Park, Burlington, Mass. 01803
Telephone: 617-272-1522 TX: 710-332-7584
Write for our new data conversion products catalog.

The Servo-Tek World of DC Servomotors

Wide range of permanent-magnet dc models available.
Servo-Tek's Permanent-Magnet DC Servomotors are precision made to give highly reliable performance. Their stability, high output-to-size ratio and speed range from 0-10,000 rpm with output torques to 2.0 oz-in make them ideal as prime movers in servomechanisms. Diameter 1.135 in. lengths up to 3.253 in. A unique field structure of Alnico VI results in minimized cogging (slot lock), a prerequisite to optimum servo performance. Models are available with a variety of operating voltages and with various mountings and integral gearing. Moderately priced with quantity discounts.

FREE CATALOG of rotating components available.

INFORMATION RETRIEVAL NUMBER 89

INSTRUMENTATION

Pulse generators give 100-MHz rep rate


Two new pulse generators, one a plug-in (Model 1916A) and one an independent instrument (Model 8007B), test high-speed TTL-S, ECL-I, ECL-II and low-power ECL to repetition rates up to 100 MHz. Each unit offers variable transition time, variable offset, and a variety of output formats and operating modes. The Model 8007B holds nonlinearity of transition slopes below 3% for transitions greater than 20 ns. Pulse transition times may be varied from 2 ns to 250 µs; rise and fall transitions may differ as much as 50:1. Pulse amplitude is 5 V, positive or negative, and dc offset may be set ±4 V, independent of amplitude.

CHECK NO. 514

Test set measures chatter of contacts

Atec, Inc., Box 19426, Houston, Tex. 77024, (713) 468-7971. $2685; 60 to 90 days.

Model 4201 Contact Chatter Test Set offers 0.1-µs resolution of duration of contact chatter observed over a preselected period or window. This window moves continuously with time, permitting uninterrupted observation, unless maximum allowable duration of chatter is exceeded. The moving window can be selected for periods from 100 µs to 1 ms in increments of 100 µs. Maximum allowable total duration of chatter during this moving period can be selected from 0 to 999.9 µs, in increments of 0.1 µs.

CHECK NO. 515

INFORMATION RETRIEVAL NUMBER 90

ELECTRONIC DESIGN 12, June 7, 1973
One part in 10 million from 0° to 55°C. Without an oven.

Unlike an oven oscillator, it's smaller, more reliable, uses less power, needs no warm-up time, and it's not as expensive. The K1098A TCXO has TTL compatible output, ±1x10⁻⁹/sec. rms short term stability, operates from 5 and 12VDC. Prototype quantities available at 10MHz for immediate delivery. Full details from Motorola Component Products Dept., 2553 No. Edgington, Franklin Park, Ill. 60131.
INSTRUMENTATION

Power-line recorder checks every cycle

Micro Instrument, 580 Upper St., Escondido, Calif. 92025. (714) 746-2010. $1950; stock.
Model 5209 sag-surge recorder provides simultaneous dual-pen recording of all power line transients, plus sags and surges. The power line is continuously monitored, point by point, every cycle to detect both fast transients or slow changes that may occur. With a frequency response of dc to 1 MHz, the instrument monitors over a voltage range of 0 to 1000 V to within ±5% accuracy. The range may be extended to 100 kV. Several analog output voltages are provided to permit operation of the recorder with fast data loggers, video recorders or scopes.

Function generator has built-in modulation

Exact Electronics, 455 S.E. 2nd Ave., Hillsboro, Ore. 97123. (503) 648-8661. $795; stock to 2 wks.
The Model 129 contains two independent generators, one for carrier and a second for AM/FM. Both the carrier and modulating signals offer sine, triangle and square waves. The carrier ranges from 0.1 Hz to 5 MHz and can be triggered (single cycle) or gated (tone burst, pulse burst) from either the internal AM/FM generator or externally. Carrier output is 10 V pk-pk into 50 Ω, 20 V pk-pk, open circuit. The output has a precision attenuator of 60 dB in 10-dB steps, plus a continuously variable attenuator of 20-dB. AM/FM frequencies range from 1 Hz to 1 MHz.
EMI SHIELDING

- Knitted wire shielding strip gaskets and special shapes.
- Wire mesh and elastomer seal/shield gaskets.
- Thin elastomer filled meshes for shielding/sealing.
- Honeycomb, screen and mesh shielded vent panels.
- Shielded optical viewing windows.
- Metal or carbon filled conductive elastomers.
- Conductive paint, adhesives, epoxies and caulking compounds.

These and more in TECKNIT's Design Guide.

TECKNIT® Technical Wire Products, Inc.

Eastern Division • 129 Dermody St., Cranford, NJ 07016 (201) 272-5500
Western Division • 427 Olive St., Santa Barbara, CA 93101 (805) 963-1867

INFORMATION RETRIEVAL NUMBER 93

Now!! Selling Direct To Public

Big Powerful 7 H.P. Briggs & Stratton Mustang RIDING MOWER

1973 Model

- Constructed of steel and built for constant rugged use. It is powered by a 7 H.P. mower with easy cut grass and needs 5 hours cut decks to fertilize distributors, clean, oil or any other lawn attachment for your lawn needs.

- One full year nationwide factory warranty
- Comes complete with illustrated parts list and full operating instructions.
- Two day service on parts in most states.
- Comes completely assembled in crate.
- Beaufifully baked on rust proof enamel finish
- Made in U.S.A.

Compare at $434.99

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2781 MAIN STREET
SAINT PETERS, GEORGIA 30456
Phone (404) 708-6809

Gentlemen: Please send me literature on your new line of snap-acting time delay relays.

Name _____________________________
Company _________________________
Address __________________________
Zip ______________________________

Texas Instruments
MS 952
P.O. Box 5012
Dallas, Texas 75222

INFORMATION RETRIEVAL NUMBER 95

TI Introduces the $1.10 Relay.

TI has come up with a new line of snap-acting time delay relays costing only $1.10 to $3.00 when ordered in quantity. That's up to 25% less than conventional creep-acting blade relays - 50% less than snap-acting blade relays - less than many conventional magnetic relays or contactors.

They're smaller than ordinary relays, too. They'll operate in any position, and they're resistant to shock and vibration. They also have a proven life that exceeds 100,000 switching cycles.

The secret is our Klaxon® snap-acting disc and a new, low-cost electrically-heated ceramic element mounted in a compact phenolic housing.

As an OEM, you owe it to yourself to find out more. Our technical literature spells it all out.

Texas Instruments
MS 952
P.O. Box 5012
Dallas, Texas 75222

Gentlemen: Please send me literature on your new line of snap-acting time delay relays.

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Texas Instruments

INFORMATION RETRIEVAL NUMBER 95

ELECTRONIC DESIGN 12, June 7, 1973 157
GENERAL ELECTRIC'S

69F MIL TYPE TANTALUM WET SLUG CAPACITOR...

Four series to choose from:

69F — Unique patented double O-ring elastomer seal, with proved superiority over other elastomer seal designs.

69F2000 — Provides two-to-three times more capacitance in the same case size, with the patented double O-ring elastomer seal.

69F3000 — Glass-to-metal hermetic seal. Fully qualified to MIL-C-3965/24, Style CL66/67.

69F4000 — Glass-to-tantalum hermetic seal. Fully qualified to MIL-C-39006/9C, Style CLR65.

Same quality features in all four:

• High Volumetric Efficiency — for minimum size and weight.
• Low Leakage Current — for timing applications.
• Broad dual rated temperature range — from -55 C to +85/125 C.
• Thixotropic gelled electrolyte — for maximum stability throughout extreme temperature ranges.

For more information on these, or any other General Electric capacitors, call your nearest GE sales office, or write Section 430-52, Schenectady, N. Y. 12345.

MAKE SOMETHING OUT OF IT!

GENERAL ELECTRIC

INFORMATION RETRIEVAL NUMBER 96
Retire the Relics.

Unless you're going into the antique electronics business . . . now's the time to replace those open-frame power supplies with today's space-saving, encapsulated power modules.

Our miniature power modules are "triple-tested" for reliability. And backed with a 2-year warranty. Because they're easy to replace, downtime is significantly reduced. And if that isn't enough ... we provide a lower cost per watt than the relics of past generations.

Delivery? Five days from receipt of order. Right from the stocking shelves of the largest manufacturer of encapsulated power supplies, Computer Products, Inc. So don't save the relics — save money, save time, and save space. Write or call us for more information today. As for the relics, maybe the Smithsonian will take them off your hands.


Here's everything you'd expect from a high-priced portable multimeter. Except a high price.

Compare our major features: Both high and low power ohms ranges; a 1 V low voltage scale (AC & DC); a DC current range of 1 µA full-scale; fuse protection; input impedance of 15 MΩ on DC; 1% precision resistors; a 4½ inch, 50 µA mirrored scale meter; frequency response flat to 150 KHz and 59 ranges; battery operated.

You'd expect to pay a lot more for a portable multi-meter like the B & K 277. Check the specs. Call your B & K distributor or write Dynascan Corporation.

$99.95

Need a small relay that will take punishment?

Our class H relay may be just the answer. Its unique actuating card assures contact reliability — over 100 million operations are standard. Available from stock too. Write for information, GTE Automatic Electric, Industrial Sales Division, Northlake, Illinois 60164.
THE X-Y EFFECT

X.
Recently, we received an assignment from customer X to work with him in the development of his new product. Our monolithic crystal filter was to be a key part of his product's system. We started with him on his project at earliest breadboard and carried through over a two year span to final manufacturing. We worked in close collaboration with X, tailoring filter and product to one another. The result is a product unique in its field, which, based on performance and cost, has gained outstanding market acceptance. Our custom monolithics helped.

Y.
Not every new product requires two years to develop. Customer Y saw an immediate market for an application of radio control. But his existing control receiver would be subject to selectivity. Prototypes were shipped.

Time was short. We were consulted, and recommended a standard model filter in less than four weeks. In addition to saving time, customer Y was able to take advantage of standard model engineering and pricing for his requirement, which eventually totaled a very modest, but highly successful, 1500 units.

And success is the name of the game. Whether it's a brand-new project or a fast retread of an old standby we've got the filters to make your design successful. First there's the industry's largest selection of standard model monolithic and tandem monolithic crystal filters. And when it comes to custom modes, our unmatched experience assures you of the sound engineering advice you need. Last but not least, our unequalled capacity gets you your production units on time. We've proved it for X and Y and we'd like to add you to our alphabet. Drop us a line or call us.

Data processing

Video expander unit reconstitutes TV images

Colorado Video, Inc., Box 928, Boulder, Colo. 80302. (303) 444-3972. $5500; 120 days.

Data fed into the Model 261 at a slow rate (30-60 s/frame) are used to build up a continuously refreshed image on a standard TV screen. Input TV signals are converted to six-bit digital format, reconverted to analog form and recorded on the magnetic disc memory. Internal circuitry detects the necessary "frame-start" and "line-sync" signals. For computer output applications, parallel six bit data can be fed to the unit's buffer inputs at standard TTL logic levels. Either the internal time base or an external signal can control the location of the image. Options include selective data erasure, storage for multiple images and multiple channels for color synthesis.

Printing calculator keeps pace with results

Victor Comptometer Corp., 3900 N. Rockwell St., Chicago, Ill. 60618. (312) 539-8200. $545-$725; 30-60 days.

The 110 char/s printing speed of the series-1900 calculators is said to be faster than for any other calculator on the market. The four members of this series range in price from $45 to $725, and they figure percentages, round-off, subtotal and total as well as providing constants. Several models have one or two memories, "change-sign" keys and multiplicand entry for the second memory. One model has automatic square root and an item-count key. The units provide switch selectable fixed or floating decimal point and have 16-digit capacity. OEMs can purchase the dot matrix impact printer separately (single-unit price is $275) quantity discounts are available.
mi·cro·temp (mɪˈkrəʊ ˈtemp) 
A patented, positive safety thermal cutoff.
It will interrupt a circuit when the operating temperature exceeds the rated temperature of the cutoff. Normally employed as a back-up safety protector to cut off power to electronic circuits or components that develop abnormal temperature build-up, this device is fast, reliable and accurate to ± 3°F.
MICROTEMPS are CSA listed and insure product safety. Costing as little as 7.5¢ each, MICROTEMPS are available in a wide range of configurations, ratings and terminations to suit your individual applications. MICROTEMPS are hermetically sealed; unaffected by vibration, shock, aging or positioning, and meet UL standard 1020. For specific details, call or write:

MICRO DEVICES CORP.
1881 Southtown Blvd., Dayton, Ohio 45439
Ph. (513) 294-0581 Telex: 28-8087

Need a small relay with a choice of termination?

Our class E relay is the answer. From printed wiring to plug-in, we offer more methods of termination than anyone. And that means you can use the least costly production method. Just write us, GTE Automatic Electric, Industrial Sales Division, Northlake, Illinois 60164.

DO-IT-YOURSELF grabber

NEW

- Simplified Assembly
- Versatile
- Comfortable Finger Grip Action
- Completely Field Serviceable
- Molded of Tough Lexan*

This test clip with gold plated hook is excellent for rapid testing of components and Wire Wrap pins. Clip is completely insulated to point of connection. Build any combination of test leads with wire up to .090 dia. Easy and comfortable to operate. Molded of rugged Lexan to resist melting when soldering. Write for literature and prices.

SIMPLIFIED ASSEMBLY

Rapid assembly or replacement of damaged lead.

MODEL 3925
hooks onto components or slips over square Wire-Wrap pins

*Lexan is a General Electric trade-mark. †Registered trade-mark of Gardner-Denver Co.

POMONA ELECTRONICS
A Subsidiary of ITT
1500 East Ninth St., Pomona, Calif. 91766
Telephone (714) 623-3463

INFORMATION RETRIEVAL NUMBER 103
DATA PROCESSING

PCM bit synchronizer has selectable rates

Coded Communications Corp., 1620 Linda Vista Dr., San Marcos, Calif. 92069. (714) 744-3710. $4500; 60 days.

Model 7130 PCM bit synchronizer offers thumbwheel-programmable rates from 1 k bit/s to 2 M bit/s with independent input and output selection in all standard IRIG codes. The unit accepts noisy data in any of the eight IRIG codes via one of four selectable input channels. It outputs an in-phase clock, regenerated (cleaned) input data, NRZ-L data, and any selected code of the eight IRIG codes. Data are detected by an integrate-and-reset circuit. The clock is generated by a phase-locked loop using wide or narrow tracking. The bit rate ranges are 1 kbit/s to 2 Mbit/s for NRZ codes and 500 bit/s to 1 Mbit/s for RZ, DM, and Bi-phi codes.

CHECK NO. 528

Analysis program also performs optimization


MAGIC, a large scale circuit-analysis program provides frequency analysis, sensitivity analysis and optimization for circuits operating between a few Hz and many GHz. The program includes built-in models for such microwave elements as transmission lines and stubs. MAGIC will adjust up to 50 circuit components to obtain a least-squares fit to any circuit response curve specified by the user. A large-scale computer such as the Univac 1108 or CDC 6000 with 48-k words of core is required to execute the program, or the user can access it on a time-shared basis from University Computing Corp. In house rental costs $2500/mo.

CHECK NO. 529

Programmable industrial controller is modular

Struthers-Dunn, 1101 State St., Bettendorf, Iowa 52722. (319) 359-0318. From $5000; stock.

A modular approach allows the engineer to add controller capacity in small increments as needed. The VIP 250 programmable controller is available with 32 to 256 I/O ports in multiples of 16. Maximum memory capacity is 4096 words, in multiples of 256. High noise immunity is obtained through use of proper logic, photo-isolated inputs and a ferroresonant power supply. No special training is required for programming which can start from relay ladder diagrams, Boolean equations or English statement—as desired. Price ranges from $5000 (128 I/O ports, 256 words) to $12,000 (256 I/O ports, 4096 words).

CHECK NO. 530

Tape punch handles a variety of tape materials

EECO, 1601 East Chestnut Ave., Santa Ana, Calif. 92701. (714) 537-5651. $1435; stock.

Model TPS9960 tape punch handles Mylar, paper-Mylar, aluminum Mylar and paper tapes and can punch 5, 6, 7 or 8 levels. The self-contained unit operates synchronously at 60 char/s and asynchronously from zero to 60 char/s. Supply and take-up reels hold up to 1000 ft of tape. Dimensions of the model TPS9960 are 10-1/2 in. deep and the 30-lb unit mounts in a standard 19-in. rack. Single-unit price is $1435 with OEM discounts available.

CHECK NO. 531
For a limited time only, Cambion's new general purpose ceramic module 801-2001-01 will be sold for ½ off the usual $30 price. It can be used in water coolers, small refrigerators, hot and cold temperature sources, spot cooling for electronic components, and many other applications. You'll also get a free copy of Cambion's Thermoelectric handbook.

To order, send name and address along with $20 check or money order. Cambridge Thermionic Corporation, 445 Concord Ave., Cambridge, Mass. 02138

**Special introductory offer**
It costs less to buy our new low cost thermoelectric module NOW.

**OPERATING CHARACTERISTICS**
- ΔT Max. at Qc Zero = (60°C)
- Max. current = (8.5 amps.)
- Nom. Voltage = (3.5 VDC)
- Th = (50°C)
- Qc Max. at ΔT Zero = (19 Watts)
- Max. Op. temp. = 100°C

Our class W relay can transfer as many as 51 circuits at one time. And do it with communications system reliability. That's why it's used for telephone switching and computer peripheral equipment applications. Write us for details on other ways to use it. GTE Automatic Electric, Industrial Sales Division, Northlake, Ill. 60164.

**Looking for one relay to do the work of four?**
DATA PROCESSING

Free-cursor digitizer relies on software

California Computer Products, 2411 W. La Palma Ave., Anaheim, Calif. 92801. (714) 821-2541. $20,764.

Five buttons on the cursor control all digitizing functions on the model 942, and the result is 0.001-in. resolution and 0.005-in. accuracy. Model 942 is a self-contained unit. The work surface is a standard drafting table with adjustments for surface tilt (0 to 90 degrees) and elevation (34 to 46 in.). One cursor button defines the origin, the second increments the 4-digit counter and the other three are used for digitizing the data. The company offers host computer software for functions such as scaling, gridding and coordinate conversion. Interfaces are available for teletypewriters and for the IBM model 029 keypunch.

CHECK NO. 533

Computer interface speeds data acquisition

BiRa Systems, 9617 Acoma S. E., Albuquerque, N. M. 87123. (505) 298-4321. See text; 30-60 days.

The MBD-11 is a 16-bit real-time microprocessor for use in data logging and control applications. It is designed to control and collect data from upwards of 150 modules such as multiplexers, a/d converters and TTL logic. The data are buffered, formatted and combined for transmission via direct-memory-access channels to the PDP-11 host computer. Most real-time data acquisition tasks are handled by plugging in circuits according to a simple flow chart. The MBD-11 can perform a complete control function in 350 ns. The unit costs $5495 with a 256-word bipolar memory.

CHECK NO. 534

Modems connect directly to phone lines

Anderson-Jacobson, 1065 Morse Ave., Sunnyvale, Calif. 94086. (408) 734-4300. From $295; stock.

Modems MU 296/12 and 396/12 are designed to replace the Bell 103 A/E and 112 B modems. Both modems connect directly to a telephone line without the need for a data-access arrangement. Both answer incoming calls automatically and provide full-duplex service. The MU 396/12 also allows automatic call origination. The modems transmit data at speeds up to 450 baud and have -50 dBm sensitivity. The purchase prices are $270 for the MU 296/12 and $295 for the MU 396/12.

CHECK NO. 535

Innovate!

with L to L, , or I connectors.

New flexibility in electronic design is possible with AirBorn's WTE series of right angle connectors. Use any combination – right angle to right angle, perpendicular, parallel, or extender boards. Two sizes: 10 and 20 contacts. Spacing: 100": 2 rows; offset. 050. Write 2618 Manana Drive, Dallas, Texas 75220, or call 214-357-0274 and let us help you INNOVATE!

AirBorn, Inc.
DUAL POSITION DRUM INDICATOR

The Minelco® M161M, L and LD internal drum-type BITE Indicators provide optimum visible indication for avionics instrumentation and control applications.

Latching or self-restoring, environmentally sealed, the M161M, L or LD are optionally available with O-ring panel seal and special finish to provide RFI shielding. Standard voltages available are 6, 12, 24 and 28. A wide choice of variations is available to meet circuit condition indicator requirements. The display drum accommodates combinations of colors and up to 5 letters, 3/32" high, to meet individual requirements.

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DC to AC Sine Wave Inverters

SPECIFICATIONS
Output Voltage Regulation:
less than ±5% for line and load
Frequency Stability:
±0.5% of fixed frequency; 0.05% optional
Total Harmonic Distortion:
less than 5% at full load and nominal line

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The new '73 Heath/Schlumberger instrumentation catalog is here...52 pages of high performance electronic equipment...all at budget-stretching prices. Whatever it is that you need in electronic equipment for test and design work, R&D applications or for teaching, Heath/Schlumberger has it...at less than you planned to spend. 600 MHz frequency counter with 7-digit LED readout and complete programmability for only $795* (left)...dual trace 15 MHz scopes only $595*...multi-range, multi-speed strip chart recorder system just $675*...a patchable mini-computer interface system, just $1250*...the famous Malmstadt-Enke Lab Stations...dozens of plug-in circuit cards...power supplies...generators...digital multimeters...and hundreds of other instruments. To get your FREE copy of this catalog now, visit your local Heathkit Electronic Center or use the coupon below.

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*Mail order prices; F.O.B. factory.

INFORMATION RETRIEVAL NUMBER 110

ELECTRONIC DESIGN 12, June 7, 1973
Minicomputer features higher throughput rate

Rolm Corp., 10300 N. Tantau Dr., Cupertino, Calif. 95014. (408) 257-6440. $18,500.

Increases in execution speed will allow the 1602 Ruggednova to solve complex time constrained problems. The 16-bit machine, designed for military environments, boasts an average speed increase of 6 times over that of its predecessor, the 1601. Computational speed and flexibility are provided by internal microprogram capability. The augmented instruction set includes a push-down stack, n-bit shift instruction and a file search instruction. Additional interrupt capability includes several preprogrammed interrupt sequences which reduce interrupt processing time. Rolm also offers the full set of software packages provided with the 1602's predecessor. The price quoted includes the CPU and an 8k x 16 bit core memory.

Fast drum plotter has three pens

California Computer Products, 2411 W. La Palma Ave., Anaheim, Calif. 92801. (714) 821-2541. $12,600; stock.

The model-936 three-pen drum plotter operates on-line or off-line and is compatible with all members of CalComp's 900-series controller family. The unit has an axial speed of 3.6 in/s (pen down) and 5.0 in/s (pen up). This allows a diagonal rate of 5.1 in/s and 7.1 in/s, respectively. Interchangeable drums enable use of 33-in. and 11.7 in. paper widths. An electronic scaling device compensates for paper-width or inking variations. A built-in cutting bar facilitates easy removal of completed plots.

Loader program is stored in a ROM device

Computerwise, Inc., 13124 S. 71 Hwy., Grandview, Mo. 64030. (816) 765-3330. $550; stock.

The RM-11A ROM loader provides program loading for PDP-11 series computers. The RM-11A is a 96-word IC read-only-memory which is contained on one printed circuit board. It plugs into any available small peripheral-interface slot in the processors. The unit is compatible with the standard absolute loader program and, in addition, performs an automatic device selection sequence for the high speed reader or low speed reader (with standard bus addresses). The ROM loader program utilizes the highest four words of read/write memory for temporary storage and leaves the bus address of the selected input device in the last word. Comprehensive documentation and a diagnostic are provided with each unit.

Metal housing reduces tape cassette problems

Conrac Corp., Cramer Div., Mill Rock Rd., Old Saybrook, Conn. 06475. (203) 388-3574. $5.50 in 1000 qty; stock.

Die-cast aluminum construction assures dimensional stability for the CM-300 metal cassette in spite of ambient temperature and humidity variations. The metal housing acts as a ground, eliminating static-charge problems that can cause tape to stick to itself and result in jamming or tearing. The replaceable foam-type pressure pad meets ANSI and ECMA standards for pressure and torque. Tape speeds are 50 in/s for read-write and 400 in/s for search. Cassette tape capacity is 300 ft with a packing density of 800 bit/in.
A sleek graceful sailing vessel glides across the sometimes green, sometimes blue Caribbean. The cargo: you. And an intimate group of lively, fun-loving shipmates.

Uniform of the day: Shorts and tee shirts. Or your bikini if you want. And bare feet.

Mission: A leisurely cruise to remote islands with names like Martinique, Grenada, Antigua—those are the ones you've heard of. Before the cruise ends, you'll know the names of many more. You'll know intimately the enchanting different mood of each...and its own beauty and charm.

Life aboard your big sailing yacht is informal. Relaxed. Romantic.

There's good food. And 'grog.' And a few pleasant comforts...but any resemblance to a plush pretentious resort hotel is accidental.

Spend 10 days exploring paradise.

Spend ten nights watching the moon rise and getting to know interesting people. It could be the most meaningful experience of your life...and it's easily the best vacation you've had.

A cruise is forming now. Your share from $245. Write Cap'n Mike for your free adventure booklet in full color. Come on and live.

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The all new ACTION RACK provides the top quality package with an exciting range of features and applications.

- Multibay Systems—The ACTION RACK is at its best arranged in series, wedges and wrap-arounds. Future system expansion is a simple and easy operation.
- Turret Display Modules—Isolate and focus attention as required in display, monitor and CRT applications.
- Accessories—A decade of experience has gone into development of these useful accessories—Panels and handles, recessed mounting rails, trim inserts, doors, leveling feet, casters, caster plate, stabilizers, power outlets, chassis slides and support angles, storage shelf, blowers, vent grilles and louvers, drawers and a variety of writing surfaces.

Engineered to provide full use of the expanded OPTIMA line of accessories and styling features at a money-saving cost. Available in 7 panel heights (22", 28", 35", 42", 52", 61", and 70") for 19" panel width and 24" panel-to-panel depth. Depth is adjusted with recessed mounting rails. ACTION RACK is delivered completely assembled and finished in two colors from a great selection of 16 vinyl colors.

Write or call OPTIMA ENCLOSURES Division of Scientific-Atlanta, Inc. 2166 Mountain Industrial Blvd. Tucker, Ga. 30084 (404) 939-6340

INFORMATION RETRIEVAL NUMBER 116

PACKAGING & MATERIALS

Foam flux offered for automated soldering

Multicore Solders, Dept. LF 122, Westbury, N. Y. 11590. (516) ED 4-7450.

Called foam fluxes, these new liquid fluxes are specially designed for automated soldering of PC boards. Type 366 is an activated noncorrosive rosin foam flux. The flux is supplied with a 38% solids content and is intended for immediate use without thinning for all electronic general-purpose soldering. Type 366A-25 has a 25% solids content. It is used where a lower rosin content is permissible. A hard, protective, nonconductive, insulating residue is left on the soldered assemblies. Both new fluxes contain WW Gum Rosin.

CHECK NO. 540

Socket accepts TO-66 9-pin IC packages

Jermyn, 712 Montgomery St., San Francisco, Calif. 94111. (415) 362-7431. $50 (500 up).

Socket A1369 enables nine-lead TO-66 devices to be mounted on heat sinks and chassis without soldering the leads. The devices are secured with two screws. A solder lug under one screw can be used for grounding. The socket material, black phenolic thermosetting plastic, is suitable for continuous operation to 150 C. The socket contacts are silver plated.

CHECK NO. 541

Maximize dissipation by using basket heat sink

Precision Dipbrase Tor, 14715 Arminta St., Van Nuys, Calif. 91402. (213) 786-6524, Stock.

Model LP-12 aluminum heat sink maximizes heat dissipation in a small space for transistors in TO-3, TO-66 and TO-36 cases. Thermal resistance with natural convection is 10.1°C/W. Using forced convection, a thermal resistance of 2.5°C/W is achieved. By mounting the heat sink on a Tor 1549-1 bracket, the thermal resistance will lower to 8.3°C/W with natural convection and 2.1°C/W with forced convection.

CHECK NO. 542

Ceramic powder gives a surface finish of 4 µin.

Comco, 9421 Telfair Ave., Sun Valley, Calif. 91352. (213) 786-5450.

A powder for ceramic substrates is 99.5% Al₂O₃, and provides substrate surface finishes of 4 µin. or better—as fired (no glazing, grinding or polishing). Substrate thicknesses range from 0.01 to 0.03 in.

CHECK NO. 543

Potting compound has mix-and-dispense bag

Allied Resin Corp., Weymouth Industrial Park, E. Weymouth, Mass. 02189. (617) 337-6070. $1.90 (100 cc).

AP 8500 is a two-part epoxy casting compound that is prepackaged in a two-section pouch. You break the divider that separates the catalyst and resin and you knead the mixture before using. Then just snip off a corner to dispense the epoxy. Working time is approximately 30 min. for 100 cc at 72 F. Cured, it is tough and semirigid. The epoxy can withstand a maximum temperature of 215 F.

CHECK NO. 544

ELECTRONIC DESIGN 12, June 7, 1973
A complete standard line of battery holders and connectors, for use with all type batteries. Aluminum or steel nickel plated, single and multiple holders.

Free engineering service for your special custom built holders.

NEW FREE CATALOG ON REQUEST

Manufacturers of Standardized Hardware for Electronics

KEystone
ELECTRONICS CORP.
49 Bleeker Street • New York, N.Y. 10012

INFORMATION RETRIEVAL NUMBER 117

Temperature Indicators for Electronics

Let you know when rated temperature is reached...with an accuracy of ± 1%

1. TEMPILABELS®: self-adhesive temperature monitors consisting of one or more heat-sensitive indicators sealed under transparent, heat resistant windows. The centers of the indicator circles turn from white to black irreversibly at the temperature ratings shown on the label. Tempilabels® are available in several sizes, and in single or multiple temperature ratings from 100° to 500°F. Accuracy is within ± 1% of the stated rating. They are particularly useful for monitoring operating temperatures of equipment or processes; obtaining temperature data of components as a guide to design and material selection; safeguarding temperature-sensitive materials in storage or transit. To serve as a permanent record, Tempilabels® can be removed from the surface and attached to a report.

2. TEMPILAQ®: materials of calibrated melting points suspended in an inert, volatile non-flammable vehicle. Available in over 100 systematically spaced temperature ratings from 100° to 2500°F. Tempilaq® indicates its temperature rating by liquefying within ± 1% of its rating. Available in bottles or spray cans.

3. TEMPILSTIKS®: temperature-indicating crayons of calibrated melting points. Available in over 100 systematically spaced temperature ratings, Tempilstiks® cover the range from 100° to 2500°F. Tempilstiks® indicate the specified temperature, by liquefying with a tolerance of ± 1% of its rating.

Detailed data and price sheets as well as samples are available upon request.

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INFORMATION RETRIEVAL NUMBER 119
TRIACs & SCR’s

NEW ELECTRICALLY ISOLATED 1/2'press-fit series

**TRIACS**
- 6A to 40A \( \left( I_{\text{RMS}} \right) \)
- 50V-600V \( \left( V_{\text{DROU}} \right) \)

**SCR’s**
- 8A to 35A \( \left( I_{\text{RMS}} \right) \)
- 50V-600V \( \left( V_{\text{DROU}} \right) \)

Three new additions to Hutson’s 1/2” press-fit series: isolated press-fit package; isolated press-fit and stud mount with BeO insulators for greatly improved thermal characteristics. All 1/2” press-fit devices feature patented Di-Mesa construction of void-free glass-passivated center gate chips.

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The X-1284 tape has both a flame-retardant polyester backing and flame-retardant adhesive system. It has a functional temperature limit of 130°C and meets flame retardancy specifications including U/L subjects 492, 510 and 94, and U.S. Highway Administration standard No. 302. The tape is highly conformable to irregular surfaces and has excellent tear resistance for fine-wire coils.

CHECK NO. 547

Connector provides electrical/thermal link


Designers of power circuits can now package with plug-in modules that disconnect thermally as well as electrically. Power circuits have traditionally been hardmounted so that they had a long mean-time-to-repair. The advantages of the plug-in concept can thus apply to power circuits, too. And external case cooling becomes practical with the thermal connector, thus simplifying environmental and EMI sealing.

CHECK NO. 548
## Delay Lines

**You name it. We’ve got it.**

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<th>Catalog Number</th>
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<th>Total No. Rise (ns ( \pm 5% ))</th>
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<th>Delay Per Tap (ns max)</th>
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Now you can choose from the broadest selection of DIP Delay Lines ever. Available today from quantity stock at any PULSE ENGINEERING regional office in the United States and Europe.

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ELECTRONIC DESIGN 12, June 7, 1973

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geneva, illinois 60134 (312) 232-4300

INFORMATION RETRIEVAL NUMBER 126
**JFET cross-reference guide**

A comprehensive cross-reference guide lists over 1300 JFET types. The guide includes all European type numbers and all manufacturers, listing both their in-house numbers as well as the 2N number designations. Teledyne Semiconductor, Mountain View, Calif.

**CHECK NO. 550**

**Anodic stripping**

The principles of anodic stripping voltammetry and the required instrumentation are described in an eight-page application note. The note shows how a specially designed cell and working electrode permit savings in analysis time over conventional apparatus. Experimental results are given to illustrate performance of the equipment. McKee-Pedersen Instruments, Danville, Calif.

**CHECK NO. 551**

**Electrical insulation**

"Electrical Insulation Materials" incorporates relevant information needed to apply sleeving, heat-shrinkable and insulated wire. The 42-page guidebook covers extruded tubing, fiberglass-coated and impregnated tubing, heat-shrinkable tubing, Conco extruded rod and Teflon sheet and phenolics, tapes and adhesives. Data includes standard and special-cut lengths; MIL-spec and UL designations; stocked colors vs colors to order and standard spooling. Commercial Plastics & Supply Corp., Cornwells Heights, Pa.

**CHECK NO. 552**

**Power tube cooling**

"Application Guide For Forced-Air Cooling of RCA Power Tubes" provides information on power tube cooling procedures that will improve tube life and reduce equipment downtime. The guide points out the need for an analysis of environmental considerations such as altitude and temperature of outside air. A step-by-step example is provided to describe procedures for selecting the blower unit. Curves, nomographs and drawings are included. RCA Commercial Engineering, Harrison, N.J.

**CHECK NO. 553**

**Beryllium and fluorometry**

Fluorometry Review provides discussions of several fluorometric analyses for beryllium and includes 30 references. Fluorometry offers the extreme sensitivity and simplicity required for the analysis of submicrogram quantities of beryllium. The flexibility of fluorometry makes it useful for analyzing the relatively large amounts of beryllium found in ores. G.K. Turner Associates, Palo Alto, Calif.

**CHECK NO. 554**

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new literature

Screens and masks

The "Handbook for Quality Screens and Masks" contains information on specifying and ordering screens and masks for thick-film printing. It includes specifications on coatings, emulsion and foil thicknesses, mesh and frame sizes and artwork generation. Industrial Reproductions, Nashua, N.H.

CHECK NO. 560

Pushbutton switches

Mechanical and electrical specifications and ordering data (both military and commercial) for eight illuminated pushbutton switches recently qualified under MIL-S-22885 and listed on QPL 2285 are described in an eight-page catalog. Marco-Oak, Anaheim, Calif.

CHECK NO. 561

Mil-Spec connectors

Four brochures illustrate connecting devices qualified to the latest military specifications. Deutsch, Banning, Calif.

CHECK NO. 562

TV and radio manuals

Master Index covers all the company's existing monochrome and color-TV manuals and all radio manuals back to the 1926-38 issue. Instructions on how to obtain material needed in the manuals or as single diagram service data are given. The 48-page index costs 50c. Supreme Publications, 1760 Balsam Rd., Highland Park, Ill. 60035.
Radio noise meter
Quick and accurate testing for RFI pollution, as required by the power industry, is performed by the radio noise meter described in Data Bulletin RFI-102B. The four-page bulletin contains ordering instructions for specifying special frequencies and for selecting appropriate antennas. Singer Instrumentation, Los Angeles, Calif.

Minicomputer systems
“The Value of Power . . . and how it saves you money on your minicomputer system,” a 256-page handbook, gives a short history of computers. Other chapters include numbers and logic; the makings of a computer; addressing modes; the instruction set; evaluating instruction sets; input, output and interrupts; internal interrupts; input, output and interrupt hardware and design considerations; read-only memory and microprogramming; system software; operating systems; and how to buy a minicomputer. General Automation, Anaheim, Calif.

PC hardware
Circuit-board hardware is illustrated in a 16-page booklet. Circuit-board supports, hold-down strips, spacers, PCB guides, card pullers, circuit-board ejectors and edge protectors are described. Richco Plastic Co., Chicago, Ill.

Sensing, interface valves
Photos, specifications, dimensional data, operational descriptions, performance ratings and curves for the company’s sensing and interface valves, components and accessories are described in a 24-page, two-color catalog. Northeast Fluidics, Cincinnati, Ohio.

Wire tester
A four-page bulletin describes and illustrates the company’s VD 36 wire tester that finds and identifies a particular wire in a mass of wires. The bulletin includes description of applications and mode of operation as well as technical data. Siemens, Iselin, N.J.

Disc-drive systems
Series-8000 cartridge disc-drive systems are described in a four-page bulletin. The bulletin contains photographs and a general description along with a list of features and specifications. Reliability, packaging, options and the interface are described. Microdata Corp., Irvine, Calif.

Temperature indicators
Thermocouple, RTD and thermometer models are described in a four-page digital temperature indicator catalog. A selection guide provides temperature range charts indicating the specifications for each model. RdF Corp., Hudson, N.H.

Flexible heating elements
Heating elements, drum heaters and temperature controllers are described in a four-page catalog. Each type of flexible silicone-rubber heating element is described, and specifications and operating characteristics are given. Electro-Flex Heat, Bloomfield, Conn.

Insulators, mounting kits
Physical, electrical and mechanical properties of insulators commonly used with semiconductor devices are featured in a 12-page catalog. Prepackaged mounting kits with Thermafilm insulators and the necessary hardware are also described. Thermalloy, Dallas, Tex.

System modules
“Modules for Systems Applications,” a two-color, 16-page brochure, describes modules that are available as OEM units for in-house system designers. These modules include tape and computer interface units, waveform analyzers, programmable pulse generators, a/d recorder/generators and single-shot modules. The brochure provides information on relations in the time domain, including pulse response vs bandpass, excess reactance, coaxial-cable equations and rise-time relationships. E-H Research Laboratories, Oakland, Calif.

You’re a penny-pinching, up-tight, lil’ switch with no spark.

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INFORMATION RETRIEVAL NUMBER 136

INFORMATION RETRIEVAL NUMBER 135

Transistors
Power transistors, hybrids and microwave transistors are described in a 68-page, two-color catalog. The catalog provides a quick reference guide to discrete power devices, hybrid power regulators, rf power devices and Schottky diodes. Man-rated space parts, JAN qualified devices and quality/reliability information are included. Solitron Devices, Inc., Riviera Beach, Fla.

CHECK NO. 573

All-digital modem packs
A 24-page brochure describes a complete line of all-digital modem packs for switched voice networks and leased-line applications. Specifications are listed along with charts depicting the probability of error vs signal-to-noise ratio. Sanders Associates, Nashua, N.H.

CHECK NO. 574

Multiplexer/a-d converter
A high-speed, low-level multiplexer/a-d converter is described in an eight-page data sheet. Vidar, Mountain View, Calif.

CHECK NO. 783

Image devices
A four-page brochure details the use of the company's video storage units in picture processing for slow-scan thermography. The brochure, Hughes Focus, is the first in a series to be published at regular intervals discussing new applications of image devices. Hughes Image Devices, Oceanside, Calif.

CHECK NO. 784

INFORMATION RETRIEVAL NUMBER 136

NEW LITERATURE
Why do so many manufacturers turn to Beyer for their input transformers? Even though they could get them from the people who supply their power transformers? Because this one has a unique winding process that permits miniaturization while maintaining studio quality frequency response, low distortion, and level capability— at reasonable cost. Because this one represents 40 years of quality manufacturing experience. Who are the manufacturers we're talking about? The leaders. Including Ampex, Ampro, Barcus-Berry, Beli P.A., Bozak, Electro-Sound, Rauland-Borg, RCA, 3M, and many others. You can obtain Beyer transformers at retail through Gotham's franchised dealer organization. Or in OEM quantities directly from Gotham. Write today:

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Image digitizers

Image digitizers are described in an illustrated six-page brochure. The brochure describes how film images are converted to computer-compatible forms and how the computer may be used to extract relevant image features and various photometric data by program control. The conversion of pictures to "digital images" is graphically illustrated. The features of five basic model types are compared in tabular form. Dicomed Corp., Minneapolis, Minn.

CHECK NO. 791

Matrix switches

Included in a guide of matrix switches for rapid circuit selection and programming are product listings, engineering drawings, specifications, operating characteristics and technical data on standard and custom-designed units. Cherry Electrical Products, Waukegan, Ill.

CHECK NO. 792

Microwave components

An illustrated 12-page guide to microwave components and calorimetric systems gives detailed specifications for the company's waveguide and coaxial waterloads and power controls. Raytheon, Wal- tham, Mass.

CHECK NO. 793

Interconnect system

An eight-page catalog describes the concept and components of the company's solderless interconnect system. Technical and test data on one-piece, low-profile (0.025-in. above board) contact/terminals are provided. Photographs, drawings and charts are included. Robinson-Nugent, New Albany, Ind.

CHECK NO. 811

Panel assemblies

Technical, descriptive and specification data on the company's panels and assemblies for telephone and other communications applications are contained in a six-page bulletin. The bulletin includes a selection guide to permit designing and specifying complete assemblies from individual components. ADC Products, Minneapolis, Minn.

CHECK NO. 812

Ceramag® ferrite beads provide a simple, inexpensive means of obtaining RF decoupling, shielding and parasitic suppression without sacrificing low frequency power or signal level. Install beads by slipping one (or more) over appropriate conductor(s) for desired effect. Sizes from .020" ID -.038" OD -.050" L. Beads available with leads for PC boards. Send for samples.
The 3½ digit DPM: easy fit, easy price.

Easy fit, easy price. Our new Series 3500 DPM measures up both ways for standard size interchangeability that gives you more in the bargain. Like the extra large (.55 char. height) 7-segment gas discharge readout.

The LED option. And, like all Faratron DPM's, it's front panel installed/removable with screw-free wedge-lock method. All this and more, in a bipolar DPM with over range indication, BCD output and Faraton's built-in quality plus. Price: $85.00 in 100 quantities.

Contact: Faratron Corp., 280 Green Street, South Hackensack, N.J. 07606; (201) 488-1140

Megohmmeters

A four-page, two-color brochure presents the advantages offered by heavy-duty industrial megohmmeters (HV and HVM series) and precision measuring scientific megohmmeters (HM series) for testing the insulation resistance on all electrical equipment to ASTM specifications and applicable MIL and UL standards at ranges up to 20-million megohms. Hiptronics, Brewster, N.Y.

Hardware options

Multiprocessing hardware options for the PDP-11 family of computers are described in a 24-page brochure. The brochure contains descriptions of three hardware devices, the Unibus switch, the Unibus window and the Unibus link.

Disc recorders

Wideband instrumentation disc recorders and their applications are described in an eight-page brochure. Specifications, typical block diagrams and information on configuration options are included.

Connector products

Contact assemblies

"A Guide to Contact Assemblies for Electromechanical Applications" discusses points to be considered in the design, specification and purchase of switch assemblies, contacts and springs. Other sections in the 20-page guide give an explanation of contact attachment, clad contacts and molded modules. Tricon Manufacturing Co., Downers Grove, Ill.

CHECK NO. 817

Zinc ferrite material

A two-page bulletin describes with charts and graphs specifications and characteristics of manganese zinc ferrite materials—available in E cores, U cores, toroids, I cores, pot cores, threaded cores and other shapes. The bulletin lists magnetic properties and applications. Fair-Rite Products, Wallkill, N.Y.

CHECK NO. 821

Thumbwheel switch modules

General-purpose Digiswitch, a compact, finger-actuated modular switch that features precise setting and high readability for general-panel applications, is described in a two-color data sheet. The brochure details the capabilities of the series-300 switch and provides a listing of typical specifications. Photograph, outline drawings and assembly dimensions graphically illustrate the modules. The Digitran Co., Pasadena, Calif.

CHECK NO. 822

PH systems


CHECK NO. 823

Coaxial connectors

Nu-Lok high-performance coaxial connectors that meet MIL-C-25516 are described in a 16-page catalog. The publication details 14 basic connector types and adapters that are available in a range of sizes and mounting styles and provides electrical, physical and environmental characteristics. Cinch Connectors, div. of TRW, Minneapolis, Minn.

CHECK NO. 824

Temperature controllers

Ninety power-output combinations possible with the company's 400 Series thermocouple temperature controller are described in two data sheets. Full dimensional specifications are given for both table-mounted and panel-mounted models. Thermo Electric, Saddle Brook, N.J.

CHECK NO. 825

Desoldering equipment

Desoldering equipment, including Bazooka solder gobblers, vacuum sources, controls, tips and accessories, are featured in an eight-page bulletin. The bulletin offers suggestions on improving desoldering efficiency, an explanation of the principle of operation and cleaning and maintenance instructions. Air-Vac Engineering Milford, Conn.

CHECK NO. 826

Vibration shock isolation


CHECK NO. 827

Lighting products

Choosing the right indicator light, switch or lampholder is made easy by the “Product Lighting Guide.” Full-color illustrations and pertinent electromechanical characteristics are included. LeeCraft Manufacturing Co., Long Island City, N.Y.

CHECK NO. 828

Electron tubes

The Electron Tube Abridged Data Book describes European electron tubes and devices. Two families of tubes—EEV and M-OV—are color coded for easy identification. An index lists over 3000 types of tubes for which there is an EEV/M-OV equivalent. English Electric Valve Co., Chelmsford, CM1 2QU, U.K.
Dynamic Measurements Corp. has expanded its line of d/a converters to include the popular Analog Devices DAC QZ and DAC QS series. These converters are directly interchangeable with the A.D. types but at substantially lower prices, the company claims. Prices 1-9 are: DAC 12 QZ BIN, $59; DAC 12 QZ BCD, $59; DAC 10 Z-I, $45; DAC 10 Z-3, $45; MDA 10 Z-25, $43; MDA 10 Z-110, $43; DAC 8 QSCB, $75; DAC 10 QSCB, $95; DAC 12 QSCB, $115; DAC 10 QSCBD, $115. Dynamic Measurements is also offering high-speed versions of the QS series with settling times of under 1 μs. These are the 222-VF8QS (DAC 8 QSCB), $95 (1-9); 222-VF10QS (DAC 10 QSCB), $115 (1-9); 222-VF12QS (DAC 12 QSCB), $135 (1-9).

CHECK NO. 852

An internally compensated operational amplifier family, pin compatible with National Semiconductor's LM112 series, is now available from Advanced Micro Devices. These circuits operate over a ±5-to-20-V range with typical power consumption of only 12 mW.

CHECK NO. 853

Inselek Co. has announced the introduction of three INS4000S series devices. They are the INS4001S (quad two-input positive NOR), the INS4009S (hex buffer-inverting) and the INS4010S (hex buffer noninverting). These devices are pin-for-pin compatible with the CD4000 series. Pricing is $3.30 (100-999) for the INS-4001S; $5.25 (100-999) for the INS4009S and INS4010S.

CHECK NO. 854

AVX Ceramics Corp. has just been granted the first QPL to MIL-C-55681-A covering ceramic chip capacitor styles CDR01-02-03-04-05-06. Approval covers the M failure level in all styles. Capacitors of this type are used in thick and thin-film military hybrid applications.
RCA has developed a laser system that can record color images and other multispectral data on black-and-white film. The system can be used to display and interpret multispectral information generated by sensors used in airplanes and spacecraft. It can be used with color scanners in facsimile systems.

CHECK NO. 866

A software package that gives full batch-processing capabilities to Nova computer users has been introduced by Data General Corp. The software package, BATCH, can run jobs in assembly language, ALGOL, FORTRAN IV and the company's new FORTRAN 5. It runs under the company's real time disc operating system (RDOS).

CHECK NO. 867

Hazeltine Corp. has introduced a low-cost teletypewriter-compatible CRT terminal, the "Hazeltine 1000." Features of the new terminal include a 960 (eighty-by-twelve) character display screen, full alphanumeric keyboard, and communication capability up to 9600 bps with a line interface conforming to EIA Standard RS 232C. The unit also offers half/full duplex transmission and parity generation and checking. Rental price is $49/month (including maintenance) based on a 12-month rental contract. Purchase price for the terminal is $1790.

CHECK NO. 882

The National Fire Protection Assoc. has released an interpretational Code pertaining to installation of outlet, switch and junction boxes and fittings.

CHECK NO. 883

In keeping with the long-term movement toward more general use of the metric system, here and abroad, General Motors' implementation to the metric system within GM will be governed by the release of new parts, metrically dimensioned, and by the normal phasing out of in-production parts.

CHECK NO. 884

Double-button switches have been added to low-profile keyboard switches by Oak Industries Inc., Switch Div. The switch stands only 0.415 in. high, including key cap, and sells for less than 25¢ each in production quantities.

CHECK NO. 885

Control Data Corp. has announced a multipartition mass-storage operating system to enhance processing capabilities of the CDC 3000 series medium-scale computer systems.

CHECK NO. 886

A program to make blind computer programmers more productive is available through Honeywell's application sharing system. The system, called Braille-All-Output (BRIALL), has been developed by the Electronic Processing Center, Inc. The company is offering the package to any Honeywell computer user that has blind programmers.

CHECK NO. 887

Transiton Electronic Corp. has added to its Schottky TTL digital logic line five MSI circuits for data selection, multiplexing and carry generator applications.

CHECK NO. 888

A miniature three-electrode lightning arrester for the protection of telephone equipment is being marketed in the U.S. by The English Electric Corp.

CHECK NO. 889

Recognition Equipment has announced that its Total Data Entry systems offer the ability to process data printed in Katakana as an optional feature. Katakana, the Japanese font derived from the basic Japanese Kangii language, is the EPP industry standard for Japan.

CHECK NO. 890

Price reductions

Alittech has reduced prices on three function generators—Model 511 (10-MHz unit with trigger-gate) to $595 from $695; Model 520 (20-MHz unit without trigger-gate) to $695 from $795; and Model 521 (20-MHz unit with trigger-gate) for $795 from $895.

CHECK NO. 891

Simpson Electric Co. has reduced the price of its 460 VOM from $395 to $375.
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**Electronic Design 12, June 7, 1973**
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**UDT PHOTOPS 450**

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The purpose of this 36-page catalog is to assist the design engineer in specifying the proper relay for a given application. The book completely describes General Purpose, Sensitive General Purpose, and Mechanical Power Relays. New products include the complete line of Class 388 General Purpose Relays.

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